# Wyrowski VirtualLab Fusion User's Manual 

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## I Introduction

In this part you can find some general notes about the concept of VirtualLab Fusion and this manual.

## 1 VirtualLab Fusion Packages

VirtualLab Fusion Standard can be extended with various packages:

- Grating Package: Grating Optical Setup, LLGA Results Generator, Fourier Modal Method / Rigorous Coupled-Wave Analysis
- Diffractive Optics Package: Session Editors, IFTA Optimization, Beam Shaper Design
- Flat Lens Package: Functional Meta Lens, Functional Modulated Metasurface, Diffractive Lens, Holographic Optical Element
- Light Shaping Package: Light Shaping Optical Setup, Cells Array Design
- Laser Resonator Package: Laser Resonator Optical Setup, Session Editors
- AR/VR/XR Package: Light Guide Optical Setup, Custom Fourier Modal Method, Footprint and Grating Analysis, Light Guide Grating Design, k-Layout Visualization, Layout Design Calculator
- Distributed Computing Package: Distributed Computing
- optiSLang Package: optiSLang Package


## 2 VirtualLab Fusion and External Tools

VirtualLab Fusion is a powerful software with a focus on designing and analyzing optical systems. There are many external programs with a different focus that extend VirtualLab Fusion's functionality even further.
Some recommended programs:

- VirtualLab Fusion allows you to transform light into arbitrary desired output fields using either the IFTA optimization ( $\varsigma$ Sec. 97) or the Cells Array Design ( $\lrcorner$ Sec. 100). Polygonal or elliptical shapes can be generated within VirtualLab Fusion. More complex patterns like logos can be generated as monochromatic images using raster graphics editors like Windows ${ }^{\text {TM }}$ Paint or GIMP (free); and then be imported into VirtualLab Fusion ( $\hookrightarrow$ Sec. 120.1.3.1).
- VirtualLab Fusion offers many ways to extend its functionality by simply writing snippets in a powerful source code editor ( $\hookrightarrow$ Sec. 7.3). However, complex projects can be developed more easily using an Integrated Development Environment (IDE), for example Visual Studio or Visual Studio Code.
- If your simulations run more than a few minutes and you want to continue with your work in the mean time, we recommend the following procedure.

1. Set the execution priority of your current VirtualLab Fusion instance to something like Below Normal, Low or Idle. This avoids that your PC reacts sluggishly due to heavy CPU usage but leads to slightly longer simulation times. This can be done with the Windows ${ }^{\text {TM }}$ Task Manager or the Process Explorer (free).
2. Start a new instance of VirtualLab Fusion where you can prepare new simulations.

- If you want to take screenshots of VirtualLab Fusion document windows for e.g. presentations, you can use Greenshot (free) or Snaglt (the program with which all screenshots in this manual have been made).
- If you want to do advanced calculations on e.g. a data array ( $\hookrightarrow$ Sec. 13), you can transfer the data to a spreadsheet software (e.g. Excel or LibreOffice Calc (free)) and do your calculations there. The transfer can be done by copying the data from a table to the Windows ${ }^{\text {TM }}$ Clipboard or by exporting the data via File > Export.
- VirtualLab Fusion can export data into various file formats ( $\hookrightarrow$ Part XVI). We recommend the following software to view or process this data.

| FILE FORMAT | RECOMMENDED SOFTWARE |
| :--- | :--- |
| Text Files | Notepad++ (free) and PSPad (free) can handle larger files than the Win- <br> dows ${ }^{\text {TM }}$ Notepad and offer advanced editing options like column-wise selec- <br> tions. V can open very large text files (with a size of several GB) very fast by <br> opening just a view lines at once. |
| Videos | Animations ( $\hookrightarrow$ Sec. 20) can be exported to avi videos which can be edited <br> and converted to other file formats using for example avidemux (free). |
| CIF / GDSII | With KLayout (free), CIF and GDSII files can be opened, edited, and con- <br> verted to e. g. OASIS and DXF format. |
| IGES/STL | Many CAD formats can be viewed online with the Autodesk Viewer (free, <br> registration required). |
| IGES | IGES files can be opened for example with the IGS Viewer (free). |
| STL | STL files can be opened and converted with Meshlab (free). |
| XML | XML files can be opened with any Internet browser. |

## 3 How to Use this Manual

The following formattings are used in the manual.

| EXAMPLE | USED FOR ... |
| :--- | :--- |
| File > Open | An entry in the ribbon ( $\hookrightarrow$ Sec. 4.2). |
| Close | Other elements of the graphical user interface, for example an entry within an <br> edit dialog or document window. |
| Example.txt | A file name or a source code example. |
| $[P E, P C, P V$, or $P E$ | A parameter available for parameter extraction. See Sec. 43.5 for details. |
| Key | A key to press. |

## II User Interface

This part explains the main window of VirtualLab Fusion and other commonly used controls.

## 4 Structure of User Interface



Figure 1. General structure of the user interface of VirtualLab Fusion.
A VirtualLab Fusion window ( $\hookrightarrow$ Fig. 1) consists of the following areas: the ribbon ( $\hookrightarrow$ Sec. 4.2) with the Quick Access Toolbar at the top, Docking Tabs ( $\hookrightarrow$ Sec. 4.3) at the right and at the bottom and a status bar ( $\hookrightarrow$ Sec. 4.4) at the very bottom. The color scheme of these controls can be set in the Global Options Dialog ( $\hookrightarrow$ Sec. 6.3). The main area of the user interface is used for document windows. A document window is also denoted as a view. Several types of documents are supported by VirtualLab Fusion, for example optical systems and harmonic fields. Sec. 4.1 gives an overview of all available document types. Document windows can be closed by double clicking on the icon in their top left corner.

Redrawing a document window can be very computationally intensive. Thus we strongly recommend to switch off redrawing during resizing via the Windows ${ }^{\text {™ }}$ Control Panel (Choose Display, then the Appearance panel, press Effects and uncheck Show windows content while dragging). In this case, any window is only drawn anew if you stop resizing it with the mouse.

Several user interface operations, such as the invocation of certain menu items, cause the appearance of modal dialog boxes. In contrast to document windows, modal dialog boxes lock the whole program, that is, such a dialog box has to be closed for other user interface elements to become accessible again. Use the Help button in the respective dialog to get context sensitive help.

In various dialogs and views context menus are supported, which are accessible by the right mouse button. The menu items displayed within a context menu depend upon the position of the mouse pointer when opening the menu.

### 4.1 Documents and Document Windows

VirtualLab Fusion provides an ever-growing variety of own document types. These documents are shown in document windows for which the main part of the VirtualLab Fusion user interface is reserved. Furthermore, VirtualLab Fusion can import and export many common file formats ( $\hookrightarrow \mathrm{Sec} . \mathrm{XVI}$ ).
The following tables list all document types of VirtualLab Fusion, their file extensions, the relation between document types and document windows (sometimes different document types share the same document window or a document type has more than one document window), and which of the following general features the documents have.

- Result document means that the document somehow show data plotted against one or more coordinates. The corresponding result windows have their own resizing mechanism ( $\hookrightarrow \mathrm{Sec} .4 .1$.1) and a document specific ribbon group in orange (instead of in dark red).
- Warn on Close means that a warning is shown if you try to close the corresponding document window with unsaved changes. These windows show a "*" on the beginning of their window title if there are unsaved changes.
- Automatic Saving means that the document is saved automatically after a certain time interval. You can configure this in the Property Browser ( $\hookrightarrow$ Sec. 4.3) of the document; by default the settings from the Global Options dialog ( $\hookrightarrow$ Sec. 6.17) are used. For this mechanism to work the document must have been saved at least once before so that a file name is known.


## Data Arrays and derived documents

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :---: | :---: | :---: |
| (Numerical) Data Array (*.da) $\hookrightarrow$ Sec. 13 | Numerical Data Array View, $\hookrightarrow$ Sec. 13.5 | Result Document |
| Chromatic Fields Set (*.cfs) | Chromatic Fields Set View, $\hookrightarrow$ Sec. 14 | Result Document |
| Light Field Object (*.Ifo) | View for field components and pulses, $\rightarrow$ Sec. 15. | Result Document |
| Non-Equidistant Field Values (*.nefv) | Ray Distribution View, $\hookrightarrow$ Sec. 17 | Result Document |
| Positions, Directions \& Wavefront Phase (*.ppd) | Ray Distribution View, $\hookrightarrow$ Sec. 17 | Result Document |
| Set of Data Arrays (*.soda) | View for Set of Objects, $\hookrightarrow$ Sec. 16 | Result Document |

Legacy result documents

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |  |
| :--- | :--- | :--- | :--- |
| Harmonic Field <br> $\hookrightarrow$ Sec. 12.1 | (*.ca2) | Harmonic Field View, $\hookrightarrow$ Sec. 12.2 | Result Document |
| Harmonic Fields Set (*.hfs) | Harmonic Fields Set View, $\hookrightarrow$ Sec. 12.2 | Result Document |  |
| Transmission (*.ca2) | Data View, $\hookrightarrow$ Sec. 12.2 .2 | Result Document |  |

## Other result documents

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| Animation (*.bms) | Animation View, $\hookrightarrow$ Sec. 20 | Result Document |
| Ray Distribution 3D (*.rays) |  |  |
| Region (*.rgn) $\hookrightarrow$ Sec. 21 | Ray Distribution View, $\hookrightarrow$ Sec. 17 | Result Document |

## Optical Setups and their variation

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| Optical Setup (*.os, ${ }^{*}$. lpd) | Two linked document windows: Optical Setup |  |
|  | View $(\hookrightarrow$ Sec. 43.1) and Optical Setup Editor <br> $(\hookrightarrow$ Sec. 43.2) | Warn on Close |
|  | Parameter Run View, $\lrcorner$ Sec. 44 | Warn on Close |
| Parameter Run (*.run) |  | Automatic Saving |
| Parametric Optimization (*.opt) | Optimization Document View, $\hookrightarrow$ Sec. 102.1 | Warn on Close |
|  |  | Automatic Saving |

## Other documents

DOCUMENT TYPE DOCUMENT WINDOW FEATURES

| Calculators (*.calc) | Various views, $\hookrightarrow$ Part XV |  |
| :---: | :---: | :---: |
| C\# / Visual Basic source code (*.cs / *.vb) | Modules View, $\hookrightarrow$ Sec. 7.2 | Warn on Close |
| Geometry (*.3d) | 3D View, $\hookrightarrow$ Sec. 5.15 |  |
| Session Editor (*.seditor) | Wizard view | Warn on Close ${ }^{2}$ |

## Documents specific for the AR/VR/XR Package

DOCUMENT TYPE
DOCUMENT WINDOW
FEATURES
Footprint and Grating Analysis Footprint and Grating Analysis Wizard, Warn on Close (*.fga) $\hookrightarrow$ Sec. 101.1
k-Layout Visualization (*.calc)
Light Guide Grating Design (*.IgDesign)

LUT Results Generator
LUT Results Generator, $\hookrightarrow$ Sec. 46
(*.lutGenerator)

[^0]Documents specific for the Diffractive Optics Package

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |  |
| :--- | :--- | :--- | :--- |
| IFTA Optimization | Document | IFTA Optimization Document, $\hookrightarrow$ Sec. 97 | Warn on Close |
| (*.dp, *.aps) |  |  |  |

Documents specific for Grating Optical Setups

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| Diffraction Orders Diagram Data <br> (*.dodd) | Diffraction Orders Diagram, $\hookrightarrow$ Sec. 19 | Result Document |
| Order Collection (*.oc) | Order Collection View, $\hookrightarrow$ Sec. 18 | Result Document |

Documents specific for Laser Resonator Optical Setups

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| Iteration Document (*.iter) | Iteration Document View, $\hookrightarrow$ Sec. 44.6 | Warn on Close |

Documents specific for Light Shaping Optical Setups

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| Cells Array Design (*.gcd) | Cells Array Design, $\hookrightarrow$ Sec. 100 | Warn on Close |
| LLGA Results Generator (*.IIga) | LLGA Results Generator, $\hookrightarrow$ Sec. 45 |  |

Documents specific for the optiSLang Package

| DOCUMENT TYPE | DOCUMENT WINDOW | FEATURES |
| :--- | :--- | :--- |
| optiSLang Optimization (*.oso) | optiSLang Optimization View, $\hookrightarrow$ Sec. 103 |  |

### 4.1.1 Resizing of Document Windows



Figure 2. Dialog for adjusting the window size of all currently open result windows.

The size of all document windows can be changed via the usual mechanisms provided by Windows ${ }^{\text {TM }}$ (dragging on the borders, using the minimize and maximize buttons). Furthermore there are several tools for this in the Windows tab of the ribbon ( $\hookrightarrow$ Sec. 4.2.4).
But for result windows ( $\hookrightarrow$ Sec. 4.1), VirtualLab Fusion offers special ways to set the window size in pixels, which can be helpful for doing screenshots for presentations:

1. Define a window size in the Global Options dialog ( $\hookrightarrow$ Sec. 6.7) which is used for newly created documents.
2. Via Windows > Change Size of Result Windows you can open a dialog ( $\hookrightarrow$ Fig. 2) to adapt the window size of all currently open result windows. This dialog allows you to choose between Set Window Size (in which case you can define the Window Size) and Minimize Windows. The latter can be useful if there are many results windows open which you do not need in the moment.
3. Change the size via the Property Browser (if available for the specific document type).

### 4.1.2 View Settings

All documents but Module Files and IFTA Optimization Documents also store the current view settings of their corresponding document window (window size, markers, color scale and alike) if saved to hard disc. For all of these document types which have a View ribbon, you can copy the view settings from another document window of the same type via the View > Copy View Settings button.

### 4.2 Ribbon



Figure 3. Controls within a ribbon.

The ribbon at the top of the main window is the main control for accessing the various features and document types of VirtualLab Fusion. As shown in Fig. 3, it consists of the File menu ( $\hookrightarrow \mathrm{Sec} .4 .2$.2) and six ribbon tabs (see table below). Various document types add a ribbon tab group to the ribbon containing further ribbon tabs. A ribbon tab has several ribbon groups each with several ribbon items, which can be buttons, menus, and the like.
Furthermore there is a quick access toolbar ( $\leftrightarrows$ Sec. 4.2.1) where you can place your most often used ribbon items. And with the compact mode button in the lower right corner of the ribbon you can reduce the icon sizes of the ribbon items and thus decrease the height of the ribbon.
When you press Alt or F10, key tips are shown which allow you to access almost all ribbon items via keyboard. The following six ribbon tabs are always available:

| RIBBON TAB | DESCRIPTION |
| :---: | :---: |
| Start | Allows you to create, load and save documents. Furthermore it contains various calculators and license information. $\leftrightarrows$ Sec. 4.2.3 |
| Sources | Provides access to all Basic Source Models ( $\leftrightarrows$ Sec. 51), Partially Coherent Source Models ( $\rightarrow$ Sec. 52), and Spectrum Generators ( $\rightarrow$ Sec. 53). |
| Functions | Contains the generators for transmissions ( $\leftrightarrows$ Sec. 67.1) and region documents ( $\leftrightarrows$ Sec. 21). |
| Catalogs | All VirtualLab Fusion catalogs ( $\rightarrow$ Part V). |
| Windows | Allows you to configure the document windows and the main window as a whole. $\leftrightarrows$ Sec. 4.2.4 |
| Help | Provides access to help files like the manual and the programming reference, some pre-configured Focus Topic files and tools for troubleshooting. <br> $\rightarrow$ Sec. 4.2.5 |

The menu of the quick access toolbar F and the context menu of the actual ribbon both have the following two entries:
ITEM DESCRIPTION

| Show (Quick Access Tool- <br> bar) | The quick access toolbar can be shown at two different locations: in the title <br> bar of the main window ("above the ribbon") or in a separate row below the <br> Below / Above the Ribbon <br> ribbon. In the first case the space available for the quick access toolbar is <br> limited, and thus some ribbon items might not be shown in the quick access <br> toolbar itself but in its menu. |
| :--- | :--- |
| Minimize the Ribbon | If this option is active, the ribbon groups are only shown if you click on the <br> caption of a ribbon tab. This option can also be toggled by double-clicking on <br> the caption of a ribbon tab. |

### 4.2.1 Quick Access Toolbar

You can place ribbon groups and most of the ribbon items in the quick access toolbar by right-clicking on them and then selecting Add to Quick Access Toolbar. Items in the quick access toolbar can be

- Removed from the quick access toolbar by right-clicking on them and then selecting Remove from Quick Access Toolbar.
- Rearranged by clicking on the Rearrange Items in Quick Access Toolbar button 숭ㅇㅇ. This button is only enabled if there are two or more items in the quick access toolbar. $\hookrightarrow$ Sec. 4.2.1.1


### 4.2.1.1 Rearranging Items in the Quick Access Toolbar



Figure 4. The dialog for rearranging the items in the quick access toolbar. It contains a list of all available items at the left and two arrow buttons in the top right corner.

The dialog shown in Fig. 4 allows you to rearrange the items in the quick access toolbar and to save and load the complete configuration of the quick access toolbar. This dialog lists all items in the quick access toolbar, even those which are currently invisible. You can select any entry of that list with the mouse and then move it up or down, or delete it.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Move Up | Moves the currently selected item one step up. |
| Move Down | Moves the currently selected item one step down. |
| Add Separator | Removes the currently selected item from the quick access toolbar. |
| Load Configuration | Adds a separator to the bottom of the list which can be then be moved like all <br> other items. |
| Saves the current configuration of the items in the quick access toolbar to <br> disk. |  |
| Loads and applies a previously saved configuration. The file Autosaved. qat <br> in the Path for User Settings ( $\hookrightarrow$ Sec. 6.17) contains the configuration valid the <br> last time VirtualLab Fusion was closed. |  |

### 4.2.2 File Menu

| ITEM | DESCRIPTION |
| :---: | :---: |
| New | Creates an empty (General) Optical Setup ( $\leftrightarrows$ Sec. 43). If you click on the arrow, you can additionally create an IFTA Optimization document ( $\rightarrow$ Sec. 97) or a module ( $\leftrightarrows$ Sec. 7.2). <br> Ctrl $+\square$ is the shortcut for a new Optical Setup and Ctrl] +M is the shortcut for a new C\# module. |
| Open | Opens one or more files in one of VirtualLab Fusion's document formats ( $\rightarrow$ Sec. 4.1). Shortcut Ctrll $+\square$ |
| Import | Imports text files, images, Zemax OpticStudio® lens and beam files and old VirtualLab Fusion formats. $\hookrightarrow$ Part XVI |
| Global Options | Opens a dialog for editing global options and parameters. $\hookrightarrow$ Sec. 6. |
| (3) Online Help | Link to application scenarios and tutorials on www.lighttrans.com. |
| Exit | Closes all open documents and exits VirtualLab Fusion. Shortcut $417+$ F4 |

When any document is open the file menu additionally contains the following menu items:

| ITEM | DESCRIPTION |
| :---: | :---: |
| HSave | Saves the currently active document to the same file the document was loaded from. For newly created documents it asks for a file name. Shortcut $\mathrm{Ctrl}+\mathrm{S}$ |
| 式 Save As | Asks for a file name and saves the document to this file. Shortcut $\text { Ctrl }+ \text { Shift }+ \text { S }$ |
| Whel Incremental Save | Allows you to quickly save a document under an automatically given file name, for example to keep the current state for reference. If the document has not been saved before, it is stored with a default name in the folder \{Path for User Settings ( $\hookrightarrow$ Sec. 6.17) \} $\backslash$ Autosaved Files. Otherwise the already given file name is used with a numeral suffix which is incremented by one with each saving in order to not overwrite files. Shortcut $\mathrm{Ctrl}+\mathrm{Alt}+\mathrm{S}$ |

For some document types, there is also an Export menu item, which allows the user to save the currently active document in a non-standard file format.
Furthermore, the 20 most recently opened documents are listed at the right of the file menu. The first 10 of these documents can also be opened with the shortcuts Ctrl+1... Ctrl+0. All entries of this list can be deleted using the $\times$ button at the top right corner of the recent files list.

### 4.2.3 Start Ribbon Tab

| ITEM | DESCRIPTION |
| :--- | :--- |
| New | Creates an empty (General) Optical Setup ( $\hookrightarrow$ Sec. 43). If you click on the <br> arrow, you can additionally create an IFTA Optimization document $(\hookrightarrow$ Sec. 97) <br> or a module ( $\hookrightarrow$ Sec. 7.2$).$ |
| Open | Opens on or more files in one of VirtualLab Fusion's document formats <br> $(\hookrightarrow$ Sec. 4.1). |


| Save | Saves the currently active document to the same file the document was |
| :--- | :--- |
| loaded from. For newly created documents it asks for a file name. |  |
| Calculators | This ribbon group contains a Calculators menu, ↔Part XV. |
| Diffractive Optics $>$ | Opens the dialog described in Sec. 99.1 which allows you to easily design a |
| "Gaussian $\rightarrow$ Top Hat" | beam shaper transforming a (super-)Gaussian input field into another super- |
| Transmission Design | Gaussian top hat. |
| Diffractive Optics $>$ | Helps you to setup the IFTA optimization document for beam shaping tasks. |
| Diffractive Beam Shaper | $\hookrightarrow$ Sec. 99.2 |

## 4．2．4 Windows Ribbon Tab

| ITEM | DESCRIPTION |
| :---: | :---: |
| Close All | Closes all currently open document windows． |
| $\square^{\square 8}$ Close All But Current | Closes all currently open document windows which are not active． |
| 梂 Close All Result Win－ dows | Closes all currently open result windows．Sec． 4.1 lists which document types are shown in result windows． |
| 品 Cascade | All document windows are cascaded． |
| \％Tile Horizontally | All document windows are tiled horizontally． |
| 1．Tile Vertically | All document windows are tiled vertically． |
| 蜀 Arrange Icons | All minimized document windows are arranged． |
| Change Size of Result Windows | Allows you to set the size of all open result windows（or to minimize them）． $\hookrightarrow$ Sec．4．1．1 |
| \｛Active Document Win－ dow Selection\} | A drop－down list to select one of the currently open documents as the active document． |
| A Rename Document | Changes the title of the currently active document window（Shortcut：F2）． |
| （ Duplicate Document | Duplicates the currently active document window．When you click on the arrow，you have the additional choice to copy only the actual document，not the view settings．In this way you can get rid of misconfigured or unwanted view settings．Examples are a diagram which shows nothing because the view range is wrong or when you get documents from colleagues but want to use your default windows size and color table configured in the Global Options dialog（ $\hookrightarrow$ Sec．6）． |
| （9）Reset Docking Tabs | Resets all docking tabs（ $\checkmark$ Sec．4．3）to their default position and size． |
| 備 Show／Hide Right Docking Tab | Shows the right docking tab if it is hidden－and vice versa．Shortcut：F4． |
| Show Status Bar | Toggles the visibility of the status bar（ $\hookrightarrow$ Sec．4．4）． |

## 4．2．5 Help Ribbon Tab

| ITEM | DESCRIPTION |
| :---: | :---: |
| 2圈 Content | Opens the help system and shows the table of contents． |
| E葍 Index | Opens the help system and shows the index． |
| 閏 Programming Refer－ ence | Opens the VirtualLab Fusion programming reference documenting useful commands for programming． |
| Assistant | This ribbon group offers context sensitive help for the currently active docu－ ment view． |
| Focus Topics | this ribbon group contains links to Focus Topic Files which demonstrate how certain tasks can be done in VirtualLab Fusion．They are grouped into several categories and updated dynamically，so that new focus topics appear in this menu as soon as they are available． <br> The Show Sample Files button determines whether VirtualLab Fusion sample files are opened when you click on a focus topic item．Else only the corre－ sponding web page is opened in your browser． |
| Diagnosis \＆CleanUp | Opens a dialog with three options： <br> －Clean up the RAM from unused VirtualLab Fusion data． <br> －Check the external components used by VirtualLab Fusion． <br> －Write a support mail（see next item）． |
| Mail Support Informa－ tion | Prepares a mail to our support and shows it in your mail program．It contains some information we need to solve your issue． |
| ${ }_{12}{ }^{\text {O }}$ First Steps | A dialog helping you getting started with VirtualLab Fusion． |
| If What＇s New | A dialog explaining what is new in the current version． |
| （1）Tips and Tricks | Link to tips and tricks which ease using our software． |
| Vif About VirtualLab <br> Ces License Information | Shows a dialog with license，version，contact，and legal information． <br> Opens the dialog for viewing and managing your VirtualLab Fusion license． $\hookrightarrow$ Sec． 10 |
| Update Information | Opens a web link which shows whether updates are available．More infor－ mation can be found in the administrator＇s manual． |
| （ᄌ）3 ${ }^{17}$ Trial Configuration | Only available in the trial version． <br> Allows you to select the additional packages for VirtualLab Fusion（ $\hookrightarrow$ Sec．1）． |

### 4.3 Docking Tabs



Figure 5. Controls within a docked tab control.
The user interface of VirtualLab Fusion contains five special tab pages:

| TAB | DESCRIPTION |
| :---: | :---: |
| Parameter Overview Tree | Only for Optical Setups <br> Provides quick access to most parameters of a Optical Setup. $\rightarrow$ Sec. 43.7 |
| Property Browser | Allows you to view and manipulate properties of the currently active document. Depending on the document type, the property browser will be divided into several panels. |
| VirtualLab Fusion Explorer | Offers a convenient way to toggle between the distinct open windows. $\rightarrow$ Sec. 4.3.1 |
| Distributed Computing | Allows you to configure server and clients for distributed computing. $\leftrightarrows$ Sec. 8 |
| Messages | Shows error, warning and status messages. It has its own context menu which allows the user to Cut $([\operatorname{Ctr1}]+\mathbb{\boxtimes})$, Copy $(\overline{\mathrm{Ctrl}}+\mathrm{C})$, Paste $([\operatorname{Ctrl}]+\mathrm{V})$ certain messages as well as to Select All (Ctrl $+\boxed{A}$ ) content and to Clear all text. If you hold the Ctrl-key while scrolling with the mouse wheel, the font size of this control changes. |
| Detector Results | Shows detector results in a tabular form whereas the latest entry is shown at the top of the table. Via its context menu you can <br> - Copy Selected Detector Results to the clipboard for easy import to spread sheet programs and text files. <br> - Specify to Show Physical Units. If you disable this option all detector results are converted to their respective base unit and no units are shown anymore. For example, " 1 nm " will then be shown as " $1 \mathrm{e}-9$ " and " $180^{\circ}$ " will be shown as " 3.1416 ". This simplifies using copied values in external programs. <br> - Usually the columns are automatically resized to show as much content as possible. But you can resize them to your likings by moving the mouse between two column headers. The cursor then switches to a double arrow with a bar and you can click and drag to change the column width. (The same is possible for the row heights.) If you switch to Fixed Column Widths, the current column widths remain even if this table is resized or new detector results are calculated (which else triggers a new automatic resizing). <br> - Clear Detector Results, i. e. clear the entire table. |

By default, the Parameter Overview Tree, the Property Browser and the VirtualLab Fusion Explorer tab pages are placed in a tab control which is docked at the right of the main window. The Messages and the Detector Results tab pages are placed in a tab control which is docked at the bottom of the main window. These two tabs are marked with a $\Delta$ if new data is written into them while another tab in the tab control they are placed in is visible.
The tab controls can be resized by dragging their borders. They also can be moved around by clicking onto their title bar and dragging them while keeping the left mouse button pressed. Usually such a moved tab control becomes a floating tab which is independent from the main window. But if you move a tab control onto a guide [.0] it becomes a docked tab control again which changes its position and size with the main window. A tab control can be docked at the left, at the right or at the bottom of the main window; besides any other docked tab control or inside any other tab control.
In the same way you can move a single tab page by clicking onto the tab and dragging it while keeping the left mouse button pressed. If you do not move a tab page into an already existing tab control it becomes its own tab control. Docked tab pages can be set into an auto hide mode which means that only its tab is shown unless you move the mouse onto the tab. This mode can be toggled with the pin at the right of its title bar.
By clicking onto the ribbon item Windows > Reset Docking Tabs all four tabs become docking tabs again and are set to their default position and size. By clicking Windows > Toggle Visibility of Property Browser (shortcut (F4) you can always make the Property Browser visible, which means that it becomes the active tab of its tab control and that the auto hide is turned off if applicable. If the Property Browser is visible and you use this ribbon item, the tab control is set to auto hide mode if it is docked and another tab in its tab control becomes the active tab.

### 4.3.1 VirtualLab Explorer



Figure 6. The VirtualLab Fusion Explorer with some sample documents, among others a Regular Beam Splitter Session Editor with associated documents.

The VirtualLab Explorer ( $\hookrightarrow$ Fig. 6) displays all currently open document windows under a central node named VirtualLab Session. For a better overview, session editors ( $\hookrightarrow$ Sec. 47) and documents generated by them are grouped under one node. The currently active document is marked red.
If you right-click with the mouse on a document window (= leaf node), this document is selected (but not activated) and a context menu with the following options opens.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rename | Opens a dialog where you can change the caption of the selected document <br> window (but not its number). |
| Minimize | Minimizes the selected document window to the lower left corner of the doc- <br> ument area. |
| Bring to Front | Brings the selected document window to the front (which means that it is no <br> longer obscured by other document windows) and makes it the active window. <br> If a document window was minimized it is reverted to normal size. <br> The same can be done by double-clicking on a tree node with the left mouse <br> button. |
| Close | Closes the selected document window. This can also be done with Shift + <br> Del. |

### 4.4 Status Bar

The bottom most part of the main window is reserved for the status bar. On the left it displays the number of CPU cores currently used for multi-core calculations. Furthermore it shows whether the Parameter Run ( $\hookrightarrow$ Sec. 44) itself runs parallel (also for Parameter Run) or only the simulation of each Optical Setup (not for Parameter Run). The multi-core configuration of VirtualLab Fusion can be changed in the Global options dialog ( $\leftrightarrows$ Sec. 6.15)
On the right of the status bar there are two gauges monitoring the current computer performance. The left one indicates the current CPU usage of VirtualLab Fusion (blue) and of all other processes (black). The right one shows the current usage of the physical memory. Memory used by other processes than the current instance of VirtualLab Fusion is indicated black. The memory used by the current instance of VirtualLab Fusion is marked green. If more than $95 \%$ of the total physical memory are used, only one red bar is shown. You can switch these gauges on or off by right clicking on them and then either checking or unchecking Use Monitoring, respectively.

## Note on CPU usage

Hyperthreading is a technique on most modern CPUs to faster switch between two threads when one is waiting for data. In this case, the operating system sees two logical cores for each physical core. Thus it is completely normal that fully parallelized algorithms use "only" all physical cores which results in a CPU usage of "only" $50 \%$.

### 4.5 Notifications and Notify Icon

If you work in other programs while long lasting simulations run in VirtualLab Fusion, you will miss when these simulations are finished. To solve this problem, VirtualLab Fusion uses Windows ${ }^{\text {™ }}$ notifications, shown as popups in the bottom right of the main screen. Notifications need a notify icon in the right part of the task bar (the notification area).
How the notifications look and behave and how long they are shown depends on the used Windows version. For example in Windows 10 notifications play a sound and they are stored in the Action Center so that you can read them later.


Figure 7. The three types of notifications used by VirtualLab Fusion.
VirtualLab Fusion offers three types of notifications ( $\hookrightarrow$ Fig. 7):

| TYPE | DESCRIPTION |
| :--- | :--- |
| Info | Shown if a simulation was completed successfully. This applies to Optical Se- <br> tups, Parameter Runs, Parametric Optimizations, and Iteration Documents. |
| Warning | Shown if a simulation is halted because the free RAM would fall short the <br> Guaranteed Amount of Remaining Physical Memory ( $\hookrightarrow$ Sec. 6.14$)$ if the sim- <br> ulation continued. |
| Error | Shown if an Optical Setup aborts its simulation due to errors. The other doc- <br> ument types mentioned above always complete successfully - they just skip <br> the current simulation if errors occur. |

By double-clicking on the icon you can activate the corresponding VirtualLab Fusion main window, i. e. bring it to the front, "un-minimize" it, and give it the focus. The latter means that you can use for example the ribbon shortcuts with Alt $+\ldots$
The notify icon has a context menu with some useful shortcuts:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Activate Main Window | Activates the corresponding VirtualLab Fusion main window, i.e. brings it to the front, "un-minimizes" it, and gives it the focus. |
| Global Options | Opens the Global Options dialog ( $\checkmark$ Sec. 6). |
| (2) Help > Content | Opens the online help system and shows the table of contents. |
| (3) Help > Index | Opens the online help system and shows the index. |
| Help > Programming Reference | Opens the VirtualLab Fusion programming reference documenting useful commands for programming. |
| (C) Help > Vif About VirtualLab | Shows a dialog with license, version, contact, and legal information. |
| x Exit VirtualLab | Closes all open documents and exits VirtualLab Fusion. |

Notifications and the notify icon can be switched off via the Global Options dialog ( $\hookrightarrow$ Sec. 6.3).

## 5 Common Controls

### 5.1 Control for Input of Values with Units

Text boxes for entering numerical values with units (in short: value text boxes) appear in numerous dialogs of VirtualLab Fusion, Fig. 8 shows an example.


Figure 8. Sample control for entering a wavelength.

Depending on the application of the control, the control is set to a certain measured quantity. If you enter a value without unit, the default unit (with no prefixes) of this physical property is used to interpret this value. If the interpreted value is less than 1 or greater or equal than 1000 then VirtualLab Fusion usually uses a unit with prefix to bring the value into that range. For example an entered length of "1234" is interpreted as 1234 meters and shown as " 1.234 km ", but of course you can enter " 1.234 km " as well.
The following table lists all measured properties and the corresponding units supported by VirtualLab Fusion. If two or more units are supported, the default unit is marked bold. Note that for the measured quantity "length", the default unit can be set by the user in the Global Options dialog ( $\hookrightarrow$ Sec. 6.5).
There are also units which you can use for entering values but which are never used by VirtualLab Fusion for output. They are marked gray in the table.

## Note for Developers

Usually values are stored internally in the default unit. For example a variable with a pressure value always contains the value in pascals, even if it was entered in kilopascals. The only exceptions to this rule are:

- Angle ( ${ }^{\circ}$ ): Values are stored in radians.
- Energy (eV): Values are stored in joules.
- Length: Values are always stored in meters, even if another default unit is set in the Global Options.
- Percentage: The actual values are stored ( $50 \% \rightarrow 0.5$ ).


## PHYSICAL PROPERTY UNITS

| No Unit | - |
| :---: | :---: |
| Absorption Coefficient | " $\mathrm{m}^{-1}$ " (or " $1 / \mathrm{m}$ ") |
| Angle ( ${ }^{\circ}$ ) | "*" (or "deg"), "т" ("pi", "Pi", or "Pl"), "rad", "mrad" |
| Angle ( $\mathrm{rad}^{\circ}$ ) | "○" (or "deg"), "r"" ("pi", "Pi", or "PI"), "rad", "mrad" |
| Arbitrary Unit | "A.U." |
| Area per Energy | "m²/J" |
| (Area per Energy) ${ }^{\mathbf{2}}$ | "m4/ ${ }^{2}$ " |
| Electric Field Strength <br> (Electric Field Strength) ${ }^{2}$ | " $\mu \mathrm{V} / \mathrm{m} ", ~ " \mathrm{mV} / \mathrm{m} ", ~ " \mathrm{~V} / \mathrm{m} ", ~ " \mathrm{kV} / \mathrm{m} ", ~ " M V / m "$ <br>  |
| Energy (eV) | "meV", "eV", "keV", "MeV", "GeV", "nJ", " $\mu \mathrm{J}$ ", "mJ", "J", "kJ", "MJ" |
| Energy (J) | "meV", "eV", "keV", "MeV", "GeV", "nJ", " $\mu \mathrm{J}$ ", "mJ", "J", "kJ", "MJ" |
| Energy per Area | "J/m ${ }^{2}$ " |
| Energy per Volume | "J/m ${ }^{3}$ " |
| Illuminance | "Ix" (or "Im/m ${ }^{2 \prime}$ ) |
| Information (Decimal) | "B", "kB", "MB", "GB", "TB", "PB", "EB", "kiB", "MiB", "GiB", "TiB", "PiB", "EiB" |
| Information (Binary) | "B", "kB", "MB", "GB", "TB", "PB", "EB", "kiB", "MiB", "GiB", "TiB", "PiB", "EiB" |
| k-Domain Electric Field Strength |  |
| (k-Domain Electric Field Strength) ${ }^{\mathbf{2}}$ |  |
| k-Domain Magnetic Field Strength | " $\mu$ A m", "mA m", "A m", "kA m", "MA m" |


| (k-Domain Magnetic Field Strength) ${ }^{2}$ |  |
| :---: | :---: |
| Length | ```"fm", "pm", "nm", " }\mu\textrm{m}", "mm", "cm", "dm", "m", "km" "in" (or "inches", or "inch", or "" "), "mil" (1/1000 inch), "ft" (or "foot", or "feet", or " "), "yd" (or "yard", or "yards"), "mile" (or "miles")``` |
| Line Density | "cycles/mm" |
| Logarithmic Level | "dB" |
| Luminance | "cd/m ${ }^{2 \prime}$ ( or " $1 \mathrm{~m} / \mathrm{sr} / \mathrm{m}^{2 \prime}$ ) |
| Luminous Energy | "(lm s)" |
| Luminous Energy Density | "( lms ) $/ \mathrm{m}^{3}{ }^{\text {" }}$ |
| Luminous Flux | "Im" |
| Luminous Intensity | "cd" (or "Im/sr") |
| Magnetic Field Strength | " $\mu \mathrm{A} / \mathrm{m}$ ", "mA/m", "A/m", "kA/m", "MA/m" |
| (Magnetic Field Strength) ${ }^{\text {2 }}$ |  |
| Percentage | "\%" |
| Per Volume | " $1 / \mathrm{m}^{3}$ ", " $1 / \mathrm{dm}^{3 ",}$, $1 / \mathrm{cm}^{3 "}$, " $1 / \mathrm{mm}^{3}$ ", " $1 / \mu \mathrm{m}^{3}$ ", " $1 / \mathrm{ft}^{3}$ ", " $1 / \mathrm{in}^{3 "}$ |
| Power | "pW", "nW", " $\mu \mathrm{W}$ ", "mW", "W", "kW", "MW", "GW" |
| Power per Area |  |
| (Power per Area) ${ }^{\mathbf{2}}$ | $\begin{aligned} & "\left(\mu \mathrm{~W} / \mathrm{m}^{2}\right)^{2 "}, \quad "\left(\mathrm{~mW} / \mathrm{m}^{2}\right)^{2 "}, \quad "\left(\mathrm{~W} / \mathrm{m}^{2}\right)^{2} ", \quad "\left(\mathrm{~mW} / \mathrm{mm}^{2}\right)^{2^{\prime \prime}}, \quad "\left(\mathrm{~W} / \mathrm{mm}^{2}\right)^{2^{\prime \prime}}, \\ & "\left(\mathrm{~W} / \mu \mathrm{m}^{2}\right)^{2 "} \end{aligned}$ |
| Power per Solid Angle | " $\mu \mathrm{W} / \mathrm{sr}$ ", "mW/sr", "W/sr" |
| Power per Solid Angle and per Area | $" \mu \mathrm{~W} / \mathrm{sr} / \mathrm{m}^{2 "}, " \mathrm{~mW} / \mathrm{sr} / \mathrm{m}^{2 "}, " \mathrm{~W} / \mathrm{sr} / \mathrm{m}^{2 "},{ }^{2} \mathrm{~mW} / \mathrm{sr} / \mathrm{mm}^{2 "}$, "W/sr/mm ${ }^{2 "}$, " $\mathrm{W} / \mathrm{sr} / \mathrm{mm}^{2}{ }^{2}$ |
| Power per Volume | "W/m ${ }^{3}$ " |
| Pressure | "Pa", "hPa", "kPa", "MPa", "GPa", "mbar", "bar", "atm" |
| Spectral Radiant Energy | "J/m" |
| Spectral Radiant Energy Density | "J/m" |
| Spectral Radiant Flux | "W/m" |
| Spectral Radiant Intensity | "W/(msr)" |
| Temperature ( ${ }^{\circ} \mathrm{C}$ ) | "K", "${ }^{\circ} \mathrm{C}$ ", " ${ }^{\circ} \mathrm{F}$ " |
| Temperature (K) | "K", " ${ }^{\circ} \mathrm{C}$ ", " ${ }^{\circ}$ " |
| Temporal Frequency | "mHz", "Hz", "kHz", "MHz", "GHz", "THz", "PHz" |
| Time | "as", "fs", "ps", "ns", " $\mu \mathrm{s}$ ", "ms", "s", "min", "h" |
| Volume per Energy | "m/J" |
| (Volume per Energy) ${ }^{2}$ | "m/ $\mathrm{J}^{2}$ " |
| Wave Number | "m ${ }^{-1}$ " (or " $1 / \mathrm{m}$ ") |

Some units contain characters which cannot be entered easily with every keyboard. Thus in addition to the replacements given in the table above, you can replace " $\mu$ " by " $u$ " and superscript digits like " 2 " by "^2" when entering a unit. The narrow no-break space used for separating multiplied units can be omitted.

By default, values are displayed with the Number of Digits specified in the Display of Numbers subcategory of the Global Options dialog ( $\hookrightarrow$ Sec. 6.5), but this can be changed via the context menu (see below).
Furthermore, a small indicator may be used in order to show whether a text box doesn't display all available digits. This indicator has to be activated in the Global Options dialog. The appearance of this indicator is depicted in Fig. 9. If the mouse is moved over the indicator, a tooltip shows the number in full precision.


Figure 9. The hidden digits indicator of a value text box.
If you enter invalid data into a value text box, its text is marked red and the dialog containing this control is locked (this means OK button, Next button, etc. are disabled). If you move the mouse over the control a tool tip with the error message is displayed.
This control can also be used for the input of integer values with no unit. In this case a spinner can be used in addition to the actual text box.
The context menu of this control has the following entries.

| ITEM | DESCRIPTION |
| :---: | :---: |
| \{Unit Selection\} | If the control is set to a measured quantity with more than one unit, there is a combo box with all available units (even those which are usually used only for input). You can select any of these units and the current value is then shown with this unit. |
| Precision | Defines how many digits are shown. You can switch between Full (10 digits) and the Default set in the Global Options dialog ( $\hookrightarrow$ Sec. 6.5). |
| Left Aligned Text | Shows the text in the text box left-aligned, which can be helpful in case not all digits can be shown at once. |
| Insert Infinity | In some cases, this control allows you to enter infinite values, where "inf" and "-inf" correspond to Positive and Negative infinity, respectively. For convenience these strings can also be entered via the context menu. |
| Undo | Allows you to undo the last text change. |
| Copy Text | Copies the text as shown in the text box into the Windows ${ }^{\text {TM }}$ clipboard, for example " 1.23 nm " or "180". Shortcut: Ctrl+C. |
| Copy Value | Copies the actual value represented by the text box to the Windows ${ }^{\text {TM }}$ clipboard, including also the non-shown digits. For example "1.234567e-9" if the text box shows "1.23 nm" (with 3 digits) or "3.1415926535897931" if the text box shows "180". Shortcut: Ctrl+Shift+C. |
| Paste | Pastes the content from the Windows ${ }^{\text {TM }}$ clipboard into the text box if possible. If the value was copied from another text box, it might change the unit. For example if you paste the value " 1.23 " into a text box showing percentages, it becomes "123 \%". Shortcut: Ctrl+V. |
| Select All | Selects the complete content of the text box. Shortcut: Ctrl + A. |

### 5.2 Control for Input of Complex Values



Figure 10. Example of a control to enter a complex value with physical units.
Left: Real and imaginary part of a complex number can be entered. Right: Amplitude and phase of a complex number can be entered.

This control consists of two controls to enter a value with a unit as described in Sec. 5.1, and two buttons. If
 pressed amplitude and phase can be entered.

### 5.3 Control for Input of Two-Dimensional Vectors

$17.453 \mathrm{~mm} \times 17.453 \mathrm{~mm}$
Figure 11. Example of a control to enter a two-dimensional vector.

This control consists of two controls to enter a physical value ( $\hookrightarrow$ Sec. 5.1), one for the $x$-direction and one for the $y$-direction. If you double click into one of these controls, the value from the other control is copied into this control. If the control is used to enter value ranges instead of a point, $a \times$ is shown between the two controls.

### 5.4 Control for Input of Double Arrays

This control can be used to enter a one- or two-dimensional array of values with double precision.

| Number of Entries |  |  |  |  |  |  |  | 11 |  | $\star$ | 7 | $\stackrel{\square}{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parameter Extraction |  |  |  |  |  |  |  |  |  |  |  |  |
| $\checkmark$ Make Entries Available for Parameter Extraction |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Values |  |  |  | 0.1 |  |  | Maximum Values |  |  | 10 |  |  |
| Array Index \#0 -> |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|  | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 |
|  | 1 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
|  | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 |
|  | 3 | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 1 |
|  | 4 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 |
|  | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
|  | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reset Table |  |  |  |  |  |  |  |  |  | Export/Import |  |  |

Figure 12. Control to enter a two-dimensional array of values with double precision.

Example for a text file for data import:
\# Comment Line
1; 2; 3
3; 2; 1
5; 6; 7

The following settings can be made for an array of values:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Number of Entries | The number of entries in the array. |
| Make Entries Available for Parameter Extraction | If you check this option, each entry of the array can be varied via Parameter Extraction ( $\leftrightarrows$ Sec. 43.5) and thus used e.g. in the Parameter Run ( $\hookrightarrow$ Sec. 44). If the array contains more than 100 entries, a warning is shown that this might slow down the tables where the parameters to vary are configured. |
| Minimum Values / <br> Maximum Values | If Make Entries Available for Parameter Extraction is checked, you can preset the minimum and maximum value for each entry here. In e.g. the Parameter Run you can later diminish the specified range, but not extend it ( $\hookrightarrow$ Sec. 44.2). |
| Table of entries | In the table you can specify the actual value of each entry. |
| Reset Table | After you have changed the Number of Entries you must reset the table, which means that the size of the table is adjusted and all cells are filled up with the default value of " 1 ". |
| Export / Import > Import Text File | You can import the values of the array from a .txt or .csv file. The file must have the format given in the marginal. |
| Export/Import > Export to Text File | You can export the values of the array into a .txt or .csv file. |
| Export / Import > Import <br> Data Array | You can import the values from any open one- or two-dimensional data array. If the data array contains more than one subset, you can choose which subset to import. If the subset to import is complex-valued, only the real value is imported. |
| Export / Import > Export <br> Data Array | You can export the values configured within the dialog into a data array. As a result of this operation the generated data array is shown as document within VirtualLab Fusion. |

### 5.5 Control for Defining a Single Direction

In many cases where a direction vector in $\mathbb{R}^{3}$ has to be defined, a special control (see Fig. 13) can be used which is introduced here.


Figure 13. Control for defining a direction vector.
Since there are several kinds of direction definition conventions ( $\hookrightarrow$ Sec. 139.2), the appearance of the control can vary strongly. The only common controls always available are

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition Type | The convention to use for defining the direction vector ( $\hookrightarrow$ Sec. 139.2) can be <br> selected here. |
| Direction | The normalized direction vector which corresponds to the entered direction <br> data. |
| Validity | An indicator which shows whether or not the entered data are consistent <br>  <br>  <br>  |

All other controls are convention-specific and will be described in the following sections Sec. 5.5.1 to Sec. 5.5.6.

### 5.5.1 Direction Vector

See also Sec. 139.2.7 for more details on this convention.

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\mathbf{X / Y / Z}$ | The components of a (not necessarily normalized) direction vector. |

### 5.5.2 Spherical Angles

See also Sec. 139.2.1.1 for more details on this convention.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Reference Axis | The coordinate system's base vector which is to be inclined by Theta and Phi. |
| Theta | Spherical angle $\theta$, measured from the reference axis in a plane constructed by <br>  Axis) by the other sphere angle $\phi$. |
| Phi | Spherical angle $\phi$, representing a rotation about the reference axis. It is measured in the plane perpendicular to the reference axis, between the $y-, z-$ or $x$-axis (depending on the choice of the Reference Axis) and the line of nodes. The latter is identical to the axis the reference axis is rotated about by the inclination angle $\theta$. |

### 5.5.3 Direction Angles

See also Sec. 139.2.2.1 for more details on this convention.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rho | The angle between the direction to be defined and the $x$-axis. This angle's <br> cosine is identical to the $x$-component of the normed direction vector. |
| Sigma | The angle between the direction to be defined and the $y$-axis. This angle's <br> cosine is identical to the $y$-component of the normed direction vector. |
| Tau | The angle between the direction to be defined and the z-axis. This angle's <br> cosine is identical to the z-component of the normed direction vector. |
| Direction inside negative <br> X/YIZ half space | This check box indicates whether or not the $x / y / z-c o m p o n e n t ~ o f ~ t h e ~ d i r e c t i o n ~$ <br> to be defined is negative. |

## 5．5．4 Cartesian Angles

See also Sec．139．2．3．1 for more details on this convention．

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reference Axis | The coordinate system＇s base vector which is to be inclined by Alpha and <br> Beta． |
| Alpha | The angle between the reference axis and the projection of the direction to be <br> defined onto the x－z－or $x-y$－plane（depending on the choice of the Reference <br> Axis）． |
| Beta | The angle between the reference axis and the projection of the direction to be <br> defined onto the y－z－or x－z－plane（depending on the choice of the Reference <br> Axis）． |

## 5．5．5 Sequence of Axis Rotations

See also Sec．139．2．4．1 for more details on this convention．

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reference Axis | The coordinate system＇s base vector which is to be rotated by the rotation <br> sequence． |
| X／Y／Z－Axis Rotation | Angle of rotation about the $\mathrm{x}-/ \mathrm{y}-/ \mathrm{z}$－axis． |
| $\boldsymbol{\square}$ | Changes the sequence of rotation by lifting the current angle one position up． |
| $\downarrow$ | Changes the sequence of rotation by lowering the current angle one position <br> down． |
| $\square$ | Flips the sequence of rotation． |
| $\square$ | Adds a new rotation． |
| $\square$ | Deletes the currently selected rotation． |

## 5．5．6 Rotation Matrix

See also Sec．139．2．6．1 for more details on this convention．

| ITEM | DESCRIPTION |
| :---: | :---: |
| Reference Axis | The coordinate system＇s base vector which is to be rotated by the rotation matrix． |
| Matrix Entries | The nine entries of the rotation matrix can bee set here． |
| 解 $->$ Copy | Copies the complete matrix to clipboard（as a string）． |
|  | Tries to paste a matrix from clipboard．It may have the format＂s11；s12；s13； s21；s22；s23；s31；s32；s33＂with s11 to s33 being strings for each of the nine matrix elements． |
| 燿 $->$ Normalize | Normalizes the matrix． |
| 袻－＞Set to Identity | Sets the matrix to the identity matrix． |
| ช－＞Transpose | Transposes the current matrix． |

### 5.6 Control for Defining a Solid's Orientation

In many cases where a solid's orientation in $\mathbb{R}^{3}$ has to be defined, a special control can be used which is introduced here.
Since there are several kinds of orientation angle conventions ( $\hookrightarrow$ Sec. 139.2), the appearance of the control can vary strongly. The only common controls always available are

| ITEM | DESCRIPTION |
| :--- | :--- |
| Orientation | Definition |
| Type | The convention to use for defining the orientation ( $\hookrightarrow$ Sec. 139.2) can be se- |
| lected here. |  |

All other controls are convention-specific and will be described in the following sections Sec. 5.6.1 to Sec. 5.6.6.

### 5.6.1 Spherical Angles

See also Sec. 139.2.1.2 for more details on this convention.


Figure 14. Control for determining an orientation via spherical angles and a rotation about the z-axis.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Theta (Spherical) | Spherical angle $\theta$, measured from the z-axis in a plane constructed by rotating the x-z-plane by the other sphere angle $\phi$. |
| Phi (Spherical) | Spherical angle $\phi$, representing a rotation about the z-axis. It is measured in the $x-y$-plane between the $y$-axis and the line of nodes. The latter is identical to the axis the whole coordinate system is rotated about by the inclination angle $\theta$. |
| Z-Axis Rotation Angle | Angle $\zeta$ of a rotation about the z-axis. |
| Swap Order | Using this button, the sequence of inclining the z-axis via $\theta$ and $\phi$ on the one hand and of rotating about the z-axis on the other hand can be flipped. If ZAxis Direction Definition is above Rotation About Z-Axis, the z-axis inclination is done first, followed by the $z$ '-axis rotation. If the sequence is the other way round, The $z$-axis rotation is done first, followed by the inclination in reference to the new rotated coordinate system. |

### 5.6.2 Direction Angles

See also Sec. 139.2.2.2 for more details on this convention.


Figure 15. Control for determining an orientation via direction angles and a rotation about the z-axis.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Rho | The angle between the new $z$ '-axis and the old $x$-axis. This angle's cosine is identical to the $x$ component of the normed $z^{\prime}$-vector. |
| Sigma | The angle between the new $z$ '-axis and the old $y$-axis. This angle's cosine is identical to the y component of the normed $z$ '-vector. |
| Tau | The angle between the new z'-axis and the old z-axis. This angle's cosine is identical to the $z$ component of the normed $z$ '-vector. |
| Z-Axis inside negative X/Y/Z half space | This check box indicates whether or not the $x / y / z$-component of the new $z$ '-vector is negative. |
| Z-Axis Rotation Angle | Angle $\zeta$ of a rotation about the z-axis. |
| Swap Order | Using this button, the sequence of inclining the z-axis (via $\rho, \sigma$, and $\tau$ ) and of rotating about the $z$-axis can be flipped. If $Z$-Axis Direction Definition is above Rotation About Z-Axis, the z-axis inclination is done first, followed by the $z$ '-axis rotation. If the sequence is the other way round, The $z$-axis rotation is done first, followed by the inclination in reference to the new rotated coordinate system. |

### 5.6.3 Cartesian Angles

See also Sec. 139.2.3.2 for more details on this convention.


Figure 16. Control for determining an orientation via Cartesian angles and a rotation about the z-axis.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Alpha | The angle between the old $z$-axis and the projection of the new $z^{\prime}$-axis onto <br> the $x$-z-plane. |
| Beta | The angle between the projection of the new $z$ '-axis onto the $y$-z-plane and <br> the old z-axis. |
| Z-Axis Rotation Angle | Angle $\zeta$ of a rotation about the $z$-axis. |
| Swap Order | Using this button, the sequence of inclining the $z$-axis via $\alpha$ and $\beta$ on the one <br> hand and of rotating about the $z$-axis on the other hand can be flipped. If $Z$ - <br> Axis Direction Definition is above Rotation About $Z$-Axis, the $z$-axis inclination <br> is done first, followed by the $z$ '-axis rotation. If the sequence is the other way <br> round, The $z$-axis rotation is done first, followed by the inclination in reference <br> to the new rotated coordinate system. |

### 5.6.4 Euler Angles

See also Sec. 139.2.5 for more details on this convention.

| Orientation Definition Type |  | Euler A | $\checkmark$ | (ii:) |
| :---: | :---: | :---: | :---: | :---: |
| i | Direction Definition |  |  |  |
|  | Angle / A |  | Value |  |
|  | Psi (Euler) | $\checkmark$ |  | $260^{\circ}$ |
|  | Theta (Euler) | $\checkmark$ |  | $10^{\circ}$ |
|  | Phi (Euler) | $\checkmark$ |  | $100^{\circ}$ |

Figure 17. Control for determining an orientation via Euler angles.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Psi (Euler) | The angle of rotation about the z-axis. |
| Theta (Euler) | The angle of rotation about the new $x^{\prime}$-axis, resulting from the former rotation. |
| Phi (Euler) | The angle of rotation about the new $z^{\prime}$-axis, resulting from the former rotation. |

### 5.6.5 Sequence of Axis Rotations

See also Sec. 139.2.4.2 for more details on this convention.


Figure 18. Control for determining an orientation via a sequence of rotations about coordinate axes.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Fix Axes | If checked，the sequence of rotations refer to fix axes．Otherwise，the non－first rotations are about axes resulting from former rotations． |
| X／Y／Z－Axis Rotation | Angle of rotation about the fix $x-/ y-/ z-a x i s$ ． |
| X＇／X＂／Y＇／Y＂／Z＇IZ＂－Axis Ro－ tation | Angle of rotation about the current $x^{\prime} / x^{\prime \prime} / y^{\prime} / y^{\prime \prime} / z^{\prime} / z^{\prime \prime}-$ axis，resulting from former rotations． |
| （ | Changes the sequence of rotation by lifting the current angle one position up． |
| （ | Changes the sequence of rotation by lowering the current angle one position down． |
| ＋ | Flips the sequence of rotation． |
| $\pm$ | Adds a new rotation． |
| $\square$ | Deletes the currently selected rotation． |

## 5．6．6 Rotation Matrix

See also Sec．139．2．6．2 for more details on this convention．

| ITEM | DESCRIPTION |
| :---: | :---: |
| Matrix Entries | The nine entries of the rotation matrix can bee set here． |
|  | Copies the complete matrix to clipboard（as a string）． |
| 笺－＞Paste | Tries to paste a matrix from clipboard．It may have the format＂s11；s12；s13； s21；s22；s23；s31；s32；s33＂with s11 to s33 being strings for each of the nine matrix elements． |
| （1） | Normalizes the matrix． |
| 简－＞Set to Identity | Sets the matrix to the identity matrix． |
| 細－＞Transpose | Transposes the current matrix． |

## 5．7 Button to Set a Document

This button（ $\hookrightarrow$ Fig．19）is labeled with Set．When you click on it a menu opens which allows you to set a result document（ $\hookrightarrow$ Sec．4．1）in various ways．Depending on the context not all entries might be available． Furthermore there might be constraints on which kind of document you can set，for example only equidistant two－dimensional data arrays with length coordinates．


Figure 19．The button to set a document．

| MENU ENTRY | DESCRIPTION |
| :--- | :--- |
| Load | Loads a data array from file. If the loaded document does not match the <br> constraints, it is shown as separate document but not set. So you can adapt <br> it via the Manipulations ribbon tab. |
| OnLY FOR GRIDDED DATA ARRAYS |  |
| Imports a data array from a bitmap or text file by means of the import wiz- |  |
| Imports. |  |
| ard described in Sec. 121.2. If the imported data array does not match the |  |
| constraints, it is shown as separate document but not set. |  |

### 5.8 Tables

Initially a table cell is always in display mode. If you want to change the content of a cell you can switch to the edit mode by double clicking on a cell or by pressing F2 when a cell is marked. It is also possible to simply start typing the new content. While in edit mode, a double click or Ctrl $+A$ marks the whole content of a cell. Quite often the content of a table cell is a physical value. Then the edit mode behaves similar to the control for input of physical values ( $\leftrightarrows$ Sec. 5.1). In particular values entered without a unit automatically get the default unit. But in contrast to this control, table cells usually not mark invalid values red but just restore the original value when you leave the edit mode. Furthermore in edit mode always all digits of a number are shown so that there is no loss of precision when editing a value.
In display mode a table has a context menu which allows you to copy the content of the currently selected cells to the Windows ${ }^{\text {TM }}$ clipboard so that they can be used in external programs like spreadsheet programs (Copy Selection). Often you can also Paste data into the table.

### 5.9 Control for Input of Data Pairs

This control ( $\hookrightarrow$ Fig. 20) is used for the input of a sample of paired values.


Figure 20. Example of control for input of data pairs.

### 5.9.1 Adding new data

There are three modes for the input of new data which are related to the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set Data Array | Allows you to load a one-dimensional, real-valued data array with matching <br> properties into the table. If you click on this button you can load the data array <br> from a file or from an already open document. $\hookrightarrow$ Sec. 5.7. |
| Add Datum | Clicking this button will open a dialog that allows the user to input a new pair <br> of values. |
| New Data Set | Clicking this button will open a dialog that allows the user to define the whole <br> range of the first column by input of a start value, an end value, and the total <br> number of values (see below). The second value is filled with a default value <br> initially and has to be set to the desired values as described in Sec. 5.9.2. |

### 5.9.1.1 Configuration of a New Set of Equidistant Data

Equidistant distributed data can be configured via the dialog described here.


Figure 21. Dialog for the definition of equidistant intervals.

| ITEM | DESCRIPTION |
| :--- | :--- |
| From | First (smallest) value for the first column. |
| To | Last (largest) value for the first column. |
| Number of Steps | Number of data pairs to enter. |

### 5.9.2 Modifying data

If you want to change any value in the table, you have to select the desired cell (by one left click or via arrow keys), then start to enter the new value. After editing just leave the cell.

### 5.9.3 Deleting data

If you want to delete one or more rows, select these rows and press Del. The complete table can be selected by marking both column headers. If a single cell is selected, pressing Del deletes the content of that cell while Shift + Del deletes the complete row.
In any case there will be a prompt for confirmation before deleting rows.

### 5.9.4 Exporting data

Marked cell contents can be copied to clipboard via Ctrl+C for further use e.g. in spreadsheet programs. Show Data Array shows the data as separate data array document ( $\leftrightarrows$ Sec. 13).

### 5.9.5 Interpolation method

Sometimes, the user can define the interpolation method to be used. In this case, also the Upper Limit is shown, this is the maximum $x$-value for which the data is defined.

VirtualLab Fusion tries to evaluate whether the entered data are equidistant or not and shows only the suitable Interpolation Methods. Note that simply changing a x-value or adding data can change the data from equidistant to non-equidistant or vice versa, thus changing the Interpolation Method. A warning is shown in that case. The actual value of the upper limit depends on the selected interpolation. For non-equidistant data and Constant Interval interpolation the Upper Limit can be set by the user. More information about interpolation method and the upper limit can be found in Sec. 13.2.

### 5.10 Validity Indicator

Validity: (0) Validity: i $^{2}$ Validity: $\otimes$
Figure 22. The different states of the control used to indicate the validity of a whole control.

In various places, a small symbol indicates the validity state of the current control ( $\hookrightarrow$ Fig. 22). The following table explains the various validity states.

| VALIDITY STATE | DESCRIPTION |
| :---: | :---: |
| 虎 | Consistency check is still in progress. |
| 0 | Everything is okay. |
| $4^{2}$ | There are several issues which might yield unexpected or unwanted results. The number of issues is shown as small red number. <br> In this state an additional libutton is shown. If you click this button a separate dialog explains all these warnings in detail. |
| $\boldsymbol{\otimes}$ | There are several issues which must be fixed before you can proceed (close the dialog with OK etc.). <br> In this state an additional libutton is shown. If you click this button a separate dialog explains all these errors in detail - and additional warnings if present. |

In the dialog showing all warnings and errors you can double click on one explanation to copy it to the Window ${ }^{\text {TM }}$ Clipboard. So you can use it for support requests.

### 5.11 Color Mapping

The Color Mapping Color control used at various locations in VirtualLab Fusion defines the mapping of a double value range to a color range and vice versa.


Figure 23. Control to set color mapping properties.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | Choose the vectorial component of the complex amplitude to be exported. <br> Note: This item is not always available. |
| Field Quantity | Choose the field quantity of the complex amplitude to be imported or exported. |
| Adapt Min / Max Values to | Adapt the color mapping to the min / max values of the specified complex <br> component in the given complex amplitude. <br> Field Extrema |
| Note: This item is not always available. |  |

### 5.12 Control for Defining Used Orders

The table in this control ( $\hookrightarrow$ Fig. 24) has two columns for 1D-periodic gratings (Direction and Order Number) and three columns for 2D-periodic gratings (Direction, Order Number X, and Order Number Y).
In the Direction column you can choose $T(+/+) / T(-/-)$ for a transmission order and $R(+/-) / R(-/+)$ for a reflection order. The expression in brackets indicates the sign of the z-component of the k-vector of the incident and the outgoing light (see also Sec. 43.9). Transmission orders have a blue background and reflection orders a red one.
In the order number column(s) you can enter the desired order number. In the Function tab of the Functional Grating ( $\hookrightarrow$ Sec. 59.1) there is an additional Efficiency column.

| Use | Direction | Order Number X | Order Number $Y$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\square$ | T ( $+/+$ ) | -2 | -2 |  |  |
| $\square$ | T (t/+) | -1 | -1 |  |  |
| $\checkmark$ | $T(+1+)$ | 0 | 0 |  |  |
| $\square$ | $T(+/+)$ | +1 | +1 |  |  |
| $\square$ | T ( $+1+$ ) | +2 | +2 |  |  |
| $\square$ | R (+/-) | -1 | 0 |  |  |

Figure 24. Control for defining the used orders of a 2D-periodic grating.
Below the table there are buttons to configure the table.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Add Order / <br> Tools > Add Order | Adds a new row to the end of the table. The initial direction and order number is taken from the currently selected row. For 1D-periodic gratings this order number is then incremented by one to allow you to easily add a sequence of consecutive orders. |
| Tools > Add Order Range | Opens a dialog where you can enter a Minimum Order and a Maximum Order and whether you Define Order Range for Reflection or for transmission. For 2D-periodic gratings you can define a minimum / maximum for $x$ - and $y$ direction separately. When you close the dialog with OK, all orders within the defined range (inclusive) are added to the end of the table; existing orders are overwritten. |
| Remove Order / <br> Tools > Remove Current Order <br> Tools > Remove All Reflection / Transmission Orders | Removes the currently selected order. This can also be done with the Del key. <br> Removes all reflection / transmission orders currently present in the table. |
| $\begin{aligned} & \text { Tools > Reset } \\ & \text { Tools > Sort } \end{aligned}$ | Resets the table so that it only shows the zeroth transmitting order. <br> Sorts the table firstly so that transmission orders appear above of the reflection orders and then by order number(s). Sorting is also done when the dialog containing this control is closed and re-opened. |
| Tools > Synchronize Efficiencies | Only if Efficiency column is shown. <br> Allows you to set one Efficiency for all reflection or transmission orders (depending on whether you Synchronize Orders for Reflection). |

### 5.13 Control for Programmable and Databased Input

This control can be used to define either a list of value pairs $(x ; y)$ or a function $f(x, y)$. If you select Programmable Input you have the following controls to program a snippet:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition | This group box allows you to program the actual snippet. Edit opens the <br> Source Code Editor $(\hookrightarrow$ Sec. 7.3$)$ to edit this snippet, and a validity indicator <br> $(\hookrightarrow$ Sec. 5.10$)$ shows whether this snippet is consistent. |
| Parameters 四 | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4 |

The Databased Input for value pairs offers a simple table for entering a preconfigured number of value pairs. Furthermore it has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set $>$ Load | Loads a data array from a .da file. The data array must contain only one <br> real-valued two-dimensional subset. |
| Set $>$ Import | Imports a data array from a bitmap or text file by means of the import wizard <br> described in Sec. 121.2. The imported data array must contain only one real- <br> valued two-dimensional subset. |
| Set $>$ Select from Docu-  <br> ments Allows you to select an already open data array, which must contain only one <br> real-valued two-dimensional subset.  |  |
| Show | Shows the current data in a separate data array view ( $\hookrightarrow$ Sec. 13.5). |
| Preview Table | A preview table showing the current data. |

### 5.14 Preview for Surface Media Sequences



Figure 25. Cross section of two lens pairs with the default color table "White and Mint". Air is marked light green. Glasses are marked by different shades of dark green. The third surface is currently selected and thus marked red.

Both the edit dialogs for a Lens System component ( $\hookrightarrow$ Sec. 57.1) and for optical stacks ( $\hookrightarrow$ Sec. 39) comprise a preview of their respective sequence of surfaces and media. This preview either shows the $x-z-$ plane for $y=$ 0 or the $y$-z-plane for $x=0$ in free aspect ratio. Fig. 25 shows a sample preview.
For surfaces the height profile in this plane is shown and for media the real refractive indices in this plane are visualized by different colors depending on the used color table. Surfaces are marked with Color 2 of the color table, the currently selected surface is marked with its Highlighting Color and a bit more thick. $\hookrightarrow$ Sec. 11.2.4.2 Absorbing regions of a surface ( $\hookrightarrow$ Sec. 35.1.1.1) and the media before and after them are not shown.
Via the context menu of the preview you can open an dialog ( $\hookrightarrow$ Fig. 26 ) for defining both the shown plane and the coloring.


Figure 26. The edit dialog to set up the view settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Show z-x-Plane / <br> Show $z-y$-Plane | This option allows you to choose whether you want to see a $z$-x-intersection (Show $z-x$-plane) or a $z-y-$-intersection (Show $z-y$-Plane). <br> This option is disabled for 1D-periodic stacks. |
| Color Table | The color table used for the preview. You can select any color table from the Customized Color Tables Menu ( $\rightarrow$ Sec. 11.2.4.1). |
| Draw Media | If you uncheck this option no media are drawn at all, but only the height profiles of the surfaces. |
| Preview Wavelength | The wavelength used for the calculation of the refractive indices. If this dialog is shown from within a grating component ( $\varsigma$ Sec. 64), the default preview wavelength is the preview wavelength set directly in the grating component. |
| Minimum Shown Refractive Index | Defines the minimum refractive index. Refractive indices less or equal this value use the start color of the color table. |
| Maximum Shown Refractive Index | Defines the maximum refractive index. Refractive indices greater or equal this value use the end color of the color table. |

### 5.15 3D View

The 3D view shows a geometry as seen with a virtual camera. The geometry can be any sequence of surfaces, thus a single surface ( $\varsigma$ Sec. 35), a Real Component ( $\leftrightarrows$ Part IX), an Optical Stack ( $\leftrightarrows \mathrm{Sec} .39$ ) or a complete Optical Setup ( $\varsigma$ Sec. 43) where light sources, ideal components and detectors are indicated by a single plane surface. For each surface the size, the height profile and the Surface Layout ( $\leftrightarrows$ Sec. 40) are shown, but no coatings or materials.
This technology is also the foundation for the 3D Ray Distribution View ( $\rightarrow$ Sec. 17.1).
The 3D view window ( $\hookrightarrow$ Fig. 27) can usually be displayed by a ( 3 button.


Figure 27. 3D view of a surface with tool bar (top middle), view cube (top right), Global Coordinate System (bottom left), simple scale (bottom right) and z-extension information (bottom).

The position and orientation of the virtual camera that captures the 3D scene can be controlled via mouse,
keyboard, and touchscreen. By default the orientation of the virtual camera is as shown in Fig. 27. In the upper part of the view there is a Tool Bar with 6 buttons which define the mouse mode, i. e. how the view behaves if you left click into the view and move the mouse while keeping the left mouse button pressed.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\bigcirc$ Magnifying Glass | Always shows a magnifying glass zooming into the area around the current mouse position. In this mode, a mouse click has no effect. |
| ¢, Zoom Window | This button allows you to define a Zoom Window. If you release the left mouse button it is zoomed into this region. |
| Q Zoom | As long as you keep the left mouse button pressed, moving the mouse up zooms into the view and moving the mouse down zooms out. |
| ↔Pan | Allows you to move the shown object within the view. |
| $\bigcirc$ Rotate | Allows you to rotate the shown object. |
| $\sum_{k=2}^{x}$ Zoom Fit | If this button is clicked, the object is zoomed and moved so that it is shown completely and as large as possible. Afterwards no mouse mode is selected. |

There is a View Cube in the upper left corner. If you click on a face, edge, or corner of this cube, the corresponding orientation is used. Clicking on the "ring" and keeping the left mouse button pressed allows you to rotate around the $z$-axis by moving the mouse.
In the lower left corner of the window there is a 3D icon that permanently shows the current axis directions of the Global Coordinate System of the geometry.
For a single surface, information about the z-extension of the surface is shown on the bottom of this control.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Left mouse button | Behavior defined by the buttons described above. |
| Ctrl + Left mouse button | Pan. |
| Shift + Left mouse but-  <br> ton Zoom in/out. <br> Mouse wheel Coarse zooming in/out. <br> $\operatorname{Ctrl}++$ Zoom in. <br> Ctrl $+\square$ Zoom out. <br> $\rightarrow, \uparrow, \leftarrow, \downarrow$ Rotate right, up, left and down by $2.5^{\circ}$ each. <br> $\operatorname{Ctrl}+$ F Zoom scene to fit perfectly in the 3D view. |  |

By right-clicking into the view a context menu with the following entries will open.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Select Elements to Show | Only available for Optical Setups <br> Opens a dialog where you can select which Optical Setup Elements shall be shown. $\hookrightarrow$ Sec. 5.15.1 |
| View Settings | Opens a dialog where you can adjust the view to your liking. You can preset these settings for all future views in the Global Options dialog ( $\hookrightarrow$ Sec. 6.3). |
| Show as Separate Document | Shows the current geometry in a separate document window for comparing or storing 3D views. The resulting document behaves nearly identically like a "normal" 3D view, only that there instead of the menu item Show as Separate Document, there is the ribbon item Windows > Duplicate Window. |
| Export to IGES | Exports the 3D scene to a IGES file after you have specified a path and name for it. Note that the scene is exported "as is", for example the outer planes are included in the file if they are visible within the scene. Furthermore, the Accuracy Factor of the view settings ( $\leftrightarrows$ Sec. 5.15.2.2) also influences the data in the resulting file. |
| Export to STL | Exports the 3D scene to a STL file after you have specified a path and name for it. Note that the scene is exported "as is", for example the outer planes are included in the file if they are visible within the scene. Furthermore, the Accuracy Factor of the view settings ( $\hookrightarrow$ Sec. 5.15.2.2) also influences the data in the resulting file. |

### 5.15.1 Select Elements to Show

For the 3D visualization of systems VirtualLab Fusion enables the user to select the Optical Setup Elements which shall be shown. Fig. 28 shows the edit dialog of the corresponding configuration tool.


Figure 28. The dialog to select the elements which shall be shown.
The upper part of the edit dialog ( $\hookrightarrow$ Fig. 28 ) shows all elements which are available. The user can select individually which component shall be shown or not.
The Selection Tools button offers the following four selection tools.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Select All | Selects all elements. |
| Unselect All | Unselects all elements. |
| Unselect Detectors and Source | Only Real and Ideal Components are selected. |
| Unselect Identity Operators and | Elements are unselected which have no optical functionality but only |
| Coordinate Breaks | aid in correctly setting up the Optical Setup. |

### 5.15.2 View Settings



Figure 29. The dialog to edit the view settings of the 3D view.

This dialog ( $\hookrightarrow$ Fig. 29) offer various options to adjust the 3D view. In the lower left corner there are the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reset All | Resets all options to the values defined in the Global Options dialog <br> $(\hookrightarrow$ Sec. 6.3). In the Global Options dialog itself, you then can reset to the <br> initial defaults. |
| Validity | With this button you can load view settings saved with the button. <br> With this button you can save the current view settings. In this way you can <br> e.g. use different view settings for different application scenarios. |
| A validity indicator ( $\hookrightarrow$ Sec. 5.10$)$ shows warnings if one feature disables an- <br> other feature. For example, rulers will not be shown if perspective distortion <br> is present because then the size of a surface changes with its distance from <br> the virtual camera. |  |

The actual view settings are grouped on the several pages which are described in the following subsections. (The page Rays is only used for the Ray Distribution View ( $\hookrightarrow$ Sec. 17) and thus explained in Sec. 17.1.3.)

### 5.15.2.1 Color Scheme

Various options to adjust the color of the background and of the surfaces.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Color Scheme | Primarily, this setting defines the brightness of the view background. But it <br> also influences the color of the view tools ( $\checkmark$ Sec. 5.15 .2 .5 ) and of the surfaces <br> when they are Uncolored. <br> You can select from Bright, Medium and Dark. |
| Background Color Gradi- <br> ent | If you select this option, the background is not shown with a solid color, but <br> has a gradient to a slightly more dark color. |
| Surface Colors | There are two color schemes for the surfaces. <br> - Colored: The surfaces of a real component are all drawn with the same <br> color which alternates between yellow and orange between subsequent <br> components. Light sources are always drawn in green, ideal compo- <br> nents in light blue, and detectors in red, respectively. Consequently, <br> single surfaces or components are always drawn yellow. <br> • Uncolored: All surfaces are either drawn in dark gray (if Color Scheme <br> is either Bright or Medium) or in light gray (for the Dark Color Scheme). |
|  | Absorbing areas between the inner definition areas ${ }^{1}$ of periodic surfaces are <br> always drawn in dark gray. |
| If checked, the surfaces are shown semi-transparent. |  |

### 5.15.2.2 Geometry

Options to define which and how triangle meshes are generated for the display of the geometry.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Show Envelopes | Toggles the visibility of the envelopes, meshes linking the borders of two consecutive surfaces within a component. There are no envelopes if the medium between the two surfaces is not solid. This feature has no effect for single surfaces or components consisting only of a single surface. <br> If this option is checked, Color and Transparency of the envelopes can be set. |
| Show Surrounding Planes | All surfaces shown in the 3D scene will be displayed with their defined (outer) definition areas ${ }^{1}$ (drawn in black if they are absorbing - otherwise the same colors as for surfaces are used). You can think of the apertures as infinitely expanded in $x$ - and $y$-direction, however, they are cut to a proper size in this view. |
| Accuracy | The accuracy factor for the sampling of the optical surface(s). The maximum accuracy factor is 15 . |
| Wireframe Mode | By default filled triangles are shown. If you check this option, the borders of the triangles are shown instead. In this way you can directly see the triangles making up the displayed geometry. |
| z-Scaling | ONLY AVAILABLE FOR SURFACES AND STACKS <br> The heights of the shown surface(s) are scaled by this factor, but for a single surface the displayed $z$-Extension remains unchanged. If the $z$-Scaling is not equal to 1, envelopes, coordinate systems, and labels will not be shown. Then the Global Coordinate System shows the scaling factor. |

[^1]
### 5.15.2.3 Geometry Markers

Options to add additional markers to the shown geometry, i. e. they are moved and scaled together with the geometry.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Coordinate Systems | If checked, a coordinate system will indicate the position and orientation of each surface. You can scale them by the given factor. |
| Labels | If checked, for surfaces the name of the surface is shown. Else the names of the component(s) are shown next to their respective first surface. The font colors resemble the color with which the corresponding component is shown. |
| Origin | If checked, a ball symbol is drawn at the origin of the Internal Coordinate System ( $\hookrightarrow$ Sec. 43.8.1) of the displayed component or at the origin of the Global Coordinate System of the displayed geometry. |
| Semi-transparent Background | Only if LAbels are shown <br> If checked, the labels are placed in a semi-transparent box to distinguish them more easily from the background. |
| Vary $x-y$-Position of Labels | OnLy if LABELS ARE SHOWN <br> By default, all labels are shown on top of the corresponding surface. So they might overlap when you look along the z-axis and the surfaces are all similar in size and orientation. So you can check this option to show them at different lateral angles (in the coordinate system of the corresponding boundary). 4 labels for example will then be shown on the right, top, left, and, bottom, respectively. |
| Font Size | Only if LABeLS ARE Shown The font size used for the labels. |

### 5.15.2.4 Perspective

Directly in the 3D view you can change the orientation of the virtual camera in an arbitrary way ( $\hookrightarrow$ Sec. 5.15). This page shows the quaternion describing this orientation. However, sometimes you want to have a welldefined orientation, e. g. for screenshots. Then you can check Pre-Defined Camera Orientation and define the direction of the $z$-axis and $x$-axis of the shown geometry relatively to your screen. Note that when you change the direction of the $z$-axis, the available directions for the $x$-axis change, as $z$ - and $x$-axis are perpendicular. By default, the camera generates an orthographic projection. This means that two surfaces of the same physical size are always shown with the same size on the screen, even if one is one centimeter away from the camera and the other one meter. If you Use Perspective Distortion, surfaces farther away are shown smaller, as in reality. But then rulers will not be shown.

### 5.15.2.5 View Tools

On this page you can change the visibility of Global Coordinate System, Tool Bar, and View Cube ( $\hookrightarrow$ Fig. 27). Furthermore you can show Rulers, either a Simple Scale in the lower right corner, or Full-Size rulers along the left and bottom border. In the latter case a measurement tool becomes available in the toolbar of the 3D view: $\Delta$. If this tool is active, first click anywhere in the 3D view starts drawing an arrow whose length is then shown. Second click fixes the end point of the arrow, third click starts a new measurement and so on.

### 5.16 Defining an ABCD Matrix

Simple optical elements can be described by so-called ABCD matrices e.g. ( $\left(\begin{array}{ll}1 & d \\ 0 & 1\end{array}\right)$ describes a free space propagation of distance $d$, or $\left(\begin{array}{cc}1 & 0 \\ -1 / f & 1\end{array}\right)$ describes an infinitely extended thin lens with focal length $f$. A system consisting of several optical elements is described by the product of their matrices (where the order of multiplication depends on the order in which the elements are passed by the light):

$$
\begin{equation*}
\mathcal{M}_{\text {system }}=\boldsymbol{\mathcal { M }}_{n-1} \times \mathcal{M}_{n-2} \times \cdots \times \mathcal{M}_{0} \tag{5.1}
\end{equation*}
$$

In this equation $\mathcal{M}_{0}$ is the first of $n$ elements passed through, $\mathcal{M}_{n-1}$ is the last.
In VirtualLab Fusion ABCD matrices can be used via the Ideal Component "ABCD Matrix Setup" ( $\hookrightarrow$ Sec. 73.1) and in the ABCD Law Calculator ( $\leftrightarrows$ Sec. 104).
In every case of application first the systems ABCD matrix has to be specified. This is done by the control shown in Fig. 30.


Figure 30. Control for defining an $A B C D$ matrix.
In this control several optical elements can be defined by ABCD matrices to describe an optical system. These elements will be arranged in a list where the order corresponds to the order in which the light passes through the elements. The properties of these elements (e.g. the focal length of a lens) have to be entered and then the ABCD matrix of the element combination (this is $\mathcal{M}_{\text {system }}$ in Eq. (5.1)) is calculated automatically. The upper part of the control shows the list, where the top entry represents the first element which is entered by the light, the bottom entry is the one where the light leaves the system. The buttons at the bottom of the control are used to edit that list.
The meaning and the functions of the control's buttons are the following:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Insert | Inserts a new element before the marked entry $(\hookrightarrow$ Sec. 5.16.1). |
| Append | Appends a new element at the end of the table $(\hookrightarrow$ Sec. 5.16 .1$)$. |
| Edit | Allows you to edit the marked element by opening the corresponding edit <br> dialog. |
| Delete | Deletes the marked elements. The marking of more than one entry is possi- <br> ble. |

You can reorder the elements by clicking on the Index cell of a certain row and dragging it to a new position. Double clicking on a certain row opens the corresponding edit dialog. You can mark multiple consecutive rows and delete them using the Del-key.

### 5.16.1 Inserting and Appending of Optical Elements

The element to be inserted or appended will be chosen by the dialog shown in Fig. 31, which will appear if the corresponding button ( $\hookrightarrow$ Fig. 30 ) is clicked.


Figure 31. Dialog for selecting an optical element to be included in the $A B C D$ matrix.
After selecting the desired element entry, followed by clicking Ok or, alternatively, just double clicking on the elements name, another modal dialog will appear, where the parameters of that element have to be entered.

### 5.16.2 Editing the Parameters of the Optical Elements

The parameters of the elements will be entered after choosing one in the dialog shown in Fig. 31 or can be changed if the button Edit in the control for creating an ABCD matrix system (Fig. 30) is pressed. Then a dialog will appear, where the needed parameters have to be entered and the corresponding ABCD matrix for that element $\left(\mathcal{M}_{i}, i=0 \ldots(n-1)\right.$, in Eq. (5.1)) will be calculated.

### 5.16.2.1 Editing a Free Space Propagation Element

Here the geometrical distance has to be entered. The dialog (see Fig. 32) shows the automatically calculated $A B C D$ matrix in its lower part.


Figure 32. Dialog for editing a free space element for $A B C D$ matrix propagation simulation.

### 5.16.2 2 Editing a Plane Interface Element

Here the real parts of the refractive indices of the preceding and the subsequent medium have to be entered. The dialog ( $\hookrightarrow$ Fig. 33) shows the automatically calculated ABCD matrix in its lower part.


Figure 33. Dialog for editing a plane interface element for $A B C D$ matrix propagation simulation.

### 5.16.2.3 Editing a Spherical Interface Element

Here the radius of the curved surface as well as the real parts of the refractive indices of the preceding and the subsequent medium have to be entered. A positive sign for the radius means that the center of curvature is on the side of the subsequent medium. The dialog ( $\hookrightarrow$ Fig. 34 ) shows the automatically calculated ABCD matrix in its lower part.


Figure 34. Dialog for editing a spherical interface element for ABCD matrix propagation simulation.

### 5.16.2.4 Editing a Spherical Mirror

Here the Radius of Curvature of a spherical mirror has to be entered. A negative radius of curvature defines a concave mirror and a positive radius defines a convex one.
The dialog ( $\hookrightarrow$ Fig. 35) shows the automatically calculated ABCD matrix in its lower part.


Figure 35. Dialog for editing a spherical mirror for $A B C D$ matrix propagation simulation.

### 5.16.2.5 Editing a Thin Lens Element

Here the Focal Length of an infinitely extended thin lens has to be entered. A negative focal length defines a concave lens and a positive focal length defines a convex one.
The dialog ( $\hookrightarrow$ Fig. 36) shows the automatically calculated ABCD matrix in its lower part.


Figure 36. Dialog for editing a thin lens element for $A B C D$ matrix propagation simulation.

### 5.16.2.6 Editing the Matrix of an Arbitrary or Composite Element

Here you can define an arbitrary matrix or an already known matrix of a more complex system, by entering the elements $A, B, C$ and $D$ directly. This is done by the dialog shown in Fig. 37.


Figure 37. Dialog for editing an arbitrary matrix for $A B C D$ matrix propagation simulation.

## 6 Global Options Dialog



Figure 38. Global Options dialog.
Global program options can be edited by the dialog shown in Fig. 38.
The options are grouped in several categories and subcategories which are shown in the tree view at the left of the dialog. The subcategories with their specific settings are explained in the following subsections. The Default Settings usually can be altered in the corresponding specific edit dialogs and Property Browser tabs. All settings but the file paths in the File Handling category can be reset, loaded, and saved with the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reset All | Resets all global program options to their initial values. Also the file path were <br> the Global Options are stores is reset. |
| Load Global Options | With this button you can load another Global Options file saved with the <br> button. The 5 most recently used files are available in a shortlist. |
| Save Global Options | With this button you can save a copy of the current Global Options to an- <br> other file path. In this way you can give your Global Options to colleagues or <br> LightTrans in case of support requests. |

The currently used Global Options file is also given in the title of the dialog and in the lower left corner of the main window.
Many of these Global Options influence the results of simulations, usually they represent a trade-off between accuracy and computational effort. Thus, in extreme cases you may obtain completely wrong results or no results at all because of too high computational effort. These settings are marked with ${ }^{\mathbb{⿶}}$ in the following subsections. And if you changed such settings, a "Changed Simulation Results" is shown also in the lower left part of the main window. Last but not least there you also see a short summary of the current multi-core settings ( $\leftrightarrows$ Sec. 6.15).

### 6.1 Default Settings $>$ Modeling Profile ${ }^{\text {『 }}$



Figure 39. The dialog to configure the default profile settings.
In this category you can open a separate dialog ( $\rightarrow$ Fig. 39) where you can edit some default settings for the profile editor ( $\hookrightarrow$ Sec. 43.4.1). This dialog has the following tabs.

### 6.1.1 Sources

Here you can set the default Wavelength which is used among others as default for the sources within an Optical Setup, but also for the generators in the Sources and the Functions ribbon.

### 6.1.2 Components \& Solvers

The settings on this tab page are explained in Sec. 43.4.2. They affect only real components ( $\rightarrow$ Part IX).

### 6.1.3 Visualization \& Detectors

The Evaluation \& View sub-tab contains the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Evaluated Field Components | Here you can set which vectorial components of a field a detector evaluates by default. You can choose between $E_{x}, E_{y}$, and/ or $E_{z}$, whereas at least one component must be selected. <br> This setting affects the Universal Detector ( $\leftrightarrows$ Sec. 74.4), the Camera Detector ( $\hookrightarrow$ Sec. 74.5.2), the PSF \& MTF detector ( $\hookrightarrow$ Sec. 74.5.3), and the Power detector ( $\varsigma$ Sec. 74.6.4). |
| Color Table | Here you can preset the Color Table used by the Universal Detector ( $\varsigma$ Sec. 74.4), the Camera Detector ( $\leftrightarrows$ Sec. 74.5.2), the PSF \& MTF detector $(~ \hookrightarrow$ Sec. 74.5.3), and the Raw Data Detector ( $\leftrightarrows$ Sec. 74.5.5). <br> For more information about color tables please see Sec. 11.2.4. |

The controls on the Free Space Propagation sub-tab are explained in Sec. 43.4.2. They affect only detectors ( $\hookrightarrow$ Part XI).

### 6.1.4 Other Settings

| ITEM | DESCRIPTION |
| :---: | :---: |
| Default System Temperature | The temperature which is used as default for all Optical Setups. Furthermore, it is used for all refractive index calculations which are independent of an Optical Setup, e.g. in the Fresnel calculator. |
| Default Air Pressure | The air pressure which is used as default for all Optical Setups. Furthermore, it is used for all refractive index calculations which are independent of an Optical Setup (e. g. in the Fresnel calculator) if air is involved as a surrounding medium. |
| Changing Temperature or Pressure Keeps the Vacuum Wavelengths Constant. | Changing the temperature of a medium will change its refractive index. A changed pressure alters the refractive index of air too. A changed medium wavelength will be the consequence. If this option is selected, the change of all media wavelengths in the system's light sources is accepted by the user. |
| Changing Temperature or Pressure Keeps the Media Wavelengths Constant. | Changing the temperature of a medium will change its refractive index. A changed pressure alters the refractive index of air too. A changed medium wavelength would be the consequence. If this option is selected on the other hand, VirtualLab Fusion will keep the media wavelengths constant by adapting all vacuum wavelengths in all of the system's light sources. Please note: This option is mainly supposed to allow a result comparison to simulations in Zemax OpticStudio®. |
| Default Embedding Material | Sets the material that is used as a default reference for relatively measured real parts of the refractive indices ( $\hookrightarrow$ Sec. 38.3). The individual controls are explained in Sec. 34.3. |
| Process Logging Level | The default logging level for optical simulations ( $\hookrightarrow$ Sec. 43.2.4). |

### 6.2 Default Settings > Coordinate Systems

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Default Definition Type | This option sets the default for defining an orientation for Optical Setup Elements as described in Sec. 43.8.2.3, Sec. 5.6 and Sec. 139.2.1. |
| Initial Axis Rotation | A so called Sequence of Axis Rotations (Sec. 139.2.4) provides no unambiguous way for defining an orientation. Thus, even the orientation of a coordinate system that is not rotated with respect to its reference coordinate system does not have a unique representation as a sequence of axis rotations. That's why this global option allows to define the value of an axis rotation sequence representing a non-rotation i.e. being in its initial state. |
| Use Component Coordinate System for Stack Preview | Only has an effect for components in a Grating Optical Setup ( $\hookrightarrow$ SEC. 64) <br> If this option is not checked, the stack preview always shows the stack in its own coordinate system. This means that the base block the stack is placed on is always left. This can be confusing if you place a stack on the front side of a component. So if you check this option, in this case the base block is shown right and the coordinate system is adapted accordingly. $\hookrightarrow$ Sec. 39.1.2 |

### 6.3 Default Settings > General View Settings

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Theme for Main Window | With this option you can select a color scheme applied to the elements of the main window (ribbon $\hookrightarrow$ Sec. 4.2, docking tabs $\hookrightarrow$ Sec. 4.3, and status bar $\hookrightarrow$ Sec. 4.4). |
| Show Notify Icon and Notifications | You can set that the notifications and the notify icon ( $\hookrightarrow$ Sec. 4.5) are shown Always, If VirtualLab Inactive or Never. Inactive means that <br> - another application or Windows gets the focus by clicking into it with the Mouse or e.g. via Alt + Tab. <br> - a dialog of VirtualLab Fusion gets opened or <br> - a docking tab of VirtualLab Fusion gets the focus if it is detached from the main window. <br> Note that notifications can also by switched off via Windows. So check also the Windows option if you cannot switch on the notifications with this option. |
| Display Duration of Tool Tips | The display duration of most tool tips, especially the ones in the ribbon ( $\leftrightarrows$ Sec. 4.2). Several other tool tips with much text have their own longer durations so that you can easily read them completely. |

### 6.4 Default Settings > General View Settings > Font

You can set up the font which is used for all dialogs and document views except:

- Title bars
- The flowchart in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1).
- The source code editor ( $\leftrightarrows$ Sec. 7.3 .1 ) and the module view ( $\hookrightarrow$ Sec. 7.2 ) which use a monospaced font.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Recommended Font | If you click this option, the Global Font is set to "Segoe UI" and a font size <br> suitable for the DPI scaling set up in the Windows system configuration. |
| Configure Font Individu- <br> ally | If you click Change ... you can choose any suitable font installed on your <br> system. You can also Adjust Font Size more precisely with the corresponding <br> text box. Note that with these settings dialogs and views in VirtualLab Fusion <br> may look ugly or even become unusable. |
| Font Size of Axis Labels | The default font size for the axis labels in 1D and 2D diagrams. |
| Font Size of Diagram $\mathbf{T i}-$ <br> tles | The default font size for the subset titles in 2D diagrams. |

### 6.5 Default Settings > General View Settings > Display of Numbers

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of Significant Dig- <br> its | Default number of significant digits for displaying floating point numbers. (Do <br> not confuse significant with total digits: $847.34 \mu \mathrm{~m}$ formatted using two sig- <br> nificant digits results in $850 \mu \mathrm{~m}$. .) |
| Use Special Number of <br> Digits for Color Legends | If checked, a special number of digits can be set which will be used for the <br> labels of color legends only. The expected precision of the color legend may <br> be less than that of all other numerical strings, so a smaller number of digits |
|  | may be defined here. |

Format of Complex Num- Complex numbers can be formatted in different ways:
bers

- Real Part / Imaginary Part: \{real part\} + i\{imaginary part\}
- Amplitude / Phase: \{amplitude\}• $\exp (\{$ phase $\cdot$ - i)
- MATLAB, a more compact variant of the Real Part / Imaginary Part format: \{real part\}+\{imaginary part\}i
- PTF, a format used for the PTF export ( $\leftrightarrows$ Sec. 120.2.4):
(\{real part\}, \{imaginary part\})
This setting influences for example the appearance of Rayleigh coefficients output by the Grating Order Analyzer ( $\rightarrow$ Sec. 84) into the Detector Results $\operatorname{tab}(\leftrightarrows$ Sec. 4.3).
Format of Physical Values In principal, large or small physical values on axes can be displayed in three different ways ( $\hookrightarrow$ Fig. 40):
- Engineering: SI prefixes are used to make the actual numbers smaller.
- Scientific: Powers of ten are used to make the actual numbers smaller.
- Standard: The numbers are kept as they are.

For a specific document window you can always change this via its Property Browser. However, you can set the default value here. In Automatic mode the suitable default mode is determined automatically, depending among others on the used unit (there are no $\mathrm{k}^{\circ}$ [kilodegrees]).

| ' | 1 | 1 | ' | 1 | 1 | 1 | 1 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.5 | 1 | 1.5 | 0.5 | 1 | 1.5 | 0.0005 | 0.001 | 0.0015 |
| $\mathrm{X}[\mathrm{mV} / \mathrm{m}]$ |  |  | $\mathrm{X}[1 \mathrm{E}-3 \mathrm{~V} / \mathrm{m}]$ |  |  | X [V/m] |  |  |

Figure 40. Example of the different formats of physical values. From left to right: Engineering, Scientific, Standard.

### 6.6 Default Settings > General View Settings > Source Code Editor

The settings in this sub-category apply to the source code editor ( $\hookrightarrow$ Sec. 7.1).
ITEM DESCRIPTION

Theme for Source Code With this option you can select the color scheme of the source code editor. Editor

Autocomplete Braces and When you enter an opening brace ( \{ [ or quotation mark " ', the source code Quotation Marks by default automatically inserts the corresponding closing character ' " ] \}). In case you are used to adding the closing character manually, you can switch off this behavior here. Note that changing this setting only becomes effective for new module views.

### 6.7 Default Settings > Document Windows

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Initial Window Size | Allows you to define the initial window size in pixels for all newly created Result Windows. ( $\hookrightarrow$ Sec. 4.1.1) |
| Use Transparent Background for Copy to Clipboard | If checked the gray background of the view is replaced by a transparent color when Copy View to Clipboard operation ( $\hookrightarrow$ Sec. 11.6) is executed. This setting doesn't affect Harmonic Fields and Harmonic Fields Set as these documents allow you to configure in detail what is how copied to the clipboard. |
| Show Legend | Sets whether or not a color legend is visible per default. |
| Color System | The color system ( $\hookrightarrow$ Sec. 6.7.1) used for real color views of Chromatic Fields Sets ( $\hookrightarrow$ Sec. 14.2) and the Light View of harmonic fields (sets) ( $\hookrightarrow$ Sec. 12.2.1). |
| Maximum Number of Table Cells | Maximum number of table cells that are displayed in the Table panel of a Data Array's view. If this value would be exceeded, no table is shown unless the user explicitly states to do so. <br> This setting also influences the automatic resizing of table cells in certain tables: Only this number of cells is resized to the actual content, all other cells use a good estimate. This can increase performance significantly. |
| Maximum Number of Rays that Allow Marker Snapping | If the number of rays in a shown ray distribution exceeds this limit, no marker snapping ( $\hookrightarrow$ Sec. 11.3.2) will be available. The limit may be set to very high values but then one possibly has to wait for a long time until snapping is available. |
| Open Non-Numerical Data Arrays in Expert Mode | If checked, any non-numerical data array ( $\lrcorner$ Sec. 13.1) is opened with activated Expert Mode ( $\leftrightarrows$ Sec. 24.1.4) by default. However, this is just an initialization setting. If the expert mode is disabled for a view before saving the object to disk, it will be re-opened with disabled expert mode too. |
| Hide Phase Artifacts | If checked, phase artifacts below the Initial Threshold are hidden by default. $\rightarrow$ Sec. 11.8. |
| Initial Threshold | This is the default artifacts threshold. For a single document it can be changed in the view panel of the property browser. $\hookrightarrow$ Sec. 11.8. |

### 6.7.1 Color System

In order to display the color of mono- or polychromatic light approximately natural, the wavelength or the spectrum of a field has to be converted to RGB values in a defined way. This algorithm uses a color space (RGB working space) which can be chosen in the Global Options dialog. The choice is valid for all real color views created afterwards.


Figure 41. Example for different color systems: Reflex at gold surface. Left: displayed with sRGB, right: LightTrans Color System.

Real color views that already existed before will keep the color system of its creation point in time. If you want to update an existing view with a new color system, you have to duplicate it via Windows > Duplicate Document after changing this option.
The available non-common color system options are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wide Gamut (Illuminant C) | Common Wide Gamut system, but with Illuminant C as white point instead of <br> D50. |
| Kodak Pro Photo (Illumi- <br> nant C) | Common Pro Photo system, but with Illuminant C instead of D50.  <br> From Monitor Uses the ColorProfile.FromScreen() method by Aurigma GraphicsMill to get <br> the color profile currently associated with the monitor. <br> XYZ Color system that identifies R, G, and B with the normalized chromaticities X, <br> Y, and Z respectively. <br> LightTrans Color System Color system that was developed by LightTrans in order to fulfill the special <br> needs of displaying light on a computer monitor as naturally as possible. |

The specifications (chromaticities of R, G, B, and the white point) of all systems available in VirtualLab Fusion:

| COLOR SYSTEM | RED | GREEN | BLUE | WHITE |
| :---: | :---: | :---: | :---: | :---: |
| NTSC | $(0.66887,0.33092)^{1}$ | (0.210,0.710) | (0.14,0.08) | (0.31006,0.31616) |
| sRGB | (0.640, 0.330) | (0.300, 0.600) | (0.150, 0.060) | (0.3127, 0.3291) |
| CIE | (0.7355, 0.2645) | (0.2658, 0.7243) | (0.1669, 0.0085) | (0.3333, 0.3333) |
| SMPTE | (0.630, 0.340) | (0.310, 0.595) | (0.155, 0.070) | (0.3127, 0.3291) |
| P22 in KDS VS19 | (0.625, 0.340) | (0.285, 0.605) | (0.150, 0.065) | (0.281, 0.311) |
| Adobe RGB | (0.640, 0.330) | (0.210, 0.710) | (0.15, 0.06) | (0.3127, 0.3290) |
| Wide Gamut (IIluminant C) | $(0.73469,0.26531)^{2}$ | $(0.11416,0.82621)^{3}$ | $(0.15664,0.01770)^{4}$ | (0.31006, 0.31616) |
| Kodak Pro Photo (Illuminant C) | (0.7347, 0.2653) | (0.1596, 0.8404) | (0.0366, 0.0001) | (0.31006, 0.31616 ) |
| From Monitor ${ }^{5}$ | (N/A) | (N/A) | (N/A) | (N/A) |
| XYZ | $(1,0)$ | $(0,1)$ | $(0,0)$ | (0.33333, 0.33333) |
| LightTrans Color System | $(0.73469,0.26531)^{6}$ | $(0.15472,0.80586)^{7}$ | $(0.12412,0.05780)^{8}$ | $(0.3127,0.3291)^{9}$ |

### 6.8 Default Settings > Document Windows > 1D Views

This subcategory allows you to set the following parameters for diagram curves:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Line Thickness | The default line thickness for curves in $x$-y-diagrams. |
| Symbol Scaling Factor | The default scaling factor for symbols of data points in $x$-y-diagrams. |
| Use Smoothed Graphics | If checked, curves in $x$-y-diagrams will be smoothed per default. Usually, <br> this may improve the diagram. But if a stepped line is shown, deactivating <br> this property may yield a better result. Important: This smoothing is done on <br> pixel level. This pixel smoothing is not to be confused with the smoothing <br> interpolation methods described in Sec. 11.2.2! |
| Initial Color for Undefined The color to be used for visualizing undefined values in diagrams initially. It <br> Values in 1D Views can be changed for each individual view. |  |
| Opacity | Opacity of the color to be used for visualizing undefined values in diagrams. |
| Marker Line Thickness | The line thickness (in pixels) to be used for markers $(\hookrightarrow$ Sec. 11.3) in 1D dia- <br> grams. |

[^2]| ITEM | DESCRIPTION |
| :---: | :---: |
| Line Color (Singlegraph Mode) | The default color for curves in $x$-y-diagrams if not in Multigraph Mode. |
| Symbol Shape (Singlegraph Mode) | The default symbol shape for data points in $x$ - $y$-diagrams if not in Multigraph Mode. |
| Symbol Color (Singlegraph Mode) | The default symbol color for data points in $x$ - $y$-diagrams if not in Multigraph Mode. |
| Color of Left-Hand y-Axis (Multigraph Mode) | The default axis color for the left-hand y-axis of 1D Data Arrays in Multigraph Mode. |
| Color of Right-Hand $y$ Axis (Multigraph Mode) | The default axis color for the right-hand y-axis of 1D Data Arrays in Multigraph Mode. |
| Symbol Shape (Multigraph Mode) | The default symbol shape for data points in $x$-y-diagrams. This default will be used in Multigraph Mode as long as the different subsets can be distinguished by different colors. If all colors have been used, the symbol will be changed for the additional subset curves. |

6.8.2 Default Settings > Document Windows > 1D Views > 1D Polar Diagram
ITEM

DESCRIPTION

| Line Color (Singlegraph Mode) | The default color for curves in polar diagrams if not in Multigraph Mode. |
| :---: | :---: |
| Symbol Shape (Singlegraph Mode) | The default symbol shape for data points in polar diagrams if not in Multigraph Mode. |
| Symbol Color (Singlegraph Mode) | The default symbol color for data points in polar diagrams if not in Multigraph Mode. |
| Color of Primary Polar Axis (Multigraph Mode) | The default axis color for the primary polar axis of 1D Data Arrays in Multigraph Mode. |
| Color of Secondary Polar Axis (Multigraph Mode) | The default axis color for the secondary polar axis of 1D Data Arrays in Multigraph Mode. |
| Color of Tertiary Polar | he default axis color for the tertiary polar axis of 1D Data Arrays in Multigraph | Axis (Multigraph Mode) Mode.

Symbol Shape (Multi- The default symbol shape for data points in polar diagrams. This default will graph Mode) be used in Multigraph Mode as long as the different subsets can be distinguished by different colors. If all colors have been used, the symbol will be changed for the additional subset curves.
Initial View of Angular De- If checked, diagrams with angular dependency will never be initialized as popendency > Always Carte- lar.
sian
Initial View of Angular De- If checked, diagrams with angular dependency will always be initialized as pendency > Always Polar polar.

Initial View of Angular De- If checked, diagrams with angular dependency will be initialized as polar if at pendency > Polar for Spe- least one of the contained subsets is of one of the checked physical properties cific Kinds of Data in the list.

### 6.9 Default Settings > Document Windows > 2D Views

The button Manage Color Tables opens a dialog where you can choose which color tables are available and create new ones ( $\varsigma$ Sec. 11.2.4.1).
Furthermore you can set the Default Color Tables with which the most false color views are initialized. That are e.g. the data array view ( $\varsigma \mathrm{Sec} .13 .5$ ) and the medium preview ( $\varsigma \mathrm{Sec} .37 .2$ ).

For complex data, each field quantity ( $\leftrightarrows$ Sec. 11.1) can be initialized with an individual color table.
Furthermore there are the following view options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Initial Color for Undefined <br> Values in 2D Views | The color to be used for visualizing undefined values in diagrams initially. It <br> can be changed for each individual view. |
| Marker Line Thickness | The line thickness (in pixels) to be used for markers ( $\checkmark$ Sec. 11.3) in 2D dia- <br> grams. |

For more information, especially about editing color tables, please see Sec. 11.2.4.

### 6.10 Default Settings > Document Windows > 3D Views

Allows you to preset the view settings of the 3D view ( $\rightarrow$ Sec. 5.15). The sub-categories are the same as for the actual view settings dialog and are thus described in Sec. 5.15.2.1 - Sec. 5.15.2.5.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Resampling in Array - Array Operations | Determines whether fields are resampled automatically during addition, subtraction, multiplication, division, and convolution of fields. $\hookrightarrow$ Sec. 22.1.1. |
| Use Embedding for Field $\times$ Transmission Operators | This option determines whether or not to embed the result of a multiplication of a field with a non-periodic transmission into a frame of zeros. |
| Disable Light View | You can disable the automatic calculation of the light view. It is still possible to start the calculation manually. $\rightarrow$ Sec. 12.2.1 |
| Use Embedding Frame for Light View | With this option you can select whether or not fields shown in the Light View ( $\leftrightarrows$ Sec. 12.2.1) are embedded in a black frame. |
| Use Standard Scaling Initially | For performance reasons, the initial scaling mode ( $\rightarrow$ Sec. 11.2.5) can be set to standard scaling, i.e. for newly created fields no minimum and maximum determination is done. It is still possible to switch to automatic scaling. |
| Show Polarization | Sets whether or not polarization shall be visualized in the Data View per default. |
| Polarization Display Mode | The display mode for polarization visualization, as described in Sec. 12.2.2.3. |
| Show Grid | Only available if the display mode is set to Polarization Ellipses. Sets whether or not a grid shall be shown which visualizes the ellipse's positions. |
| Show Arrows | Only available if the display mode is set to Polarization Ellipses. Sets whether or not arrows shall indicate the direction of rotation for the ellipses. |
| Scaling | Only available if the display mode is set to Polarization Ellipses. A scaling factor for the ellipses. |
| Polarization Plane | What plane of polarization shall be visualized? |

### 6.12 Default Settings > Sampling Dialog ${ }^{\text {s }}$

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Points | The number of sampling points in $x$ - and y-direction, used if these values <br> cannot be determined automatically. |
| Sampling Distance | Default sampling distance in $x$ - and $y$-direction, used if these values cannot <br> be determined automatically. |
| Array Size | Default array size in x-and y-direction for a newly created field, used if these <br> values cannot be determined automatically. |
| Oversampling Factor | The default oversampling factor used for sources ( $\hookrightarrow$ Part VIII), transmissions <br> ( Sec. 67) and propagation operators ( $\hookrightarrow$ Part XIII). The suggested sampling <br> distance will be divided by this value. |
| Size of Embedding Frame | A zeroized frame with the given width (in sampling points) is added to newly <br> generated light distributions, unless specified otherwise in the edit dialog of <br> the light source. |
| (Sampling Points) | The greater this factor the larger the generated field will be. A factor of 1 <br> (default) means the field size VirtualLab Fusion uses normally as automatic <br> setting. Increasing this factor increases the field size. Vice versa, setting this <br> factor to values between 0 and 1 decreases field size. |
| Field Factor | Newly created harmonic fields or transmissions have a soft edge whose width <br> can be pre-defined by this value (relative to the smaller of the both values of <br> the aperture size). |
| Relative Edge Width |  |

If you have filled the text boxes for one direction, you can copy the values over to the other direction by double clicking on the text boxes for the other direction. This behavior is also implemented in many other dialogs.

Any two of the three parameter pairs labeled Sampling Points, Sampling Distance, and Array Size are editable at the same time. Which parameters are editable can be chosen by the corresponding check boxes. The unchecked third parameter pair is calculated as the array size is always equal to the product of the number of sampling points and the sampling distance.

### 6.13 Performance

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| FFT Algorithm | Since VirtualLab Fusion 4.10 the Intel Math Kernel Library is included in <br>  <br>  <br>  <br>  <br>  <br>  <br> VirtualLab Fusion offering better performance for Fast Fourier Transform <br> (FFT) calculations. However, if you want to do your simulations with the pre- <br> viously used VirtualLab FFT library you can check this option. |
| Field Size Truncation Fac- | Determines the behavior of the Accelerated Sinc Interpolation operator, |
| tor for Accelerated Sinc | which is also used for Automatic Resampling in Array - Array Operations. <br> Interpolation $\sqrt{S}$ |

### 6.14 Performance > RAM Consumption

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Warn Before Exceeding <br> Specified Limits | VirtualLab Fusion allows to check certain performance constraints before a <br> data field is created. If such a constraint is violated it means that the resulting <br> data field might be too large for the computer's RAM. In this case, the user is <br> asked to confirm that such a field should really be created because creating <br> too large fields can freeze your PC for quite a while. |
|  | With the Warn Before Exceeding Specified Limits check box, the user can <br> enable or disable this mechanism completely. The settings Maximum Num- <br> ber of Sampling Points per Field, Maximum Number of Field Set Members, <br> and Guaranteed Amount of Remaining Physical Memory allow to adjust the |
| performance constraints individually. |  |



Figure 42. The warning dialog shown if due to the creation of a new field the used physical memory would exceed the warning level.

### 6.15 Performance > Multi-Core

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Use Multiple Cores | You can enable multi-threading with this option. If enabled, parts of the Fourier Modal Method used for grating simulation always use all cores that are available on the system and cannot be controlled by the value of Number of Cores To Use. <br> This setting also influences whether the math library used for the Fourier Modal Method runs in a parallelized version or not. But for this setting to take effect a restart is required. |
| Number of Cores To Use | If you Use Multiple Cores, this number controls how many cores are used for parallel processing for tasks (design, simulation, parameter run). But as there can be parallelized tasks running within parallelized tasks or because of tasks running in the background, VirtualLab Fusion can use more than the set number of cores. You can increase this number if VirtualLab Fusion doesn't use all physical cores. You should decrease this number if VirtualLab Fusion doesn't respond anymore during calculations. |
| Number of Parallel Iterations for Parameter Run Loop | If you Use Multiple Cores, by default the Parameter Run ( $\varsigma$ Sec. 44) starts $n$ parallel simulations of the underlying Optical Setup ( $\leftrightarrows$ Sec. 43) where $n$ is the Number of Cores To Use. Then however for example your RAM consumption might get too high, so you can set a lower number instead. $n=1$ means that one simulation is done after each other, only the simulation of each Optical Setup runs in parallel. <br> This option can be set globally here - or for each Parameter Run separately via its Property Browser. |
| Optimize Performance for Very Fast Iterations | There is a performance optimization for parallel execution of short lasting iterations in VirtualLab Fusion. However, it turned out that this optimization then slows down certain more long lasting simulations. Thus if you perform e. g. a parallel Parameter Run with very many short simulations which are unexpectedly slow, you can try to switch on this setting. |

### 6.16 Optional Dialogs

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Pop up Warning Mes- <br> sages | Warning messages are always printed in the Messages panel. If this option <br> is checked warning messages are additionally shown in a message box. |
| Pop up Error Messages | Error messages are always printed in the Messages panel. If this option is <br> checked error messages are additionally shown in a message box. |
| Duplication State for Op- <br> erations on Data Arrays | These settings are used for manipulations of Numerical Data Arrays as de- <br> scribed in Sec. 24.3. If Operate on Calling Object is selected, the original <br> data will be manipulated. This will be not the case if Duplicate is chosen. Ask <br> Every Time means that a dialog will ask whether duplication is desired every <br> time a manipulation is called. |
| What to Do With the Data <br> in the Temporary Folder | The unpacked contents of a Zemax ZAR archive will be deleted after clos- <br> ing VirtualLab Fusion. If Ask For Save is activated, the dialog described in <br> After ZAR Unpacking |
| Sec. 124.4.5 will open every time a ZAR file has been imported, which allows <br> to save the unpacked archive contents before deleting. If Discard and Delete <br> on Program Closing is checked on the other hand, the temporary folder con- <br> taining the unpacked archive will be deleted without further notice. |  |

### 6.17 File Handling

| ITEM | DESCRIPTION |
| :---: | :---: |
| Full Import / <br> Simple and Limited Import | Normally import of Zemax OpticStudio® Lens Files is done using the socalled ZOS-API, i.e. direct access to an installed Zemax OpticStudio®. If Zemax OpticStudio® is not installed or not licensed we fall back on a simple and limited import instead, which directly reads the Lens Files. However, the check whether Zemax OpticStudio® is installed can take quite a while so you can set to always use the simple and limited import without prior initialization of the ZOS-API. Further details can be found in Sec. 124.4. |
| Path for 'Zemax OpticStudio®' User Data | A path needed for import of Zemax OpticStudio® lens files. The path can be changed with the - -button. If you want to access the path directly you can click on the path label. |
| Path for User Settings | Path where among others user-defined catalogs are saved. It can be changed with the $\square$-button. If you want to access the path directly, e.g. for backup, you can click on the path label. |
| Path for Temporary Files | Path where temporary files are stored. The path can be changed with the $\square$-button. If you want to access the path directly, e.g. for cleanup, you can click on the path label. |
| Automatic Saving | Whether certain documents will be saved automatically after the specified time interval to avoid data loss. Only affects Optical Setups, Parameter Runs, and Parametric Optimizations which have already been saved at least once. This default can be overwritten via the Property Browser ( $\hookrightarrow$ Sec. 4.3) of these documents. |
| Use New File Format | In one of the next versions, a new file format will replace the current one (which is no longer supported by Microsoft). With checking this option you can already test the new file format with your files. But keep in mind that this feature still has $\beta$ status and errors might occur. |

### 6.18 Classic Field Tracing

This subcategory has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Default Free Space Prop- <br> agation Method for Link- | The entry Default Free Space Propagation Method for Linkages allows to <br> select a free space propagation method. The selected method is used as <br> ages |
| default operator for any new linkage of an Optical Setup. |  |

## 7 Programming

VirtualLab Fusion offers two ways of programming own functionality:

1. VirtualLab Fusion Modules provide an opportunity to automatize or provide arbitrary processes done within VirtualLab Fusion, for example customized export routines. C\# and Visual Basic syntax is supported. A module must contain a method "Run" in a class "VLModule" as this is the starting point for the execution of a module. Newly generated modules contain such a method by default.
2. In Programmable Items you just return a value depending on certain input parameters. For example in the Programmable Light Source ( $\hookrightarrow$ Sec. 51.8) you define the complex field value in dependance on the position $(x ; y)$. Other parameters like sampling and Jones vector are handled by VirtualLab Fusion and thus there is no need to program it yourself. These so-called "snippets" are much simpler than VirtualLab Fusion modules. Only C\# syntax is supported for snippets.

For both modules and snippets, you can use all "public" functions and properties of the VirtualLabAPI.dll and the VirtualLab.Programming.dll by Wyrowski Photonics as well as of the .Net Framework of Microsoft Corp. The VirtualLabAPI.dIl contains the complete programming interface of VirtualLab Fusion which underlies continuous changes. Modules and snippets using functionality from this DLL may require changes with a new version of VirtualLab Fusion. In contrast, the VirtualLab.Programming.dll has been especially designed for the needs of external users - all classes in this file are kept stable. Thus there is no need for code changes with a new version of VirtualLab Fusion if you use only methods from this file.

Keep in mind that in your code you must precede a class name with the "namespace" the class is located in. This is needed to distinguish classes with the same name. For example VirtualLabAPI.Core.Numerics.MathFunctions.DivisionRemainder $(a, b)$ calls the function DivisionRemainder in the MathFunctions class located in the VirtualLabAPI.Core.Numerics namespace.
If you insert a line like using VirtualLabAPI.Core.Numerics; in the header of your module file, you can use the class names of the specified namespace directly, e. g. MathFunctions.DivisionRemainder. Some often required namespaces as for example System, System.Drawing, VirtualLabAPI.Core.Common, and VirtualLabAPI.Core.FieldRepresentations are always predefined.

The following documents and web sites give further information.

| DOCUMENT | DESCRIPTION |
| :--- | :--- |
| MSDN Library | General introduction to C\# |
| .Net Class Library Refer- | All functions and properties of the .Net Framework 4.8 by Microsoft Corp. The |
| ence (MSDN) | members of the often needed System.Math class can be found here. |
| Programming Reference | Description of public members of both the VirtualLab.Programming.dll and <br> for VirtualLab Fusion |
|  | the VirtualLabAPI.dII. The current version of the programming reference can <br> be accessed via $?>$ Programming Reference. |

The Modules View is described in Sec. 7.2, the Source Code Editor for snippets is described in Sec. 7.3. Both share the same control to enter the actual source code, $\hookrightarrow$ Sec. 7.1

### 7.1 Source Code Editor Control



Figure 43. This screenshot shows some of the features of the control to enter source code. The numbers are explained in the text.

The control itself ( $\hookrightarrow$ Fig. 43) has the following features which support you in programming in a fast and convenient way.

| Line Numbers（1） | This column shows the line numbers．Syntax errors are always given with the line number where they occur．You can go to a specific line with the Go To entry of the context menu．The line number column is also the place where bookmarks（ $\hookrightarrow$ Sec．7．1．1）are shown．If you click on a line number the whole line is selected． |
| :---: | :---: |
| Outlining（2） | By clicking on any $\square$ button in the outlining column，you can collapse the corresponding code block（for example a complete method）to a small rect－ angle with a gray outline．If the cursor hovers above said rectangle，you see a preview of the code block．You can expand a collapsed code block using the $\oplus$ button next to it． <br> Own code blocks can be defined by embracing them with \＃region＜Name＞ and \＃endregion．The context menu（and the ribbon of modules）offer func－ tionality to collapse／expand all code blocks． |
| Line Modificators（3） | In this column，changed lines are marked yellow（green if they have been saved）． |
| Syntax Highlighting | To maintain readability，strings，numbers，keywords，identifiers and so on all have their own color．In the Global Options dialog（ $\hookrightarrow$ Sec．6．3）you can choose among many predefined color themes．Obvious syntax errors are marked with a red zigzag line（4）． |
| XML Comments（5） | Methods，class variables and so on should be commented with XML com－ ments．They are then shown in the Syntax Tooltips（8）if you use them some－ where else．If you enter／／／directly above the variable or method，a XML comment skeleton is generated automatically． |
| Code Completion | If you start entering e．g．a variable name and then press Ctrl＋Space，it is completed automatically if the letters you have already entered identify the wanted name uniquely．If this is not the case，a menu（6）opens where you can select the desired name with the arrow keys or Page Up and Page Down and use it with Enter．If you type further letters the selection is narrowed down．In the bottom of that menu you can activate filters so that for example only methods are shown． |
| Code Snippets（7） | In the Code Completion menu（5）there are also some code snippets，marked by 吴三。 <br> Example：The for snippet is expanded to for（int i＝0；$i<l e n g t h$ ； i＋＋）\｛ \}. After this snippet has been expanded, all occurrences of the variable i are highlighted．If you now change that variable name，all three oc－ currences are changed at the same time．If you press Tab，you jump to the variable length which you can also change．If you press Enter you leave the snippet． |
| Syntax Tooltips（8） | If you are entering the name of a method and then an open round bracket （which means that you start entering the parameters of the method），a Syntax Tooltip is shown．It shows the XML comment（5）of the method itself and of the currently entered parameter．Syntax Tooltips are also shown if you navigate in the Code Completion menu（6）or if you move the mouse over a variable or method name． |


| Horizontal Split | If you click on the button marked with 9 in Fig. 43 and drag your mouse, you <br> can create and move a gray splitter bar separating two views of the source <br> code editor. In this way you can work on two parts of the source code at the <br> same time. If you want to remove the split view, simply drag the splitter bar <br> to very top of the editor. |
| :--- | :--- |
| Scrollbar Annotations (10) | Different colors in the scrollbar mark for example saved changes (yellow <br> squares), unsaved changes (green squares), syntax errors (red squares), <br> bookmarks (black squares), occurrences of the current search string (orange <br> squares), and the current line (dark blue line). |
| If you finish a code block (by entering a semicolon or a closing curly bracket <br> in C\#), all lines in the block are aligned automatically so that child code blocks <br> are indented with respect to the parent code block. If you start a new line with |  |
| Enter, it is also indented automatically. |  |

## Useful keyboard and mouse commands

- You can change the font size in this control via the mouse wheel while pressing the Ctrl key.
- When you press the Ctrl key and move the mouse over the name of a variable or method defined in the current module, you can click it to jump to the position where this element was declared.
- The control supports selection of rectangular code blocks (= a certain column range in consecutive lines). You create such a selection by navigating to the desired start point and then expand the selection via Alt + Shift $+\leftarrow / \rightarrow / \uparrow / \downarrow$ or holding Alt while creating the selection with the mouse. Such a block selection also allows you to write in consecutive lines at once.


### 7.1.1 Context Menu

The context menu of the Source Code Editor Control has the following entries.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\square^{6}$ ) Undo | Undoes the last edit(s). Shortcut Ctrl + Z . |
| (c)Redo | Redoes the last undone action(s). Shortcut $\mathrm{Ctrl}+\mathrm{Y}$. |
| \% Cut | Copies the current selection to the Windows ${ }^{\text {TM }}$ Clipboard and then deletes it. Shortcut Ctrl]. X . |
| $\square$ Copy | Copies the current selection to the Windows ${ }^{\text {TM }}$ Clipboard. Shortcut Ctrl + C. |
| Paste | Pastes the current (text) content of the Windows ${ }^{\text {TM }}$ Clipboard to the cursor position. Shortcut Ctrl +V . |
| 固 Select All | Selects the whole source code. Shortcut $\mathrm{Ctrl}+\mathrm{A}$ |


| Find | All occurrences of the word the cursor is currently placed on are marked or- <br> ange. Furthermore, a resizable pop-up in the bottom right corner opens where <br> you can change the search string and the search options. For example if there <br> is an active selection, you can switch here whether to search in the Current <br> Document or in the Selection Only. Shortcut Ctrl + F. |
| :--- | :--- |
| Ge To |  |

### 7.2 Module View



Figure 44. Example of a VirtualLab Fusion module document.

In Fig. 44 the view of a newly created $\mathrm{C} \#$ module is shown as an example of the general view of VirtualLab Fusion modules. It comprises the following three parts (from top to bottom).

| ITEM | DESCRIPTION |
| :---: | :---: |
| \{Source Code Editor\} | $\hookrightarrow$ Sec. 7.1 |
| \{Error Panel\} | Displays possible compiling errors and warnings, including the line in which they occurred and an error code by which you can find further information online. When you double-click on a message the cursor in the source code editor jumps to the corresponding line. With the yellow buttons on top of this panel you can filter to see either only warnings or only errors. |
| \{Status Bar\} | The left part gives general status messages, which are also logged into the Messages tab ( $\hookrightarrow$ Sec. 4.3). The right part shows the current position of the cursor, counted in lines (Ln) and characters (Ch). |

The size of the module view can be changed freely by mouse drag, as well as the size of the error panel and its columns.

### 7.2.1 Advanced Settings

The Module View can be also used to specify additional external reference DLLs. Fig. 45 shows the tab page that can be used to specify external references for modules.


Figure 45. The Advanced Settings tab of a module.
The definition of external references is described in more detail in Sec. 7.3.4.

### 7.2.2 File Menu

If you click $\|$ Save or $\mathbb{H a}_{\boldsymbol{W}}$ Save As in the File menu the correct file extension (.cs for C\# and .vb for Visual Basic) is set automatically. Print opens a dialog specifying which region of the source code is to be printed with which printer. Clicking OK in this dialog starts the printing process.

The shortcut Ctrl $+\mathbb{M}$ can be used to create a new $\mathrm{C} \#$ module.

## 7．2．3 Ribbon Items

| ITEM | DESCRIPTION |
| :---: | :---: |
| －Run | Compiles and then executes the correct source code（Shortcut F5）．If you click this button it turns into a $\square$ Stop button（Shortcut $\widehat{\text { Shift }+\boxed{F 5}) \text { to stop the }}$ execution of the code． |
| \％Compile | Compiles the implemented source code and shows the resulting compiler errors and warnings both in the errors panel and in the messages panel of the main window．Shortcut F6． |
| 图 Select All | Selects the whole source code．Shortcut Ctrl +A |
| \％Cut | Copies the current selection to the Windows ${ }^{\text {TM }}$ Clipboard and then deletes it． Shortcut Ctrl + X． |
| Copy | Copies the current selection to the Windows ${ }^{\text {TM }}$ Clipboard．Shortcut Ctrl + C． |
| Paste | Pastes the current（text）content of the Windows ${ }^{\text {TM }}$ Clipboard to the cursor position．Shortcut Ctrll+V ． |
| Undo （c）Redo | Undoes the last edit（s）．Shortcut Ctrl＋Z． <br> Redoes the last undone action（s）．Shortcut $\overline{C t r l}+\widehat{S h i f t}+\mathrm{Y}$ ． |
| 俍 Find | Opens a dialog where you can enter an arbitrary string．The Find Options allow you to configure the behavior of this dialog in detail．By pressing the Bookmark All button all matching lines in the source code are marked as bookmark（see below）．Shortcut Ctrl + F． |
| 朝 Replace | Opens a dialog with which you can replace an arbitrary string by another arbitrary string．The Find Options allow you to configure the behavior of this dialog in detail．Shortcut $\mathrm{Ctrl}+\mathrm{H}$ ． |
| 三 Comment Lines | Comment Lines marks all currently selected lines with a comment symbol，so that they are not part of the actual source code．Shortcut Ctrl + Shift + C |
| ® Uncomment Lines | Removes all comment symbols from the beginning of the currently selected lines．Shortcut Ctrl + Shift $+U$ |
| $\begin{aligned} & \text { Collapse All/ } \\ & \text { Expand All } \end{aligned}$ | The source code editor supports outlining，i．e．code blocks like a method can be collapsed to a single line to gain a better overview of the source code． Collapse All collapses all such blocks and Expand All expands all such blocks． |
| Bookmarks | This ribbon group provides support for bookmarks allowing you to jump be－ tween regions of your source code．Bookmarked lines are indicated by a blue rectangle in the line number column．Toogle Bookmark creates a bookmark in the current line if there is no bookmark present．Otherwise，the already ex－ isting bookmark is removed．With $\%$ Next Bookmark and \％Previous Book－ mark you can jump to the next and previous bookmark in your source code， respectively．Clear All Bookmarks deletes all bookmarks． |

## 7．3 Source Code Editor for Snippets

This dialog（ $\hookrightarrow$ Fig．46）consists of various tabs which are explained in the following sections and the following controls at its bottom：

| ITEM | DESCRIPTION |
| :--- | :--- |
| timport Snippet | Imports a snippet from a .snp-file. A dialog lets you select which parts of the <br> snippets are imported (all by default, with a Selection Tools button you can <br> Select All or Unselect AII). In this way you can for example keep your source <br> code unchanged while importing the global parameters. |
| Check Consistency | Exports a snippet into a .snp-file. This file can then be used to import the <br> snippet or parts of it into another programmable item. |
| Checks whether the implemented snippet is in correct C\# syntax. Compiler <br> errors and warnings are shown in the validity indicator ( $\hookrightarrow$ Sec. 5.10) right to <br> the Check Consistency button. Clicking the 国-button displays further infor- <br> mation including the exact location of the error or warning. <br> Shortcut: F6, or Shift + F6 if you want to see the errors or warnings imme- <br> diately. |  |

### 7.3.1 Source Code Tab



Figure 46. The Source Code Tab for snippets.

The Source Code tab of the Source Code Editor ( $\hookrightarrow$ Fig. 46) shows two panels.
The left panel contains the source code. Some regions of the source code are made read-only to ensure that it is suitable for the intended purpose. You can only edit the following regions:

- Additional using directives: Allows you to define additional namespaces containing classes you need. See also the box in Sec. 7.
- Main method: The actual snippet function that must be implemented (Example: In case of a programmable optical surface this method has to return a height value in dependency of the position $(x ; y)$ ).
- Snippet body: Additional methods, properties or variables can be specified here. They can be used for example to store some intermediate results between consecutive executions of the main method.

You can use functionality from the ．NET framework and from the classes documented in the VirtualLab Pro－ gramming Reference which you can find in the help menu（？）of the ribbon．The code must be entered in C\＃ syntax．
The features of the actual source code editor are explained in Sec．7．1．
The right panel contains a list of global parameters．By double clicking on them you can insert them at the cursor position in the source code．

## 7．3．2 Global Parameters Tab

Most snippets have predefined global parameters，for example $x$ and $y$ where the function is evaluated．The Global Parameters tab allows you to define further global parameters．These parameters can then be changed by the end users without using the Source Code Editor（ $\hookrightarrow$ Sec．7．4）．

| Variable Name | Type |  |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Boolean－Variable | Boolean | Edit | 目 | Value：False |  |  |
| Boundary Response | Boundary Response | Edit | 目 | Value：Aperture |  |  |
| Complex＿Variable | Complex Value | Edit | R | Value： $2.236067977 \cdot \exp (1.107148718 \cdot \mathrm{i}) \mathrm{kA} \mathrm{m}$ |  |  |
| DoubleuVariable | Double Value | Edit | 目 | Value： 500 mm （Allowed range： 0 mm ．．． 1 m ） |  |  |

Figure 47．The table to edit the Global Parameters．
This tab has the following controls（ $\hookrightarrow$ Fig．47）．

| ITEM | DESCRIPTION |
| :--- | :--- |
| \｛Table $\}$ | A table with all Global Parameters，see below． |
| Add | Adds a new variable with the initial type Double Value to the bottom of the <br> table． |
| Remove | Removes the currently selected variable from the table after inquiring whether <br> you really want to do so． |
| （Move Up） | Moves the currently selected variable up by one row． |
| （Move Down） | Moves the currently selected variable down by one row． |

The table with the Global Parameters has the following columns：

| COLUMN | DESCRIPTION |
| :---: | :---: |
| Variable Name | A variable name must be unique and a valid C\# identifier - which mainly means that it must not contain spaces and special characters like ' $/$ ' and that it must not start with a number. <br> To make the names shown in the control for end users ( $\hookrightarrow$ Sec. 7.4) more legible, you can add the special character ' $v$ ' which will there be replaced by a space and a double underscore which will be replaced by a hyphen. So for example the variable "Sub__SamplingFMM" becomes "Sub-Sampling FMM" for the end user. |
| Type | The type of the parameter. Can be either double (= a floating point number), integer, complex, string, or several types of vectors, double arrays, data arrays, regions, and catalog entries. |
| Edit | Opens an edit dialog where you can edit the Variable Name and the value of the parameter. See below. |
| 年 | Opens a simple text editor where you can enter the help text shown in the Parameters group box of programmable items. This editor optionally allows you to specify HTML formatting. |
| Description | Shows the current value of the parameter and additional information. |



Figure 48. Edit dialog for a general parameter of type Double Vector 2D.

The edit dialog for a general parameter has the following entries (Fig. 48 shows an example).

| ITEM | DESCRIPTION |
| :---: | :---: |
| Variable Name | The unique name of the variable which must be a valid C\＃identifier（see note in Sec．7．3．2）． |
| $\checkmark$ | Allows you to enter the special character＇$u$＇which will be replaced by a space in the control for end users（ $\leftrightarrows$ Sec．7．4）． |
| Physical Quantity | OnLY FOR DOUBLES，COMPLEX VALUES，AND DOUBLE VECTORS． <br> Allows you to choose any of the physical quantities listed in Sec．5．1．Note that in the source code tab（ $\leftrightarrows$ Sec．7．3．1）all variables are always given in their respective base unit（e．g．meters for a length and radians for an angle）． |
| Value | A control to define the actual value of the parameter．Depends on the type of the parameter： <br> －Double Value ${ }^{\text {PV }}: \hookrightarrow$ Sec． 5.1 <br> －Double Array 1D ${ }^{\text {P® }}$ and Double Array 2D ${ }^{\text {PE：}} \hookrightarrow$ Sec． 5.4 <br> －Boolean ${ }^{[\mathrm{PC}: ~ A ~ d r o p-d o w n ~ l i s t ~ t o ~ s e l e c t ~ b e t w e e n ~ T r u e ~ a n d ~ F a l s e . ~}$ <br> －Integer Value ${ }^{\mathrm{PVV}}$ ：A spinner where invalid input is marked red and ex－ plained with a tooltip． <br> －Complex $\left.{ }^{\mathrm{DV}: ~}\right\lrcorner$ Sec． 5.2 <br> －Integer Vector $2 D^{\mathbb{P V}}$ and Double Vector $2 D^{\mathrm{PV}}$ ：$\leftrightarrows$ Sec． 5.3 <br> －Double Vector $3 D^{\mathbb{P V}}$ ：Three controls for entering a physical value $(\hookrightarrow$ Sec．5．1），one for $x-, y$－，and $z$－dimension，respectively． <br> －String ${ }^{\text {®C：}}$ A text box <br> －Data Array 1D，Data Array 2D，Data Array Gridless，Region 1D ${ }^{\text {PE }}$ and Region 2D ${ }^{\text {PEE }}$ ：A Set button（ $\leftrightarrows$ Sec． 5.7 ）to load the document from a file or to use an already open document as well as a button to Show the currently set document in a separate window． <br> －Boundary Response ${ }^{\text {阴 }}$ ，Material ${ }^{\text {䦻 }}$ ，Medium ${ }^{\text {『® }}$ ，Stack ${ }^{\text {䦻，}}$ ，Surface ${ }^{\text {国：}}$ $\hookrightarrow$ Sec． 34.1 |
| Minimum Value／ Maximum Value | ONLY FOR DOUBLES，INTEGERS AND VECTOR TYPES <br> These values are used to restrict the allowed input values in the Parameters group box of programmable items and in the Parameter Run．For vectors， each component of the vector gets this value range constraint． |

## 7．3．3 Snippet Help Tab

On the Snippet Help tab you enter a help text and additional helpful information concerning the whole snippet． This information is then available for the end user via the（3）Help－button at the bottom of the Parameters tab of the programmable item（ $\leftrightarrows$ Sec．7．4）．


Figure 49. The Snippet Help tab of the Source Code Editor.
It has the following controls ( $\hookrightarrow$ Fig. 49).

| ITEM | DESCRIPTION |
| :---: | :---: |
| Title | Control to enter the title of the snippet. |
| Author | Control to enter the author(s) of the snippet. |
| Version | Control to enter the version of the snippet, e.g. "1.1a". |
| Last Modified | Allows you to enter the date the snippet was last modified. You can either enter the date directly in your local date format or use the $\square$ control to choose the date visually. |
| Interpret Text as HTML | If checked, the text inside the \{Help Text Box\} is interpreted as being HTML. So, HTML tags can be used for formatting (For example you can use <b>...<b/> to make some text bold and <i>...<i/> to make it italic.). If not checked, such tags will be ignored but line breaks will occur in the result just as entered in the defining text box. Please note: The state of this option will apply to the help texts of global parameters ( $\hookrightarrow$ Sec. 7.3.2) as well. |
| License | A license can be specified here to be applied to the source code. Pressing the tools buttons Defined is chosen, a license can be entered freely. The license description will appear in the Preview and Snippet help view below the text entered in the \{Help Text Box\}. |
| \{Help Text Box\} | Control to enter a description of the snippet. Scrolling with the mouse wheel while holding the Ctrl key changes the font size of this control. |
| Load Image | Loads an image from disk which will be part of the snippet help and which serves for illustrating relations, variable meanings etc. |
| Delete Image | Deletes a previously inserted image. |
| Scale Factor | Scales an inserted image. |
| Preview | The help of the snippet as the end user will see it. |

### 7.3.4 Advanced Settings Tab



Figure 50. The Advanced Settings tab of the source code editor. As one of the given External References is invalid (marked red), the Validity control shows an error. The text box Number of Resulting Physical Values (for Optimization) is only visible for Programmable Items returning a list of DetectorResultObject.

This tab ( $\hookrightarrow$ Fig. 50) allows you to load External References, i. e. managed DLLs whose classes you want to use. "Managed" refers to a special type of DLLs created with the .Net framework. This tab has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| List of References | The list of already defined external references. |
| Add (Absolute) | Opens a file open dialog where you can select a new managed DLL to be <br> added to the list. |
| Add (Relative) | Adds a new managed DLL to the list. The reference DLL can be specified <br> by a relative path. The set up is done within an additional dialog, which is <br> described below. If the specified DLL cannot be found the corresponding row <br> in the List of References is marked red and the validity control shows an error <br> ( $\hookrightarrow$ Fig. 50 ). |
| Remove | Removes the selected DLL from the List of References. |
| Edit | Editing of the path of the selected DLL. |

By clicking on the Add (Relative) button a dialog is shown which can be used to specify a relative path to a managed DLL.
Fig. 51 shows the edit dialog for relatively linked references.


Figure 51. Dialog for specifying relative links to referenced DLLs.

The user can enter the relative path directly within the text box at the bottom of the dialog. Additionally the list box at the top of the dialog can be used which assists the user in specifying the correct syntax for the relative links. By double clicking on an item within the list the selected directory key is added to the name of the reference DLL. The following relative directories are available

| ITEM | DESCRIPTION |
| :--- | :--- |
| \$AppDir\$ | The directory from which VirtualLab Fusion is started (typically the installation <br> directory). |
| \$ModuleDir\$ | The directory where the module is stored. This option is only available in the <br> Module View. $\hookrightarrow$ Sec. 7.2. |

### 7.4 Programmable Items for End Users

Programmable items usually have two distinct user groups: The developer which can use the source code editor described in Sec. 7.3 and the end user who just wants to change the parameters. The former can also be LightTrans or your local distributor.
The controls for the end user are in a Parameters group box ( $\hookrightarrow$ Fig. 52) directly in the edit dialog of the programmable item itself, thus he needs not to enter the source code editor.


Figure 52. Example for the Parameters group box of a programmable item. The scrollbar indicates that there are more parameters to be set than can be shown at once.

Each global parameter ( $\rightarrow$ Sec. 7.3.2) of the snippet defining the programmable item has its own type-depending control(s) to change the value:

| TYPE OF PARAMETER | CONTROL(S) |
| :---: | :---: |
| Double Value ${ }^{\text {PV }}$ | $\hookrightarrow$ Sec. 5.1 |
| Double Array 10 ${ }^{\text {PE }}$ / | $\checkmark$ Sec. 5.4 |
| Double Array 2D ${ }^{\text {PEE }}$ |  |
| Boolean | A checkbox |
| Integer Value ${ }^{\text {PVV }}$ | A spinner where invalid input is marked red and explained with a tooltip. |
| Complex | $\hookrightarrow$ Sec. 5.2 |
| Integer Vector 2D ${ }^{\text {PV }}$ / Double Vector 2D ${ }^{\text {PV }}$ | $\hookrightarrow$ Sec. 5.3 |
| Double Vector 3D ${ }^{\text {PV }}$ | Three controls for entering a physical value ( $\hookrightarrow$ Sec. 5.1), one for $x-, y$-, and z-dimension, respectively. |
| String | A text box |
| Boundary Response <br> Material ${ }^{[P E}$ / Medium ${ }^{[P E}$ \| <br> Stack ${ }^{\text {PE }} /$ Surface ${ }^{\text {PE }}$ | $\hookrightarrow$ Sec. 34.1 |
| Data Array 1D / Data Array 2D / Data Array Gridless / Region 1D / Region 2D | A Set button ( $\hookrightarrow$ Sec. 5.7) to load the document from a file or to use an already open document as well as a button to Show the currently set document in a separate window. |

Furthermore there are two buttons at the bottom of this control.

| ITEM | DESCRIPTION |
| :--- | :--- |
| As Separate Window | Allows you to show all parameters in a separate resizable window for a better <br> overview. |
| ? Help | Displays help information for the whole snippet and / or the individual param- <br> eters (if provided by the developer). |

Note that this group box is not visible if the snippet contains neither global parameters nor help information.

## 8 Distributed Computing

VirtualLab Fusion can be used to perform parameter run evaluations using Distributed Computing. To enable this technique the user needs to start a server directly in VirtualLab Fusion and configure the calculation network (meaning the calculation clients that shall be used for the simulations).
Fig. 53 show the control panel for the configuration of the distributed computing server inside VirtualLab Fusion.

| Distributed Computing |  |
| :--- | :--- |
| Server Tools | ㅜ |
| Start Server | + Add Clients on Remote Machine |

## VirtualLab Explorer Assistant Distributed Computing

Figure 53. The network for distributed computing can be configured directly in VirtualLab Fusion. The user can start a server and configure the client network.

By pushing the Start Server button a new server will start in the running VirtualLab Fusion instance. It should be noticed that per machine only one server can be started, because the communication between server and clients is done via network and for that the different ports will be used.
For the communication between server and clients (and the server support tool) the following ports should be accessible:

- 23001 [TCP \& UDP]
- 23002 [TCP \& UDP]
- 23003 [TCP \& UDP]

After the server is started the caption of the Start Server button will be changed to Stop Server. In addition, several additional buttons and controls get visible or active.
Fig. 54 show the user interface after the server was started.


Figure 54. After starting the server inside VirtualLab Fusion the user can modify the calculation network using the available controls.

If the server is running three different regions will be available for modification and investigation of the calculation network.

- Server Tools - In this section of the user interface the user can stop the server, adapt the calculation network, start a file watcher and specify some setting of the server. A detailed explanation of the server tools can be found in Sec. 8.1.
- Clients - Below the server tool section a table listing all connected clients is displayed. Within this table the user can investigate the current status of all clients per remote machine. Details on the client list can be found in Sec. 8.2.
- Logging - On the bottom of the control panel for distributed computing the user can find a text box, in which the communication within the calculation network is logged. Here it will be shown when a new calculation is given to the server, a calculation is distributed to a client within the network and also when a simulation is finished and the results are returned from the calculation client to the server. Below the logging window there is a button to clear the logging information. In addition, the user has the option to disable the logging checking the box Disable Logging below the logging window. It is recommended to deactivate the logging for a large number calculations, because the logging would slow down the performance of the server.


### 8.1 Server Tools

In the user interface section Server Tools several tools are available to start/stop or modify the server and the connected calculation network. The following tools can be accessed here:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Start Server | If no server is actually running you have the option to start the server. Please <br> note that you can only start one server per machine. In case a server is <br> already running, VirtualLab Fusion offers the option to attach to the running <br> server. In this case it is possible to use an existing calculation network. The <br> calculation network can only be modified within the VirtualLab Fusion instance <br> which started the server. |
| Stop Server | If a server was started, the Start Server button is changed to a Stop Server <br> button. If you click on the Stop Server button, VirtualLab Fusion will ask for a <br> confirmation that you really like to stop the server. If you confirm your choice, <br> the server and all connected clients will be closed. |
| Configure Server | By clicking on the configuration wheel next to the Stop Server button a dia- <br> log is opened in which you can specify some processing parameters for the <br> running server. The settings you can do here are explained in the Sec. 8.1.1. |
| Add Clients on Remote | The server supports to start clients on remote machines. There for a server <br> support tool needs to run in the machines on which you like to enable the start <br> of clients. In Sec. 8.1.2 the work flow how to add clients on a remote machine <br> in a user-friendly way is explained. |
| Start File Watcher | In addition to the parameter run, we also offer the option to feed new simu- <br> lation tasks to the distributed computing network via hard disc. Therefor you <br> simply need to use the Start File Watcher tool. Here the user can select a <br> folder which is checked regular by VirtualLab Fusion. This option can be use- <br> ful if you are working with external programs (like python) and like to benefit <br> from the automatic distribution of calculations. In case a new os file is stored <br> in the folder watched by VirtualLab Fusion, the task is distributed in the cal- <br> culation network and as soon as the results are present they are available in <br> a sub folder as XML file. |

### 8.1.1 Server Options

By clicking on Server Options a dialog is shown in which several options can be configured.
Fig. 55 show the dialog to configure the server options.


Figure 55. The dialog to configure the server options.
In general VirtualLab Fusion support to restart a client automatically after a specified number of calculations was done on the client, or if the RAM usage of one client is above a user defined threshold. It is recommended to keep the options as they are set by default. In case you are facing some irregular behavior of the clients these options could be adapted to solve the irregularity.

### 8.1.2 Add Clients on Remote Machine

VirtualLab Fusion supports to add clients to a running distributed computing server directly from the server side. This can be done by clicking on the Add Clients on Remote Machine button. Fig. 56 shows the dialog to add clients on remote machines.


Figure 56. The dialog which can be used to select the host machine on which the clients shall be started

On the top of the dialog you find a table which list all available host machines on which the server can start clients. To enable a host machine to start clients automatically, the server support tool has to run on the host machine. The server support tool is a special executable which can be found in the installation directory of VirtualLab Fusion. Simply start the file VirtualLab.DistributedComputing.ServerSupportService.exe and keep it open.
In the server support tool you will find a logging box which displays the information when a server requested to start a user defined number of clients.
In the table each host machine is represented by one line in the table. The following columns are available within the table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Select | The first column can be used to select whether you like to start one or more <br> clients on the host machine. If you select a host machine within the table you <br> can specify how many clients shall be started on the host machine. |
| Host Machine | The host machine name is used to identify the host machine. |
| Running Clients | Ine column Running Clients you can see how many clients are already run- <br> ning on the corresponding host machine. This information includes all clients <br> If you select a host machine within the table, the cell entry for specifying the <br> number of clients to start will become active. The number of clients per remote <br> machine which is reasonable depends on the host machine (and its current <br> usage) as well on the simulation tasks you like to distribute. |
| CPU | The table provides the information of the current CPU usage of the host ma- <br> chine. This information is updated frequently. |
| RAM | The table provides the information of the current RAM usage of the host ma- <br> chine. This information is updated frequently. |

On the bottom of the dialog two buttons are located to save and load the settings for the configuration of the calculation network. By clicking on the save button a text file is generated, which contains all necessary information given in the table above. When loading a previously stored configuration file, the information will be read again from the text file and all matching information will be synchronized with the table settings. In
case the information within the text file does not match the found host machines, per mismatch a warning is displayed. Only the matching information will be used for synchronization.

### 8.2 Clients

In the section Clients a list of all connected clients to the current server is shown. Fig. 57 shows the table for a sample situation where 17 calculation clients are connected on 5 different host machines.


Figure 57. The Clients control contains a list of all connected clients in the current calculation network.

In the table each host machine is represented by one line. Per host machine multiple clients could be running, which is displayed in the corresponding table entry. The table provides the following information.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Status | The status column is used to mark that status of each host machine by an intuitive color. The used colors have the following meaning: <br> - Green: No connected client on the corresponding host machine is performing a calculation task. <br> - Yellow: Some (but not all) connected clients on the corresponding host machine are performing a calculation task. <br> - Red: All connected clients on the corresponding host machine are performing a calculation task. <br> - Gray: The clients on the corresponding host machine are set to in active (which means they are connected but are not used for distribution of calculation tasks) |
| Host Machine | In this column the name of the host machine is plotted. |
| Clients | In the Clients column, the user can check how many clients are connected for the corresponding host machine. In addition you can also find the information how many of the connected clients are currently performing a calculation job provided by the server. |
| CPU | For monitoring purposes it is important to see the current CPU usage of the host machine. This information is given here. |
| RAM | For monitoring purposes it is important to see the current RAM usage of the host machine. This information is given here. |


| Active | In the Active column you can check whether a host machine is active or not. |
| :--- | :--- |
| By default the machines are all set to active, but there could be situation where |  |
| the user might decide to don't use a specific host machine (e.g. if this ma- |  |
| chine is needed for some other calculations). In this case one could remove |  |
| all clients from the corresponding host machine, or set them to inactive. If the |  |
| user set the clients on the host machine to be inactive and the clients are cur- |  |
| rently already doing some calculations, the calculations will be finished and |  |
| there will be no newly distributed calculation tasks to the clients of the host |  |
| machine. The inactive status is also visible via the Status column within the |  |
| client list (color is set to gray). |  |

It is a very typical situation, that there are more calculation tasks provided to the distributed computing network than there are available clients. In case all clients are already occupied and a new calculation task if given to the server for distributed computing, this simulation will be added to the calculation queue. As soon as a client is ready with the calculation task assigned to it the next task from the queue is automatically assigned to this client. Below the table listing all client information you can find the Number optical setups in queue.

## 9 Command Line Arguments

VirtualLab Fusion can be controlled not only via the graphical user interface but also via command line arguments. Multiple such commands can then be collected in a batch file.
The ribbon item File > Export > Create Batch Mode Files asks for a folder and creates there a sample batch file from the current Optical Setup which calculates the results for the current simulation engine. Furthermore a sample XML file is created containing the original values of all variable parameters of the Optical Setup.

## Restrictions on the passed arguments

Note that as batch files use another code page than Windows ${ }^{\mathrm{TM}}$ programs, paths in the batch file containing non-ASCII characters are passed to VirtualLab Fusion incorrectly. Thus the result and logging files might be stored in a wrong folder or the Optical Setup might not be simulated at all. Thus the paths should only contain the standard Latin characters a-z and A-Z, numbers, spaces and the special characters !\#\$\%\&'()+,-.;=@^_\{\}~ .
Furthermore the letter combination \" yields unexpected results. Thus path arguments must not end with 1.

## Hints

- The commands are case insensitive. For example you can use -perform0s, -Perform0s, or -performOS.
- In the parameters you can use any environment variable like \%TEMP\% (= path to the temp folder) or \%VirtualLab_AppDir\% (= path to the VirtualLab.exe from which the last export to batch mode or to optiSLang was executed).
- All commands described below can be used only exclusively. Only file names, -startUpModule, and -globalOptions can be used together.

The available commands are listed below. (The arguments in curly brackets are user-defined parameters, the arguments in square brackets indicate optional arguments.)
virtuallab.exe $\{1\}$ [\{2\} [\{3\} ...]]
Opens the specified files in VirtualLab Fusion. VirtualLab Fusion documents ( $\hookrightarrow$ Sec. 4.1) are opened as document windows. For files which can be imported ( $\hookrightarrow$ Part XVI) the corresponding import dialog is opened. After you close this dialog, the dialog for the next importable file is opened, if specified.

```
virtuallab.exe {1} [{2} [{3} ...]] -convert {4}
```

This command allows you to save a bunch of files in the most recent file format and file extension.
The specified files ( $\{1\},\{2\}, \ldots$ ) are opened and saved to the specified output directory $\{4\}$. You can also specify directories, then all files in this directory and its subdirectories are converted. Duplicate file names are made unique by adding ".bak" and maybe a number.
Old VirtualLab files ( $\leftrightarrows$ Sec. 130) are imported using default options. Errors are logged to an errors.log file in the output directory.
With this command VirtualLab Fusion is started in the "batch mode" where no VirtualLab Fusion windows are opened.
virtuallab.exe -perform0S \{1\} \{2\} [-parameters \{3\}] [-engine \{4\}] [-subfolder] [-noLogfile] This command allows you to simulate an arbitrary Optical Setup ( $\hookrightarrow$ Sec. 43); its results are then saved automatically. With this command VirtualLab Fusion is started in the "batch mode" where no VirtualLab Fusion windows are opened.

| ARGUMENT(S) | DESCRIPTION |
| :---: | :---: |
| -performOS $\{1\}\{2\}$ | The mandatory argument -performOS must be followed by the path and file name of the Optical Setup to be simulated ( $\{1\}$ ) and the folder where all output is stored (\{2\}). <br> Results are written into a results.xml file. Complex documents which cannot be saved into this XML file are stored as separate documents, the results.xml file then contains only a reference to that file. <br> If warnings or errors occur during the simulation, they are written into a ProcessingInfo.log file (unless -noLogFile is specified). If Pop up Error Messages or Pop up Warning Messages is activated in the Global Options dialog ( $\hookrightarrow$ Sec. 6.16), the corresponding messages are also shown in a message box. <br> -performLPD is a synonym for this command. |
| -parameters $\{3\}$ | With this optional argument you can specify a XML file with parameter values. These values are then used for the simulation instead of the original parameter values. You can use File > Export > Create Batch Mode Files to create a sample XML file named parameters.xml with the correct format ( $\rightarrow$ Sec. 124.1). |
| -engine $\{4\}$ | With this optional argument you can specify the simulation engine to be used. "0" refers to Classic Field Tracing, "1" to General Profile, "2" to Ray Results Profile, and "4" to System: 3D visualization ( $\leftrightarrows$ Sec. (a)). Other numbers refer to the index of the analyzer to be used for the simulation. If this parameter is not specified, "2" for Ray Results Profile is used. For Laser Resonator Optical Setups always the Eigenmode Analyzer is used. |
| -subfolder | If this optional parameter is specified, a subfolder in the output folder \{2\} is generated where the result and logging files are stored. In this way consecutive calls of the virtuallab. exe do not overwrite already calculated results. The name of the subfolder is <Name of simulation engine> (<Date and Time>). |
| -noLogfile | If this optional parameter is specified, a ProcessingInfo.log file is not created and thus errors and warnings get lost. This avoids problems occurring when hundreds of consecutive iterations are started via batch mode. |

## virtuallab.exe -performModule \{1\}

With this command a module ( $\hookrightarrow$ Sec. 7) instead of an Optical Setup can be processed in "batch mode" without VirtualLab Fusion windows. Compiler warnings and errors as well as text messages are written to a ProcessingInfo.log file in the same folder as the module. Note that showing results in the VirtualLab Fusion User Interface does not work in the batch mode, so you have to save them to your hard drive. The parameter $\{1\}$ is the path and file name of the module.
-run is a synonym for this command.
virtuallab.exe -startupModule \{1\}
Loads, compiles and executes an arbitrary module ( $\hookrightarrow$ Sec. 7) during startup of VirtualLab Fusion. Afterwards execution of VirtualLab Fusion continues normally. This allows you among others to ensure that certain Global

Options are set during start up, program a timer to remind you every 30 minutes that you need a break or open VirtualLab Fusion files you always need.
The parameter $\{1\}$ is the path and file name of the module executed during startup.

```
virtuallab.exe -globalOptions {1}
```

Specifies the Global Options file ( $\hookrightarrow$ Sec. 6) to be loaded. So you can setup two VirtualLab links on your desktop each using their own Global Options; e. g. one with many digits for numbers and big result windows for setting up systems and the other one with only three digits and default window size for screenshots.

## 10 License Information Dialog

The licenses of VirtualLab Fusion can be managed using an integrated dialog, which can be found at the Start > License Information ribbon item ( $\hookrightarrow$ Fig. 58). Fig. 59 shows the dialog that displays the current license information that is stored in the USB dongle.

```
vif About VirtualLab
9}\mathrm{ License Information
N(N)
    License
```

Figure 58. The License and Update ribbon items of VirtualLab Fusion.


Figure 59. The dongle dialog to manage the licensing of VirtualLab Fusion.
The current license status is displayed in the upper section of the dialog. Depending on the license model, the License Duration can be

- "Unlimited" or
- an expiration date until which the package can be used

Also shown is the last quarter the update service is valid for, the number of users for each package and the internal Dongle ID.

In the following we explain how licenses can be added or renewed.
After you have bought additional licenses we will ask you to send us your current license file. This file is obtained by pressing the button Save License Information ( $\hookrightarrow$ Fig. 60).


Figure 60. Press the button "Save License Information".

Then a file dialog will be opened, where you can choose the destination for saving the license file ( $\hookrightarrow$ Fig. 61). The resulting file has the extension "c2v" and has to be sent by email or ftp to LightTrans.


Figure 61. File dialog for saving the " $c 2 v$ ".

You will receive the modified license file from us. In order to activate the new licenses, the file has to be opened by pressing the Apply License Update button ( $\hookrightarrow$ Fig. 62) in the license information panel.


Figure 62. Press the button "Apply License Update".
Thereby another file dialog is shown ( $\hookrightarrow$ Fig. 63) and you have to select the received "v2c" file. After this step the license on the USB key is updated and the new license conditions are active for VirtualLab Fusion.


Figure 63. File dialog for applying the "v2c".

## III Result Documents

In VirtualLab Fusion there are several document types which show data plotted against one or more coordinates. This part explains these Result Documents.

All Result Documents (but Animations) have a View ribbon. Sec. 11 explains most of the entries in that ribbon. The x-axis of all these views points to the right and the y-axis to the top. As a result, if the data represents a light field, its $z$-axis is directed out of the monitor. Thus you see light always as it would look like through a transparent screen, as least if the light propagates in positive z-direction, $\hookrightarrow$ Sec. 131.3.

## 11 Basic Concepts

### 11.1 Field Quantity

## Availability

Only for complex-valued data

## Accessible:

- Ribbon: View > Field Quantity ribbon group
- Property browser: View > Field Quantity
- Context menu: Field Quantity

Often complex-valued data are to be shown, but only real-valued data can be shown in an intuitive way. The Field Quantity of a view determines which real-valued data are extracted from the complex-valued data. The following choices are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Re Real part | Real part $a$ of a complex number $z=a+i b$ |
| Im Imaginary part | Imaginary part $b$ of a complex number $z=a+i b$ |
| $\boldsymbol{A}$ Amplitude | Amplitude $A$ of a complex number $z=A \exp [i \phi]$ |
| $\varphi$ Phase | Phase $\phi$ of a complex number $z=A \exp [i \phi]$ |
| $A^{2}$ Squared Amplitude | Squared amplitude $A^{2}$ of a complex number $z=A \exp [i \phi]$ |
| $A_{\varepsilon}^{2}$ Summed Squared Am- | OnLY FOR HARMONIC FIELDS AND HARMONIC FIELDS SETS <br> plitudes |
| Sum of the Squared Amplitudes of multiple vectorial components <br> $(\hookrightarrow$ Sec. 12.2.2.2). If you select this option, there is an additional com- <br> bobox in the property browser and the context menu, respectively, where <br> you can select which vectorial components are to be combined: $E_{x}$ and $E_{y}$, <br> $E_{z}$ and $E_{x}, E_{z}$ and $E_{y}$, as well as all vectorial components, respectively. In <br> the ribbon this can be done via the launcher button of the Field Quantity <br> group. |  |

The current field quantity is also displayed in the center of the status bar of each harmonic field data view.

### 11.2 Value Scaling

There are several features which influence the scaling of the values.

### 11.2.1 Interpolated View

## Availability

Only for harmonic fields, harmonic fields sets and 2D chromatic fields sets.

## Accessible:

- Ribbon: View > Interpolated View
- Property browser: View > Interpolated View
- Context menu: Interpolated View

You can apply an interpolation on the view without manipulating the underlying data.

- If view interpolation is deactivated, this corresponds to the nearest neighbor interpolation ( $\hookrightarrow$ Sec. 13.2.2). The shown value of each screen pixel is determined according to the value of the nearest corresponding data point.
- If view interpolation is activated, the output is smoothed using the following interpolation methods ( $\hookrightarrow$ Sec. 131.4):
- Cubic 4 point for two-dimensional data,
- Cubic 6 point for one-dimensional data.


### 11.2.2 View Interpolation Modes

## Availability

Only for 1D or gridded 2D data array based documents except for 2D chromatic fields sets.

## Accessible:

- Ribbon: View > Value Scaling > No Interpolation / Pixelated View / Interpolated View / (RealValued) Smoothing
- Property browser: View > View Interpolation > No Interpolation / Pixelated View / Interpolated View / Real-Valued Smoothing
- Context menu: View Interpolation > No Interpolation / Pixelated View / Interpolated View / (RealValued) Smoothing

The views of data-array based documents ( $\hookrightarrow$ Sec. 13) can be smoothed without changing the contained data. The following options are available:

- No Interpolation: AVAILABLE FOR 1D DOCUMENTS ONLY Only the values at the data point coordinates will be drawn.
- Pixelated View: The value of the nearest neighbor (in equidistant case) or of the neighbor with the nearest lower coordinate (in non-equidistant case) will be shown. This will result in some kind of "stepped" curve (1D) or pixelated diagram.
- Interpolated View: only available if a smoothing interpolation method is stored with the docUMENT
The interpolation which is stored at the displayed object will be used for smoothing the view.
- (Real-Valued) Smoothing: available if the document is complex-valued or if no smoothing inTERPOLATION METHOD IS STORED WITH THE DOCUMENT
A cubic 6 point interpolation (in equidistant case) or a linear interpolation (in non-equidistant case) is applied for smoothing the shown data. In case of complex-valued data the interpolation will be applied to
the currently shown field quantity (amplitude, phase, real part, imaginary part, squared amplitude) only, i.e. the smoothing works real-valued.


### 11.2.3 Triangle Interpolation

## Availability

Only for dot diagrams

## Accessible:

- Ribbon: View > Show Triangles
- Property browser: View > Show Triangles

Using Show Triangles you can obtain a smooth data representation out of dot diagram. In this mode, the View tab of the property browser has an additional option to Show Triangles Borders. The effect of these two options is illustrated in Fig. 64.


Figure 64. The left window shows the normal dot diagram. The right window shows the same data with Show Triangles and Show Triangles Borders.

### 11.2.4 Color Tables

## Availability

For documents based on 2D data arrays, Jones Matrix Transmissions, Harmonic Fields, and Harmonic Fields Sets

## Accessible:

- Ribbon: View > Value Scaling group
- Property Browser: View > Color Table
- Context menu: Color Table

For two-dimensional views, several color tables are available. The principle of the mapping of colors to data values in the range $\left[x_{\min }, x_{\max }\right]$, is shown in Fig. 65.


Figure 65. Principle of color mapping via color table. a) Mapping of one value $x$, b) Mapping of the whole range [ $x_{\text {min }}, x_{\text {max }}$ ]

Via the View ribbon, the Property Browser or the context menu you can choose from a list of color tables. The tables can be managed via View > Manage Color Tables or the Global Options dialog ( $\varsigma$ Sec. 6.9). The corresponding dialog is described in Sec. 11.2.4.1.
You can edit the current table via the ribbon item Start > Edit Color Table or via context menu item Color Table > Edit Color Table.... In this case the dialog described in Sec. 11.2.4.2 opens.
For the view of two-dimensional Numerical Data Arrays or some view modes of objects that contain Data Arrays, a distinct color table per field quantity ( $\leftrightarrows$ Sec. 11.1) can be set.

### 11.2.4.1 Managing Color Tables



Figure 66. Dialog for managing the color tables.
On the left-hand side of this dialog ( $\hookrightarrow$ Fig. 66) you have two lists of color tables: Predefined Color Tables provided by Wyrowski Photonics and User-Defined Color Tables. On the right-hand side you have the Customized Color Tables Menu. This is the menu shown among others in the View ribbon, the Property Browser, and the context menu. You can add a color table to this menu from any of the lists on the left-hand side using the
corresponding $\Rightarrow$ button or by double-clicking. Conversely, you can move an entry from the customized menu back to the "stock" with the button or by double-clicking.
The entries in the Customized Color Table Menu can be sorted with the $\uparrow$ and the $\checkmark$ button, respectively. Entries which are used as default for certain field quantities ( $\hookrightarrow$ Sec. 6.9) are underlined.
The currently selected color table can be edited with the $W$ button. Then the dialog described in Sec. 11.2.4.2 opens. Each color table has to have a unique name.
The User-Defined Color Tables section has the following additional buttons:

| BUTTON | DESCRIPTION |
| :--- | :--- |
| iin | Imports a previously exported color table from a file. If the name of the im- <br> ported color table is already used, a " (1)" is appended to its name. |
| "吹 | Exports a color table to a file. |

### 11.2.4.2 Editing a Color Table

Each color table can be edited via the dialog shown in Fig. 67.


Figure 67. Edit dialog for a color table.

ITEM
DESCRIPTION

| $\downarrow$ | Inverts the color sequence. |
| :--- | :--- |
| $\uparrow$ | Moves the selected color up. |
| $\downarrow$ | Moves the selected color down. |
|  | Inserts a new color to the sequence. |
| $\square$ | Removes the selected color from the sequence. |
| Interpolate Colors | If checked, a linear interpolation is applied to the color sequence, so a smooth <br> color profile is mapped to continuous data values. Otherwise, discrete colors <br> are mapped. |
|  |  |

## Mapping Function <br> The type of the function that maps colors to data values can be selected here.

- Linear Function: The color index $c_{l i n}$ for a given value $v$ and normalized to the range $[0 \ldots 1]$, is calculated via $c_{\text {lin }}=(v-\min ) /(\max -\min )$. The values min and max define the data value range to be shown in the view (min $<=v<=\max$ ).
- Exponential Function: At first, the linear color index $c_{\text {lin }}$ is calculated from value $v$ according to the formula given for the Linear Function. At second, the color index $c_{\text {exp }}$ is calculated via $c_{\text {exp }}=$ $\left(e^{c_{l i n} \cdot p}-1\right) /\left(e^{p}-1\right)$. The parameter $p$ is the Function Parameter which has to be defined separately.
- Logarithmic Function: At first, the linear color index $c_{l i n}$ is calculated from value $v$ according to the formula given for the Linear Function. At second, the color index $c_{\log }$ is calculated via $c_{\log }=$ $\ln \left(c_{\text {lin }}\left(e^{p}-1\right)+1\right) / p$. The parameter $p$ is the Function Parameter which has to be defined separately.
- Power Function: At first, the linear color index $c_{\text {lin }}$ is calculated from value $v$ according to the formula given for the Linear Function. At second, the color index $c_{\text {pow }}$ is calculated via $c_{\text {pow }}=c_{\text {lin }}^{p}$. The parameter $p$ is the Function Parameter which has to be defined separately.

| Function Parameter | All available types of mapping functions, except from Linear Function, allow <br> to specify one parameter $p$ which can be set here. It influences the slope of <br> the selected mapping function and has to lie within the interval $] 0 \ldots 100]$. |
| :--- | :--- |
| Unique Name | The unique name of the color table. This is the name under which it is stored <br> in the list of user-defined color tables ( $\hookrightarrow$ Sec. 11.2 .4 .1 ). If you close the dialog <br> and there is already a user-defined color table with the same name, you can <br> choose whether to change the name or to overwrite the old color table. |
| Marker Color 1 | First color to be used for selection markers like rectangular / elliptic marker <br> or line marker. |
| Transparent | The Color 1 may be transparent. So transparency can be switched on and <br> off here. |
| Marker Color 2 | Second color to be used for selection markers like rectangular / elliptic marker <br> or line marker. |
| Highlighting Color | Sometimes some parts of a marker have to be highlighted. The color to be <br> used for this can be set here. |
| Suggest Marker Colors | Pressing this button will suggest some colors which can be used as marker <br> colors. |
| Preview | When you edit the color table of a document window, there is a Preview but- <br> ton. If you click it, the current color table is directly applied to the document <br> window (but Cancel still reverts it back to the original color table). |

## Note on marker colors

For Jones Matrix Transmissions, Harmonic Fields, and Harmonic Fields Sets, Marker Color 2 is used to draw the markers. For drawing polarization ellipses ( $\hookrightarrow$ Sec. 12.2.2.3), marker color 1 and 2 are used (depending on their direction of rotation). The polarization grid is drawn with the Highlighting Color.

### 11.2.4.3 Display of Undefined Values

In some cases, a data point of a Data Array, Chromatic Fields Set etc. does not contain a defined numerical value. This may be e.g. a result of a division by zero.
Since this kind of value can not be mapped onto a color via a color table, it will be marked by an independently defined color. This may look like shown in Fig. 68.


Figure 68. Example for the color indicator of undefined values.

The color which indicates undefined values can be set via property browser ( $\hookrightarrow$ Sec. 13.5.1.2 and Sec. 13.5.1.3). The Global Options dialog allows to define the default colors to be used for 1D views and 2D views ( $\hookrightarrow$ Sec. 6.8 and Sec. 6.9).

### 11.2.5 Scaling Mode

## Availability

## Accessible:

- Ribbon: View > Scaling Mode ribbon menu
- Property browser: View > Scaling Mode (for Harmonic Fields and Harmonic Fields Sets) View > Auto Scaling of Data (for data array based documents)
- Context menu: Scaling Mode (for Harmonic Fields and Harmonic Fields Sets)

The upper and the lower limit of the chosen color palette ( $\hookrightarrow$ Sec. 11.2.4) are mapped to the minimum and maximum value of the currently visible field quantity ( $\hookrightarrow$ Sec. 11.1). There are three possibilities of how the minimum and maximum values are determined:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Scaling | The minimum and maximum values are calculated from the field. |
|  | OnLY FOR HARMONIC FIELDS AND HARMONIC FIELDS SETS <br> This mode depends on the selected field quantity $(\hookrightarrow$ Sec. 11.1$)$. For real and <br> imaginary part the value range $[-1,1]$ is used. The standard value range for <br> amplitude and intensity is $[0,1]$, and for phase it is $[-\pi, \pi]$. |
|  | The Displayed Data Range can be specified within the View panel of the prop- <br> erty browser. |

There is also the possibility to use User-Defined Scaling in a way that a marked rectangular / elliptical or onedimensional range is scaled optimally:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Selection Based Scal- | The minimum and maximum values of the view are set to the value range |
| ing | within the current rectangle / elliptical or range selection ( $\hookrightarrow$ Sec. 11.3.4). |

In one-dimensional views, the value range determines the range of the y-axis. In two-dimensional views, the value range is displayed besides the color scale on the right hand side.

### 11.2.6 Brightness

## Availability

For the two-dimensional views showing real colors

## Accessible:

- Ribbon: see below
- Property browser: View > Brightness Factor

For documents showing real colors a brightness factor can be used to make darker regions visible. A factor of 1.0 refers to the brightest image where the colors are not yet distorted due to overexposure.

You can enter the brightness factor directly in the View tab of the ribbon or the property browser. Or you use the controls shown in Fig. 69. The left bulb decreases the brightness by 0.1, while the left bulb increases it by the same amount.

| 8 | 1.0 | 8 |
| :--- | :--- | :--- |
| $\Theta$ | - | $\oplus$ |

Figure 69. The controls for adjusting the brightness in the View tab of the ribbon

However, the eye is a logarithmic "detector" (Weber-Fechner law). Thus you often need quite large brightness factors to see the desired dark regions. To compensate this, there is an exponential trackbar below the bulbs. With it you can set the brightness to powers of $\sqrt[5]{10}$.
The minimum brightness is 0.1 and the maximum brightness is 1000 .

### 11.3 Markers and Selections

## Availability

...for Selection Mode

## Accessible:

- Ribbon: View > Selection Mode ribbon menu
- Property browser: View > Selection Mode (for data array based documents)
- Context menu: Selection Mode

Within a diagram view, a portion of the displayed data can be selected for further evaluations and operations, e. g. the Selection Based Scaling ( $\hookrightarrow$ Sec. 11.2.5) or the Normalize with Respect to Selection ( $\hookrightarrow$ Sec. 22.9). Fig. 70 shows a selection example for a 1D data array, Fig. 71 an example for the 2D view of a 2D data array.


Figure 70. Example for the point marker (Magenta) and the range marker (Red) in a 1D Numerical Data Array view.


Figure 71. Example for the point marker, the line marker, and the elliptic/rectangular marker in a $2 D$ Numerical Data Array view.

Each kind of marker can be drawn into a view with the mouse if the corresponding Selection Mode is selected. There are four modes for 2D views:

- Rectangle or Ellipse Marker ${ }^{1}$
- Line Marker
- 交 Point Marker
- No Marker

And there are three modes for 1D views:

- |\& Range Marker
- Is Point Marker
- No Marker

If the corresponding mouse mode is selected, then the markers can be configured with the mouse as follows:

MARKER

## Point Marker

## Range Marker

## MANIPULATION POSSIBILITIES

- Set the point marker at a certain position by left-clicking there.
- Move the point marker either via arrow keys or by dragging with the mouse.


## Line Marker

- Set the line marker by left-clicking on the desired start position, keeping the left mouse button pressed while moving to the desired end position. The end position of the resulting line marker is marked with an arrow head. Restricted line angles can be achieved holding Ctrl pressed while dragging.
- Change either the start or the end position by dragging with the mouse. Restricted line angles can be achieved holding Ctrl pressed while dragging.
- Move the line marker either via arrow keys or by dragging the line center (marked by a circle) with the mouse.
- Create a maximized default line marker by double-clicking on the view.
- Set the range marker by left-clicking on the desired position of one border, keeping the left mouse button pressed while moving to the desired opposite border.
- Change any of the borders by dragging with the mouse.
- Move the range marker either via arrow keys or by dragging the range center (marked by a half-circle).
- Create a maximized range marker by double-clicking on the view.


## Rectangle Marker

- Set the rectangle marker by left-clicking on the desired position of one corner, keeping the left mouse button pressed while moving to the desired opposite corner.
- Change any of the borders by dragging with the mouse.
- Change any of the corners by dragging with the mouse.
- Move the rectangle marker either via arrow keys or by dragging the center of the rectangle (marked by a circle) with the mouse.
- Create a maximized rectangle marker by double-clicking on the view.

Note that the Selection Mode is the same for all document windows. If you change it for a one-/ two-dimensional document, you change it for all other one-/ two-dimensional documents as well.

[^3]For Harmonic Fields and Harmonic Fields Sets, the markers are drawn red or black, the latter for rainbow or reverse rainbow color scale. For 1D data array based documents the point marker is drawn magenta and the range marker is drawn red. For 2D data array based documents the colors of the markers can be set in the edit dialog of the currently used Color Table ( $\hookrightarrow$ Sec. 11.2.4.2).
If a line marker is visible, the current cross section defined by the marker is shown below the 2D data.
After you have defined a marker ( $\hookrightarrow$ Sec. 11.3) it stays visible in the view until you turn it off. This can be done as follows.

## Availability

...for Marker Visibility

## Accessible:

- Ribbon: View > Show ... Marker
- Property browser:
- For Harmonic Fields and Harmonic Fields Sets: View > Display Selection Marker, View > Display Profile Line, and Point Manipulation > Display Marker, respectively
- For data array based documents: View | Selections > Show Rectangle or Ellipse Marker, View | Selections > Display Range Marker, View | Selections > Display Line Marker, and View | Selections > Display Point Marker, respectively
- Context menu: Marker Visibility


### 11.3.1 Setting Exact Marker Coordinates

In the Property Browser you can set the exact coordinates either in point or in physical coordinates. This can be done at different locations for data array based documents or for Harmonic Fields and Harmonic Fields Sets which are summarized in the following table.

| MARKER | DATA ARRAY BASED DOCUMENTS | HARMONIC FIELDS (SETS) |
| :---: | :---: | :---: |
| Point Marker | Property Browser: Selections > Selection (Point) | Property Browser: Point Manipulation > Clicked Position |
| Line Marker | Property Browser: Selections > Selection (Line) | Property Browser: View > Profile Line |
| Range Marker | Property Browser: Selections > Selection (Range). The $\square$ button opens the dialog described in Sec. 11.3.1.1. <br> Ribbon: View > Selection Tools > Edit Range Marker Coordinates ( $\rightarrow$ Sec. 11.3.1.1) | ```Property Browser: View > Selection (Range) Ribbon: View > Selection Tools > Edit Range Marker Coordinates (}\hookrightarrow\mathrm{ Sec. 11.3.1.1)``` |
| Region Marker | Property Browser: Selections > Selection (Region). The... button opens the dialog described in Sec. 11.3.1.2. <br> Ribbon: View > Selection Tools > Edit RectanguIar Marker Coordinates ( $\leftrightarrows$ Sec. 11.3.1.2) | Property Browser: View > Selection <br> (Region) <br> Ribbon: View > Selection Tools > Edit Rectangular Marker Coordinates ( $\hookrightarrow$ Sec. 11.3.1.2) |

In the Property Browser of data array based documents you can set Selections > Coordinate Snapping Selection to false. Then the markers no longer "snap" to the sampling points. Consequently, you then can enter the marker coordinates only in physical coordinates, not in point coordinates.

For gridless 2D data arrays and ray tracing results, coordinate snapping is never active for the rectangle marker and always active for the line and the point marker. Thus in the Property Browser this option is not shown. Furthermore, you cannot change the coordinates of the line and the point marker in the Property Browser, and elliptic selections are not available.

### 11.3.1.1 Edit Range Marker Coordinates

By clicking View > Selection Tools > Edit Range Marker Coordinates an edit dialog for editing the range marker coordinates opens.


Figure 72. Dialog for editing the coordinates of a range marker in the view of a Numerical Data Array or Data Array based document.

Available options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Position / Size Mode | If selected, the input values will be one coordinate and size of the range. |
| Start / End Mode | If selected, the input values will be the left coordinate and the right coordinate <br> of the range. |
| Position to Enter | AvAILABLE IN POSITION / SIZE MODE ONLY. <br> The coordinate which is to be set can be specified here. |
| Left / Right | The left or right border coordinate. |
| Center $\leftrightarrow$ | The center coordinate. |
| Width | The width spanned by the range. |
| The coordinates are de- | A note which indicates that the coordinates to be edited are descending co- <br> scending. |

### 11.3.1.2 Edit Rectangular Marker Coordinates

By clicking the ribbon item View > Selection Tools > Edit Rectangular Marker Coordinates an edit dialog for editing the rectangular marker coordinates opens.


Figure 73. Dialog for editing the coordinates of a rectangular or elliptic marker in the view of a Numerical Data Array or Data Array based document.

Available options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Position / Size Mode | If selected, the input values will be one pair of coordinates and width and <br> height of the rectangle. |
| Corner Mode | If selected, the input values will be the bottom-left-coordinates and the top- <br> right-coordinates of the rectangle. |
| Position to Enter | AvAILABLE IN PositIon / SIZE MODE oNLY. <br> The pair of coordinates which are to be set can be specified here. |
| Left / Right The left or right border coordinate. <br> Bottom / Top The bottom or top coordinate. |  |
| Center $\leftrightarrow$ / Center $\downarrow$ | The horizontal center or vertical center coordinate. |
| Width / Height | The width or height. |
| Keep Aspect Ratio | If selected, changing the width or height will adapt the corresponding size in <br> order to keep the aspect ratio constant. |

### 11.3.2 Point Information

If a point marker is visible, the Selections tab of the Property Browser (it is named Point Manipulation for Harmonic Fields and Harmonic Fields Sets) shows the data at the selected location as shown in Fig. 74.


Figure 74. Example for using the point marker. In the left, there is a field with activated point marker. The corresponding values at this position are displayed in the property browser (right).

For complex data, real and imaginary part, amplitude, squared amplitude, and phase are shown. For Light View ( $\hookrightarrow$ Sec. 12.2.1) and real color display ( $\hookrightarrow$ Sec. 14.2) the RGB values at the current position are shown. For data array based documents, you can also retrieve interpolated values between adjacent data points if Selections > Coordinate Snapping Selection in the Property Browser is set to 'false'. Usually the interpolation method ( $\hookrightarrow$ Sec. 13.2) of the data array is used. If Selections > Use Own Interpolation Method is set to 'false' instead, nearest neighbor interpolation (or constant interval interpolation, in case of non-equidistant data) will be used.
For data array based documents there is another, faster access to a point's value however. One has to hover the mouse cursor above the point of interest holding the Shift button pressed. A tooltip-kind-of label will appear then, showing the coordinates currently hovered above as well as the data value(s) at this position as shown in Fig. 75.


Figure 75. If the mouse cursor is moved over the view of a data array based document, a tooltip-like label shows value and coordinates.

### 11.3.3 Point Manipulation

For Harmonic Fields and Harmonic Fields Sets, single point data may be manipulated via the property browser tab named Point Manipulation, shown in Fig. 74 (right-hand side). The new value just has to be entered there. In case of data array based documents, the workflow is different. The values on the Selections tab of the Property Browser are read-only, but single point values can be edited in the Value at ( $x, y$ ) tab of the document view itself as described in $\hookrightarrow$ Sec. 13.5.3.

### 11.3.4 Selection Tools

Within the View > Selection Tools menu there are various selection tools which ease setting up a selection:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Select All | Sets a rectangle or range marker which includes the whole data. |
| Center Range/ Rectangular Selection | The center of the selection is set to e.g. $(0 \mathrm{~m} ; 0 \mathrm{~m})$ if both axes have the physical quantity Length. |
| Edit Range Marker Coordinates | Opens a dialog for editing the coordinates of the marker ( $\hookrightarrow$ Sec. 11.3.1.1). |
| Edit Rectangular Marker Coordinates | Opens a dialog for editing the coordinates of the marker ( $\hookrightarrow$ Sec. 11.3.1.2). |
| Detect Rectangular I Range Selection | Detects a selection containing a given power portion ( $\varsigma$ Sec. 11.3.4.1). |
| Retrieve Marker Coordinates for Data Array Based Documents | Copies the physical coordinates of all markers from another document window. If a marker to copy does not fully fit into the coordinate ranges of the axes, it is truncated accordingly. But if it lies completely out of the data, it is not copied. Note that coordinate snapping ( $\hookrightarrow$ Sec. 11.3.1) and different physical units might cause the copied markers to be not at the expected location. |
| Retrieve Rectangular <br> Marker Coordinates <br> for Harmonic Fields (Sets) | Copies the physical coordinates of the rectangular (or range) marker from another document window. If the marker to copy does not fully fit into the coordinate ranges of the axes, it is truncated accordingly. |

The exact coordinates of a selection can also be edited using the Property Browser ( $\hookrightarrow$ Sec. 11.3.2).

### 11.3.4.1 Detect Rectangular / Range Selection

By using either the ribbon item View > Selection Tools > Detect Rectangular Selection or View > Selection Tools > Detect Range Selection, the selection within a view can be set to the smallest possible selection which contains a given portion of the amplitudes sum or the squared amplitudes sum of the whole data. Which of the two ribbon items is available depends on the dimensionality of the data in the current document.

| Detect Selection |  |
| :--- | :---: |
| Use on Amplitudes | OUse on Squared Amplitudes |
| Portion of Amplitudes Sum in Selection | Barycenter of Field Values $\checkmark$ |
| Center of Selection |  |
| $\boxed{V}$ Enforce Quadratic Selection | Cancel |
|  |  |
|  |  |

Figure 76. Dialog for detecting selections (for a Numerical Data Array).

The dialog shown in Fig. 76 allows you to set the following parameters for this operation.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use on Amplitudes / <br> Use on Squared Ampli- <br> tudes | Allows you to set whether the amplitudes sum or the squared amplitudes <br> sum is evaluated. This choice is only available for certain document types <br> (see below). |
| Portion of (Squared) Am- <br> plitudes Sum in Selection | Portion of the (squared) amplitudes sum of the whole data to be contained in <br> the selection. |
| Center of Selection | You can choose between three options: <br> - Automatic: No specific center point is used. The algorithm just tries to <br> minimize the resulting selection. |
| - Barycenter of Field Values: The selection will be centered around the |  |
| barycenter of the field values (= the power center for Harmonic Fields |  |
| and Harmonic Fields Sets). |  |
| - Window Center: The resulting selection will be in the center of the win- |  |
| dow. |  |

Depending on from where this selection tool is executed the names and visibility of the controls mentioned above differs. For example Harmonic Fields and Harmonic Fields Sets always contain electric field strength data. In this case it is more intuitive to use a certain portion of the power of the whole field, which is proportional to the squared amplitudes sum. Thus:

- For a Harmonic Field you always determine a portion of the power.
- For a Jones Matrix Transmission you always determine a portion of the squared values sum.
- For a complex-valued Numerical Data Array or data array based document you can choose whether you want to determine a portion of the amplitudes sum or of the squared amplitudes sum (as described above).
- For a real-valued data array based document you always determine a portion of the values sum.
- For a real-valued Numerical Data Array you can choose whether you want to determine a portion of the values sum or of the squared values sum.


### 11.4 Zoom

## Availability

## Accessible:

- Ribbon: View > © Zoom In, View > Q Zoom Out, View > © Show All, View > Q Zoom Into Selection, View > 图 Data Restricted Zoom
- Property Browser: see below
- Context menu: Zoom
- Shortcuts: Ctrl ++ (numpad) to zoom in, Ctrl +- (numpad) to zoom out, and Ctrl +0 (numpad) to show all.

Four operations are available to change the zoom factor:

| ITEM | DESCRIPTION |
| :---: | :---: |
| © Zoom In | Increase zoom factor by factor $\sqrt{2}$. |
| Q Zoom Out | Decrease zoom factor by factor $\sqrt{2}$. |
| (2) Show All | Show the whole field. This is the default for newly created fields. |
| Q Zoom Into Selection | Set the visible area equal to the current range / rectangle selection. |
| -¢+ Center to Origin | Available for all views except that of Harmonic Fields, Harmonic Fields Sets and Jones Matrix Transmissions <br> Centers the view to the coordinate origin $(0,0)$ in case of 2D data, 0 in case of 1D data, no matter whether or not the origin lies within the coordinate range of the sampled data. If it lies outside, Data Restricted Zoom is deactivated automatically. |
| [莪 Data Restricted Zoom | Available for all views except that of Harmonic Fields, Harmonic Fields Sets and Jones Matrix Transmissions Toggles the Data Restricted Zoom state, see Sec. 11.4.1. |

Inside the View panel of the Property Browser, you can set the visible view area using the following options:

- Coordinate Range: Allows to set the coordinate range of 1D diagrams directly.
- x-Axis Range / y-Axis Range: Allows to set the coordinate ranges of 2D diagrams directly.
- Zoom Factor: Allows to set the zoom factor, given in Zoom Factor Unit/s. That means that a zoom factor of $z$ corresponds to $z$ screen pixels covering the physical value range given in Zoom Factor Unit/s.
- Data Restricted Zoom: Available for all views except that of Harmonic Fields, Harmonic Fields Sets and Jones Matrix Transmissions
Toggles the Data Restricted Zoom state, see Sec. 11.4.1.
- Show Rectangle/Markers for Whole Extension: If Data Restricted Zoom is deactivated, this option allows to toggle the visibility of a rectangular/range marker which shows the domain covered by the actual given data.

Furthermore, you can use the mouse wheel to zoom in or out by a factor $\sqrt{2}$ at the position of the mouse cursor.

### 11.4.1 Data Restricted Zoom

With a few exceptions, most of the diagram views provide the feature of toggling the Data Restricted Zoom state. If activated (the default), the maximum view area for a diagram is the range covered by the underlying data. So, if the complete domain with defined data is shown, no more zoom out is possible. However, if the Data Restricted Zoom is deactivated, the user may zoom out (nearly) unlimited. An example is shown in Fig. 77.


Figure 77. Example for unrestricted zoom out. The actual domain of the underlying data is marked by the magenta rectangle (which can be switched off via Property Browser).

Such a view beyond the limits of the data domain provides some benefits: For example, comparing of diagrams with different domains of definition is much easier. Furthermore, sometimes there is a need to see how the data are extrapolated outside the actual coordinate range.

### 11.5 Aspect Ratio

## Availability

## Accessible:

- Ribbon: View > Aspect Ratio ribbon menu
- Property browser: View > Aspect Ratio (for harmonic fields and harmonic fields sets)

View > True To Scale (for data array based documents)

- Context menu: Aspect Ratio

In views showing two-dimensional data, VirtualLab Fusion supports three ways how the aspect ratio between the two axes is determined.

ITEM DESCRIPTION

True To Physical Scale
The data is displayed on the screen so that the same physical extent on the $x$ - and $y$-axis corresponds to the same number of pixels on the screen. That means the data is displayed as it would be visible within an experiment, with true to scale representation.
蓉 True To Pixel Scale
ONLY FOR HARMONIC FIELDS AND HARMONIC FIELDS SETS
Each sampling point of the data is mapped to a pixel square on the screen. If the vertical and horizontal sampling distances are not equal, the same distance on the screen in $x$ - and $y$-direction corresponds to different physical extents.

Free Aspect Ratio The aspect ratio is chosen for optimal fitting of the data into the document window. Thus, resizing the document window changes the aspect ratio. The same distance on the screen in $x$ - and $y$-direction may correspond to different physical extents as well as to a different number of sampling points.

### 11.6 Copy View to Clipboard

## Availability

Accessible:

- Ribbon: View > Copy View to Clipboard
- Context menu: Copy to Clipboard (for harmonic fields and harmonic fields sets)
- Shortcut: Ctrl+C

Copies the current view to the Windows ${ }^{\text {TM }}$ clipboard.
For data array based documents the view is copied as shown. In the Global Options dialog ( $\hookrightarrow$ Sec. 6.7) you can set whether the gray background of the view is copied or transparency is used instead.
For harmonic fields and harmonic fields set you can configure the generated graphics using the dialog described in the following section.

### 11.6.1 Copy View to Clipboard (Dialog for Harmonic Fields and Harmonic Fields Sets)

Several options are available for copying a field view to the clipboard, which can be set by using the dialog shown in Fig. 78. There are several groups of controls within this dialog, which are described in the following.


Figure 78. Dialog to adjust settings for copying a harmonic field view to clipboard.

The controls of the group View to be Copied determine which parts of the harmonic fields view are to be copied to the clipboard.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Both 1D and 2D View | Copy two-dimensional view and one-dimensional profile line view. |
| 2D View | Copy only two-dimensional view. |
| 1D View | Copy one-dimensional view. |

The following Options group controls which features of the view are included when copying to the clipboard.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Copy Axes | Determines whether the labels at the corners of the two-dimensional view are <br> copied. |
| Copy Selection Marker | Determines whether the lines representing the rectangle / range marker <br> $(\hookrightarrow$ Sec. 11.3) are copied. |
| Copy Profile Line | Determines whether the red arrow representing the line marker ( $\hookrightarrow$ Sec. 11.3) <br> in the two-dimensional view is copied. |
| Copy Point Manipulation  <br> Cross Determines whether the cross hair representing the point marker <br> $(\hookrightarrow$ Sec. 11.3) is copied. <br> Copy Color Scale Determines whether the legend on the right hand side of the two-dimensional <br> view is copied. <br> Copy Grid Lines Determines whether grid lines are copied in the one-dimensional view. <br> Color of Labels and Axes Edit color of axis lines and labels of one and two-dimensional view. <br> Color of Grid Lines |  |

A field view can be copied to the clipboard in two different ways: as windows meta file and as bitmap. Since windows meta file export corresponds to a vector graphics, the graphics is highly resolved. However, for some target programs, the result of the clipboard import of meta files can look erroneous due to incompatibilities. In such cases, exporting the view via a bitmap object in the clipboard can give better results.

When using windows meta file clipboard export, the background is always transparent.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Convert to Bitmap | Bitmap mode of clipboard copying. |
| Bitmap Size | Size of the generated bitmap in pixels. |
| Preserve Aspect Ratio of  <br> View If checked, the bitmap size in $X$ and $Y$ direction are coupled for ensuring that <br> the aspect ratio of the view is maintained.  |  |
| Background Color | Background Color to be used in the bitmap. |

### 11.7 Graphics Add-Ons

## Availability

Only for data array based documents.

## Accessible:

- Ribbon: View > Configure All

All data array (based) views may show additional information, called "graphics add-ons" or simply "add-ons", which overlay the actual data. These add-ons may e.g. be regions, point clouds, polarization ellipses etc. If there are more than one add-on, all are layered in an order which can be user-specified.
The ribbon button Graphics Add-ons > Configure All calls the dialog shown in Fig. 79 which allows to configure all contained graphics add-ons.


Figure 79. Dialog for configuring the graphics add-ons of a view.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index | The layer index. Index \#1 corresponds to the bottom layer which is drawn <br> above the data first. The row with the highest index will be the upmost layer <br> which is drawn at last. |
| Up/Down | Moves the add-on up or down in the layer order. |
| Name | Name of the add-on. |
| Subsets | Shows for which subsets the add-on is available. |
| Visible | Allows to show or hide the add-on. |
| Appearance | Opens another dialog for editing the individual view settings for the add-on. <br> See Sec. 11.7.1-Sec. 11.7.3. |

### 11.7.1 Configuration of Common Graphics Add-ons



Figure 80. Dialog for configuring the view settings of common graphics add-ons like regions or meshes.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Draw Border | If checked, a border will be drawn. |
| Border Color | If Draw Border is selected, this sets the color of the border line. |
| Border Width | If Draw Border is selected, this sets the width of the border line. |
| Draw Filling | If checked, the shown areas will be filled. |
| Filling Color | If Draw Filling is selected, this sets the color of the filling. |
| Filling Opacity | If Draw Filling is selected, this sets the opacity of the filling: $0 \%$ means full <br> transparency, $100 \%$ will create completely non-transparent fillings. |

### 11.7.2 Configuration of Point Cloud Add-Ons



Figure 81. Dialog for configuring the view settings of point cloud add-ons.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Dot Size | The size of the points. |
| Color | The color of the points. |

### 11.7.3 Configuration of Polarization Ellipse Add-Ons



Figure 82. Dialog for configuring the view settings of polarization ellipses.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Line Width | The thickness of the drawn lines. |
| Draw Arrows | If chosen, the Direction of Rotation will be indicated by small arrows. |
| Different Colors | If chosen, the Direction of Rotation will be indicated by different colors. |
| Clockwise Color | If Different Colors is selected, this sets the color for clockwise ellipses. |
| Counterclockwise Color | If Different Colors is selected, this sets the color for counterclockwise ellipses. |
| Minimum Cell Size | Size on the screen which shall be occupied by the ellipses at least. If the <br> zoom factor is high enough, the ellipses of each single sampling point are <br> shown and may be even larger than this minimum size. Please see the note <br> below for more information. |
| Extraction via Nearest | If an extraction is necessary because more than one sampling point is cov- <br> ered by Minimum Cell Size (Screen Pixels), this parameter determines the <br> extraction strategy. Either only the point with the position nearest to the el- |
| Neighbor / Average | lipse's center is used alone or the Jones vectors of all points covered by the <br> cell are averaged. Please see the note below for more information. |
| Draw Grid | If chosen, a grid indicates the areas each ellipse is calculated from. <br> Grid Color |

Note on the extraction (calculation) of the shown polarization ellipses:
It is only possible to see every single polarization ellipse in the data if the zoom factor is high enough. Only if the display of a single sampling point occupies a minimum number of screen pixels, there is enough space to draw the ellipse which corresponds to this sampling point. This case can be seen in Fig. 83, on the left-hand side. The (cell) size which shall be used to draw an ellipse at least can be set in the view settings dialog: Minimum Cell Size (Screen Pixels).
In many cases the minimum screen area to draw an ellipse will cover more than one single sampling point. This is shown in Fig. 83, on the right-hand side. There are two possibilities for determining the contributions of the sampling points to each ellipse: Either the average Jones vector of all covered points is used to calculate the ellipse or only that sampling point is used which is located nearest to the ellipse's center position. These alternatives can be chosen in the view settings dialog by selecting either Extraction via Average or Extraction via Nearest Neighbor.


Figure 83. The display of the polarization ellipses depends on the zoom factor. Left-hand side: The zoom is large enough to show each single ellipse for each sampling point. Right-hand side: For a smaller zoom factor, the ellipse is extracted (either via averaging or by nearest neighbor selection) from the points covered by the minimum ellipse cell size.

### 11.8 Suppressing Numerical Phase Artifacts

## Availability

Only available for Harmonic Fields, Harmonic Fields Sets, Numerical Data Arrays or Data Arrays with the physical meaning Electric Field or Electromagnetic Field ( $\leftrightarrows$ Sec. 24.1.4). This feature applies only if either the phase is shown as field quantity ( $\leftrightarrows$ Sec. 11.1) or if polarization ellipses ( $\leftrightarrows$ Sec. 12.2.2.3, $\rightarrow$ Sec. (c)) are visible.

## Accessible:

- Ribbon: View > 悗 Hide Phase Artifacts
- Property browser: View > Hide Phase Artifacts
- Context menu: 懁 Hide Phase Artifacts


### 11.8.1 Numerical Artifacts in Phase View of Diagrams

Some calculations produce numerical inaccuracies in the real and imaginary part of complex numbers. The phase $\phi$ of a complex number may be sensitive to such inaccuracies due to its dependence on both of these parts. In VirtualLab Fusion the phase is defined as follows:
$\phi=\left\{\begin{array}{llll}\arctan \left(\frac{\mathrm{Im}}{\mathrm{Re}}\right) & : \operatorname{Re}>0 & \\ \arctan \left(\frac{\mathrm{Im}}{\mathrm{Re}}\right)+\pi & : \operatorname{Re}<0 & \text { and } & \mathrm{Im}>0 \\ \arctan \left(\frac{\mathrm{Im}}{\operatorname{Re}}\right)-\pi & : \operatorname{Re}<0 & \text { and } & \mathrm{Im} \leq 0 \\ +\frac{\pi}{2} & : \operatorname{Re}=0 & \text { and } & \mathrm{Im}>0 \\ -\frac{\pi}{2} & : \operatorname{Re}=0 & \text { and } & \mathrm{Im}<0 \\ 0 & : \operatorname{Re}=0 & \text { and } & \mathrm{Im}=0\end{array}\right.$
Normally there is no visible effect on a diagram view of these data because of the very small magnitude of numerical inaccuracies, but there are two cases where artifacts in the phase values may appear:

1. If both the real and the imaginary part are nearly zero (i.e. the amplitude is nearly zero too), these inaccuracies have consequences for the phase (due to the fraction ( $\mathrm{Im} / \mathrm{Re}$ ) in the arctangent), though not for the amplitude $\left(\operatorname{Re}^{2}+\mathrm{Im}^{2} \approx 0\right)$. So despite the vanishing amplitude the phase has randomly distributed values.
2. If the real part is less than zero but the imaginary part is nearly zero ( $-\epsilon<\operatorname{Im}<+\epsilon$ ), the amplitude is not affected $\left(\mathrm{Re}^{2}+\mathrm{Im}^{2} \approx \mathrm{Re}^{2}\right)$, but the phase is (see case no. 2 and no. 3 in the definition of $\phi$ above). Thus the phase jumps accidentally between $\pi$ and $-\pi$.

An artifacts threshold $t$ can be set in the View panel of the property browser.
This parameter $t$ has the following meanings:

1. A phase value in a diagram is displayed as zero if its amplitude value $A$ satisfies $A<t \cdot A_{\max }$, where $A_{\text {max }}$ is the maximum amplitude value in the data.
2. The phase value is displayed as $-\pi$ in the display if its imaginary part value $\operatorname{Im}$ satisfies $t \cdot \operatorname{Re}<\operatorname{Im}<0$. If Hide Phase Artifacts is activated for a diagram view, both conditions will be tested and the view will hide these kinds of artifacts. The data of the field document itself will remain unchanged.

### 11.8.2 Numerical Artifacts in Polarization Ellipses

If the amplitude for both of the vectorial components used for calculating a polarization ellipse is nearly zero, numerical artifacts have a strong effect on that ellipse.

So these artifacts can be suppressed as well: Polarization ellipses are calculated only if the amplitudes of both of the respective vectorial components are below $t \cdot A_{\max }$, where $A_{\max }$ is the maximum amplitude over the complete data of both vectorial components.
In case of ellipses shown in a Harmonic Field view or a Harmonic Fields Set view ( $\hookrightarrow$ Sec. 12.2.2.3), the threshold $t$ can be set dynamically via property browser.
If polarization ellipses shall be calculated by an EM detector ( $\leftrightarrows$ Sec. 74.4.5.1) or as a manipulation for an already existing electric or electromagnetic field ( $\hookrightarrow$ Sec. 32.3), then the threshold has to be specified in the respective dialog.

### 11.8.3 Default Settings for Suppression of Numerical Phase Artifacts

In the Global Options dialog ( $\hookrightarrow$ Sec. 6.11) , one can set whether phase artifacts are hidden by default and set a default threshold $t$ as well.

## 12 Harmonic Fields and Harmonic Fields Sets

### 12.1 Harmonic Field Data

For locally polarized harmonic fields the two electric field components $E_{x}$ and $E_{y}$ are stored, from which all other field components can be reconstructed. For globally polarized fields, only the scalar field $U(x, y)(\hookrightarrow$ Sec. 131.1) is stored.
The field data are stored as field values on an equidistantly sampled grid. The number of sampling points in x- and y-direction, $N_{x}$ and $N_{y}$ can be chosen freely in the x- and y-direction respectively. For storing twodimensional fields both $N_{x}$ and $N_{y}$ are greater than 1. One-dimensional fields are typically stored with $N_{y}=1$. More technical notes can be found in Sec. 131.
The Data tab of the property browser (Current Data for harmonic fields sets) allows you to view and alter these settings, among others:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Complex Amplitude Type | Shows whether the field is locally or globally polarized and whether it is in <br> spatial or spectral domain. |
| Embedding Material | The material of the homogeneous medium in which the field is defined. |
| Jones Vector | OnLY FOR GLOBALLY PoLARIZED FIELDS <br> Allows you to change the Jones vector. $\hookrightarrow$ Fig. 84 |
| Wavelength | With this parameter you can change the wavelength of the field. <br> Is Complex |
| Shows whether the imaginary part is stored as explained above. |  | | Allows you to change the overall size of field. The number of sampling points |
| :--- | :--- |
| and the actual data remains unchanged. |

This tab is only available in the data view of harmonic fields or harmonic fields sets.


Figure 84. How to edit the Jones vector via the property browser. The controls of the resulting dialog are the same as for setting the Jones vector of a newly generated field, $\hookrightarrow$ Sec. 48.3.

### 12.1.1 Spherical Phase Radius

Sampling of a large spherical phase (e.g. a lens with short focal length) would require a very small sampling distance and thus many sampling points for correctly sampling the spherical phase in the border areas of the field. Therefore, VirtualLab Fusion can handle the spherical phase radius as a separate factor multiplied to the sampled aberrations of the spherical phase. This means that the sampling distance has to be chosen only for accurate sampling of the aberrations.
Many of the internal operations of VirtualLab Fusion, as for example the homogeneous medium propagation operators ( $\hookrightarrow$ Sec. 93), take into account the stored spherical phase radius.
In harmonic fields sets, a separate spherical phase radius is stored for each harmonic field. Thus, spherical phase radius functions are not available in the light view of harmonic fields sets.
For newly created harmonic fields, VirtualLab Fusion detects and stores the spherical phase radius automatically.

If you want to change this stored value, you can use several entries in the Manipulations $>\varphi /$ Phase Manipulations ribbon item:

- Set Analytical Parameter: Sets the analytical spherical phase radius to a new value. The corresponding dialog is explained in Sec. 22.5.2.
- Remove Analytical Parameter: Removes the analytical spherical phase radius.

These manipulations do not change the resulting phase, at least as long as the sampling distance is fine enough for the new aberrations (phase minus analytical spherical phase radius).
The property browser ( $\hookrightarrow$ Sec. 4) offers similar functionality: In the Data panel (for harmonic fields) or the Current Data panel (for harmonic fields sets), you can set Has Spherical Phase Radius to false or true. Setting to false corresponds to removing the spherical phase radius. Furthermore you can set the Spherical Phase Radius. If you want not only to remove the stored value, but also the spherical phase information present in the sampled phase data, you can use the entry Manipulations $>\varphi /$ Phase Manipulations $>$ Remove Sampled Spherical Phase. Manipulations > 部麜 Sampling Manipulations > Resample According to Spherical Phase allows to resample a field so that the spherical phase radius can be removed without resulting undersampling. Detectors $>\ln ^{\mathbf{N}}$ Spherical Phase Radius detects the optimal value of the spherical phase radius.
How the spherical phase radius is determined from sampled data is describe in Sec. 137.6.

### 12.2 View for Harmonic Fields and Harmonic Fields Sets

The view of both Harmonic Fields and Harmonic Fields Sets is divided into two tab pages: the Light View ( $\hookrightarrow$ Sec. 12.2.1) which displays the field as the eye or a camera would see it, and the Data View ( $\hookrightarrow$ Sec. 12.2.2) which shows directly the data.
These documents allow you to use markers and selections ( $\hookrightarrow$ Sec. 11.3), zoom into the view ( $\hookrightarrow$ Sec. 11.4), change its aspect ratio ( $\leftrightarrows$ Sec. 11.5), copy the view to clipboard ( $\hookrightarrow$ Sec. 11.6).
Furthermore, View > Copy View Settings allows you to copy the view settings (value scaling, markers and so on) from another matching document window.
If a line marker ( $\hookrightarrow$ Sec. 11.3) is shown for two-dimensional fields, also a one-dimensional cross section is shown in one common view window ( $\hookrightarrow$ Fig. 85).


Figure 85. Harmonic Field View with Profile Line.

A Harmonic Fields Set usually contains more than one harmonic field. Its light view shows the incoherent superposition of all member harmonic fields.

### 12.2.1 Light View



Figure 86. Example of a two-dimensional light view.

The light view shows the light distribution close to reality. This means that the complex amplitude visible in the data view is

- embedded in a zeroized field (if Use Embedding Frame for Light View is switched on in the Global Options dialog, $\hookrightarrow$ Sec. 6.11),
- interpolated with cubic 8 point interpolation to smooth the data, and
- set to summed squared amplitudes as field quantity (Sec. 11.1).

For two-dimensional light views, you can switch between two modes in the ribbon:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Visual Perception | The (non-linear) perception of the human eye is simulated. For single har- <br>  <br>  <br>  <br> monic fields the color is directly calculated from the wavelength. This means, <br> that infrared $(>830 \mathrm{~nm})$ and ultraviolet fields $(<360 \mathrm{~nm})$ are not visible in <br> this mode. For harmonic fields sets, the resulting color at a certain position is <br>  <br>  <br> calculated from the wavelengths of the single harmonic fields, weighted ac- <br>  <br>  <br>  <br>  <br>  <br> cording to their amplitude at this position. This display uses the Bitmap class <br> provided by Aurigma for appropriate colors. |
| Linear Intensity Detec- | The data is shown as you would see it with a linear detector. You can choose <br> the color table $(\hookrightarrow$ Sec. 11.2 .4$)$ for this mode. |

In the visual perception mode, most view settings are not available. However, you can set the brightness as described in Sec. 11.2.6. In the linear detection mode, you can set the color table ( $\hookrightarrow$ Sec. 11.2.4) and the scaling mode ( $\hookrightarrow$ Sec. 11.2.5). Furthermore, View > Show Legend allows you to switch off the legend for the two-dimensional view.
The calculation of the light view of a newly created harmonic field can be very time consuming, especially for harmonic fields sets. During this calculation, the following screen appears:


Figure 87. Light View during calculation.

At this stage, you can continue working as the light view calculation is done in the background. However, if you want to save CPU power for more important calculations, you can press Cancel. Then on the light view tab the following text is shown:


Figure 88. Light View if calculation has been aborted or not yet started because it was disabled in the Global Options.

As you can see, it's possible to Restart the light view calculation. If you want the light view to be disabled by default, you can do so in the global options dialog (Sec. 6.11). Then the light view tab of a newly created field document looks similar to Fig. 88, i. e. it's possible to start the light view calculation manually. Furthermore, the light view tab looks similar to Fig. 88 if the calculation is aborted due to lack of RAM.

### 12.2.2 Data View

The data view shows directly the data arrays ( $\hookrightarrow$ Sec. 131). It allows you to set the shown field quantity ( $\hookrightarrow$ Sec. 11.1), show polarization information ( $\hookrightarrow$ Sec. 12.2.2.3), and adjust the value scaling ( $\hookrightarrow$ Sec. 11.2). Furthermore, View > Show Legend allows you to switch off the legend for the two-dimensional view. Additional features for the data view are described in the following subsections.

### 12.2.2.1 Harmonic Field Selection

## Availability

## For Harmonic Fields Sets

## Accessible:

- Ribbon: View > Harmonic Field Selection ribbon group (see below)
- Property browser: Document > Current Member

In the ribbon you can go through all harmonic fields within a Harmonic Fields Set with the control shown in Fig. 89, either by using the arrow buttons or by entering the index of the harmonic field directly.


Figure 89. The controls to select an harmonic field in the ribbon.

### 12.2.2.2 Vectorial Component

## Availability

## Accessible:

- Ribbon: View > E-Field ribbon group
- Property browser: View > Vectorial Component
- Context menu: Vectorial Component

If the field quantity ( $\hookrightarrow$ Sec. 11.1) is not set to Summed Squared Amplitudes, one of the three vectorial components $E_{x}, E_{y}$, or $E_{z}$ can be selected for being displayed within the data view.
In VirtualLab Fusion $E_{z}$ is calculated according to

$$
\begin{equation*}
E_{z}(x, y)=\left[\mathcal{F}^{-1}\left(-\frac{1}{k_{z}}\left(k_{x} \cdot\left[\mathcal{F} E_{x}(x, y)\right]\left(k_{x}, k_{y}\right)+k_{y} \cdot\left[\mathcal{F} E_{y}(x, y)\right]\left(k_{x}, k_{y}\right)\right)\right)\right](x, y) \tag{12.1}
\end{equation*}
$$

where $\mathcal{F}$ denotes a Fourier transform and $\mathcal{F}^{-1}$ an inverse Fourier transform.

### 12.2.2.3 Polarization

## Availability

## Accessible:

- Ribbon: View > Polarization ribbon group
- Property browser: View > Show Polarization
- Context menu: Polarization

In the data view, it's possible to display the polarization of harmonic fields or fields sets in three different modes.

| MODE | DESCRIPTION |
| :---: | :---: |
| $\overrightarrow{\text { ® Ellipses }}$ | Ellipses are drawn over the data view as shown in Fig. 91. This display mode shows the complete polarization ellipses, but only with coarse sampling. |
| ${ }^{2}$ Angles of Ellipses | Shows the angles of the major axis of the ellipses to the x-axis with finer sampling. |
| Eccentricities of Ellipses | Shows the (numerical) eccentricity $e$ of the ellipses with finer sampling. |

For all these modes you can specify the plane for which you want to see the polarization via a combobox. If you select the currently selected polarization display mode again, you switch off the polarization view - which can also be done in the property browser via View > Show Polarization group > Show.
You can open a dialog with specific polarization view settings ( $\hookrightarrow$ Fig. 90), either via the context menu (Polarization > View Settings) or the launcher button ${ }_{\mathrm{m}}$ of the View > Polarization ribbon group.


Figure 90. Dialog for changing the polarization view settings.


Figure 91. Example of a data view with polarization ellipses.

This dialog has the following items:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Show Polarization | Toggles the display of any Polarization Display Mode on or off. |
| Polarization Display Mode | As described above, there are three polarization display modes: Polarization <br> Ellipses, Angles of Ellipses, and Eccentricities of Ellipses. |
| Show Grid | Displays a grid between the Polarization Ellipses. <br> Show Arrows <br> Displays arrows which indicate the rotational direction of the electrical field <br> vector $E_{\mathrm{xy}}$ vector in the Polarization Plane. <br> Scaling <br> Polarization PlaneFactor scale up and scale down the polarization ellipses. The standard <br> value is 1.0 , the minimum value is 0.5. |

Default values for these settings can be defined in the Harmonic Field View tab of the Global Options dialog ( $\hookrightarrow$ Sec. 6).
The display of the polarization is influenced by the phase artifacts setting ( $\hookrightarrow$ Sec. 11.8).

### 12.2.2.4 Norm and Power

The View panel of the property browser of harmonic fields and harmonic fields sets has the section Norm and Power. This section contains the following entries:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Norm in Selection | Shows the norm $N$ within the current selection for the displayed vectorial component ( $\hookrightarrow$ Sec. 12.2.2.2). See Sec. 75.4.7 for details on the calculation of the norm $N$. Furthermore the ratio between Norm in Selection and Norm of Whole Component is shown in percent. This entry is only shown if a selection is visible ( $\hookrightarrow$ Sec. 11.3.4). |
| Norm of Whole Component. | Shows the norm $N$ of the displayed vectorial component as defined in Sec. 75.4.7. |
| Power in Selection (Component) | This value is calculated from the Norm in Selection and Eq. (12.2). Furthermore the ratio between Power in Selection (Component) and Power in Whole Component is shown in percent. This entry is only shown if a selection is visible. |
| Power in Selection (Field) | Sum of Power in Selection (Component) for both $E_{x}$ - and $E_{y}$-component. Furthermore the ratio between Power in Selection (Field) and Power in Whole Field is shown in percent. This entry is only shown if a selection is visible. |
| Power in Whole Component | This value is calculated from the Norm of Whole Component and Eq. (12.2). |
| Power in Whole Field | Sum of Power in Whole Component for both $E_{x}$ - and $E_{y}$-component. |

The power properties are not shown for harmonic fields and harmonic fields sets in spectral domain.
From a given norm $N$ of a certain region the power $P$ is calculated as

$$
\begin{equation*}
P=n \frac{\epsilon_{0}}{2} c \delta x \delta y N \tag{12.2}
\end{equation*}
$$

with $\delta x$ is the sampling distance in $x$-direction and $\delta y$ is the sampling distance in $y$-direction. For one-dimensional fields the sampling distance in the unmodulated direction is assumed to be 1 meter. $n$ is the refractive index derived from the Embedding Medium of the field, $\epsilon_{0}$ is the dielectric constant and $c$ is the vacuum speed of light.

## 13 Data Arrays

Data Arrays are designed as containers for any data that represent mappings from any N -dimensional real space $\mathbb{R}^{N}$ (more specific from a domain $X \subset \mathbb{R}^{N}$ ) to any M-dimensional complex space $\mathbb{C}^{M}$ (more specific to a co-domain $Y \subset \mathbb{C}^{M}$ ). An example is shown in Fig. 92 for $N=2$ and $M=3$.


Figure 92. Example for mapping $\mathbb{R}^{2} \rightarrow \mathbb{C}^{3}$.

The components $x_{1}, x_{2}, \ldots, x_{N}$ of the variable $x \in X$ are usually called "coordinates", while $y \in Y$ is named "dependent variable" or simply "data". Each set of all values of a certain dimension $Y_{i}=y_{i}\left(x_{1}, x_{2}, \ldots, x_{N}\right)(1 \leq$ $i \leq M)$ is called "Data Array Subset" or "Data Subset".
Although not all data structures in VirtualLab Fusion are based on Data Arrays at the moment, we plan to introduce them systematically and successively as standard data container.
The most important types of data arrays are gridded 1D and 2D data as illustrated in Fig. 93 and Fig. 94. They show equidistantly sampled data, which is no restricting condition for Data Arrays in general.


Figure 93. Example for equidistant 1D Data Array.


Figure 94. Example for equidistant 2D Data Array.
For small $N$ as in the figures Fig. $93(N=1)$ and Fig. $94(N=2)$, the notations for the variables usually differ slightly: For 1D data the coordinate is called $x$ and the data variable is $y$, while for 2D data usually the coordinates are marked by $x$ and $y$, whereas the dependent variable is called $z$.
In some cases, two-dimensional data are not distributed on a grid but completely irregular ( $\hookrightarrow$ Fig. 95). We call this type Gridless Data Array. Gridless Data Arrays may contain several subsets, same as gridded (i.e. equidistant and non equidistant) ones. No interpolation is available for this kind of array.


Figure 95. Example for a Gridless Data Array.
The view for data arrays is explained in Sec. 13.5.

### 13.1 Types of Data Arrays

In many cases, there is no specific physical meaning associated with a Data Array. Although coordinates and subset values got physical units ( $\hookrightarrow$ Sec. $5.1, \hookrightarrow$ Sec. $24.4, \hookrightarrow$ Sec. 24.5 .1 ), the object itself is not interpreted as having a physical meaning in any case.
Nonetheless, in some cases such a specific meaning is given to a Data Array. An Electric Field object is such a Data Array with a specific interpretation. Whether or not there is a physical meaning given to a data array is indicated by its caption, as shown in Fig. 96. All general, i.e. non-specific, Data Arrays are called Numerical Data Arrays and got a gray caption. All other Data Array objects have a different, type specific caption color.


Figure 96. Example for two different types of Data Arrays. Left: Numerical Data Array. Right: Electric Field.
The most important difference in handling between Numerical Data Arrays and more specific Data Arrays is the availability of manipulations ( $\hookrightarrow$ Sec. 24). The handling of specific Data Arrays is restricted to features and properties which make sense for the given physical meaning type.

### 13.2 Interpolation Methods

Distinct interpolation methods are available for equidistant and non-equidistant data arrays. For twodimensional data arrays, the described rules are applied separately to $x$ - and $y$-direction, respectively. The interpolation methods for non-equidistant data are given in Sec. 13.2.1, the interpolation methods for equidistantly sampled data in Sec. 13.2.2.

### 13.2.1 Interpolation Methods for Non-Equidistant Data

If the data array does not contain equidistantly sampled data, there are two different non-equidistant interpolation methods available: Constant Interval interpolation and Linear interpolation.
In case of complex data, a Real Part / Imaginary Part linear interpolation is distinguished from an Amplitude / Phase linear interpolation. This is due to the fact that, generally, a linear interpolation on real part and imaginary part doesn't result in a linear interpolation in amplitude and phase and vice versa.
The principle of the non-equidistant interpolation methods is shown in Fig. 97.

## a) Non-equidistant 'Constant Interval' interpolation method


b) Non-equidistant linear interpolation method


Figure 97. The two non-equidistant interpolation methods. In case of Constant Interval interpolation (upper part a)), each data point at coordinate $x_{i}$ defines a constant value for the interval $\left[x_{i}, x_{i+1}\left[\right.\right.$. The value $x^{*}$ marks the upper limit of the last coordinate interval.
The coordinate extent (colored in light green) is identical to that coordinate range where interpolation is possible. Values outside the coordinate extent (i.e. lying in the range colored in pale violet) are accessible via extrapolation (Sec. 13.3). In this example, a Constant with Value extrapolation is shown, using a constant value of $y_{e}$. Please note that $y_{e}$ is used for the linear interpolation in the interval $\left[x_{N}, x^{*}[\right.$ as well (lower part b)).

### 13.2.2 Interpolation Methods for Equidistant Data

From the interpolation methods explained in detail in Sec. 131.4, for performance reasons only the following can be used for the view of data arrays:

- Nearest Neighbor Interpolation
- Linear (Amplitude/Phase): Only for complex-valued data. ${ }^{1}$
- Linear (Real/Imaginary Part)
- Cubic 4 Point
- Cubic 6 Point
- Cubic 8 Point
- Truncated Sinc

The appropriate interpolation method has to be chosen according to the physical meaning of the data which

[^4]shall be interpolated, and according to the acceptable computational effort. It can be changed for example with the manipulation explained in Sec. 24.4.

### 13.3 Extrapolation

In certain circumstances, it is possible that a Data Array has to deliver values outside its coordinate range (aka. coordinate extent).
The following extrapolation modes are available (for equidistant as well as non-equidistant data):

- Equal to the Nearest Border Data Point: A constant extrapolation of the outmost data points is done.
- Zero: All outlying points are considered to be of value 0 .
- Constant with Value: All outlying points are considered to be of a value to be specified by the user.
- Periodically Continued: The whole data of the array are periodically continued, using a period of the array's 'coordinate extent'.


### 13.4 Import of Data Arrays

For a variety of equidistantly sampled data an import into VirtualLab Fusion is possible. This data will be converted into a Data Array which can be used for many different purposes then. This kind of import is described in Sec. 121.2.

### 13.5 Data Array View

There are three types of Data Arrays, each having a different view.

| TYPE | DESCRIPTION |
| :--- | :--- |
| Data Array 1D | Data are distributed over one-dimensional coordinates. From this data, inter- <br> polation methods can create a continuous function. |
| Data Array 2D | Data are distributed over a two-dimensional grid. From this data, interpolation <br> methods can create a continuous function. |
| Gridless Data Array | The data are given at arbitrary positions in a two-dimensional plane. Either <br> the data are shown non-interpolated which results in a dot diagram. If mesh <br> data are available, a linear interpolation inside the mesh triangles can be used <br> as well. |
|  |  |

The document window of a Data Array consists of three panels: the Diagram panel ( $\hookrightarrow$ Sec. 13.5.1), the Table panel ( $\hookrightarrow$ Sec. 13.5.2), and the Value at $(x, y)(\hookrightarrow$ Sec. 13.5.3) panel. The latter is not available for Gridless Data Arrays.

### 13.5.1 Diagram Panel

The Diagram panel contains a diagram that visualizes the contained data. There are different views for Data Arrays 1D, Data Arrays 2D, and Gridless Data Arrays, respectively, see Fig. 98 to Fig. 101.
These views allow you to

- specify which subset is to be shown ( $\hookrightarrow$ Sec. 13.5.1.1)
- set the shown field quantity ( $\hookrightarrow$ Sec. 11.1)
- switch between interpolated and non-interpolated view ( $\hookrightarrow$ Sec. 11.2.1)
- set the scaling mode ( $\hookrightarrow$ Sec. 11.2.5)
- use markers and selections ( $\hookrightarrow$ Sec. 11.3)
- zoom into the view ( $\hookrightarrow$ Sec. 11.4)
- change its aspect ratio ( $\leftrightarrows$ Sec. 11.5) and
- copy the view to clipboard ( $\hookrightarrow$ Sec. 11.6) .

In case of Data Arrays with more than one subset, the ribbon button View > 执 Equalize Scaling switches the scaling mode for the current Field Quantity to User-Defined Scaling ( $\hookrightarrow$ Sec. 11.2.5) and copies the value range of the currently shown subset to all other subsets.
Furthermore the appearance of the diagrams can be adjusted in the following ways via the View tab of the Property Browser.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Font Size of Axis Labels | The size of the axis labels and tick labels in points. |
| Font Size of Title | The size of the title in points. |
| Format | The format for the label and the tick values of the respective axis can be <br> specified here as Engineering where a prefix in front of the unit is used, or as <br> Scientific where an exponential description is used, or as Standard where SI <br> units and thus no prefixes are used. |

For the settings which are specific for 1D Data Arrays see Sec. 13.5.1.2, for 2D Data Arrays see Sec. 13.5.1.3 and for Gridless Data Arrays see Sec. 13.5.1.4.


Figure 98. Example for a Cartesian diagram view of a 1D data array.


Figure 99. Example for a polar diagram view of a 1D data array.


Figure 100. Example for the diagram view of a 2D data array in 2D mode, including a profile line ( $\hookrightarrow$ Sec. (b)).


Figure 101. Example for the diagram view of a gridless data array.

### 13.5.1.1 Subset Selection

## Availability

For data arrays with more than one subset and disabled Multigraph Mode (in case of 1D data)

## Accessible:

- Ribbon: View > Subset Selection group (see below)
- Property browser: View > Subset Index
- Context menu: Data Subset Index
- Shortcuts: Page Up and Page Down

In the ribbon you can go through all subsets of a data array with the control shown in Fig. 102, either by using
the arrow buttons or by entering the subset index directly．Below this control the description of the current subset is given．

```
4 2 % of 3 
```

Figure 102．The controls to select a specific subset in the ribbon．

## 13．5．1．2 Specific View Features for 1D Data Arrays

## （a）Cartesian 1D Diagram in Singlegraph Mode

The ribbon item View＞Multigraph Mode allows to switch between the display of one single subset and multiple subsets $\hookrightarrow$ Sec．（b）if more than one subset is given．
View $>$ 虚 Axes Options＞Descending Coordinates（x－Axis）allows to show an inverted coordinate axis．
The item View＞掊，Axes Options＞Transposed View will swap the directions of the independent（ $x$－）and the dependent（ y －）axis．
The ribbon item View＞埧 ，Axes Options＞Logarithmic Scaling（x－axis）toggles between a logarithmic and a linear scaling of the coordinate axis if the complete coordinate range is positive．
View $>$ 虞 Axes Options＞Logarithmic Scaling（y－axis）is a switch between a logarithmic and a linear scaling of the $y$－axis if the values to be displayed are completely positive．
The following specific parameters can be set via the View tab of the Property Browser：

| ITEM | DESCRIPTION |
| :---: | :---: |
| General＞Show Polar Dia－ gram | Only if the data array represents an angular dependency． <br> Switches between a polar diagram view（ $\hookrightarrow$ Sec．（c））and a Cartesian diagram view． |
| $\begin{aligned} & \text { General > Transposed } \\ & \text { View } \end{aligned}$ | If True，the vertical axis and the horizontal axis of the diagram will be trans－ posed．The independent variable will then be shown in the vertical direction． |
| General＞Legend Visible | Only available if at least one undefined value in data array． <br> The visibility of the legend for the color which visualizes undefined values can be set here． |
| Lines and Symbols＞Line Color | Color of line which connects the displayed data points．If set to Transparent， the line will not be shown． |
| Lines and Symbols＞Line Thickness | Thickness of line which connects the displayed data points．Has to be a pos－ itive integer． |
| Lines and Symbols＞ Symbol Color | Only available if Symbol Shape is not No Symbol． Color of the symbols which mark the data points． |
| Lines and Symbols＞ Symbol Scaling Factor | Only available if Symbol Shape is not No Symbol． <br> The size of the symbols（except Small Dot）can be scaled using this factor． |
| Lines and Symbols＞ Symbol Shape | Shape of the symbols which mark the data points．If set to No Symbol，sym－ bols will be switched off． |
| Lines and Symbols＞Use Smoothed Graphics | If activated，the graphics will be smoothed．Usually，this may improve the diagram．But if a stepped line is shown，deactivating this property may yield a better result．Important：This smoothing is done on pixel level．This pixel smoothing is not to be confused with the smoothing interpolation methods described in Sec．11．2．2！ |


| Lines and Symbols > Alignment of Undefined Color Legend | Only available if at least one undefined value in data array. Allows to set the position of the legend for the color which visualizes undefined values within the diagram. |
| :---: | :---: |
| Lines and Symbols > Color for Undefined Value | Only available if at least one undefined value in data array. Color to be used for visualizing undefined values. |
| Lines and Symbols > Opacity for Undefined Value | OnLy available if at least one undefined value in data array. The opacity of the visualization of undefined values can be set here. |
| Multigraph Options Multigraph Mode | Only available if more than one subset given in the data array. <br> Via the Multigraph Mode it is possible to switch between the display of one single subset and multiple subsets. $\leftrightarrows$ Sec. (b) |
| X-Axis > Descending Coordinates | If selected, the diagram will be shown with descending coordinates. Otherwise the coordinates will be ascending. |
| X-Axis > Logarithm Scaling | If set to True, the x -axis scaling will be logarithmic instead of linear. |
| X-Axis > Minimum Number of Ticks | A guiding value for the automatic tick labeling of the $x$-axis can be set here. The axis will have at least the number of ticks which is set by this value. |
| Y-Axis > Description | If Is Description User Defined is set to True, a user-defined axis label can be set here. Otherwise the currently shown subset's description is displayed here. |
| Y-Axis > Is Description User Defined | If True, a user defined label can be set instead of showing a label based on the respective subset description. |
| Y-Axis > Logarithmic Scaling | If set to True, the $y$-axis scaling will be logarithmic instead of linear. |
| Y-Axis > Minimum Number of $y$-Axis Ticks | A guiding value for the automatic tick labeling of the y -axis can be set here. The axis will have at least the number of ticks which is set by this value. |
| Y-Axis > Read Labels from Inside | The orientation of the $y$-axis labels can be specified here. |

## (b) Cartesian 1D Diagram in Multigraph Mode

## Availability

For data arrays with more than one subset

## Accessible:

- Ribbon: View > Multigraph Mode
- Property browser: View > Multigraph Options > Multigraph Mode

The Multigraph Mode allows to display more than one subset at once in the diagram of a 1D Data Array. Fig. 103 shows an example.


Figure 103. Example for the Multigraph Mode.


Figure 104. Dialog for configuring the Multigraph Mode.

Via View > 萻 Subset Settings, the Multigraph Mode can be configured. The dialog shown in Fig. 104 provides the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Graphs＞Subset \＃ | The index of the subset represented by that table row． This column is read－only． |
| Graphs＞Description | The description of the subset． <br> This column is read－only．（Sec．24．5．1 shows how to edit the description．） |
| ```Graphs > Physical Prop- erty``` | The physical property of the subset． <br> This column is read－only．（Sec．24．5．1 shows how to edit the physical prop－ erty．） |
| Graphs＞Ordinate | This option allows to choose whether the curve shall be associated to the Left－Hand y－axis，the Right－Hand y－axis or shall be＜Not Displayed＞at all． <br> Important：All subsets to be displayed with respect to the same axis has to have the same physical property！Furthermore，there has to be one subset for the left－hand $y$－axis at least． <br> If the button is pressed，the synchronization of the ordinate is enforced for all subsets． |
| Graphs＞Color | This allows to select a color for the curve which represents the subset．Ini－ tially，it is identical to the color of the associated $y$－axis in order to depict the association． <br> If the button is pressed，the synchronization of the color is enforced for all subsets． |
| Graphs＞Symbol | A symbol for displaying the data points can be selected here． <br> If the button is pressed，the synchronization of the symbol is enforced for all subsets． |
| Graphs＞Dash Pattern | This allows to select a dash pattern for the curve which represents the subset． If the ${ }^{2}$ button is pressed，the synchronization of the dash pattern is enforced for all subsets． |
| Ordinates＞Left／Right Axis＞Rename？ | If this button is pressed，a user－defined Description can be set for the respec－ tive ordinate． |
| Legend＞Visible | The visibility of the graphs legend can be set here． |
| Legend＞Alignment | Available if the legend is visible． <br> The position of the legend inside the diagram can be set． |
| Legend＞Opacity | Available if the legend is visible． <br> The legend＇s opacity in the range between 0 and $100 \%$ ． |

The ribbon item View＞纯 Show Legend allows to toggle the visibility of the multigraph legend．In case of undefined values in the diagram，the visibility of the legend for the color which visualizes undefined values is toggled as well．
View＞管 Axes Options＞Descending Coordinates（x－Axis）allows to show an inverted coordinate axis．
The item View $>$ 虙，Axes Options $>$ Transposed View will swap the directions of the independent（ $x$－）and the dependent（ $y$－）axis if no right－hand axis is used．
The ribbon item View＞掊 Axes Options＞Logarithmic Scaling（x－axis）toggles between a logarithmic and a linear scaling of the coordinate axis if the complete coordinate range is positive．
View＞㨟 Axes Options＞Logarithmic Scaling（Left／Right y－axis）is a switch between a logarithmic and a linear scaling of the left－hand（or right－hand）y－axis if the values to be displayed are completely positive． In multigraph mode，there are several specific settings accessible via the View tab of the Property Browser：

| ITEM | DESCRIPTION |
| :--- | :--- |
| General > Show Polar Dia- | OnLY IF THE DATA ARRAY REPRESENTS AN ANGULAR DEPENDENCY. |
| gram | Switches between a polar diagram view ( $\hookrightarrow$ Sec. (d)) and a Cartesian diagram |
| view. |  |


| Y－Axis Left／Right－Hand＞ Is Description User De－ fined | If True，a user defined label can be set instead of showing a label based on the respective subset description． |
| :---: | :---: |
| Y－Axis Left／Right－Hand＞ Color | The color of the left－hand or right－hand y－axis． |
| Y－Axis Left／Right－Hand＞ Logarithmic Scaling | If set to True，the y －axis scaling will be logarithmic instead of linear． |
| Y－Axis Left／Right－Hand＞ Minimum Number of y－Axis Ticks | A guiding value for the automatic tick labeling of the $y$－axes can be set here． The axes will have at least the number of ticks which is set by this value． Important：Changing the value for one axis，that of the other $y$－axis will be changed as well． |
| Y－Axis Left／Right－Hand＞ Read Labels from Inside | The orientation of the axis labels can be specified here． |

## （c）Polar Diagram in Singlegraph Mode

```
Availability
For data arrays with angular dependency
Accessible:
－Ribbon：View＞墎 Axes Options＞Polar Diagram
－Property browser：View＞General＞Show Polar Diagram
```

The ribbon item View＞㗲 Axes Options＞Polar Diagram allows to switch between the display of a polar diagram and a Cartesian diagram in case an angular dependency is shown．
View $>$ 噟 Axes Options＞Logarithmic Scaling（Radial Axis）toggles between a logarithmic and a linear scaling of the radial axis if the values to be displayed are completely positive．
The following specific parameters can be set via the View tab of the Property Browser：

| ITEM | DESCRIPTION |
| :--- | :--- |
| General＞Show Polar Dia－ <br> gram | Switches between a Cartesian diagram view（ $\lrcorner$ Sec．（a））and a polar diagram <br> view． |
| General＞Orientation of <br> Half Circle | The orientation of the half circle（Top，Bottom，Left，Right）can be set here． <br> General＞Legend Visible |
| ONLY AVAILABLE IF AT LEAST ONE UNDEFINED VALUE IN DATA ARRAY． <br> The visibility of the legend for the color which visualizes undefined values can <br> be set here． |  |
| Azimuthal Axis＞Number <br> of Grid Lines／Quadrant | How many angular tick lines shall be visible per quadrant？ |
| Azimuthal Axis＞Orienta－ | The orientation（Horizontal，Radial，Tangential）of the angular labels can be |
| tion of Angular Labels | set here． |
| Azimuthal Axis＞Show | If True，the angular labels are shown in radian，otherwise in degrees． |
| Angles in Radian |  |


| Lines and Symbols > Line Color | Color of line which connects the displayed data points. If set to Transparent, the line will not be shown. |
| :---: | :---: |
| Lines and Symbols > Line Thickness | Thickness of line which connects the displayed data points. Has to be a positive integer. |
| Lines and Symbols > Symbol Color | Only available if Symbol Shape is not No Symbol. Color of the symbols which mark the data points. |
| Lines and Symbols > Symbol Scaling Factor | Only available if Symbol Shape is not No Symbol. <br> The size of the symbols (except Small Dot) can be scaled using this factor. |
| Lines and Symbols > Symbol Shape | Shape of the symbols which mark the data points. If set to No Symbol, symbols will be switched off. |
| Lines and Symbols > Use Smoothed Graphics | If activated, the graphics will be smoothed. Usually, this may improve the diagram. But if a stepped line is shown, deactivating this property may yield a better result. Important: This smoothing is done on pixel level. This pixel smoothing is not to be confused with the smoothing interpolation methods described in Sec. 11.2.2! |
| Lines and Symbols > Alignment of Undefined Color Legend | Only available if at least one undefined value in data array. <br> The position / alignment of the legend for the color to be used for visualizing undefined values. |
| Lines and Symbols > Color for Undefined Value | Only available if at least one undefined value in data array. Color to be used for visualizing undefined values. |
| Lines and Symbols > Opacity for Undefined Value | Only available if at least one undefined value in data array. The opacity of the visualization of undefined values can be set here. |
| Multigraph Options > Multigraph Mode | Only available if more than one subset given in the data array. <br> Via the Multigraph Mode it is possible to switch between the display of one single subset and multiple subsets. $\hookrightarrow$ Sec. (d) |
| Radial Axis > Description | If Is Description User Defined is set to True, a user-defined axis label can be set here. Otherwise the currently shown subset's description is displayed here. |
| Radial Axis > Is Description User Defined | If True, a user defined label can be set instead of showing a label based on the respective subset description. |
| Radial Axis > Logarithmic Scaling | If set to True, the radial axis scaling will be logarithmic instead of linear. |
| Radial Axis > Minimum Number of Radial Axis Ticks | A guiding value for the automatic tick labeling of the radial axis can be set here. The axis will have at least the number of ticks which is set by this value. |

## (d) Polar Diagram in Multigraph Mode

## Availability

For data arrays with angular dependency and more than one subset

## Accessible：

- Ribbon：View＞迬 Multigraph Mode
- Ribbon：View＞蠚 Axes Options＞Polar Diagram
－Property browser：View＞Multigraph Options＞Multigraph Mode
－Property browser：View＞General＞Show Polar Diagram

The Multigraph Mode allows to display more than one subset at once in the diagram of a 1D Data Array．Fig． 105 shows an example．


Figure 105．Example for the Multigraph Mode of a polar diagram．


Figure 106．Dialog for configuring the Multigraph Mode for a polar diagram．
Via View＞盆 Subset Settings，the Multigraph Mode can be configured．The dialog shown in Fig． 106 provides the following settings：

| ITEM | DESCRIPTION |
| :---: | :---: |
| Graphs＞Subset \＃ | The index of the subset represented by that table row． This column is read－only． |
| Graphs＞Description | The description of the subset． <br> This column is read－only．（Sec．24．5．1 shows how to edit the description．） |
| ```Graphs > Physical Prop- erty``` | The physical property of the subset． <br> This column is read－only．（Sec．24．5．1 shows how to edit the physical prop－ erty．） |
| Graphs＞Ordinate | This option allows to choose whether the curve shall be associated to the Primary，the Secondary，or the Tertiary radial axis or whether the subset shall be＜Not Displayed＞at all． <br> Important：All subsets to be displayed with respect to the same axis has to have the same physical property！Furthermore，there has to be one subset for the primary radial axis at least．If the tertiary axis is supposed to be used， at least one subset has to be associated with the secondary axis，additionally． If the button is pressed，the synchronization of the ordinate is enforced for all subsets． |
| Graphs＞Color | This allows to select a color for the curve which represents the subset．Initially， it is identical to the color of the associated radial axis in order to depict the association． <br> If the button is pressed，the synchronization of the color is enforced for all subsets． |
| Graphs＞Symbol | A symbol for displaying the data points can be selected here． <br> If the button is pressed，the synchronization of the symbol is enforced for all subsets． |
| Graphs＞Dash Pattern | This allows to select a dash pattern for the curve which represents the subset． If the ${ }^{2}$ button is pressed，the synchronization of the dash pattern is enforced for all subsets． |
| Ordinates＞Primary／Sec－ ondary／Tertiary Axis＞ Rename？ | If this button is pressed，a user－defined Description can be set for the respec－ tive ordinate． |
| Legend＞Visible | The visibility of the graphs legend can be set here． |
| Legend＞Alignment | Available if the legend is visible． <br> The position of the legend inside the diagram can be set． |
| Legend＞Opacity | Available if the legend is visible． <br> The legend＇s opacity in the range between 0 and $100 \%$ ． |

The ribbon item View＞剖 Show Legend allows to toggle the visibility of the multigraph legend．In case of undefined values in the diagram，the visibility of legend for the color which visualizes undefined values is toggled as well．
The ribbon item View＞㩰 Axes Options＞Polar Diagram allows to switch between the display of a polar diagram and a Cartesian diagram in case an angular dependency is shown．
View $>$ 費 Axes Options＞Logarithmic Scaling（Primary／Secondary／Tertiary Radial Axis）toggles between a logarithmic and a linear scaling of a certain radial axis if the values to be displayed are completely positive （and if the respective axis is in use，of course）．

In multigraph mode, there are several specific settings accessible via the View tab of the Property Browser:

| ITEM | DESCRIPTION |
| :---: | :---: |
| General > Show Polar Diagram | Switches between a Cartesian diagram view ( $\hookrightarrow$ Sec. (b)) and a polar diagram view. |
| General > Orientation of Half Circle | The orientation of the half circle (Top, Bottom, Left, Right) can |
| General > Legend Visible | The visibility of the multigraph legend can be toggled here. Furthermore, in case of undefined values in the diagram, the visibility of the legend for the color which visualizes undefined values is toggled as well. |
| Azimuthal Axis > Number of Grid Lines/Quadrant | How many angular tick lines shall be visible per quadrant? |
| Azimuthal Axis > Orientation of Angular Labels | The orientation (Horizontal, Radial, Tangential) of the angular labels can be set here. |
| Azimuthal Axis > Show Angles in Radian | If True, the angular labels are shown in radian, otherwise in degrees. |
| Lines and Symbols > Line Thickness | Thickness of line which connects the displayed data points. Has to be a positive integer. |
| Lines and Symbols > Symbol Scaling Factor | Only available if Symbol Shape is not No Symbol. <br> The size of the symbols (except Small Dot) can be scaled using this factor. |
| Lines and Symbols > Use Smoothed Graphics | If activated, the graphics will be smoothed. Usually, this may improve the diagram. But if a stepped line is shown, deactivating this property may yield a better result. Important: This smoothing is done on pixel level. This pixel smoothing is not to be confused with the smoothing interpolation methods described in Sec. 11.2.2! |
| Lines and Symbols > Alignment of Undefined Color Legend | Only available if at least one undefined value in data array. The position / alignment of the legend for the color to be used for visualizing undefined values. |
| Lines and Symbols > Color for Undefined Value | Only available if at least one undefined value in data array. Color to be used for visualizing undefined values. |
| Lines and Symbols > Opacity for Undefined Value | Only available if at least one undefined value in data array. <br> The opacity of the visualization of undefined values can be set here. |
| Multigraph Options > <br> Multigraph Mode | Only available if more than one subset given in the data array. Via the Multigraph Mode it is possible to switch between the display of multiple subsets and one single subset. $\hookrightarrow$ Sec. (c) |
| Multigraph Options > Legend Alignment | Only available if the legend is visible. <br> Allows to set the alignment of the multigraph legend. |
| ```Opacity``` | Only available if the legend is visible. <br> The multigraph legend's opacity in the range between 0 and $100 \%$. |
| Radial Axis (Primary / Secondary / Tertiary) > Description | If Is Description User Defined is set to True, a user-defined axis label can be set here. Otherwise the currently shown subset's description is displayed here. |

Radial Axis (Primary / Sec- If True, a user defined label can be set instead of showing a label based on ondary / Tertiary) > Is De- the respective subset description.
scription User Defined
Radial Axis (Primary / Sec- The color of the respective radial axis.
ondary / Tertiary) > Color
Radial Axis (Primary / Sec- If set to True, the respective radial axis scaling will be logarithmic instead of ondary / Tertiary) > Loga- linear.
rithmic Scaling
Radial Axis (Primary / Sec- A guiding value for the automatic tick labeling of the radial axes can be set ondary / Tertiary) > Min- here. The axes will have at least the number of ticks which is set by this value. imum Number of Radial Important: Changing the value for one axis, that of the other radial axes will Axis Ticks be changed as well.

### 13.5.1.3 Specific View Features for 2D Data Arrays

The features described in this section are available for 2D Data Arrays only.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Color Table | $\hookrightarrow$ Sec. 11.2.4 |
| Color for Undefined Val- <br> ues | The color to be used for visualizing undefined values. (Can be set via Property <br> Browser only.) |
| 3D Mode | $\hookrightarrow$ Sec. (a) |
| Show Legend | Allows to switch off the color legend. |
| Show 1D Profile | Shows or hides the 1D profile which shows a section along the line marker <br> below the 2D diagram. $\hookrightarrow$ Sec. (b) |

(a) 3D Mode

## Availability

## Accessible:

- Ribbon: View > Diagram in 3D Mode
- Property browser: View > 3D Mode

Visualization of a 2D data array can be done either in 2D mode (as shown in Fig. 100) or in 3D mode (as in Fig. 107).


Figure 107. Example for the diagram view of a 2D data array in 3D mode.
The 3D mode offers some specific mouse interactions:

| MOUSE (+ KEYBOARD) | VIEW OPERATION |
| :--- | :--- |
| ACTION |  |
| Left button + move | Free rotation |
| $\mathrm{X} / \mathrm{Y} / / \mathrm{Z}$ key + left button + | Constrained rotation |
| move |  |
| Shift + left button + move | Translation |
| Ctrl + left button + move | Zoom |
| up/down |  |

You can adjust the view in the property browser (View > 3D Options group):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Camera Direction | Sets the perspective (i.e. the direction) of the view. |
| Camera Distance Parame- <br> ter | Decimal number that describes the camera distance in an arbitrary unit. It <br> affects the spatial distortion of the view and has to be larger than 1.0. |
| Camera <br> X/YIZ | Rotation <br> Draw Contours |
| Camera Direction |  |
| ONLY AVAILABLE IF THE CURRENTLY SET COLOR TABLE IS STEPPED, I. E. IF IT <br> ISN'T INTERPOLATED. <br> If set to True, contour lines are drawn at the borders between two different <br> colors. |  |
| Font Size Factor | A value for rescaling the labels inside the 3D view. |
| Show Data While Interact- | If set to True, the diagram will be visible during mouse interaction. |
| Show Mesh | If set to True, a mesh grid will be displayed instead of colors. |


| Zone Method | The type of drawing the zones. Possible values are Contours, which looks <br> nice but is slow, and Cells, which doesn't look as nice, but is faster. |
| :--- | :--- |
| Zoom Factor | Factor that determines the zoom of the view. |

(b) Profile Lines Only enabled if the Line Marker is visible.

If a line marker is visible in the 2D diagram, by default the data along the selected line is shown as a profile line in a 1D diagram below the 2D diagram. This 1D diagram shares many of the features of a normal 1D diagram ( $\hookrightarrow$ Sec. 13.5.1.2).
Please note that the starting coordinate of the 1D diagram corresponds to the line coordinates in the 2D diagram only if the line is oriented exactly vertically or horizontally (which can easily be achieved holding Ctrl pressed while dragging the mouse). In case of a sloping line, no reasonable starting coordinate can be extracted, so the 1D diagram will start at the value 0.
If point marker and rectangle or ellipse marker intersect with the profile line, they are also shown there. Vice versa, if the point marker is moved within the profile line, this change is also shown in the 2D diagram.
The separator line between 1D diagram and 2D diagram can be dragged with the mouse to change the relative sizes of these diagrams. This can also be done via the Property browser (View > General > Height of 1D Profile). Or you can disable the profile completely there (View > Selection (Line) > Show 1D Profile).

## (c) Polarization Ellipses

## Availability

Available only for Electric Fields or Electromagnetic Fields

## Accessible:

- Ribbon: View > Show xy-/yz-/zx-Ellipses

The ribbon menu item View > Graphics Add-ons $\gg \circ$ Show xy-/yz-/zx-Ellipses is only available if a vectorial component of an electric field is currently shown and if the graphics add-on for visualizing polarization ellipses is available for the corresponding subset. It allows to toggle the visibility of the ellipses for this vectorial field component.
The corresponding configuration button allows to configure the view settings of the currently shown polarization ellipses via the dialog described in Sec. 11.7.3.

### 13.5.1.4 Specific View Features for Gridless Data Arrays

| ITEM | DESCRIPTION |
| :---: | :---: |
| Color Table | Allows to set the color table to use. $\hookrightarrow$ Sec. 11.2.4 |
| Dot Size | Not available for views of type 'Distribution of Pupils With Values'. The size of the dots. Can be set either via the ribbon item View > Dot Size or the View tab of the property browser. |
| Background Color | Usually the dots do not fill the whole diagram region so the background can be seen. By clicking on View > Background Color, either a predefined color can be chosen or a new color can be defined via More Colors. The entry Background Color in the View tab of the property browser has more predefined colors. There you can also directly enter the name or the RGB values (separated by comma and space) of the desired color. |
| Show Triangles | Available only if mesh data are stored with the data array. <br> If checked, the triangles of the mesh are shown as described in Sec. 11.2.3. |
| Pupils Rendering | Available only for views of type 'Distribution of Pupils With Values'. Allows to configure the view settings for the pupils shown as described below in Sec. (a). |

(a) Configuration of a Distribution of Pupils With Values


Figure 108. Dialog for configuring a Distribution of Pupils With Values.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Color Table | The color table used for mapping the pupil's values to colors |
| Filling Opacity | Opacity of the filling colors. $0 \%$ means complete transparency, $100 \%$ means <br> no transparency at all. |
| Draw Border | If checked, the pupil's borders are drawn. |
| Border Color | VISIBLE ONLY IF DRAW BORDER IS SELECTED. |
|  | The color of the borders. |
| Border Width | VISIBLE ONLY IF DRAW BORDER IS SELECTED. <br>  <br>  |

### 13.5.2 Table Panel

The Table panel provides a table showing the data points for each coordinate or pair of coordinates.

There is an upper limit for the number of table cells that are displayed. If this threshold which can be set via the Global Options dialog ( $\hookrightarrow$ Sec. 6.7) is exceeded, no table will be displayed for performance reasons. The display of the table can be enforced despite the bad performance by pushing the button Show Table Anyway, which will be visible in this case.

| Diagram Table Valve at $(x, y)$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| x | Component Ex |  | Component Ey |  | - |
|  | (Amplitude) | (Phase) | (Amplitude) | (Phase) |  |
| -483.707 $\mu \mathrm{m}$ | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad |  |
| -429.961 $\mathrm{\mu m}$ | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad |  |
| -376. 216 um | 1.13236E-07 V/m | -0.047242 rad | $6.53771 \mathrm{E}-08 \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| -322.471 $\mu \mathrm{m}$ | $17.5424 \mu \mathrm{~V} / \mathrm{m}$ | -0.047242 rad | $10.1281 \mu \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| -268.726 $\mu \mathrm{m}$ | $616.528 \mu \mathrm{~V} / \mathrm{m}$ | -0.047242 rad | $355.953 \mu \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| -214.981 $\mathrm{\mu m}$ | $8.62026 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $4.97691 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| -161.236 um | $65.5015 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $37.8173 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| -107.49 $\mathrm{\mu m}$ | $272.914 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $157.567 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| -53.7452 $\mu \mathrm{m}$ | $646.446 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $373.226 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad | E |
| 0m | $866.025 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $500 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| $53.7452 \mu \mathrm{~m}$ | $646.446 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $373.226 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| $107.49 \mathrm{\mu m}$ | $272.914 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $157.567 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| 161.236 um | $65.5015 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $37.8173 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| $214.981 \mu \mathrm{~m}$ | $8.62026 \mathrm{mV} / \mathrm{m}$ | -0.047242 rad | $4.97691 \mathrm{mV} / \mathrm{m}$ | 3.09435 rad |  |
| $268.726 \mu \mathrm{~m}$ | $616.528 \mu \mathrm{~V} / \mathrm{m}$ | -0.047242 rad | $355.953 \mu \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| 322.471 mm | $17.5424 \mu \mathrm{~V} / \mathrm{m}$ | -0.047242 rad | $10.1281 \mu \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| 376.216 um | 1.13236E-07 V/m | -0.047242 rad | $6.53771 \mathrm{E}-08 \mathrm{~V} / \mathrm{m}$ | 3.09435 rad |  |
| $429.961 \mu \mathrm{~m}$ | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad |  |
| $483.707 \mathrm{\mu m}$ | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad | $0 \mathrm{~V} / \mathrm{m}$ | 0 rad | - |

Figure 109. Example for the table view of a 1D data array.


Figure 110. Example for the table view of a 2D data array.

The context menu in the table panel contains the following entries:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Edit Selected Data Point... | Opens a dialog for editing the value(s) of the data point which is associated <br> with the currently selected cell(s) ( $\hookrightarrow$ Sec. 24.16). |
| Mark Selected Range in <br> Diagram | ONLY AVAILABLE FOR ONE-DIMENSIONAL DATA. <br> If a range of rows is selected within the table, this menu item will mark the <br> corresponding coordinate range in the diagram. |
| Mark Selected Point in Di- | ONLY AVAILABLE FOR ONE-DIMENSIONAL DATA. <br> If a single row is selected within the table, this menu item will mark the corre- <br> sponding coordinate in the diagram. |
| Copy Selection | This will copy the content of the selected table cells to the clipboard. |

The View panel of the property browser has the following entries for the table panel:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Field Quantity | ONLY ENABLED FOR COMPLEX DATA ARRAYS AND IF THE OPTION SHOW Two <br> COMPLEX PARTS IS FALSE. <br> The field quantity ( $\hookrightarrow$ Sec. 11.1) to show in the table. |
| Show Two Complex Parts | ONLY ENABLED FOR COMPLEX DATA ARRAYS. <br> If True, the table shows both complex parts for each data point. Otherwise, <br> only one field quantity is shown at a time. |
| Amplitude Phase Mode | OnLY ENABLED FOR compLEX DATA ARRAYs AND IF THE OPTION SHOw Two <br> CompLEX PARTS IS TRUE. <br> Here can be set whether the table shall show amplitude and phase (True) or <br> real and imaginary part (False). |
| Number of Digits | The number of significant digits to be shown for the entries in the table. |
| Show Units | With this option you can show the entries in the table without physical units. <br> In this way copied entries can be more easily processed in external programs <br> like e.g. spreadsheet software. |

### 13.5.3 Value at $(x, y)$ Panel

If the value (or the values of more than one subset) at one certain position has (have) to be identified, this can be done via this Value at ( $x, y$ ) panel. Here, simply the coordinates have to be entered, than the value(s) is (are) displayed as shown in Fig. 111 for 1D and Fig. 112 for 2D data. If a point marker ( $\hookrightarrow$ Sec. 11.3) is visible in the View Panel, its position will be filled in here automatically.


Figure 111. Example for the view for a value at a position $(x, y)$ of a 1D data array.


Figure 112. Example for the view for a value at a position $(x, y)$ of a 2D data array.

| Second Coordinate | ONLY AVAILABLE FOR TWO-DIMENSIONAL DATA. <br> Second coordinate to get the value(s) for. |
| :--- | :--- |
| Show Amplitude and <br> Phase of Complex Values | If checked, complex data will be displayed as amplitude and phase instead <br> of real part and imaginary part. |
| Use Own Interpolation | ONLY AVAILABLE IF THE INTERPOLATION METHOD IS NOT SINC (Fourier TRANS- <br> FORM). <br> Method |
| If checked, the interpolation method of the data array will be used in order <br> to calculate the value(s) at a position that lies between adjacent data points. <br> Otherwise, nearest neighbor interpolation (or constant interval interpolation, <br> in case of non equidistant data) will be used. <br> Opens a dialog for editing the value(s) of the currently shown data point <br> ( $\leftrightarrows$ Sec. 24.16). |  |

## 14 Chromatic Fields Set View

The Chromatic Fields Set View can display the squared amplitude distribution of one- or two-dimensional fields. This view is also used as preview in the Light Sources Catalog, in particular the same context menu is used there. However the preview uses a special toolbar is show which is described in Sec. 14.4.
There are two settings which strongly influence the available view settings: the wavelengths mode ( $\hookrightarrow$ Sec. 14.1) and the color mode ( $\hookrightarrow$ Sec. 14.2).
Interpolated view ( $\hookrightarrow$ Sec. 11.2.1), markers and selections ( $\hookrightarrow$ Sec. 11.3), zoom ( $\hookrightarrow$ Sec. 11.4), aspect ratio ( $\hookrightarrow$ Sec. 11.5) , and Copy View To Clipboard ( $\hookrightarrow$ Sec. 11.6) are available independently from these modes.

### 14.1 Wavelength Selection

## Availability

Accessible:

- Ribbon: View > Wavelength Selection group
- Property browser: View > Summation Mode and View > Wavelength Index
- Context menu: Wavelengths Mode and Wavelength Index

There are two Wavelength Modes available:

## MODE

DESCRIPTION
Summed Wavelengths
Adds the values of all wavelengths to one field.
${ }^{[ }$[a Single Wavelengths Only one wavelength is shown at a time. In the ribbon you can go through Mode all wavelengths of a Chromatic Fields Set with the control shown in Fig. 113, either by using the arrow buttons or by entering the wavelength index directly. Below this control the currently selected wavelength is given.

## 42

Figure 113. The controls to select a wavelength index in the ribbon.

### 14.2 Color Mode

## Availability

Only for two-dimensional Chromatic Fields Sets
Accessible:

- Ribbon: View > Color Mode menu
- Property browser: View > Color Mode
- Context menu: Color Mode

There are two Color Modes available:

| MODE | DESCRIPTION |
| :--- | :--- |
| False Color | The squared amplitudes are shown as data arrays. Thus this mode has the <br> same view functionality as for Numerical Data Arrays ( $\leftrightarrows$ Sec. 13.5). Adds the <br> values of all wavelengths to one field. |
| ONLY AVAILABLE IF AT LEAST ONE OF THE WAVELENGTHS IN THE CHROMATIC <br> FiELDS SET IS IN THE VISIBLE RANGE (360 - 830 NM). |  |
| Considers the field as an intensity distribution (which, in general, can be poly- <br> chromatic) and displays it as the human eye would perceive it. This mode <br> allows you to adjust its brightness ( $\leftrightarrows$ Sec. 11.2.6). Consequently, if a point <br> marker is shown the Selections tab of the property browser not only shows the <br> squared amplitude at its current position, but also the red-green-blue values. |  |

### 14.3 Maximum Lightness

## Availability

Only for two-dimensional Chromatic Fields Sets in Single Wavelength and Real Color mode

## Accessible:

- Ribbon: View > Maximum Lightness
- Property browser: View > Maximum Lightness
- Context menu: Maximum Lightness

If a chromatic fields set is displayed in Single Wavelength and Real Color mode, there are two lightness modes available: The Maximum Lightness may be switched ON or OFF.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Maximum Lightness | OnLY AVAILABLE IN SINGLE WAVELENGTH AND REAL COLOR MODE. |
|  | Toggles the usage of the Maximum Lightness mode. If the button is pressed, |
| all single wavelength views will be scaled to maximum lightness indepen- |  |
| dently. If it is not pressed, no maximum scaling is done which allows to com- |  |
| pare all single wavelengths views with each other. |  |

As an example, a chromatic fields set is shown in Fig. 114 (in Summed Wavelengths mode) and in Fig. 115 (in Single Wavelengths mode with and without Maximum Lightness activated).


Figure 114. Real Color view of a chromatic fields set with five different wavelengths in Summed Wavelengths mode.


Figure 115. All single wavelengths views of the chromatic fields set shown in Fig. 114. Left hand side: Deactivated Maximum Lightness allows comparison of the different wavelengths. Right hand side: Activated Maximum Lightness scales every wavelength view to its maximum which allows a better examination of faint regions.

### 14.4 Toolbar (For the Preview in the Light Sources Catalog)

| ITEM | DESCRIPTION |
| :---: | :---: |
| Color Mode | Switches the color mode, $\hookrightarrow$ Sec. 14.2. |
| Wavelength Mode | Switches the wavelengths mode, $\hookrightarrow$ Sec. 14.1. |
| Previous Wavelength Index | Only available in Single Wavelength Mode. Show the field with the next smaller wavelength. |
| Wavelength Index | Only available in Single Wavelength mode. <br> Show the field with the wavelength corresponding to the specified index. |
| Next Wavelength Index $\boldsymbol{\Theta}$ | Only available in Single Wavelength mode. Show the field with the next larger wavelength. |
| Separate Chromatic <br> Fields Set $Q$  | Shows the preview as separate Chromatic Fields Set which you can save or convert to a Numerical Data Array. |

## 15 Pulse and Field Component

For the display of pulses ( $\hookrightarrow$ Sec. 74.6.5), spectra ( $\hookrightarrow$ Sec. 53 ) and the results of the Extraction Tools ( $\hookrightarrow$ Sec. 23.2) a special document type Light Field Object is available which plots complex-valued field data versus wavelength, frequency, or time. The following 6 display variants are possible.

| DISPLAY VARIANT | DESCRIPTION |
| :--- | :--- |
| Field Component At One <br> Point | Plots field data versus an index or the wavelength. This results in a one- <br> dimensional diagram. |
| Pulse Component At One | Plots field data versus wavelength, frequency, or time. This results in a one- <br> dimensional diagram, Fig. 116 shows an example. Carrier wavelength, carrier <br> angular frequency, or time shift are stored as additional information. |
| Field Component At Line | Plots field data along a line versus an index. This results in a two-dimensional <br> diagram. |
| Pulse Component At Line | Plots field data along a line versus wavelength, frequency, or time. This <br> results in a two-dimensional diagram, Fig. 117 shows an example. Carrier <br> wavelength, carrier angular frequency, or time shift are stored as additional <br> information. |
| Field Component | Contains multiple subsets each storing two-dimensional field data at a certain <br> index. This results in a two-dimensional diagram. |
| Pulse Component | Contains multiple subsets each storing two-dimensional field data at a certain <br> wavelength, frequency, or time. This results in a two-dimensional diagram, <br> Fig. 118 shows an example. Carrier wavelength, carrier angular frequency, <br> or time shift are stored as additional information. |

All these document windows consist of three tab pages. Carrier wavelength, carrier angular frequency, or time shift are shown in an expandable information box ( $\hookrightarrow$ Fig. 116 - Fig. 118). Despite this the view is essentially the same as for Numerical Data Arrays ( $\hookrightarrow$ Sec. 13.5).


Figure 116. Example for a 1D diagram showing a Gaussian pulse.


Figure 117. Example for a 2D pulse component view.


Figure 118. Example for a pulse component view.

## 16 Set of Objects

Sometimes it is useful to group various objects of the same type together. For example a detector might yield several data arrays with different sampling. Besides the settings inherited from the underlying objects this view allows to switch between the contained objects.
Currently only a set of data arrays is supported. Note that for your convenience, a set of data arrays with only one data array is converted automatically to a single numerical data array.

## Availability

...of the controls to switch between the data arrays:
Accessible:

- Ribbon: View > Data Array Selection ribbon group
- Property browser: View > Data Array Index

In the very top of the document view ( $\hookrightarrow$ Fig. 119), there is a double label. The left part indicates the name of the object, the right part the name of the current subset. The gray area between the two labels can be used to change their relative sizes by dragging with the mouse.

| 6月, 2: Set of 2D Data Arrays |  |  |  | $\square$ | 回 | $x$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iteration Step of 1 |  | b | Electric Field (x-Domain, Equidistant) |  |  |  |
| Diagram | Table | Value |  |  |  |  |

Figure 119. Example for the double label of a Set of 2D Data Arrays. Here the Electric Field subset for Iteration Step of 1 is shown.

The view settings for data arrays are explained in Sec. 13.5.

### 16.1 The View Area and Switching Between Objects

Different objects may own different definition areas. Usually, the view area is restricted to this definition area. So, switching between objects with differing definition areas may lead to "jumping" view ranges if the definition areas overlap only partial or not at all.
If, however, the option Data Restricted Zoom is deactivated ( $\hookrightarrow$ Sec. 11.4.1), the zoom factor is not limited anymore and jumping view areas are avoided.
An additional feature leads to a more convenient switching behavior even if Data Restricted Zoom is kept activated: If the option called Unified Max Extension is checked, one unified definition area is calculated from all single definition areas of the contained objects.

## Availability

...of the Unified Max Extension feature:
Accessible:

- Ribbon: View > Zoom \& Aspect Ratio ribbon group > Unified Max Extension


## 17 Ray Distribution View

The view for Ray Distributions consists of two tab pages: the 3D View tab draws the rays directly in the threedimensional system view ( $\hookrightarrow$ Sec. 17.1) and the 2D View tab draws the rays intersecting with a certain plane ( $\hookrightarrow$ Sec. 17.2).
The latter tab shows either Field Properties or Ray Properties which influences the available view settings. Which of these modes is available depends on how the Ray Distribution has been generated:

| GENERATION VIA... | 3D VIEW | 2D VIEW <br> (FIELD PROPERTIES) | 2D VIEW <br> (RAY PROPERTIES) |
| :--- | :--- | :--- | :--- |
| General Profile <br> ( $\checkmark$ Sec. 43.4) | $\mathbf{x}$ | $\boldsymbol{v}$ | $\boldsymbol{v}$ |
| Ray Results Profile ( $\checkmark$ Sec. 43.4) | $\mathbf{x}$ | $\mathbf{x}$ | $\boldsymbol{v}$ |
| Ray Tracing System Analyzer <br> $(\leftrightarrows$ Sec. 43.4 .5$)$ | $\boldsymbol{v}$ | $\boldsymbol{x}$ | $\boldsymbol{v}$ |

### 17.1 3D View



Figure 120. Ray Distribution for a focusing lens showing the 3D View tab page.
Into the 3D view the surfaces of an optical setup can be drawn together with rays passing through them. This view is essentially the same as the standard 3D view ( $\hookrightarrow$ Sec. 5.15 ), except for the following differences:

- The context menu has the additional options Select Tracing Sequence ( $\hookrightarrow$ Sec. 17.1.1) and Filter Blocked Rays ( $\hookrightarrow$ Sec. 17.1.2).
- The view settings dialog has the additional page Rays with which you can define the layout of the rays. $\hookrightarrow$ Sec. 17.1.3
- If you export the view to the IGES format via the context menu, the rays are also exported into this file.
- The document window has a property browser and a View ribbon tab.

In the View ribbon you can

- specify which subset is to be shown ( $\hookrightarrow$ Sec. 17.3)
- adjust the colors of the rays ( $\hookrightarrow$ Sec. 17.4) and
- copy the view to clipboard ( $\hookrightarrow$ Sec. 11.6)

Furthermore this ribbon tab has the following controls specific to the 3D View of Ray Distributions:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Stride | For a better overview you can define a stride $n$ which means that only every $n^{\text {th }}$ ray is drawn. |
| Ray Thickness | With this option you can make the rays be drawn larger or smaller. |
| Settings <br> \{Predefined Camera <br> Orientations\} | Opens the view settings dialog. $\hookrightarrow$ Sec. 5.15.2 <br> There are 6 predefined camera orientations available: View orthogonal to xy-Plane and xy-Plane (Rear) (anti-parallel and parallel to the z-Axis, respectively), view orthogonal to zx-Plane and zx-Plane (Rear) (anti-parallel and parallel to the y-Axis, respectively), view orthogonal to zy-Plane and zy-Plane (Rear) (parallel and anti-parallel to the x-Axis, respectively). |
|  | Filters all rays blocked by a certain aperture. $\hookrightarrow$ Sec. 17.1.2 |

Most of these options can also be set via the View tab of the property browser.

### 17.1.1 Select Tracing Sequence

If a complex optical system is shown in the Ray Distribution 3D view, it may be hard to keep track of all ray paths. Thus this tool, available via the context menu of the view, allows you to define the shown tracing sequence by switching off ray paths.


Figure 121. The dialog to select the shown tracing sequence.
The upper part of its edit dialog ( $\hookrightarrow$ Fig. 121) shows all ray paths in execution order. A ray path either runs

- between two Optical Setup Elements,
- between two surfaces of a real component, or
- through one surface of a real component.

The Selection Tools button allows you to either Select All ray paths or to Unselect All.

### 17.1.2 Filter Blocked Rays

With this tool you can define that all rays blocked at the aperture of a certain surface are not shown at all. This can make the relevant ray paths more clear.
In the edit dialog of this tool you can select whether you want to apply that filter and if so, which boundary defines the blocking aperture. Fig. 122 shows an example.


Figure 122. In the left view all rays are shown. In the right view all rays not passing the selected aperture (marked by the red arrows) are not shown.

### 17.1.3 Rays Page



Figure 123. The Rays page of the View Settings dialog.
With this page ( $\hookrightarrow$ Fig. 123) of the View Settings dialog ( $\hookrightarrow$ Sec. 5.15 .2 ) you can define how the rays are visualized.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Show Rays | If this options is unchecked, you see only the pure Optical Setup without any <br> rays. |
| Ray Thickness | With this option you can make the rays be drawn larger or smaller. |
| Stride | For a better overview you can define a stride $n$ which means that only every <br> $n^{\text {th }}$ ray is drawn. |
| Single Color | If you select this option, all rays are drawn with the same color. If you click on <br> the $\square$-button you can either choose a predefined color or define your own. |
| Wavelength | With this option, all rays are colored as the human eye would perceive the <br> corresponding wavelength. Invisible wavelengths are drawn black. |
| Color Table | With this option, the different wavelengths are drawn with different colors de- <br> fined by the selected color table. |
| Colorize Boundary Tran- | With this option you can define that rays within a boundary operator are em- <br> sition Rays in Different <br> Color |

### 17.2 2D View



Figure 124. 2D View tab page of the Ray Distribution view with visible Boundary Index control.

The 2D View of a Raytracing Result view ( $\hookrightarrow$ Fig. 124) is based on gridless data arrays. It allows you to

- specify which mode is to be shown ( $\hookrightarrow$ Sec. 17.3)
- set the scaling mode ( $\hookrightarrow$ Sec. 11.2.5)
- adjust the colors of the rays ( $\leftrightarrows$ Sec. 17.4)
- use markers and selections ( $\leftrightarrows$ Sec. 11.3)
- zoom into the view ( $\hookrightarrow$ Sec. 11.4)
- change its aspect ratio ( $\hookrightarrow$ Sec. 11.5) and
- copy the view to clipboard ( $\hookrightarrow$ Sec. 11.6)

Furthermore this view has the following features specific to the 2D View of Ray Distributions:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Field Properties / <br> 图 Ray Properties | Only available if the Ray Distribution has been calculated via General Profile ( $\hookrightarrow$ Sec. 43.4) <br> With this ribbon menu you can define whether the field properties ( $\hookrightarrow$ Sec. 17.2.1) or the ray properties ( $\hookrightarrow$ Sec. 17.2.2) shall be displayed. If this ribbon item is not visible only ray properties are available. This option can also be set via the property browser (View > Show Field Quantities). |
| Dot Size | Allows you to adjust the size of the dots. Can be set either via the ribbon item View > Dot Size or the View tab of the property browser. |
| Background Color | Usually the dots do not fill the whole diagram region and thus you see its background color. If you click on View > Background Color, you can either choose a predefined color or define your own using More Colors. The entry Background Color in the View tab of the property browser has more predefined colors. There you can also directly enter the name or the RGB values (separated by comma and space) of the desired color. |
| Show Triangles | Switches the triangle interpolation ( $\hookrightarrow$ Sec. 11.2.3) on and off. <br> This feature is not available if the ray property Direction is shown. If the ray property Position is shown, only the triangles borders are shown. For further information about ray properties see Sec. 17.2.2. |

If the Ray Distribution was obtained with the Raytracing System Analyzer ( $\hookrightarrow$ Sec. 43.4.5), the view contains an additional control to select the Boundary Index ( $\hookrightarrow$ Fig. 124). Using this control you can visualize the ray distribution at various boundaries.
If a point marker is visible, the Ray Selection tab of the property browser shows both the field and the ray properties of the currently selected ray.

### 17.2.1 Field Properties

If the 2D view of a raytracing result is in the Field Properties mode, you can select the Field Component ( $E_{x}$, $E_{y}$, and so on; $\hookrightarrow$ Sec. 17.2.1.1) and the Field Quantity ( $\hookrightarrow$ Sec. 11.1).
In the View tab of the property browser you can define whether to Apply Energy Conservation. The energy conservation is based on the size of the triangles spanned by the rays which usually does not work if you are in the focus.

### 17.2.1.1 Field Component

## Availability

## Accessible:

- Ribbon: View > Field Component ribbon group
- Property browser: View > Field Component
- Context menu: Edit View Settings ( $\hookrightarrow$ Sec. 17.2.3)

The field component can be either $E_{x}, E_{y}, E_{z} H_{x}, H_{y}$, or $H_{z}$. The formulas for calculating the distinct field components are given in Sec. 131.

### 17.2.2 Ray Quantities

## Availability

## Accessible:

- Ribbon: View > Ray Quantity ribbon group
- Property browser: View > Quantity
- Context menu: Edit View Settings ( $\hookrightarrow$ Sec. 17.2.3)

If it is in the Ray Properties mode, the 2D view of a Ray Distribution can visualize one of the following ray quantities.

| RAY QUANTITY | DESCRIPTION |
| :---: | :---: |
| Position 图 | Plots the rays at their actual positions in the shown $x-y$-plane. If there is more than one mode given and the coloring mode is set to Color by Table, the colors indicate the respective mode index of each ray. |
| Direction 图 | The direction of a ray can be described by the direction vector $s$ which has an absolute value of 1 . If you select this ray quantity, you can change the Direction Visualization Mode in the View tab of the property browser. This option allows you to plot the rays either into the $s_{x}-s_{y}$-plane, or to color the rays according to the $s_{x^{-}}, s_{y^{-}}$, or $s_{z}$-component while plotting them into the x -y-plane. |
| Optical Path Length ${ }^{\text {nz }}$ | The rays are plotted at their actual positions in the shown $x-y$-plane and colored according to their optical path length. |
| Absorption $\stackrel{\mathrm{i}^{\text {dem }}}{ }$ | The rays are plotted at their actual positions in the shown $x-y$-plane and colored according to the absorption. |

### 17.2.3 View Settings Dialog



Figure 125. The dialog to edit the view settings of a Ray Distribution.

This dialog ( $\hookrightarrow$ Fig. 125) allows you to set the most important view parameters at once. It can be opened via the context menu of the view.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Visualization of | Only available for documents calculated with General Profile, othERWISE ONLY RAY PROPERTIES ARE SHOWN <br> Allows you to determine whether you want to see any of the Field Properties or any of the Ray Properties. |
| Field Component | Only available in Field Properties mode The field component ( $\hookrightarrow$ Sec. 17.2.1.1) to show. |
| Field Quantity | Only available in Field Properties mode The field quantity ( $\varsigma$ Sec. 11.1) to show. |
| Apply energy conservation | Only available in Field Properties mode <br> The energy conservation is based on the size of the triangles spanned by the rays which usually does not work if you are in the focus. Thus you can switch it off in this case. |
| Ray Quantity | Only available in Ray Properties mode The ray quantity ( $\hookrightarrow$ Sec. 17.2.2) to show. |


| Direction Visualization Mode | Only available for Direction as Ray Quantity <br> The direction of a ray can be described by the direction vector $s$. This option allows you to plot the rays either into the $s_{x}-s_{y}$-plane, or to color the rays according to the $s_{x}-$, $s_{y^{-}}$, or $s_{z}$-component while plotting them into the x - y plane. |
| :---: | :---: |
| Add Wavefront Response to Optical Path Length | Only available for Optical Path Length as Ray Quantity Ideal components and light sources might add a wavefront response independent from the actual optical path length. By checking this option the wavefront response is added to the shown optical path length. |
| Show Triangles | Not for the Ray Quantity Direction in $F(S X, S y)$ mode If checked the triangle interpolation ( $\leftrightarrows$ Sec. 11.2.3) is applied. |
| Show Borders of Triangles | Only available if Show Triangles is checked <br> Draws the borders of the triangles used for the triangle interpolation. |
| Dot Size | Not available if Show Triangles is checked Allows you to adjust the size of the dots representing the rays. |
| Single Color | Not for the ray properties Absorption, Optical Path Length, and Direction (in $\operatorname{SX}(X, Y), S y(X, Y)$, or $\operatorname{Sz}(X, Y)$ ) mode <br> If you select this option, all rays are drawn with the selected color. |
| Wavelength | Not for the ray properties Absorption, Optical Path Length, and DiRection (in $\operatorname{SX}(X, Y), S y(X, Y)$, or $S z(X, Y)$ ) mode <br> With this option, all rays are colored as the human eye would perceive the corresponding wavelength. Invisible wavelengths are drawn black. |
| Color Tables | With this option, the different rays are drawn with different colors defined by the selected color table. For complex data, this can be set per field quantity. Please note that the shown colors do not map onto any quantity of some physical meaning in some cases: If ray positions or directions in the $s_{x}-s_{y}-$ plane are shown, the color indicates the mode index of each ray (in case there is more than one mode). |
| Opacity | Only available in Field Properties mode <br> If the default opacity of 1 is lowered, the rays become more and more transparent and thus also rays "below" the topmost rays become more and more visible. |
| Background Color | Usually the dots do not fill the whole diagram region and thus you see its background color. If you click on this button, you can either choose a predefined color or define your own. |

### 17.3 Mode Selection

## Availability

For Ray Distributions with more than one subset

## Accessible:

- Ribbon: View > Subset Selection group
- Property browser: View > Subset Selection group

A Ray Distribution can have multiple wavelengths and incoherent modes. For each combination of wavelength and incoherent modes there can be multiple coherent modes. In the view ribbon there is the control shown in Fig. 126 with which you can set Wavelength \#, Incoherent Mode \# and Coherent Mode \#, either by using the arrow buttons or by entering the index directly. If you check the corresponding check box all modes of the respective type are shown.
The same can be done with the View > Subset Selection group of the property browser. It also shows the currently selected wavelength, not only the wavelength index.


Figure 126. The controls to select specific mode(s) in the ribbon. The second wavelength out of three possible wavelengths is selected. There is only one incoherent mode so the corresponding arrow buttons are disabled. All coherent modes for the currently selected wavelength and for the currently selected incoherent mode are shown.

### 17.4 Coloring Rays

## Availability

## Accessible:

- Ribbon: View > Color by Wavelength, View > Color by Table, View > Single Color
- Property browser: View > Color Mode
- Context menu (3D View): View Settings > Rays ( $\hookrightarrow$ Sec. 17.1.3)
- Context menu (2D View): Edit View Settings ( $\hookrightarrow$ Sec. 17.2.3)

You can color rays in the following ways:

| MODE | DESCRIPTION |
| :--- | :--- |
| Color by Wavelength | With this option, all rays are colored as the human eye would perceive the <br> corresponding wavelength. Invisible wavelengths are drawn black. |
| With this option, the different rays are drawn with different colors defined by <br> the selected color table and the shown quantity. <br> If the shown quantity is the position or the direction in the $s_{x}-s_{y}$-plane or if the <br> 3D view is shown, each distinct wavelength or incoherent mode gets its own <br> color from the selected color table. |  |
|  | If you select this option, all rays are drawn with the selected color. |

## 18 Order Collection View

An Order Collection document contains the coordinates, efficiencies and Rayleigh coefficients of all (transmitted or reflected) diffraction orders of a grating. What exactly is shown depends on the settings on the Data to Show tab of the Property Browser. There you have the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Coordinate Type | The coordinates versus which the individual orders are plotted: either the <br> order numbers, the spherical angles $\theta$ and $\phi$, the Cartesian angles $\alpha$ and $\beta$, <br> the wave vector components $k_{x}$ and $k_{y}$, or the position $(x ; y)$. In the latter <br> case you can set a Distance for which the positions are calculated. |
| Allows to set whether the efficiencies or certain Rayleigh coefficients ( $E_{x}, E_{y}$, |  |
| $E_{z}$, TE, TM) of the orders are shown. |  |

If angles or positions are used as coordinates, evanescent orders are never shown, regardless of the selection strategy.


Figure 127. Efficiencies of a grating invariant in y-direction for conical incidence, plotted versus Cartesian angles.
The selected data is shown in a Gridless Data Array and shares most of its features ( $\hookrightarrow$ Sec. 13.5). Fig. 127 shows an example.
In contrast to Gridless Data Arrays, the Order Collection view has the following additional features:

- You can convert the complete data into an equidistant data array, plotted versus order numbers. This can be done via the ribbon item Manipulations $>\vec{\exists} \boldsymbol{\varepsilon}$ Create Equidistant Data Array or by pressing F3.
- In the table always the order numbers are shown, even if the coordinates are spherical coordinates for example.
- If you extract 1D data along a selected line ( $\hookrightarrow$ Sec. 24.14.1), the order numbers are added as labels to the resulting data array.
- If you select a certain order with the Point Marker ( $\hookrightarrow$ Sec. 11.3), all coordinates and all data (efficiency and Rayleigh coefficients) are shown in the Selections tab of the Property Browser.


## 19 Diffraction Orders Diagrams

The diffraction orders diagram serves for visualizing angles and efficiencies of diffraction orders in a plane as shown in Fig. 128.

You can zoom in or zoom out the diagram with the mouse wheel or with the following ribbon buttons to be found in View.

| ITEM | DESCRIPTION |
| :--- | :--- |
| © Zoom In | Increase zoom factor by factor $\sqrt{2}$. |
| Q Zoom Out | Decrease zoom factor by factor $\sqrt{2}$. |
| \& Show All | Show all data. This is the default for newly created diagrams. |

The displayed value range can be adjusted more precisely via the Property Browser: For polar diagrams you can change the Maximum of the value-axis via the property browser. For bar and line diagrams you can change Minimum and Maximum of both $x$ - and $y$-axis. If you change Auto Scale to True, the $y$-axis is reset to its default values.
The context menu of the diagram allows to select the data to be shown:
ITEM
DESCRIPTION
Choose Diffractive Orders This will open a configuration dialog explained in Sec. 19.1. to Show


Figure 128. Example for a Diffraction Orders Diagram.

The Table panel ( $\hookrightarrow$ Fig. 129) shows the diffraction order values in a tabular form. The Order column shows the type and index of the diffraction order ("T" marks the transmitted orders, " $R$ " the reflected orders, and "l" the incident wave). The second and the third column show the angle and the efficiency of each order respectively.

The context menu of the table allows to copy the currently selected data:
ITEM DESCRIPTION

Copy Selection to Clip- Copies the selected data to the clipboard so that they can be used in external board programs like spreadsheet programs.


Figure 129. The table panel of a Diffraction Orders Diagram.

### 19.1 Select Diffraction Orders to Show

For a better overview, you can reduce the number of orders shown in a Diffraction Orders Diagrams. For the selection of the orders to be shown, this dialog can be used ( $\hookrightarrow$ Fig. 130).


Figure 130. The Dialog for selecting the diffraction orders to show.

You can select the Type of Orders you want to see and restrict the angular range to be shown.
Additionally, either a Stride can be set (a stride of $n$ means that only every $n^{\text {th }}$ order is shown) or single orders can be selected via the checkboxes in the table rows. Furthermore, you can Select All data points or Select None.

## 20 Animation View

An animation is a sequence of raster graphics images which can be shown smoothly one after another. A single image is also referred to as frame.


Figure 131. Example of an Animation View.
Fig. 131 shows the animation view which contains the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\mathbf{I}$ | Allows you to run the animation in forward / reverse order. If Repeat Animation <br> is set in the Animation Options dialog ( $\leftrightarrows$ Sec. 20.3), the animation will be <br> started again automatically if the end is reached. |
| $\boldsymbol{m}$ | Pauses a running animation. <br> With these buttons you can jump to the first and the last frame of the anima- <br> tion, respectively. |

The button corresponding to the currently active "action" (pause / play forwards / play backwards) is disabled. There is also the possibility to go through the animation using the scrollbar. In the bottom-right corner you can see the index of the current frame and the overall number of frames.
An animation can be exported into various file formats ( $\hookrightarrow$ Sec. 123).

### 20.1 Ribbon Items

The following ribbon items are available on the Animation ribbon tab:

| ITEM | DESCRIPTION |
| :---: | :---: |
| 岛 Copy Frame | Copies the current frame into the Windows ${ }^{\text {TM }}$ clipboard（as an image）． |
| of Cut Frame <br> 图 Paste Frame | Moves the current frame into the Windows ${ }^{\text {TM }}$ clipboard（as an image）． <br> Pastes an image from the clipboard into the animation．The image can be inserted（Paste＞Insert Frame）before the currently selected frame or ap－ pended（Paste＞Append）to the end of the animation．In both cases the number of frames will increase by one． <br> If the size of the pasted image does not match the size of those images al－ ready in the animation，a resizing is done which maintains the aspect ratio of the pasted image． |
| $\chi_{\square}$ Delete Frame | Deletes the current frame． |
| 咎Swap Frames | Swaps two frames．The source frame and the destination frame can be cho－ sen in a separate dialog． |
| 腺Stitch Animations | Stitches two animations，i．e．places them either side by side or one below the other．$\hookrightarrow$ Sec． 20.2 |
| 餗 Animation Options | Opens the animation options．$\hookrightarrow$ Sec． 20.3 |

All of these items but Stitch Animations are also accessible via the context menu of the animation view．

## 20．2 Stitch Animations

Using the ribbon item Animation＞低 Stitch Animations stitches two animations，i．e．places them either side by side（＝＂horizontally＂）or one below the other（＝＂vertically＂）．The animations to stitch must have the same number of frames．


Figure 132．The dialog with the options for stitching animations．

This tool is applied on one animation．Then a dialog（ $\hookrightarrow$ Fig．132）opens where you can set the second animation and other options．

| ITEM | DESCRIPTION |
| :--- | :--- |
| Select Second Animation | Allows you to select the second animation from any other already opened <br> animation． |
| Stitch Orientation | If you select Horizontally the two animations are placed side by side．If the <br> two animations do not have the same height in pixels，the animation with the <br> smaller height is resized accordingly． <br> If you select Vertically the two animations are placed one below the other．If <br> the two animations do not have the same width in pixels，the animation with <br> the smaller width is resized accordingly． |
| Space Between Anima－  <br> tions You can add up to 1000 pixels of black space between the two animations to <br> separate them more clearly． |  |

Note that you can apply this tool recursively to stitch more than two animations. Fig. 133 shows an example.


Figure 133. Four stitched animations: First the two upper and the two lower animations, respectively, were stitched horizontally with a Space Between Animations of 40 pixels. Then the two resulting animations were stitched vertically with a Space Between Animations of 20 pixels.
The upper part shows the phase of the near field of the grating, the lower the phase of the Rayleigh coefficients. Left: transmission, right: reflection.

### 20.3 Animation Options

Using the ribbon item Animation > 碃Animation Options or the context menu the dialog shown in Fig. 134 can be opened.


Figure 134. Dialog to adjust the settings for the Animation View.

The following settings are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Properties | The bitmap size, the used color format, and the number of frames are shown. |
| Frames per Second / <br> Frame Duration / <br> Whole Duration | Allows you to enter the animation speed. |
| Repeat Animation | If checked a running animation will automatically be started again if it reaches <br> the last frame. |
| Free Aspect Ratio | If checked the animation will be stretched to use the complete available <br> space. Otherwise the aspect ratio of the animation will be maintained and <br> unused parts of the view are colored black. |

## 21 Regions

Region documents simply store the information whether a certain position belongs to (lies inside) a certain region or not. Such a region document can be used as Evaluation Region in the Diffractive Optics Merit Functions detector ( $\hookrightarrow$ Sec. 74.6.2) or as Optimization Region in the IFTA Optimization document ( $\hookrightarrow$ Sec. 97).
A region can be generated in the following ways:

| METHOD | DESCRIPTION |
| :---: | :---: |
| Create a new region document | Create a new rectangular, elliptical, polynomial, sampled or composed 2D region ( $\leftrightarrows$ Sec. 21.1), or an interval, sampled or composed 1D region ( $\leftrightarrows$ Sec. 21.2). |
| Create signal region document from selection | Manipulations > 胃 Selection Related Operations > Create Signal Region from Selection creates a sampled region which has the same sampling parameters as the current harmonic field or Jones matrix transmission document. The current range or rectangle marker defines the actual signal region, independent from the values in the original document. |
| Convert to sampled region document | A harmonic field or a Jones matrix transmission can be converted to a sampled region document using Manipulations > $\rightrightarrows$ Create Sampled Region. In this case you are asked for a relative threshold and all values having a squared amplitude larger than the maximum squared amplitude times this value are regarded as being 'inside' the region. |

### 21.1 Generating a 2D Region

Via Functions $>$ Region (2D) 2D regions can be generated. The dialog is shown in Fig. 135.


Figure 135. Dialog for generation of a two-dimensional region document.
The following general parameters are used for the specification of each 2D region, independent from its respective type:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Region Type | The type of the region to be created. This can be Rectangular Region, Ellip- <br> tic Region, Simple Polygon Region, Sampled Region, or Composed Region. <br> These types are described below ( $\rightarrow$ Sec. 21.1.1 to Sec. 21.1.5. |
| Spectral Domain | Determines whether or not the region is intended for using in the spectral or <br> spatial domain. |
| Region Name | A user defined name for the region to be created. |

Extrapolation Mode: Val- This setting defines how to handle points which lie outside the domain of the ues Outside Domain are actual region. The following options can be set:

- All 'Outside Region': All outlying points do not belong to the region.
- All 'Inside Region': All outlying points do belong to the region, despite lying outside the domain.
- Periodically Continued: The whole domain of the region is continued periodically in every direction.
- Equal to the Nearest Border Data Point: A constant extrapolation of the outmost data points is done. Meaning, if the nearest border point belongs to the region, the considered outlying point belongs to the region too.


### 21.1.1 Generating a Rectangular Region

The specific parameters for creating a rectangular region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Center $\mathbf{X} / \mathbf{Y}^{[\operatorname{PV}]}$ | These values specify the center point of the rectangle. |
| Width / Height ${ }^{[\operatorname{PV}]}$ | The extension of the rectangle. |
| Keep Aspect Ratio | If checked, a change in width or height will change the other extension value <br> in a way keeping the ratio of the sides, resp. |
| Rotation Angle ${ }^{[\mathrm{PV}]}$ | An angle for rotating the rectangle around its Center. |

### 21.1.2 Generating an Elliptic Region

The specific parameters for creating an elliptic region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Center $\mathbf{X} / \mathbf{Y}^{[\mathbb{P V}}$ | These values specify the center point of the ellipse. |
| Half Axis $\mathbf{X} / \mathbf{Y}^{\boxed{P V}}$ | The half axes of the ellipse in each dimension. |
| Keep Aspect Ratio | If checked, a change in one of the half axes will change the other half axis in <br> a way keeping the ratio of the sides, resp. |
| Rotation Angle ${ }^{\boxed{P V}}$ | An angle for rotating the ellipse around its Center. |

### 21.1.3 Generating a Simple Polygon Region

A simple polygon is a polygon without intersecting edges. Such polygons, containing an arbitrary number of points, can be defined here.
The specific parameters for creating a simple polygon region are listed in the following table:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Polygon Vertices table | In this table the Name, $x$-Coordinate ${ }^{\mathbb{P V}}$, and $y$-Coordinate ${ }^{[\mathrm{PV}}$ of each vertex can be edited. |
| Append New | Opens a dialog for specifying a new polygon vertex and appends it to the list. |
| Insert New | Opens a dialog for specifying a new polygon vertex and inserts it into the list, above the currently selected row. |
| Remove | Removes the currently selected polygon vertex. |
| Move Up / Down | Moves the currently selected row up or down, resp. |
| ```Transform > Scale (Keep Center)``` | Allows to scale the whole polygon by means of a (to be entered) factor. The center of the polygon's axis aligned bounding box will be kept constant. |
| Transform > Rotate (Around Center) | Allows to rotate the whole polygon by means of a (to be entered) angle. The rotation will be done around the center of the polygon's axis aligned bounding box. |
| ```Transform > Shift (Trans- late)``` | Allows to shift / translate the complete polygon by means of a (to be entered) vector. |

Please note: The order of the vertices is important for each polygon with more than three vertex points.

### 21.1.4 Generating a Sampled 2D Region

A sampled region is defined by a finite number of sampling points on a grid, each point defining its area being either inside of outside the actual region.

The specific parameters for creating a sampled region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampled Region Data | The sampled region data can be set or shown here. This region data has to <br> be defined via a real-valued Numerical Data Array (2D) with one single subset <br> ( $\lrcorner$ Sec. 13). All values unequal zero will be interpreted as being 'inside' the <br> region. |
|  |  |

### 21.1.5 Generating a Composed 2D Region

A composed region is built by one or more subregions ${ }^{[\boxed{ } E]}$. The combination is defined by a composition mode which corresponds to one of several logical operations. These operations and their meanings are shown in the following list:

| OPERATOR | REGION COMPOSITION |
| :--- | :--- |
| Intersection (AND) | A given point is inside the actual region if and only if it lies in each of the <br> subregions respectively. |
| Union (OR) | A given point is inside the actual region if and only if it lies in one of the <br> subregions at least. |
| Antivalence (XOR) | A given point is inside the actual region if and only if it lies in an odd number <br> of subregions. |
| Difference | A given point is inside the actual region if it lies only in the first subregion in <br> the table but in none of the other subregions. |

Since composed regions may be used as subregions as well, a combination of several different composition modes is possible.

The specific parameters for creating a composed region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subregions table | The unique index (\#), the region Type, as well as the Name of each subregion <br> are shown here. |
| Edit Subregion | Opens a dialog for editing the currently selected subregion. <br> New SubregionOpens a dialog for creating a new subregion which will be appended to the <br> table entries. <br> Deletes the currently selected subregion. |
| Molete Subregion Up / Down | Moves the currently selected subregion one row up or down resp. This is <br> needed in case of the Composition Mode 'Difference' only. |
| Composition Mode | The mode for combining the subregions. See the list above. |

The edit dialog for creating or changing subregions provides the following additional options: provides a new default region for each of the region types, allows to select an open region document or to load a region document from hard disc, $\mathrm{H}_{\mathrm{l}}$ allows to save the current region, and Q will show the current region as new document.

### 21.2 Generating a 1D Region

Via Functions > Region (1D) 1D regions can be generated. The dialog is shown in Fig. 136.


Figure 136. Dialog for generation of a one-dimensional region document.

The following general parameters are used for the specification of each 1D region, independent from its respective type:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Region Type | The type of the region to be created. This can be Interval Region, Sampled Region, or Composed Region. These types are described below ( $\hookrightarrow$ Sec. 21.2.1 to Sec. 21.2.3. |
| Spectral Domain | Determines whether or not the region is intended for using in the spectral or spatial domain. |
| Region Name | A user defined name for the region to be created. |
| Extrapolation Mode: Values Outside Domain are | This setting defines how to handle points which lie outside the domain of the actual region. The following options can be set: <br> - All 'Outside Region': All outlying points do not belong to the region. <br> - All 'Inside Region': All outlying points do belong to the region, despite lying outside the domain. <br> - Periodically Continued: The whole domain of the region is continued periodically in every direction. <br> - Equal to the Nearest Border Data Point: A constant extrapolation of the outmost data points is done. Meaning, if the point with the smallest coordinate inside the domain belongs to the region, all points with smaller coordinates belong to the region too. The same applies for the point with the largest coordinate in the domain and all points with larger coordinates as well. |

### 21.2.1 Generating an Interval Region

The specific parameters for creating an interval region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Center $\mathbf{X}^{\mathbb{P V}}$ | This value specifies the center point of the interval. |
| Width $^{\boxed{P V}}$ | The extension of the interval. |

### 21.2.2 Generating a Sampled 1D Region

A sampled region is defined by a finite number of sampling points, each point defining its interval being either inside of outside the actual region.
The specific parameters for creating a sampled region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampled Region Data | The sampled region data can be set or shown here. This region data has to <br> be defined via a real-valued Numerical Data Array (1D) with one single subset <br> ( $\hookrightarrow$ Sec. 13). All values unequal zero will be interpreted as being 'inside' the <br> region. |

### 21.2.3 Generating a Composed 1D Region

A composed region is built by one or more subregions ${ }^{[\boxed{ } E]}$. The combination is defined by a composition mode which corresponds to one of several logical operations. These operations and their meanings are shown in the following list:

| OPERATOR | REGION COMPOSITION |
| :--- | :--- |
| Intersection (AND) | A given point is inside the actual region if and only if it lies in each of the <br> subregions respectively. |
| Union (OR) | A given point is inside the actual region if and only if it lies in one of the <br> subregions at least. |
| Antivalence (XOR) | A given point is inside the actual region if and only if it lies in an odd number <br> of subregions. |
| Difference | A given point is inside the actual region if it lies only in the first subregion in <br> the table but in none of the other subregions. |

Since composed regions may be used as subregions as well, a combination of several different composition modes is possible.

The specific parameters for creating a composed region are listed in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subregions table | The unique index (\#), the region Type, as well as the Name of each subregion <br> are shown here. |
| Edit Subregion | Opens a dialog for editing the currently selected subregion. |
| New Subregion | Opens a dialog for creating a new subregion which will be appended to the <br> table entries. |
| Delete Subregion | Deletes the currently selected subregion. <br> Move Up / Down |
| Moves the currently selected subregion one row up or down resp. This is <br> needed in case of the Composition Mode 'Difference' only. |  |
| Composition Mode | The mode for combining the subregions. See the list above. |

The edit dialog for creating or changing subregions provides the following additional options: default region for each of the region types, $\because$ allows to select an open region document or to load a region document from hard disc, $H$ allows to save the current region, and $Q$ will show the current region as new document.

### 21.3 Region View

The region view visualizes region documents ( $\leftrightarrows$ Sec. 21). The user can see what points lie inside or outside the actual regions respectively.
The views provide options for zooming as described in Sec. 11.4 and for copying the view to the clipboard as described in Sec. 11.6. For two-dimensional regions, the aspect ratio behavior can be specified ( $\hookrightarrow$ Sec. 11.5). Markers as described in Sec. 11.3 can be used in views for sampled regions only. For 2D regions, a smoothing option can be (de)activated via property browser.
Furthermore, the view settings of different region views can be copied among regions of the same dimensionality.

# IV Manipulations: Processing Data 

In VirtualLab Fusion there are several document types which store oneor two-dimensional data.

Their Manipulations ribbon tab contains several operations to modify this (mostly) sampled data which are described in this part of the manual. Furthermore it contains Conversions ( $\leftrightarrows$ Sec. 30) to convert one document type into another.

## 22 Manipulations of Complex Amplitude Documents

Complex Amplitude Documents, namely Harmonic Fields and Jones Matrix Transmissions, have the manipulations available which are described in the following subsections. The ribbon group Manipulations > Conversions is explained in Sec. 30.1, the ribbon group Manipulations > Fourier Transformation (Space) in Sec. 31.1.

### 22.1 Array - Array Operations

Via the ribbon menu Manipulations > $\mathrm{m}_{\mathrm{m}}^{\mathrm{m}}$ Array - Array Operations several operations for two array operands are available:

- The four basic operations Addition, Subtraction, Multiplication, and Division as well as the convolution of two fields, all of which are explained in Sec. 22.1.1.
- Inserting of one array into another, $\hookrightarrow$ Sec. 22.1.2.


### 22.1.1 Arithmetic Operations

There are four basic arithmetic operations for arrays: addition, subtraction, multiplication, and division. Furthermore there is the convolution of two Complex Amplitude Documents $U_{1}$ and $U_{2}$, calculated by

$$
\begin{equation*}
U_{1} \star U_{2}=\mathcal{F}^{-1}\left[\left(\mathcal{F} U_{1}\right) \cdot\left(\mathcal{F} U_{2}\right)\right] \tag{22.1}
\end{equation*}
$$

The first operand is always the currently selected Complex Amplitude Document; the second operand can be selected from any open Complex Amplitude Document.
These operations can also be invoked by using the corresponding keys: $\square, \square, *, \square$, and $\#$, respectively. In this case the currently selected document is taken as the second operand while the previously selected Complex Amplitude Document is taken as first operand.
In case that the two arrays of an arithmetic array-array operation have not the same sampling distance or the same array size, at least one of the fields or transmissions has to be resampled before the calculation, because the underlying operation works pointwise.
The following table shows which parameter has to be adjusted in what case for each operation. The second and the third column show how the sampling distance $\Delta_{\text {new }}$ and the array size $S_{\text {new }}$ of the resulting array are determined by the sampling parameters of the operands (indices 1 and 2). Before starting the calculation, the array(s) that has got sampling parameters different from that of the result field will be resampled.

Important: The sampling parameters for the directions x and y are checked and adjusted independently!

| Operation | $\Delta_{\text {new }}$ | $S_{\text {new }}$ |
| :--- | :---: | :---: |
| Addition | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |
| Subtraction | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |
| Multiplication | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\min \left(S_{1}, S_{2}\right)$ |
| Division | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\min \left(S_{1}, S_{2}\right)$ |
| Convolution | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |

If a Transmission has to be resampled, the user can choose one out of two possible types of interpolation. For this reason a dialog will appear, shown in Fig. 137.


Figure 137. Dialog for determining the interpolation type for resampling of a transmission.
The options are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| continuous | If chosen, the transmission will be interpolated using the Cubic 8 Point Inter- |
|  | polation $(\hookrightarrow$ Sec. 13.2.2). |
| pixelated | If chosen, the transmission will be interpolated using the Nearest Neighbor <br>  <br>  |

Different types of Complex Amplitude Documents (Harmonic Field vs. Transmission) cannot be used as operands in every possible combination; Sec. 135.1 gives a summary of all combinable types and their result for all operations.

### 22.1.2 Insert Array

Inserts a selected array into the current array at a certain position whereas the corresponding data of the current array will be overwritten. This operation is done in pixel coordinates, the position ( $0 ; 0$ ) corresponds to the bottom left corner. The dialog is shown in Fig. 138. The array size of the original Complex Amplitude Document is not changed, which means that the inserted array might be cut off.


Figure 138. Dialog for inserting an array.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Array to insert | The array to be inserted into the currently active array. |
| Insert Position | Position, where the bottom left corner of the inserted array shall be located. |
| (Pixel Coordinates) | Can be negative. |

### 22.2 Operations with Constant

Via the ribbon menu Manipulations >com Operations with Constant several operations with one field operand are available, which are described in the following.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\pm=$ C Set to Constant | Set field to the given constant value. |
| ${ }^{+}$A Addition | Add the given constant value to all field positions. |
| ${ }^{\mathrm{a}} \mathrm{C}$ Multiplication | Multiply the given constant value to all field positions. |
| \#/C Division | Divide all field positions by the given constant. |
| ${ }_{\text {act Raise to Power }}$ | Raise all field positions to the power of the given constant value. |

For setting the constant values to operate with, the dialog shown in Fig. 139 appears. Here you can enter a complex number by specifying either real part and imaginary part or amplitude and phase.


Figure 139. Dialog for operation with one field operand.
If you choose the mode Operate Complex, the two double numbers to enter are treated as the parts of one complex number, either in Real / Imaginary or in Amplitude / Phase Representation. Then the operations are done as a complex addition, multiplication or raise-to-power for each sampling point. If Operate Separately is chosen, the first entry operates only on the real part / amplitude of the field and the second number only on the imaginary part / phase, depending on the choice of Representation. In the following table you can see how these operations work and what the respective meanings of $c_{1}$ and $c_{2}$ are. The original complex value of a sampling point $(z=a+i b \equiv A \exp [i \phi])$ is changed by the operation with the constants $c_{1}$ and $c_{2}$ to the result shown in the two last columns.

| OPERATION | REPRESENTATION | RESULT OF OPERATION |  |
| :--- | :--- | :--- | :--- |
|  |  | Operate Complex | Operate Separately |
| Add Constant | Real / Imaginary | $(a+i b)+\left(c_{1}+i c_{2}\right)$ | $\left(a+c_{1}\right)+i\left(b+c_{2}\right)$ |
|  | Amplitude / Phase | $A \exp [i \phi]+c_{1} \exp \left[i \widetilde{c_{2}}\right]$ | $\left(A+c_{1}\right) \exp \left[i\left(\phi+\widetilde{c_{2}}\right)\right]$ |
| Multiply Constant | Real / Imaginary | $(a+i b) \cdot\left(c_{1}+i c_{2}\right)$ | $\left(a \cdot c_{1}\right)+i\left(b \cdot c_{2}\right)$ |
|  | Amplitude / Phase | $A \exp [i \phi] \cdot c_{1} \exp \left[i \widetilde{c_{2}}\right]$ | $\left(A \cdot c_{1}\right) \exp \left[i\left(\phi \cdot c_{2}\right)\right]$ |
| Divide by Constant | Real / Imaginary | $(a+i b):\left(c_{1}+i c_{2}\right)$ | $\left(a: c_{1}\right)+i\left(b: c_{2}\right)$ |
|  | Amplitude / Phase | $A \exp [i \phi]:\left(c_{1} \exp \left[i \widetilde{c_{2}}\right]\right)$ | $\left(A: c_{1}\right) \exp \left[i\left(\phi: c_{2}\right)\right]$ |
| Raise to the Power of | Real / Imaginary | $(a+i b)^{c_{1}+i c_{2}}$ | $\left(a^{c_{1}}\right)+i\left(b^{c_{2}}\right)$ |
| Constant | Amplitude / Phase | $(A \exp [i \phi])^{c_{1} \exp \left[i \widetilde{c_{2}}\right]}$ | $\left(A^{c_{1}}\right) \exp \left[i \phi^{c_{2}}\right]$ |

$\widetilde{c_{2}}$ indicates that this value is an angle, i.e. you can enter it with the unit 'rad', 'pi', or 'o' ( $\hookrightarrow$ Sec. 5.1).

### 22.3 Field Quantity Operations

For real-valued data, the ribbon menu Manipulations > 领 Field Quantity Operations contains only the option to convert it to a complex-valued one.

For complex-valued data, this ribbon menu provides several transformations with respect to field quantities. Field quantities are explained in Sec. 11.1.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Extract | This submenu contains entries for all field quantities. The entry Imaginary Part constructs a field, where the real part is set to zero and the imaginary part is copied from the current field. Phase creates a field with the same phase as the current field, whereby the amplitude is set to one. All remaining submenu entries copy the corresponding field quantity to the real part of the resulting field, whereby the imaginary part of the resulting field is equal to zero. |
| Move | The submenu entries are labeled according to which field quantity of the resulting field is filled from which field quantity of the current field. For example, Phase to Real Part copies the phase of the current field to the real part of the resulting field, whereby the imaginary part of the resulting field is set to zero. |
| Swap | The corresponding submenu entry allows to swap real part and imaginary part. |

### 22.4 Amplitude / Real Part Manipulations

The ribbon menu Manipulations $>$ 甭 $/$ / Amplitude / Real Part Manipulations lets you perform the following operations with respect to amplitudes:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Normalize | Normalize the current field by dividing the field at all positions by the globally maximal amplitude. |
| Normalize According to Range Selection / <br> Normalize According to Rectangular Selection | Normalizes the current array by dividing it (at all sampling points) by the maximum amplitude within the current selection. |
| Clip | Clips the current field to a given maximum amplitude. At all positions, where the amplitude is above this maximum value, the amplitude is set to the maximum value preserving the original phase. At all remaining positions the field is not changed. The scaling mode ( $\lrcorner$ Sec. 11.2.5) of the newly generated field is set to Automatic Scaling. |
| Lift Positive | Searches for the minimum value of the real part of the field and subtracts that value from all field positions. For a real-valued field this corresponds to adding the minimum value which ensures a non-negative field. |
| Simulate Sinc Modulation Due to Pixelation | Analytical simulation of the pixelation effect of a transmission in the far field for a plane wave illumination. This function is to be applied on a harmonic field already being in the far field. $\hookrightarrow$ Sec. 138.1.2 |
| Compensate Sinc Modulation Due to Pixelation | Analytical compensation of the pixelation effect of a transmission in the far field for a plane wave illumination. This function can be used to make a compensation of the sinc-effect for the desired output field (far field) before starting a transmission design. $\hookrightarrow$ Sec. 138.1.2 |

### 22.5 Phase Manipulations

The ribbon menu Manipulations $>\varphi /$ Phase Manipulations contains several operations for manipulating the phase of the current field.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $z^{*}$ Conjugate | Performs a transformation in which each complex number $z=a+i b$ is replaced by $z^{\star}=a-i b$. |
| (\$) Unwrap Phase | This operation tries to generate a real valued data array which contains the unwrapped smooth phase of the current field, i. e. to remove $2 \pi$ jumps. During unwrapping, a simple line by line phase unwrapping algorithm is used. However, for two-dimensional fields unwrapping is neither unique nor always possible. For example, fields containing phase dislocations ( $\hookrightarrow$ Sec. 67.8.2) are generally unwrappable. A precondition for successful unwrapping is a sufficient sampling of the phase information. If the current complex amplitude contains information about a dominating spherical phase ( $\hookrightarrow$ Sec. 12.1.1), this information is taken into account during the unwrapping process. |
| Remove Phase Dislocations in Rectangular Selection | Phase dislocations ( $\hookrightarrow$ Sec. 67.8.2) are searched and tried to be removed in the current selection. For removing a certain phase dislocation with charge $c$ ( $\hookrightarrow$ Sec. 67.8.2), a transmission of a phase dislocation with charge $-c$ is multiplied to the array at the same position. This operation is repeated for all phase dislocations which were found within the current selection. |
| Modify Phase | The operations which can be done via the appearing dialog are described below ( $\checkmark$ Sec. 22.5.1). |
| Set Analytical Parameter | Sets the analytical spherical phase radius to a new value. This manipulation does not change the resulting phase, at least as long as the sampling distance is fine enough for the new aberrations (phase minus analytical spherical phase radius). The corresponding dialog is explained in Sec. 22.5.2, the concept of the spherical phase radius in Sec. 12.1.1. |
| Remove Analytical Parameter | Removes the analytical spherical phase radius. This manipulation does not change the resulting phase, at least as long as the sampling distance is fine enough for complete phase information. This can be ensured by using Manipulations >䮤 Sampling Manipulations > Resample According to Spherical Phase first. <br> The concept of the spherical phase radius is explained in Sec. 12.1.1. |
| 奴 ${ }^{W}$ Remove Sampled <br> Spherical Phase | If a spherical phase radius is set, the corresponding spherical phase will be subtracted. For that purpose, the array will be divided by an appropriate spherical phase function (see Eqs. (41.25)-(41.26)). |

### 22.5.1 Modify Phase

Some phase modifying operations can be done via the dialog shown in Fig. 140.


Figure 140. Dialog for phase manipulation operations.
The options are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Constant | Replace or superimpose given constant phase. |
| Lens Transmission | Replace or superimpose lens transmission with the given focal length (see <br> also Sec. 67.5.2). <br> Replace or superimpose spherical phase with given radius (see also <br> Sec. 41.3.7). If you set the spherical phase radius to a value greater than <br> $10^{5}$ m, the harmonic field is set to have no spherical phase radius. |
| Random | Replace phase by random phase. The additional parameters correspond <br> to those of the random phase transmission generator as described in <br> Sec. 67.7 .2. |
| Replace Phase | If selected, the current phase is replaced by the newly created phase. |
| Superimpose Phase | If selected, the newly created phase is superimposed to the current field by <br> multiplying the corresponding complex transmission function. |

### 22.5.2 Set Spherical Phase Radius



Figure 141. Dialog for setting the spherical phase radius.
The dialog for changing the analytical spherical phase radius of a harmonic field ( $\hookrightarrow$ Fig. 141) has the following entries:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Detect Spherical Phase <br> Radius | If this check box is checked, VirtualLab Fusion tries to detect a dominating <br> spherical phase radius in the field. |
| Spherical Phase Radius | If the check box Detect Spherical Phase Radius is unchecked, you can set <br> the radius to a specific value. If you set the spherical phase radius to a value <br> greater than $10^{5} \mathrm{~m}$, the harmonic field is set to have no spherical phase radius. |

Further details about the detection of a spherical phase factor can be found in Sec．137．6．

## 22．6 Lateral Displacement

The ribbon menu Manipulations＞通 Lateral Displacement allows you to do some transformations with regard to the $x$－and $y$－coordinates of the array．

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\Delta \triangle$ Mirror Horizontally | Applies transformation $u(x, y) \rightarrow u(-x, y)$ ，that is the field is mirrored hori－ zontally by a mirror that corresponds to the $y$－axis． |
| $\checkmark$ Mirror Vertically | Applies transformation $u(x, y) \rightarrow u(x,-y)$ ，that is the field is mirrored verti－ cally by a mirror that corresponds to the x－axis． |
| $\triangle$ Rotate in $\mathrm{x}-\mathrm{y}$－Plane | Rotates the field by the given angle（ $¢$ Sec．22．6．1）． |
| 萝 $\ddagger$ Shift | Shifts content of the current field by a given number of sampling points． |
| $\zeta$ Transpose | Applies transformation $u(x, y) \rightarrow u(y, x)$ ，that is the field is mirrored by a mirror that corresponds to a diagonal in the $x-y$－plane． |

## 22．6．1 Rotation in $x-y$－plane

| Rotate Array |  |  | $\times$ |
| :---: | :---: | :---: | :---: |
| Rotation Angle |  | $20^{\circ}$ |  |
| Sampling Points |  | 85 x | 85 |
| Interpolation Method |  |  | $\checkmark$ |
| Suggest Sampling | Ok | Cancel | Help |

Figure 142．Settings for Rotation in $x-y$－Plane．
The dialog shown in Fig． 142 allows you to enter settings for the rotation of complex amplitudes in the $x$－y－plane．

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rotation Angle | Angle by which the field is to be rotated around the z－axis． |
| Sampling Points | Number of sampling points after rotation．The sampling distance of the origi－ <br> nal field is retained． |
| Interpolation Method | Interpolation method to be used（ $\hookrightarrow$ Sec．13．2．2） |

## 22．7 Array Size Manipulations

The ribbon menu Manipulations＞酆 Array Size Manipulations provides the following operations that change the size of an one－or two－dimensional array：

| ITEM | DESCRIPTION |
| :---: | :---: |
| Embed / Extract (Pixel Dimensions) | Changes the number of sampling points. If the number of sampling points is increased then the array is embedded, that means the newly created surrounding sampling points are filled with zero values. Otherwise, i.e. if the number of sampling points is decreased then the new array is extracted. Embedding as well as extracting is done centered. |
| Embed / Extract (Physical Dimensions) | This option works like Embed / Extract (Pixel Dimensions), but the size of the new array is defined in physical units. |
| Embed in Double Sized Array (Center) | This operation corresponds to using Embed / Extract (Pixel Dimensions) with embedding to the double array size. The original array will be centered in the result array. The new sampling points are set to zero. |
| $\square$ Embed in Double Sized Array (Corner) | This operation corresponds to using Embed / Extract (Pixel Dimensions) with embedding to the double array size. But the original array will be the bottom left quadrant in the resulting array. The new sampling points are set to zero. |
| $\square$ Make Hermitian | This operation corresponds to Embed in Double Sized Array (Corner), but in addition the upper right quadrant is filled by the complex conjugate of the original array in order to ensure that the result is Hermitian ( $\lrcorner \mathrm{Sec} .67 .7 .2$ ). |
| \#Replicate Twice | Fill the resulting array by 2 (one-dimensional case) or $2 \times 2$ (two-dimensional case) replications of the original array. This operation is equivalent to use Replicate Periodically with the double array size and a shift of $(0,0)$. |
| 罵Replicate Periodically | This operation is typically used for increasing the number of sampling points to the given array size. The newly created array is filled by periodically replicating the contents of the current one ( $\leftrightarrows$ Sec. 22.7.1). |
| Extract Range Selection / <br> Extract Rectangular Selection | Creates a new array which contains the selected portion of the current array. |
| ${ }^{\text {A }}$ Extract Profile Line | Extracts the one-dimensional cross-section defined by the line marker ( $\leftrightarrows$ Sec. 11.3) to a separate one-dimensional harmonic field ( $\rightarrow$ Sec. 22.7.2). |

### 22.7.1 Replicate Periodically



Figure 143. Dialog for periodic replication.
A new array is created, filled by periodically replicating the contents of the current array. In the dialog ( $\rightarrow$ Fig. 143) the following parameters have to be entered:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Points | Size of the new array (in number of sampling points). |
| Shift | This value indicates which point of the current array is set at the lower left <br> corner of the replicated one. So the value has to lie inside the source array. |

### 22.7.2 Extract Profile Line

The one-dimensional cross section marked by a Profile Line in a two-dimensional array can be extracted using Manipulations > 畵 Array Size Manipulations > Extract Profile Line.


Figure 144. Dialog for extraction of a profile.

The dialog shown in Fig. 144 is used to define the extraction. The following parameters can be entered:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Interpolation | The type of interpolation that shall be used to find the equidistant sampling <br> points of the resulting array if the points on the line in the initial array are not <br> equidistant. |
| Coordinates | Determines whether the Start and End coordinates shall be given in physical <br> units or as the indices of sampling points. |
| Start | Starting point of the line to extract. Initially the start coordinates of the profile <br> line are filled in here. |
| End | End point of the line to extract. Initially the end coordinates of the profile line <br> are filled in here. |
| Number of Sampling | The number of sampling points the resulting array shall contain. |
| Points | If checked and a Spherical Phase Factor is given for the array, it will be re- <br> moved from the phase of the resulting array. |
| Remove Spherical Phase |  |
| Factor | Restores the values which were stored for the last call of this operation, i.e. <br> if the dialog was last closed using OK. With this option you can easily extract <br> the same profile line from various harmonic fields. If these recent values do <br> not fit in the current array, this button is disabled and a warning is shown. |
| Recent Parameters |  |

## 22．8 Sampling Manipulations

The ribbon menu Manipulations＞騳 Sampling Manipulations provides the following operations that change the sampling distance：

| ITEM | DESCRIPTION |
| :---: | :---: |
| 炜 Interpolate | Using this manipulation（ $\hookrightarrow$ Sec．22．8．1），the sampling parameters of an array can be changed，whereby the originally stored physical information shall be preserved．This operation can also be executed by clicking directly on the upper part of the Manipulations＞騸 Sampling Manipulations menu． |
| $\eta_{2_{\pi}}$ Oversample Twice（Ze－ roized） | The number of sampling points is doubled by splitting each sampling point into $2 \times 2$ new points of half the original sampling distance．The new point with the same physical position contains the old complex value，the remaining sampling points are filled with zero． |
| $77^{2}$ Oversample Twice （Sinc FFT Interpolation） | This is equivalent to use Interpolate with the interpolation method Sinc （Fourier Transformation）－interpolation，half the original sampling distance， and a zero point of $(0,0)$ ． |
| $\Gamma_{24}$ Oversample Twice （Nearest Neighbor Inter－ polation） | The number of sampling points is doubled by splitting each sampling point into $2 \times 2$ new points of half the original sampling distance．All new points contain the value of the original sampling point．In this way propagation methods consider the original data as pixelated data． |
| $\Gamma_{3} 4$ Oversample $3 \times$（Near－ est Neighbor Interpola－ tion） | The number of sampling points is tripled by splitting each sampling point into $3 \times 3$ new points of one third the original sampling distance，containing the value of the original sampling point．In this way propagation methods consider the original data as pixelated data． |
| Resample According to Spherical Phase | If a spherical phase radius is set，this option resamples the array in a way that the corresponding spherical phase will be sampled correctly（according to the Whittaker Shannon theorem，see［Goo68］）．In the Optical Setup，this can be done with the ideal component Ideal Components＞Manipulators＞ Sample Spherical Phase Radius． |

## 22．8．1 Interpolation

This operation is available via Manipulations＞騳Sampling Manipulations＞Interpolate． Its edit dialog（ $\hookrightarrow$ Fig．145）has the following settings：

| ITEM | DESCRIPTION |
| :--- | :--- |
| Interpolation Method | The used interpolation method．$\hookrightarrow$ Sec．13．2．2 |
| Sampling Points | The number of sampling points the new array shall contain． |
| Sampling Distance | The sampling distance of the new array． |
| Array Size | The array size of the new array． |
| Copy from．．． | By pressing this button a dialog will appear where another harmonic field can <br> be selected to copy the sampling parameters from． |
| Zero Point | Zero point of the resulting field relative to the zero point of the original array． |
| Document Parameters | Fills the controls according to the sampling parameters of the currently se－ <br> lected array． |



Figure 145. Dialog for adjusting the interpolation settings.
22.8.2 Field Size and Sampling Manipulation in the Optical Setup

| Edit Field Size and Sampling |  |  |  | $\times$ |
| :---: | :---: | :---: | :---: | :---: |
| Geometry / Channels | Preparation of Field Position Before Operator ApplicationKeep Lateral Position and Orientation of FieldBring Field into Operator Plane but Keep Lateral Position of FieldBring Field into Operator Plane and Center to Optical Axis of Operator |  |  |  |
| Position/ Orientation | Change Field Size Scale Field Size by Factor $\square$ <br> 1 Set Field Size |  |  |  |
| Function | Change Field Sampling Scale Sampling Distance by Oversampling Factor Set Sampling Distance Optimize Sampling Distance (Accuracy F | 1 | 1 |  |
|  | Settings <br> Interpolation Method <br> Accelerated Sinc Keep Analytic Parameters Recalculate Analytic Parameters |  |  |  |
|  |  | OK Cancel | Help |  |

Figure 146. The Field Size and Sampling Manipulation dialog.

As you can see in Fig. 146, the Field Size and Sampling Manipulation dialog has four group boxes: Preparation of Field Position Before Operator Application, Change Field Size, Change Field Sampling, and Settings.
Within the region Preparation of Field Position Before Operator Application the user can specify how the incident field position of the Field Size And Sampling operator shall be defined. The has three different options:

- Keep Lateral Position and Orientation of Field
- Bring Field into Operator Plane but Keep Lateral Position of Field
- Bring Field into Operator Plane and Center to Optical Axis of Operator

The meaning of each option is explained within a sketch accessible by clicking on the info label in more detail.

The Change Field Size box has the following entries:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Scale Field Size ${ }^{\text {PV }}$ | The size of the output field is $n$ times larger than of the incoming field. $n$ is a vector to allow different scaling for $x$ - and $y$-direction. |
| Set Field Size ${ }^{[\mathrm{PV}}$ | You can directly set the field size in physical coordinates. |
| Calculate Field Size from Sampling Points ${ }^{[V]}$ | The field size is calculated from the specified number of sampling points ( $x$ and $y$-direction) and the sampling distance of the incoming field. |
| Optimize Field Size (Accuracy Factor) ${ }^{[\mathrm{PV}}$ | The field size is calculated automatically according to the power portion specified in the Global Options dialog ( $\hookrightarrow$ Sec. 6.12). The given accuracy factor enlarges the field by the given factor. |

The Change Field Sampling box has the following entries:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Scale Sampling Distance by Oversampling Factor ${ }^{\text {DV }}$ | The sampling distance in the output field is $n$ times smaller than in the incoming field. $n$ is a vector to allow different sampling for $x$ - and $y$-direction. |
| Set Sampling Distance ${ }^{[\sqrt{V V}}$ | You can directly set the sampling distance for both x - and y -direction. |
| Optimize Sampling Distance (Accuracy Factor) ${ }^{\text {DV }}$ | The sampling distance is calculated automatically. With the accuracy factor you can reduce the sampling distance by the given factor. In this case the Interpolation Method is fixed to Accelerated Sinc Interpolation ( $\varsigma \mathrm{Sec} .13 .2$.2). |

The Settings box has the following entries:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Interpolation Method | The used interpolation method. $\lrcorner$ Sec. 13.2.2. |
| Keep Analytic Parameter | Specify whether analytic parameters like the spherical phase radius are taken |
| Recalculate Analytic $P$ Pa- from the incoming field or calculated anew. <br> rameter  |  |

The remaining controls of this dialog are explained in Sec. 66.

### 22.9 Selection Related Operations

All operations in the ribbon menu Manipulations > 湿 Selection Related Operations affect the selected area of the array only. These are:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Fill Range Selection / Fill Rectangular Selection | Sets the sampling points within the selection to a user-defined complex value c. Keep in mind that for globally polarized fields the new $E_{x}$ values within the selection are $J_{\mathrm{x}} \cdot c$ and the new $E_{y}$ values are $J_{\mathrm{y}} \cdot c$, with $J$ being the Jones vector. |
| x Clear Range Selection / Clear Rectangular Selection | Sets the sampling points within the selection to zero. |
| Clear Inverse of Range Selection / <br> Clear Inverse of Rectangular Selection | Sets the sampling points outside the selection to zero. |
| Extract Range Selection / <br> Extract Rectangular Selection | Creates a new array which contains the selected portion of the current array. |
| Extract Profile Line | Extracts the one-dimensional cross-section defined by the line marker ( $\rightarrow$ Sec. 11.3) to a separate one-dimensional harmonic field ( $\rightarrow$ Sec. 22.7.2). |
| 迹 Normalize According to Range Selection / Normalize According to Rectangular Selection | Normalizes the current array by dividing it (at all sampling points) by the maximum amplitude within the current selection. |
| Remove Phase Dislocations in Rectangular Selection | Phase dislocations ( $\leftrightarrows$ Sec. 67.8.2) are searched and tried to be removed in the current selection. For removing a certain phase dislocation with charge $c$ ( $\leftrightarrows$ Sec. 67.8.2), a transmission of a phase dislocation with charge $-c$ is multiplied to the array at the same position. This operation is repeated for all phase dislocations which were found within the current selection. |
| Create Signal Region from Selection | This item creates a region document ( $\leftrightarrows$ Sec. 21). The result will be a sampled region which has the same sampling parameters as the current harmonic field or Jones matrix transmission document. The selected range or rectangle marker will define the actual signal region, independent of the values inside the original selection. |

### 22.10 Polarization Change

All operations in the ribbon menu Manipulations > 做 Polarization Change affect somehow the Jones Vector $J$ of a globally polarized field ( $\leftrightarrows$ Sec. 131.1).

## ITEM

DESCRIPTION
Convert to Locally Polar- Converts the current globally polarized field to the more general type of a ized Field locally polarized one corresponding to

$$
\begin{align*}
& E_{x}(x, y)=J_{x} U(x, y)  \tag{22.2}\\
& E_{y}(x, y)=J_{y} U(x, y) . \tag{22.3}
\end{align*}
$$

| Split into Globally Polarized Fields | Splits a locally polarized field into two globally polarized fields which correspond to the $E_{x}$ and the $E_{y}$ component of the original field. The new Jones vectors are $(1,0)^{T}$ and $(0,1)^{T}$. This option can be used to reduce memory and time consumption if you have a locally polarized field with negligible $E_{y}$ field <br> (e.g. after geometric optics propagation with Fresnel effects considered). |
| :---: | :---: |
| W Change Jones Vector | Opens a dialog ( $\hookrightarrow$ Fig. 147) which allows you to set the Jones Vector. The controls of this dialog are the same as for setting the Jones vector of a newly generated field, $\leftrightarrows \mathrm{Sec} .48 .3$. This operation can also be done via the (Current) Data tab of the property browser ( $\rightarrow$ Fig. 148). |
| General | A general Jones Matrix Multiplication ( $\leftrightarrows$ Sec. 22.10.1). Its edit dialog is explained in Sec. 22.10.1.1. |
| Linear Polarization | A Jones Matrix Multiplication ( $\neg$ Sec. 22.10.1) describing a linear polarization. Its edit dialog is explained in Sec. 22.10.1.2. |
| Phase Shift | A Jones Matrix Multiplication ( $\varsigma$ Sec. 22.10.1) describing a phase shift. Its edit dialog is described in Sec. 22.10.1.3. |
| Retardation | A Jones Matrix Multiplication ( $\leftrightarrows$ Sec. 22.10.1) describing a retardation. Its edit dialog is described in Sec. 22.10.1.4. |
| Rotation | A Jones Matrix Multiplication ( $\leftrightarrows$ Sec. 22.10.1) describing a rotation. Its edit dialog is described in Sec. 22.10.1.5. |

## Application on Harmonic Fields Sets

For a Harmonic Fields Sets these manipulations are applied separately on each member field. The resulting fields are then combined into a new Harmonic Fields Sets (two for Split into Globally Polarized Fields).
Note that a Harmonic Fields set can contain both globally and locally polarized fields. In this case both Convert to [Pure] Locally Polarized Field and Split into [Pure] Globally Polarized Fields are available.


Figure 147. Dialog used to edit the Jones vector.


Figure 148. How to edit the Jones vector via the property browser.

### 22.10.1 Jones Matrix Multiplication

Some optical elements and devices influence the polarization state of light. Mathematically this process can be described by a change of the electric field vector by a matrix, called Jones matrix $\mathcal{J}$

$$
\begin{equation*}
E_{\mathrm{xy}}^{\text {out }}=\mathcal{J} \cdot E_{\mathrm{xy}}^{\text {in }} \tag{22.4}
\end{equation*}
$$

For globally polarized fields, this means a change of the Jones vector:

$$
\begin{equation*}
J_{\text {out }}=\mathcal{J} \cdot J_{\text {in }} . \tag{22.5}
\end{equation*}
$$

Since Transmissions contain their own Jones matrix $\mathcal{J}^{(T)}$, the effect of a Jones Matrix Multiplication can be "added" to the transmission by applying former to the latter, which corresponds to the mathematical operation

$$
\begin{equation*}
\mathcal{J}_{\text {out }}^{(T)}=\mathcal{J} \cdot \mathcal{J}_{\text {in }}^{(T)} . \tag{22.6}
\end{equation*}
$$

For your convenience, the four important cases of Linear Polarization, Phase Shift, Retardation, and Rotation are implemented as separate manipulations in VirtualLab Fusion (described in the following sections Sec. 22.10.1.2 to Sec. 22.10.1.5). That means, the user does not have to enter the Jones matrix but only one single parameter describing the appropriate physical effect. For other cases a General Jones matrix can be defined ( $\hookrightarrow$ Sec. 22.10.1.1).

### 22.10.1.1 General

For the multiplication of an arbitrary Jones matrix this manipulation is used.


Figure 149. Controls for defining the parameters of an arbitrary Jones matrix multiplication.

The following parameters are available for a General Jones Matrix Multiplication ( $\hookrightarrow$ Fig. 149):

ITEM
DESCRIPTION

| Jones Matrix | Matrix with four complex entries. |
| :--- | :--- |
| Representation | Representation of the complex values in the Jones matrix. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

### 22.10.1.2 Linear Polarization

A linear polarizer is a kind of optical filter that will pass only that part of $E_{x y}$ which oscillates in a certain direction. If this direction is given by an angle $\alpha$, the corresponding Jones matrix is given by

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos ^{2} \alpha & \sin \alpha \cos \alpha  \tag{22.7}\\
\sin \alpha \cos \alpha & \sin ^{2} \alpha
\end{array}\right)
$$



Figure 150. Controls for defining the parameters of a linearly polarizing Jones matrix multiplication.
The following parameters are available for a Linear Polarization function ( $\hookrightarrow$ Fig. 150):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Polarization Angle | The angle of the plane of polarization of the filtered, linearly polarized light. |
| Type | Here you can select one of the two special cases Along x Direction, which <br> corresponds to a polarization angle of $\alpha=0^{\circ}$, which means that the compo- <br> nent $E_{y}$ is set to 0, or Along y Direction, which corresponds to a polarization <br> angle of $\alpha=90^{\circ}$, which means that the component $E_{x}$ is set to 0. The case of <br> an arbitrary polarization angle is called General. |
| Jones Matrix | The resulting Jones matrix that describes the linear polarization. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |

### 22.10.1.3 Phase Shift

A Phase Shift adds a phase difference $\phi$ to both $E_{x}$ and $E_{y}$. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
\exp (i \phi) & 0  \tag{22.8}\\
0 & \exp (i \phi)
\end{array}\right)
$$



Figure 151. Controls for defining the parameters of a Phase Shift.
The following parameters are available for a Phase Shift function ( $\hookrightarrow$ Fig. 151):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Phase Shift | The phase shift $\phi$ for both $E_{x}$ and $E_{y}$. |
| Jones Matrix | The resulting Jones matrix that describes the phase shift. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

### 22.10.1.4 Retardation

Retarders as e.g. quarter-wave plates or half-wave plates "retard" $E_{y}$ against $E_{x}$ by a phase difference $\phi$. Thereby linearly polarized light can be transformed into circularly polarized and vice versa, for example. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
1 & 0  \tag{22.9}\\
0 & \exp (-i \phi)
\end{array}\right)
$$

| Parameters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase Delay | 0 rad | Type | General | $\checkmark$ |
| Jones Matrix |  |  |  |  |
| $\left(\begin{array}{ll}J_{x x} & J_{x y} \\ \\ J y x & J_{y y}\end{array}\right)=($ | $\begin{array}{ll}1+ \\ 0 & +\end{array}$ |  | $0+$ $1+$ | $\left.\begin{array}{l}0 i \\ 0 i\end{array}\right)$ |
|  |  |  | $\checkmark$ Hermitian Matrix | $\checkmark$ Unitary Matrix |

Figure 152. Controls for defining the parameters of a Jones matrix retardation.
The following parameters are available for a Retardation function ( $\hookrightarrow$ Fig. 152):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Phase Delay | The phase shift $E_{y}$ shall get. |
| Type | Here you can select one of the two important special cases Quarter-Wave <br>  <br> Retarder, which corresponds to a phase delay of $\pi / 2$, used for transforming <br> linearly polarized light to circularly polarized and vice versa, or Quarter-Wave <br>  <br> Retarder, which corresponds to a phase delay of $\pi$, used for transforming <br> right-circularly polarized light into left-circularly and vice versa. The case of <br> an arbitrary phase delay is called General. |
| Jones Matrix | The resulting Jones matrix that describes the retardation. <br> Hermitian Matrix |
| Indicates whether the matrix is Hermitian. |  |

### 22.10.1.5 Rotation

The angle of rotation $\theta$ of the plane of polarization determines the Jones matrix as follows

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos \theta & -\sin \theta  \tag{22.10}\\
\sin \theta & \cos \theta
\end{array}\right)
$$



Figure 153. Controls for defining the parameters of a Jones matrix rotation.
The following parameters are available for a phase rotation function ( $\hookrightarrow$ Fig. 153):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rotation Angle | The angle by which the plane of polarization shall be rotated. |
| Jones Matrix | The resulting Jones matrix that describes the rotation of the plane of polar- <br> ization. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

### 22.11 Miscellaneous

The ribbon menu Manipulations $>$ Miscellaneous contains various special manipulations e.g. to introduce discrete value levels.

### 22.11.1 Resample to Angular Coordinates

This manipulation converts a given Harmonic Field into a Data Array with angular coordinates. To this end for a spatial field first a Fourier transform is done.
to Angular Coordinates.pdf to Angular Coordinates.png to Angular Coordinates.eps
Figure 154. Options for resampling a harmonic field to angular coordinates.

The edit dialog ( $\hookrightarrow$ Fig. 154) for this manipulation has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Components | Allows you to select any combination of $E_{x}, E_{y}$ and $E_{z}$. |
| Coordinate Type | Whether you want to use Cartesian Angles or Spherical Angles. |
| Oversampling Factors | By default a good automatic sampling is used. However you can create more <br> sampling points for Alpha and Beta or Phi and Theta, respectively, by increas- <br> ing the oversampling factors. |

### 22.11.2 Hard Quantization

The menu item Manipulations > Quantization > Hard Quantization opens a dialog which allows you to enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively.
The quantization is performed independently for amplitude and phase. For each position $(x, y)$ the original field value $u(x, y)=A \exp [i \phi]$ is replaced by $A^{\prime} \exp \left[i \phi^{\prime}\right]$, where

$$
A^{\prime}= \begin{cases}A & \text { if } q=0  \tag{22.11}\\ A_{\max } & \text { if } q=1 \\ \frac{A_{\max }}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\text {max }}}\right\rceil & \text { otherwise }\end{cases}
$$

(where $\lfloor\cdot\rceil$ denotes the rounding-to-nearest-integer operation) and

$$
\phi^{\prime}= \begin{cases}\phi & \text { if } Q=0  \tag{22.12}\\ \frac{2 \pi}{Q} \cdot\left\lfloor\frac{Q(\phi+\pi)}{2 \pi}\right\rceil-\pi & \text { otherwise }\end{cases}
$$

$A_{\text {max }}$ is the maximum amplitude within the input field. Compared to the definition of the phase quantization operator $\Pi_{\text {quant, } Q}$ used during IFTA optimization ( $\hookrightarrow$ Sec. 97), which corresponds to the case of $q=1$, the definition given in this section allows simultaneous amplitude and phase quantization. Furthermore, the special cases for $q=0$ and $Q=0$ have been included for maintaining the original amplitude and phase, respectively. In cases of $q=1$ the amplitude is set to one. If $Q=1$, the resulting field has a zero phase.

### 22.11.3 Soft Quantization

The menu item Manipulations > Quantization > Soft Quantization opens a dialog which allows you to enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively. Furthermore a projection strength $\lambda$ can be entered.
The quantization is performed independently for amplitude and phase. For each position $(x, y)$ the original field value $u(x, y)=A \exp [i \phi]$ is replaced by $A^{\prime} \exp \left[i \phi^{\prime}\right]$. The amplitude $A^{\prime}$ is obtained by

$$
A^{\prime}= \begin{cases}A & \text { if } q=0  \tag{22.13}\\ A_{\max } & \text { if } q=1 \wedge C_{1}=\text { true } \\ \frac{A_{\max }}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\max }}\right\rceil & \text { if } q>1 \wedge C_{2}=\text { true } \\ A & \text { otherwise }\end{cases}
$$

with the Boolean terms

$$
\begin{align*}
& C_{1}=\left(\left|\frac{A}{A_{\max }}-1\right| \geq 0.5 \lambda\right)  \tag{22.14}\\
& C_{2}=\left(\left|\frac{A}{A_{\max }}-\frac{1}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\max }}\right\rceil\right| \geq \frac{\lambda}{2(q-1)}\right) \tag{22.15}
\end{align*}
$$

The phase $\phi^{\prime}$ is calculated from

$$
\phi^{\prime}= \begin{cases}\phi & \text { if } Q=0 \vee C_{3}=\text { true }  \tag{22.16}\\ \frac{2 \pi}{Q} \cdot\left\lfloor\frac{Q(\phi+\pi)}{2 \pi}\right\rceil-\pi & \text { otherwise }\end{cases}
$$

with the Boolean term

$$
\begin{equation*}
C_{3}=\left(Q>0 \wedge\left|\phi-\frac{2 \pi}{Q} \cdot\lfloor Q /(2 \pi) \phi\rceil\right|>\lambda \pi / Q\right) \tag{22.17}
\end{equation*}
$$

$A_{\max }$ is the maximum amplitude within the complex amplitude field.
Compared to the definition of the phase quantization operator $\Pi_{\text {softquant, },}^{\lambda}$ used during IFTA optimization ( $\hookrightarrow$ Sec. 97), which corresponds to the case of $q=1$, the definition given in this section allows for simultaneous amplitude and phase quantization. Furthermore, the special cases for $q=0$ and $Q=0$ have been included for maintaining the original amplitude and phase, respectively. If $Q=1$, the resulting field has a zero phase.

### 22.11.4 Floyd-Steinberg Quantization

The menu item Manipulations > Quantization > Floyd-Steinberg Quantization opens a dialog which allows you to enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively.
The result of the Floyd-Steinberg quantization contains only field values from the set

$$
\begin{equation*}
M_{(q, Q)}=\left\{A \exp [i \phi]: A \in M_{q} \wedge \exp [i \phi] \in M_{Q}\right\} \tag{22.18}
\end{equation*}
$$

where the sets $M_{q}$ and $M_{Q}$ are given by

$$
\begin{equation*}
M_{q}=\left\{\frac{j A_{\max }}{q-1}: j=0 \ldots q-1\right\} \tag{22.19}
\end{equation*}
$$

and

$$
\begin{equation*}
M_{Q}=\left\{\exp \left[-i \pi\left(-1+\frac{2 \pi j}{Q}\right)\right]: j=0,1, \ldots, Q-1\right\} . \tag{22.20}
\end{equation*}
$$

$A_{\text {max }}$ is the maximum amplitude within the complex amplitude field.
In contrast to the quantization types described in the previous two sections, the Floyd-Steinberg quantization is not a pointwise operation. That is, the quantization result at a position $(x, y)$ does not depend only on the field value $u(x, y)$ but also on the field values on neighboring positions. The basic idea of the Floyd-Steinberg quantization is to distribute the error, which was made by the quantization at a certain position, to the neighboring positions.
During the application of the Floyd-Steinberg quantization an iteration through all field positions is performed row by row, whereby within each row positions are considered consecutively from left to right. At a considered position $(x, y)$ firstly a hard quantization is performed ( $\leftrightarrows$ Sec. 22.11.2). After that the quantization error is calculated from the difference between $u(x, y)$ and the obtained quantization value.
This difference is spread using the weighting factors shown in Fig. 155 to four neighboring positions, which are considered in following iterations.


Figure 155. Weighting factors for distribution of quantization errors to neighboring positions during Floyd-Steinberg quantization.

### 22.12 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

### 22.13 Fourier Transform

For a detailed discussion of Fourier transforms $\hookrightarrow$ Sec. 31 .

## 23 Manipulations of Harmonic Fields Sets

Harmonic Fields Sets support the following manipulations.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\sum_{g}$ Indexwise Addition | The current and the last active Harmonic Fields Set can be summed in－ dexwise．That means simply to add their member harmonic fields with the same index respectively．So the fields of the result set are calculated by $u_{\text {new }, i}=u_{1, i}+u_{2, i}$ ．If one of the initial fields sets has more members than the other one，the surplus fields are just appended．This operation can also be done with the + key． |
| 忛 Remove Sampled <br> Spherical Phases | If a spherical phase radius is set for any member field，the corresponding spherical phase will be subtracted．For that purpose，the member field will be divided by an appropriate spherical phase function（see Eqs．（41．25）－（41．26））． |
| 䤖 Sampling Manipula－ tions | Provides operations that change the sampling distance of all member fields． $\hookrightarrow$ Sec．23．1． |
| 玲 Extraction Tools | These tools can be used to extract partial information from a Harmonic Fields Set．$\leftrightarrows$ Sec． 23.2 |
| 46）Polarization Change | Either converts all member fields to globally or locally polarized ones or ap－ plies a Jones Matrix Multiplication on each member field．（ $\hookrightarrow$ Sec．22．10） |

The ribbon group Manipulations＞Member Harmonic Fields is explained in Sec．23．3，the ribbon group Manip－ ulations＞Conversions in Sec．30．2，and the ribbon group Manipulations＞Fourier Transformation（Space）in Sec．31．1．

## 23．1 Sampling Manipulations

The ribbon menu Manipulations＞驩 Sampling Manipulations provides the following operations that change the sampling distance of all member fields：

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\mathfrak{F F i}^{2}$ Oversample Twice （Sinc FFT Interpolation） | Uses the interpolation method Sinc（Fourier Transformation）（ $\leftrightarrows$ Sec．13．2．2） to halve the original sampling distance of each member field． |
| Resample According to Spherical Phase | If a spherical phase radius is set for a member field，this option resamples the field in a way that the corresponding spherical phase will be sampled correctly（according to the Whittaker Shannon theorem，see［Goo68］）．In the Optical Setup，this can be done with the ideal component Ideal Components ＞Manipulators＞Sample Spherical Phase Radius． |

## 23．2 Extraction Tools

The following tools can be used to extract partial information from a Harmonic Fields Set．

| ITEM | DESCRIPTION |
| :--- | :--- |
| Point Profile Extraction | Extracts the complex value on a user-defined position and plots this value <br> versus the index or the wavelength of each Harmonic Fields Set member. <br>  <br> $\hookrightarrow$ Sec. 23.2 .1 |
| Line Profile Extraction | Extracts the complex values along a user-defined line and plots these values <br> versus the index or the wavelength of each Harmonic Fields Set member. <br> $\hookrightarrow$ Sec. 23.2.2 |
| Rectangle Extraction | Converts the Harmonic Fields Set into a Field Vector Component (member <br> fields versus field index) or into a Pulse Component (member fields versus <br> wavelength). $\hookrightarrow$ Sec. 23.2 .3 |

### 23.2.1 Point Profile Extraction

The Point Profile Extraction extracts the complex value on a user-defined position and plots this value versus the index or the wavelength of each Harmonic Fields Set member.
Fig. 156 shows the edit dialog of the Point Profile Extraction tool.

| Settings Point Profile Extraction |  |  |  |
| :---: | :---: | :---: | :---: |
| Extraction Parameters |  |  |  |
| Detect At (x,y) | $0 \mathrm{~mm} \times$ | 0 mm | Copy From |
| Vectorial Component | Ex Component |  |  |
| Evaluation ParametersEvaluate Field Data over Field IndexEvaluate Field Data over Wavelength |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  | Ok | Cancel | Help |

Figure 156. Edit dialog for the Point Profile Extraction tool.

The following parameters can be specified by the user:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Detect At ( $\mathbf{x , y}$ ) | The position from which the data shall be extracted. Initially, the current cross <br> position is set. The button Copy From can be used to copy the cross position <br> from a present Harmonic Fields Set in VirtualLab Fusion. |
| Vectorial Component | The vectorial component (Ex Component, Ey Component, or Ez Component) <br> to be evaluated by the evaluation tool. |
| Evaluate Field Data over | Defines whether the complex value shall be shown in dependency on the <br> index in the Harmonic Fields Set. |
| Field Index | Defines whether the complex value shall be shown in dependency on the <br> wavelength of each Harmonic Field. This option is only available if each |
| Wavelength | wavelength in the Harmonic Fields Set is unique. |

The resulting diagram contains the complex value in dependence on the user-defined independent variable (index or wavelength). This diagram supports to switch between the different field quantities. More details can be found in Sec. 15.
Fig. 157 shows a sample output of the Point Profile Extraction.


Figure 157. Sample result of a Point Profile Extraction.

### 23.2.2 Line Profile Extraction

The Line Profile Extraction extracts the complex values along a user-defined line and plots these values versus the index or the wavelength of each Harmonic Fields Set member.
Fig. 158 shows the edit dialog of the Line Profile Extraction tool.


Figure 158. Edit dialog for the Line Profile Extraction tool.

The following parameters can be configured in the edit dialog.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Start At ( $\mathbf{x}, \mathbf{y}$ ) | The start position of the line to be extracted. Initially, the start position of <br> the current profile line is set. The button Copy From can be used to copy <br> the starting point of the line from a present Harmonic Fields Set in VirtualLab <br> Fusion. |
| End At ( $\mathbf{x}, \mathbf{y} \mathbf{y}$ | The end position of the line to be extracted. Initially, the end position of the <br> current profile line is set. The button Copy From can be used to copy the end <br> point of the line from a present Harmonic Fields Set in VirtualLab Fusion. |
| Vectorial Component | The vectorial component (Ex Component, Ey Component, or Ez Component) <br> to be evaluated by the evaluation tool. |
| Evaluate Field Data over <br> Field Index | Defines whether the complex value shall be shown in dependency on the <br> index in the Harmonic Fields Set. |
| Evaluate Field Data over | Defines whether the complex value shall be shown in dependency on the <br> wavelength of each Harmonic Field. This option is only available if each <br> wavelength in the Harmonic Fields Set is unique. |

The resulting diagram contains the complex value in dependence on the user defined independent variable (index or wavelength). This diagram supports to switch between the different field quantities. More details can be found in Sec. 15.

### 23.2.3 Rectangle Extraction

The Rectangle Extraction converts the Harmonic Fields Set into a Field Vector Component (member fields versus field index) or into a Pulse Component (member fields versus wavelength).
Fig. 159 shows the edit dialog of the Rectangle Extraction tool.


Figure 159. Edit dialog for the Rectangle Extraction tool.

The following parameters can be configured in the edit dialog.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Center Point | The user can specify the center point of the rectangle which should be eval- <br> uated. |
| Size | The size of the rectangle which should be extracted. The button Copy From <br> can be used to copy the Center Point and the Size of the rectangle from a <br> present Harmonic Fields Set in VirtualLab Fusion. |
| Resolution | The user can select whether he like to specify the resolution or the sampling <br> points of the rectangle which should be generated by the tool. |
| Sampling Points | The user can select whether he like to specify the resolution or the sampling <br> points of the rectangle which should be generated by the tool. |
| Vectorial Component | The vectorial component (Ex Component, Ey Component, or Ez Component) <br> to be evaluated by the evaluation tool. |
| Evaluate Field Data over | Defines whether the complex value shall be shown in dependency on the <br> index in the Harmonic Fields Set. |
| Field Index | Defines whether the complex value shall be shown in dependency on the <br> wavelength of each Harmonic Field. This option is only available if each <br> wavelength in the Harmonic Fields Set is unique. |
| Evaluate Field Data over |  |
| Wavelength |  |

The resulting document ( $\hookrightarrow$ Sec. 15) contains the complex values in dependence on the user defined independent variable (index or wavelength). It supports to switch between the different field quantities.

### 23.3 Accessing the Members of a Harmonic Fields Set

The ribbon group Manipulations > Member Harmonic Fields contains the following items to access the member fields of the current Harmonic Fields Set.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Append Field | Appends either the selected Harmonic Field or all members of the selected <br> Harmonic Fields Set to the current Harmonic Fields Set as last element(s). <br>  <br> Note that parameters must be suitable as mentioned below. The dialog is <br> shown in Fig. 160. |
| Inserts either the selected Harmonic Field or all members of the selected |  |
| Harmonic Fields Set to the current Harmonic Fields Set at the given Index. |  |
| Note that parameters must be suitable as mentioned below. The dialog is |  |
| shown in Fig. 161. |  |

All members of a Harmonic Fields Set must

- be all either in spatial or in spectral domain ( $\leftrightarrows$ Sec. 31.1),
- all propagate in either positive or negative z-direction ( $\hookrightarrow$ Sec. 131.3), and
- be all either one or two-dimensional.

The embedding material of the harmonic fields set is determined from the very first member field added to a harmonic fields set.


Figure 160. Dialog for appending a field.


Figure 161. Dialog for inserting a field.


Figure 162. Dialog for replacing a field.

| Delete Harmonic Field |  |
| :--- | ---: |
| Index of Harmonic Field | $1-1$ |
|  | $\square$ Ok |
|  |  |
|  |  |

Figure 163. Dialog for deleting a field.


Figure 164. Dialog for extracting a field.

### 23.4 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

### 23.5 Fourier Transform

For a detailed discussion of Fourier transforms $\hookrightarrow$ Sec. 31 .

## 24 Manipulations of Data Arrays

### 24.1 Manipulations for Different Types of Data Arrays

There are very different kinds of manipulations for the different types of Data Arrays available. The most important distinctions which can be made regarding Data Arrays are with reference to:

- the dimensions of the coordinates (usually 1D vs. 2D),
- complex-valued data vs. real-valued data,
- the regularity of the value distribution (equidistant vs. non-equidistant [but gridded] vs. non-gridded [i.e. "gridless"]),
- the physical meaning of the object (e.g. Numerical Data Array vs. Electric Field vs. Magnetic Field, etc.).

For more details about these properties please see Sec. 13.

### 24.1.1 Distinction of 1D vs. 2D

Whether or not a specific manipulation is available for 1D or 2D data is indicated in each of the sections which describe the manipulations and conversions.

### 24.1.2 Distinction of Complex-Valued Data vs. Real-Valued Data

Whether or not a specific manipulation is available for complex-valued or real-valued data is indicated in each of the sections which describe the manipulations and conversions.

### 24.1.3 Regularity of Value Distribution

Whether or not a specific manipulation is available for equidistant or non-equidistant (but gridded) data is indicated in each of the sections which describe the manipulations and conversions.
For gridless data only a few operations are available: Manipulations > 壆 Selection Related Operations > A Extract 1D Data Along Selected Line ( $\hookrightarrow$ Sec. 24.12) and Manipulations > 苗 Lateral Displacement > ! Transpose ( $\hookrightarrow$ Sec. 24.11).

### 24.1.4 Distinction With Respect to the Physical Meaning of a Data Array / Using the Expert Mode

Numerical Data Arrays are predestined objects for arbitrary manipulations because they lack any fixed physical meaning but are mere data containers ( $\hookrightarrow$ Sec. 13.1). So one does not have to care whether a desired operation makes sense in a physical way and if it will be possible.
On the other hand, Data Arrays with a specific physical meaning provide only those manipulations which make sense in the specific physical context.
Consequentially, the full spectrum of manipulations and conversions are available for Numerical Data Arrays only.
If you want to manipulate a physical object in a kind not directly available to the given type of object anyway, there are two ways to achieve that:

- Either the object is converted to a Numerical Data Array first ( $\hookrightarrow$ Sec. 30.1.1),
- or the Expert Mode is activated first: Manipulations > Expert. This will enable all operations.


### 24.2 Handling of Subsets

Many manipulations can be done either for the Current Subset or for All Subsets. In this case the corresponding ribbon item is kind of a menu with said two entries. However, if you click directly on the ribbon item, this manipulation is invoked directly for the current subset.

### 24.3 Manipulate a Data Copy or the Original Data?

For each single manipulation of a Numerical Data Array object one can decide whether or not this operation shall create a new object and leave the source object unchanged. This decision is requested via the dialog shown in Fig. 165.


Figure 165. Dialog asking whether or not a Numerical Data Array manipulation shall operate on a duplicate.
The dialog will appear every time a manipulation is called, unless Don't ask again for any manipulation of 1D/2D Numerical Data Arrays. has been checked eventually. In this case, the last choice will be remembered and used for any manipulation of a Numerical Data Array of the same dimension (either 1D or 2D).
If a stored duplication setting has to be changed, this can be done via the Global Options Dialog as described in Sec. 6.16.

### 24.4 Editing the Coordinate and Interpolation Settings

The ribbon item Manipulations >始位Coordinate and Interpolation Settings allows to edit the coordinate range(s), to change the meaning of the coordinates, and to switch between the interpolation methods as well. These settings can be done via the dialog shown in Fig. 166.


Figure 166. Dialog for changing the coordinate and interpolation settings of an equidistantly sampled, two-dimensional Numerical Data Array.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Description | The caption of the coordinate axis, i. e. the name or meaning of the coordi- <br> nate. |
| Physical Property | The physical property (e.g. Length) of the coordinates. An overview of all <br> supported physical properties and the corresponding units is given in Sec. 5.1. |
| Interpolation Method | The type of interpolation which is used if a value between adjacent sampling <br> points has to be interpolated. The available interpolation methods are ex- <br> plained in Sec. 13.2. |


| Dimensions | The dimensions along the axis can be determined either via Sampling Distance, Array Size, or Coordinate Extent. |
| :---: | :---: |
| Sampling Distance | For equidistantly sampled data, the distance $\Delta x$ or $\Delta y$ between two adjacent coordinates. Important: Changing this value will not result in a resampled Numerical Data Array. This can be done by the resampling operation though, described in Sec. 24.13.1. |
| Array Size | The distance between the coordinates of the first and the last data point. |
| Coordinate Extent | Available only if the Interpolation Method is set to Nearest NeighBOR. <br> The distance between the lower boundary of the nearest neighbor interval of the first data point and the upper boundary of the interval of the last data point. |
| Positioning | The position of the axis can be determined either via entering a Start Coordinate or by defining that the axis range shall be centered. This can be done referring to the exact center (Center Around Zero) or to the coordinate of the data point which has the next higher coordinate to the exact center (Center Around Zero Node). |
| Center Around Zero | If chosen, the coordinate range will be centered around 0 . |
| Center Around Zero Node | For an odd number of sampling points, this will be the same as CenterAround Zero. If chosen for an even number $N$ of sampling points, the coordinate range will be set in the following way: That sampling point whose (zero based!) index equals $N / 2$ will get the coordinate 0 . |
| Start Coordinate | The coordinate of the first sampling point. |
| Equals minimum boundary of first interval | Available only if the Positioning mode is set to Sampling Distance and the interpolation Method is set to Nearest Neighbor. <br> If checked, the start coordinate refers to the lower boundary of the nearest neighbor interval of the first data point instead of the coordinate of the first data point itself. |
| Upper Boundary of Last Interval | Available only for non-equidistantly sampled data. <br> This value defines the upper boundary coordinate of the last interval ( $\rightarrow$ Sec. 13.2.1). |
| Extrapolation Mode | In certain circumstances, it is possible that a Data Array has to deliver values outside its genuine coordinate range. The following options can be set for Extrapolation Mode: Outside Values are: <br> - Equal to the Nearest Border Data Point: A constant extrapolation of the outmost data points is done. <br> - Zero: All outlying points are considered to be of value 0 . <br> - Constant with Value: All outlying points are considered to be of a value to be specified. <br> - Periodically Continued: The whole data of the data array are periodically continued, using a period of the array's 'coordinate extent'. |

This button allows to copy settings from another Numerical Data Array as described in $\hookrightarrow$ Sec. 24.4.1.

### 24.4.1 Copy of Coordinate and Interpolation Settings

If the coordinate and interpolation parameters of one Numerical Data Array shall be copied to another one, this can be done by using the button 首.


Figure 167. Dialog for copying the coordinate and interpolation settings of another Numerical Data Array.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Data Array to Copy from | The Numerical Data Array to be copied from can be chosen here. |
| Settings to Copy | Which of the parameters shall be copied are to be specified. |

### 24.5 Editing Subsets

The list of subsets of a Numerical Data Array can be edited as well as some of the subsets' parameters themselves.

### 24.5.1 Change Subset Parameters

Some subset specific parameters can be edited via the dialog shown in Fig. 168.

| Change Subset Parameters |
| :--- |
| Subset \# Description Physical Property Precision <br> 1 Measurement \#1  Absorption Coefficient <br> 2 Error \#1 Percentage Double Precision <br> 3 Measurement \#2 Absorption Coefficient Double Precision <br>   OK Cancele Precision |

Figure 168. Dialog for editing the subset specific parameters.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Description | The name or meaning of the respective subset. |
| Physical Property | The kind of physical quantity of the respective subset's data. |

### 24.5.2 Append Subset(s) from Another Data Array

At first, another Numerical Data Array (the source array) has to be selected for copying the subsets from. This may be the object to be manipulated (the target array) itself. Then, the subsets to be copied and appended can be chosen in the dialog shown in Fig. 169.


Figure 169. Dialog for selecting the subsets to be appended.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subsets for Appending | The subsets to be appended can be chosen here by name. |
| Selection Tools $>$ Select | This tool will mark all subsets as selected at once. |
| All |  |
| Selection Tools $>$ Unse- <br> lect All | This tool will mark all subsets as not selected at once. |

If the coordinates of the data points in the source array are not identical to that in the target array, the user may choose between two options as described in Sec. 24.6.2.

### 24.5.3 Delete Subset(s)

The subsets to be removed can be chosen in the dialog shown in Fig. 170.


Figure 170. Dialog for selecting the subsets to be removed.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subsets for Removing | The subsets to be removed can be chosen here by name. |
| Selection Tools $>$ Select | This tool will mark all subsets as selected, except the currently shown. |
| All but Current |  |
| Selection Tools $>$ <br> lect All |  |

### 24.5.4 Extract Subset(s)

The subsets to be extracted can be chosen in a similar dialog as shown in Fig. 170.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subsets for Extracting | The subsets to be extracted can be chosen here by name. |
| Selection Tools $>$ Select <br> All but Current | This tool will mark all subsets as selected, except the currently shown. |
| Selection Tools $>$ Unse- <br> lect All | This tool will mark all subsets as not selected at once. |

### 24.5.5 Sum all Subsets

This operation will calculate the sum of all contained subsets. If the data are complex, the user can choose whether to do a complex addition or to do a real-valued addition of one of the field quantities.

### 24.6 Array-Array Operations

 are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subtraction | Calculates the sum of two Numerical Data Arrays. |
| Multiplication | Calculates the difference of two Numerical Data Arrays. |
| Division | Calculates the product of two Numerical Data Arrays. |
| Convolution | Calculates the quotient of two Numerical Data Arrays. |
|  | Calculates the convolution $A_{1} \star A_{2}=\mathcal{F}^{-1}\left[\left(\mathcal{F} A_{1}\right) \cdot\left(\mathcal{F} A_{2}\right)\right]$ of two Numerical |
|  | Data Arrays $A_{1}$ and $A_{2}$. |

The operations Addition, Subtraction, Multiplication, and Division can also be invoked by using the corresponding keys: $\square, \square, *$, and $\boxed{\square}$, respectively. In this case the currently selected document is taken as the second operand while the previously selected Numerical Data Array is taken as first operand.

### 24.6.1 Handling Multiple Subsets

Numerical Data Arrays may contain more than one subset. Table 24.3 shows the behavior of the array-array operations for all possible cases of subset numbers.

| No. of subsets $m$ <br> in 1st operand |  | No. of subsets $n$ in 2nd operand <br> $n=1$ |  | $n>1$ |
| :---: | :---: | :---: | :---: | :---: | | $m=1$ | $s_{1} \circ s_{2}$ | User query |
| :---: | :---: | :---: |
| $m>1$ | User query | $n=m: s_{1} \circ s_{2}$ <br> $n \neq m:$ Error |

Table 24.3: Array-Array Operation modes depending on the respective numbers of subsets.

The expression $s_{1} \circ s_{2}$ means that the desired operation simply will be done on the corresponding subsets of the Data Arrays $A_{1}$ and $A_{2}$. User query stands for a dialog which asks the user how to proceed (Fig. 171).


Figure 171. Dialog which asks the user how to operate if one of the operands contains more than one subset.
The user may decide whether the single subset of the operand $A_{1}$ shall be processed with all $N$ subsets of the other operand $A_{2}\left(s_{1} \circ s_{2}^{(1)}, s_{1} \circ s_{2}^{(2)}, \ldots, s_{1} \circ s_{2}^{(N)}\right)$ or just with the currently visible subset $i$ of the operand with more than one subset $\left(s_{1} \circ s_{2}^{(i)}\right)$. The array-array operations are undefined if both of the operating arrays contain a different number of subsets $(n \neq m, \quad n>1, \quad m>1)$.

### 24.6.2 Handling Differing Coordinate Grids

If the coordinate grids of the two operands are not identical, there's no straightforward determination of the resulting coordinate grid. The dialog shown in Fig. 172 helps to make a decision.


Figure 172. Dialog which informs about coordinate related differences between the operands. It allows to choose between two options as well.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Difference | What parameter is different? |
| Operand \#1 | The parameter values of operand \#1. |
| Operand \#2 | The parameter values of operand \#2. |
| Severity | Indicates whether the difference is critical or non-critical. |
| Calculate Common Coordinates | The set of coordinates of the resulting array will be a union of the coordinate sets of both of the original arrays. The data of both of the operands will be interpolated to this new grid. Usually, this merge mode will lead to a nonequidistant coordinate grid. |
| Keep the Coordinates of Operand \#1 | Available only for an Array-Array operation $\hookrightarrow$ Sec. 24.6. <br> The set of coordinates of the resulting array will be identical to that of operand \#1. In order to get the values from operand \#2 for executing the operation, interpolation will be used. |
| Keep the Coordinates of Operand \#2 | Available only for an Array-Array operation $\hookrightarrow$ Sec. 24.6. <br> The set of coordinates of the resulting array will be identical to that of operand \#2. In order to get the values from operand \#1 for executing the operation, interpolation will be used. |
| Keep the Coordinates of the Target Data Array | Available only for an Append Subsets operation $\hookrightarrow$ Sec. 24.5.2. <br> The set of coordinates of the resulting array will be identical to that of the target array (which is modified by the operation). In order to get the values from the source array for executing the operation, interpolation will be used. |

### 24.7 Operations with Constant

Via the ribbon menu Manipulations $>\operatorname{cominin}$ Operations with Constant several operations with one field operand are available. In case of operating on a Numerical Data Array containing more than one subset, it is possible to do each of these operations either on a single subset (i.e. the currently shown subset) or on all of the subsets.

| ITEM | DESCRIPTION |
| :---: | :---: |
| ${ }^{*}=\mathrm{C}$ Set to Constant | Sets all data points to the given constant value. |
| ${ }_{1+C}$ Add Constant | Adds the given constant value to all data points. |
| ${ }^{10} \mathrm{C}$ Multiply Constant | Multiplies the given constant value to all data points. |
| $\# / C$ Divide by Constant | Divides all data points by the given constant. |
| $\pi^{18}$ Raise to Power of Constant | Raises all data points to the power of the given constant value. |

For setting the constant values to operate with, the dialog shown in Fig. 173 is used.


Figure 173. Dialog for operation with one field operand.
If you choose the mode Operate Complex, the two double numbers to enter are treated as the parts of one complex number, either in Real / Imaginary or in Amplitude / Phase Representation. Then the operations are done as a complex addition, multiplication or raise-to-power for each data point. If Operate Separately is chosen, the first entry operates only on the real part / amplitude of the field and the second number only on the imaginary part / phase, depending on the choice of Representation. In the following table you can see how these operations work and what the respective meanings of $c_{1}$ and $c_{2}$ are. The original complex value of a data point $(z=a+i b \equiv A \exp [i \phi])$ is changed by the operation with the constants $c_{1}$ and $c_{2}$ to the result shown in the two last columns.
OPERATION REPRESENTATION RESULT OF OPERATION
Mode: Operate Complex Mode: Operate Separately

| Add Constant | Real / Imaginary | $(a+i b)+\left(c_{1}+i c_{2}\right)$ | $\left(a+c_{1}\right)+i\left(b+c_{2}\right)$ |
| :--- | :--- | :--- | :--- |
|  | Amplitude / Phase | $A \exp [i \phi]+c_{1} \exp \left[i \widetilde{c}_{2}\right]$ | $\left(A+c_{1}\right) \exp \left[i\left(\phi+\widetilde{c_{2}}\right)\right]$ |
| Multiply Constant | Real / Imaginary | $(a+i b) \cdot\left(c_{1}+i c_{2}\right)$ | $\left(a \cdot c_{1}\right)+i\left(b \cdot c_{2}\right)$ |
|  | Amplitude / Phase | $A \exp [i \phi] \cdot c_{1} \exp \left[i \widetilde{c}_{2}\right]$ | $\left(A \cdot c_{1}\right) \exp \left[i\left(\phi \cdot c_{2}\right)\right]$ |
| Divide by Constant | Real / Imaginary | $(a+i b):\left(c_{1}+i c_{2}\right)$ | $\left(a: c_{1}\right)+i\left(b: c_{2}\right)$ |
|  | Amplitude / Phase | $A \exp [i \phi]:\left(c_{1} \exp \left[i \widetilde{c}_{2}\right]\right)$ | $\left(A: c_{1}\right) \exp \left[i\left(\phi: c_{2}\right)\right]$ |
| Raise to the Power of Constant | Real / Imaginary | $(a+i b)^{c_{1}+i c_{2}}$ | $\left(a^{c_{1}}\right)+i\left(b^{c_{2}}\right)$ |
|  | Amplitude / Phase | $(A \exp [i \phi])^{c_{1} \exp \left[i c_{2}\right]}$ | $\left(A^{c_{1}}\right) \exp \left[i \phi^{c_{2}}\right]$ |

$\widetilde{c_{2}}$ indicates that this value is an angle, i. e. you can enter it with the unit 'rad', 'pi', or 'o' (see Sec. 5.1 for details).

### 24.8 Field Quantity Operations

For real-valued data arrays, the ribbon menu Manipulations > 㰹 Field Quantity Operations contains only the option to convert it to a complex-valued one.
For complex-valued data arrays, this ribbon menu provides several transformations with respect to field quantities. Field quantities are explained in Sec. 11.1.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Extract | The chosen field quantity will be extracted as real value and stored into the resulting object. |
| Move | The entries in this submenu are labeled according to which field quantity of the resultant is filled from which field quantity of the source object. For example, Manipulations > 罝 Field Quantity Operations > Phase to Real Part copies the phase of the current Numerical Data Array to the real part of the resultant one, whereby the imaginary part of the resultant object is set to zero. |
| Swap | The entry in this submenu allows you to swap real part and imaginary part. |

### 24.9 Value Scaling

The ribbon menu Manipulations $>$ Value Scaling allows you to perform the following operations with respect to the data values (the amplitudes in case of complex-valued data):

| ITEM | DESCRIPTION |
| :---: | :---: |
| Scale to Given Range | In a separate dialog you are asked for the new minimum and maximum of the values in the array. Normalize for example corresponds to setting the minimum to zero and the maximum to one. |
| Normalize | Normalize the current array by dividing the array at all positions by the maximum value / amplitude. |
| Normalize According to Range Selection / <br> Normalize According to Rectangular / Elliptical Selection | Normalizes the current array by dividing it (at all data points!) by the maximum value/amplitude within the current selection. |
| Clip Values | Clips the current array to a given maximum value/amplitude. At all positions, where the value/amplitude is above this maximum value, the value / amplitude is set to the maximum value (preserving the original phase for complex valued data). At all remaining positions the array is not changed. The scaling mode of the view ( $\hookrightarrow$ Sec. 11.2.5) of the newly generated array is set to Automatic Scaling. |
| Lift Positive | Searches for the minimum value (of the real part) of the array and subtracts that value at all array positions. For a real-valued array this corresponds to adding the minimum value which ensures a non-negative array. |
| Delete Numerical Phase Artifacts | Removes the numerical artifacts described in Sec. 11.8.1 permanently, which mainly means that amplitudes having less than $t$ times the maximum amplitude are set to zero. In a dialog you can enter this relative threshold $t$. |

### 24.10 Phase Manipulations

These manipulations are only available for complex-valued Numerical Data Arrays.

The ribbon menu Manipulations $>\varphi /$ Phase Manipulations contains several operations for manipulating the phase of the current array.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $z *$ Conjugate | Performs a transformation in which each complex data value $z=a+i b$ is replaced by $z^{\star}=a-i b$. |
| (Y) Unwrap Phase | This operation tries to generate an array which contains the unwrapped phase of the current array, i.e. to remove $2 \pi$ jumps. During unwrapping, a simple line by line phase unwrapping algorithm is used. However, for twodimensional arrays unwrapping is neither unique nor always possible. For example, arrays containing phase dislocations ( $\hookrightarrow$ Sec. 67.8.2) are generally unwrappable. A precondition for successful unwrapping is a sufficient sampling of the phase information. |
| Remove Phase Dislocations in Rectangular / Elliptical Selection | Phase dislocations ( $\hookrightarrow$ Sec. 67.8.2) are searched and tried to be removed inside the currently marked selection. For removing a certain phase dislocation with charge $c$ ( $\hookrightarrow$ Sec. 67.8.2), a transmission of a phase dislocation with charge $-c$ is multiplied to the array at the same position. This operation is repeated for all phase dislocations which were found within the current selection. |
| Modify Phase | The operations which can be done are described in Sec. 22.5.1. |

### 24.11 Lateral Displacement

The ribbon menu Manipulations > Lateral Displacement allows you to do some transformations with regard to the $x$ - and $y$-coordinates of the array.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\Delta \triangle$ Mirror Horizontally | Applies the transformation $u(x, y) \rightarrow u(-x, y)$, so the array is mirrored horizontally by a mirror that corresponds to the $y$-axis. |
| $\checkmark$ Mirror Vertically | This manipulation is available for two-dimensional Numerical Data Arrays only. <br> Applies the transformation $u(x, y) \rightarrow u(x,-y)$, so the array is mirrored vertically by a mirror that corresponds to the x-axis. |
| $\triangle$ Rotate in $x-y$-Plane | THIS MANIPULATION IS AVAILABLE FOR TWO-DIMENSIONAL, EQUIDISTANTLY SAMpled Numerical Data Arrays only. <br> Rotates the array by the given angle ( $\leftrightarrows$ Sec. 22.6.1). |
|  | This manipulation is available for equidistantly sampled Numerical Data Arrays only. <br> Shifts the data of the current array by a given number of data points. |
| $\square$ Transpose | This manipulation is available for two-dimensional Numerical Data Arrays only. <br> Applies the transformation $u(x, y) \rightarrow u(y, x)$, so the array is mirrored by a mirror that corresponds to a diagonal in the $x-y$-plane. |

### 24.12 Array Size Manipulations

The ribbon menu Manipulations > 豐 Array Size Manipulations provides the following operations that change the size of an one- or two-dimensional array:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Change Array Size (Pixel Dimensions) | AVAILABLE FOR EQUIDISTANTLY sampled Numerical Data Arrays only. Changes the number of data points. If the number is increased then the newly created surrounding data points are filled according to the extrapolation settings of the array ( $\varsigma \mathrm{Sec} .24 .4$ ). Otherwise, i. e. if the number of data points is decreased then the new array is extracted. Both operations are done centered. |
| Change Array Size (Physical Dimensions) | AVailable for equidistantly sampled Numerical Data Arrays only. This option works like Change Array Size (Pixel Dimensions), but the size of the new array is defined in physical units. |
| - Double Size (Center) | Available for equidistantly sampled Numerical Data Arrays only. This operation corresponds to using Change Array Size (Pixel Dimensions) with embedding to the double array size. The original array will be centered in the result array. The new data points are set according to the extrapolation settings of the array ( $\leftrightarrows$ Sec. 24.4). |
| $\square$ Double Size (Corner) | AVAILABLE FOR EQUIDISTANTLY sampled Numerical Data Arrays only. This operation corresponds to using Change Array Size (Pixel Dimensions) with embedding to the double array size. But the original array will be the bottom left quadrant in the resulting array. The new data points are set according to the extrapolation settings of the array ( $\checkmark$ Sec. 24.4). |
| $\square$ Make Hermitian | Available for equidistantly sampled Numerical Data Arrays only. <br> At first, the array size will be doubled and the original data shifted to the lower left quadrant of the new array (just like Double Size (Corner) does). In addition, the upper right quadrant is filled by the complex conjugate of the original array in order to ensure that the result is Hermitian ( $\rightarrow$ Sec. 67.7.2). The upper left and lower right quadrant are filled with zero values. |
| HReplicate Twice | Fill the resulting array by 2 (one-dimensional case) or $2 \times 2$ (two-dimensional case) replications of the original array. This operation is equivalent to use Replicate Periodically with the double array size and a shift of ( 0,0 ). |
| \#\# Replicate Periodically | This operation creates a new array which is filled by periodically replicating the contents of the current one ( $\leftrightarrows$ Sec. 24.12.1). |
| Extract Range Selection / <br> Extract Rectangular / Elliptical Selection | Creates a new array which contains the selected portion of the current array. |
| Extract Equidistant 1D Data Along Selected Line | This manipulation is available for two-dimensional numerical Data Arrays only. <br> Extracts a one-dimensional cross-section defined by the line marker ( $\leftrightarrows$ Sec. 11.3) to a separate one-dimensional harmonic field ( $\leftrightarrows$ Sec. 24.14.1). |

### 24.12.1 Replicate Periodically

With this manipulation you can replicate a data array periodically along the $x$ - and/or y-direction. This can be useful if the data array shows something which is periodic or invariant in at least one direction. Fig. 174 shows an example.


Figure 174. The Wyrowski Photonics logo replicated periodically using the settings shown in Fig. 175.


Figure 175. Dialog for replicating a Numerical Data Array periodically.
The dialog shown in Fig. 175 has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Replication Factor $\mathbf{X}$ | Specifies how often the data is replicated in $x$-direction. Can be an arbitrary <br> value larger than or equal to 1 if the $x$-axis is sampled equidistantly. Otherwise <br> you are restricted to integer values, which is also stated by an li-icon having <br> a tooltip. |
| Replication Factor $\mathbf{Y}$ | OnLY FOR Two-DImENSIONAL DATA ARRAYs <br> Specifies how often the data is replicated in y-direction. Can be an arbitrary <br> value larger than or equal to 1 if the $y$-axis is sampled equidistantly. Otherwise <br> you are restricted to integer values, which is also stated by an Ii-icon having <br> a tooltip. |
| Keep Original Array Cen- |  |
| tered | OnLY FOR EQUIDISTANT DATA ARRAYS <br> If you check this option, the original data array is placed in the center of the <br> resulting data array. Otherwise (and for data arrays being non-equidistant <br> in at least one direction) it is placed in the bottom-left corner in case of two- <br> dimensional data arrays and on the left side in case of one-dimensional data <br> arrays. |

## 24．13 Sampling Manipulations

These manipulations are only available for equidistantly sampled Numerical Data Arrays．

The ribbon menu Manipulations＞駞塁 Sampling Manipulations provides the following operations that change the sampling distance：

| ITEM | DESCRIPTION |
| :---: | :---: |
| 湮 Equidistant Resam－ pling | Using this manipulation（ $\hookrightarrow$ Sec．24．13．1），the sampling parameters of an array can be changed，whereby the originally stored physical information shall be preserved．This operation can also be executed by clicking directly on the upper part of the Manipulations＞騳 Sampling Manipulations menu． |
| $\prod_{\boxed{2} \pi}$ Oversample Twice（Ze－ roized） | The number of data points is doubled by splitting each data point into $2 \times$ 2 new points of half the original sampling distance．The new point with the same physical position contains the old complex value，the remaining data points are filled with zero． |
| $17_{12}^{2}$ Oversample Twice （Sinc FFT Interpolation） | This is equivalent to use Interpolate with the interpolation method Sinc （Fourier Transformation）－interpolation，half the original sampling distance， and a zero point of $(0,0)$ ． |
| $\Gamma_{2}$ Oversample Twice （Nearest Neighbor Inter－ polation） | The number of data points is doubled by splitting each data point into $2 \times 2$ new points of half the original sampling distance．All new points contain the value of the original data point． |
| $\Gamma_{3}$ ，Oversample $3 \times$（Near－ est Neighbor Interpola－ tion） | The number of data points is tripled by splitting each data point into $3 \times 3$ new points of one third the original sampling distance，containing the value of the original data point． |

## 24．13．1 Equidistant Resampling

Equidistant Numerical Data Arrays can be resampled using an interpolation method．This operation＇s parameter are specified via the dialog shown in Fig． 176.


Figure 176．Dialog for resampling an equidistant Numerical Data Array．

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sampling Points | The new number of sampling points. |
| Sampling Distance Array Size | The new distance between the coordinates of two adjacent sampling points. <br> Available only if not Fix Coordinate Extent is activated. <br> The resulting new array size, defined as the distance between the coordinates of the last data point and the first data point (see Fig. 177). |
| Coordinate Extent | Available only if the Fix Coordinate Extent is activated. <br> The resulting new coordinate extent, defined as the complete range covered by all sampling points including the whole sampling distances around first and last coordinate. So this range is one sampling distance greater than Array Size (see Fig. 177). Relevant only if input and output data array contain the Nearest Neighbor Interpolation method. |
| Fix Array Size | Available only if the input and output data array contain the Nearest Neighbor Interpolation method. <br> If activated, the array size (instead of the coordinate extent) will be kept constant (see Fig. 177). |
| Fix Coordinate Extent | Available only if the input and output data array contain the Nearest Neighbor Interpolation method. <br> If activated, the coordinate extent (instead of the array size) will be kept constant (see Fig. 177). |
| Interpolation Method | The type of interpolation that is used to calculate the sampling points of the result. A method different from that contained in the input data array can be selected here. Which method will be stored with the output depends on the selected state of the option Keep Interpolation Method of the Numerical Data Array Unchanged. |


| Keep | Interpolation | If Interpolation Method differs from the Numerical Data Arrays inherent inter- |
| :--- | :--- | :--- | :--- |
| Method of | the Numeri- | polation method, this box allows to decide whether or not the used method |
| cal Data Array Unchanged | shall be adopted by the resulting Data Array. |  |



Figure 177. Difference between array size and coordinate extent for data arrays with nearest neighbor interpolation method.

### 24.14 Selection Related Operations

All operations in the ribbon menu Manipulations > Selection Related Operations affect the selected area of the array only. These are:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Fill Range Selection / <br> Fill Rectangular / Elliptical <br> Selection | Sets the sampling points within the selection to a user-defined value $c$. |
| Clear Range Selection / Clear Rectangular / Elliptical Selection | Sets the sampling points within the selection to zero. |
| Clear Inverse of Range Selection / <br> Clear Inverse of Rectangular / Elliptical Selection | Sets the sampling points outside the selection to zero. |
| Extract Range Selection / <br> Extract Rectangular / Elliptical Selection | Creates a new data array which contains only the selected portion of the current data array. |
| Extract Equidistant 1D Data Along Selected Line | This manipulation is available for two-dimensional Numerical Data Arrays only. <br> Extracts the one-dimensional cross-section defined by the line marker ( $\leftrightarrows$ Sec. 11.3) to a separate one-dimensional data array. $\hookrightarrow$ Sec. 24.14.1 |
| Extract 1D Data Along Selected Line | THIS MANIPULATION IS THE ONLY AVAILABLE ONE FOR GRIDLESS DATA ARRAYS. Extracts all data points lying exactly on the line marker ( $\hookrightarrow$ Sec. 11.3) to a separate one-dimensional, non-equidistant data array. |
| Extract Subset Data at One Point | This operation extracts the value(s) a data array has at a certain position. $\rightarrow$ Sec. 24.14.2 |
| 雭 Extract Cross Profile at Point | ONLY FOR TWO-DIMENSIONAL DATA ARRAYS WITH VISIBLE POINT MARKER. <br> Out of the current position of the point marker, two one-dimensional cross sections are extracted: one along the x-position of the marker and one along the $y$-position of the marker. The two cross sections are shown as separate data arrays. |
| Normalize According to Range Selection / <br> Normalize According to Rectangular/Elliptical Selection | Normalizes the current array by dividing it (at all sampling points!) by the maximum amplitude within the current selection. |
| Remove Phase Dislocations in Rectangular / Elliptical Selection | THIS MANIPULATION IS AVAILABLE FOR TWO-DIMENSIONAL, EQUIDISTANTLY SAMpled Numerical Data Arrays only. <br> Phase dislocations ( $\leftrightarrows$ Sec. 67.8.2) are searched and tried to be removed in the current selection. For removing a certain phase dislocation with charge $c$ ( $\hookrightarrow$ Sec. 67.8.2), a phase dislocation with charge $-c$ is multiplied to the array at the same position. This operation is repeated for all phase dislocations which were found within the current selection. |

### 24.14.1 Extraction of 1D Data Along Line

This manipulation is available for two-dimensional Numerical Data Arrays only.
Via Manipulations > Selection Related Operations > Extract Equidistant 1D Data Along Selected Line or via Manipulations > 稫 Array Size Manipulations > Extract Equidistant 1D Data Along Selected Line, an equidistantly sampled 1D Numerical Data Array can be extracted out of a 2D Numerical Data Array. This will be done along a previously defined line marker ( $\leftrightarrows$ Sec. 11.3). The dialog shown in Fig. 178 allows you to define more extraction parameters.


Figure 178. Dialog for defining the parameters for extracting an equidistantly sampled 1D Numerical Data Array out of a 2D Numerical Data Array.

The following parameters can be set, largely to define the new coordinate axis:

| ITEM | DESCRIPTION |
| :--- | :--- |
| No. of Data Points to Ex- <br> tract | The number of equidistantly distributed data points in the resulting 1D Nu- <br> merical Data Array. |
| Method of Source Array | If chosen, the extraction method uses the interpolation method of the 2D <br> source array for getting each data point's value. |
| Nearest Neighbor / Con- <br> stant Interval | If chosen, the extraction method uses nearest neighbor interpolation (con- <br> stant interval interpolation in case of nonequidistant data) for getting each <br> data point's value. |
| New Axis Description | The description of the target Numerical Data Array's coordinate can be set <br> here. |
| New Axis Physical Prop- <br> erty of Axis | The physical property of the target Numerical Data Array's coordinate can be <br> set here. |
| New Interpolation Method | The interpolation method of the 1D target array can be set here. |

New Coordinate Position- The mode for calculating the coordinates in the 1D target array has to be ing defined here.

- CenterAround Zero will calculate the new coordinates in a way that zero will be exactly in the center.
- Center Around Zero Node is the same in case of an odd number of resulting data points, but in case of an even number, the data point at the left of the exact center of the coordinate range will get the coordinate zero.
- The mode Start Coordinate allows you to define the value of the start / the lowest coordinate.

New Coordinate Positioning > Equals minimum boundary of first interval

If the mode Start Coordinate is chosen, the target interpolation method is set to Nearest Neighbor, and this option is set, the given coordinate will refer to the minimum boundary of the first data point. If not set, it refers to the center of the first nearest neighbor interval.

### 24.14.2 Extraction of 1D Data at One Point

This operation extracts the value(s) a data array has at a certain position. The position is specified by the point marker ( $\hookrightarrow$ Sec. 11.3).
If the data array contains only one subset, the value at the given position is simply logged into the Messages $\operatorname{tab}(\hookrightarrow$ Sec. 4.3). In this case always the interpolation method of the source array is used to get the value if the marker is placed between data points.


Figure 179. Dialog for defining the parameters for extracting an equidistantly sampled 1D Numerical Data Array from the data at one point.

If the data array contains more than one subset, the data within each subset at the given position becomes one data point in the resulting one-dimensional data array. In this case the dialog shown in Fig. 179 opens where the following parameters can be set, largely to define the new coordinate axis:

| Method of Source Array | If chosen, the extraction method uses the interpolation method of the 2 D source array for getting each data point's value. |
| :---: | :---: |
| Nearest Neighbor / Constant Interval | If chosen, the extraction method uses nearest neighbor interpolation (constant interval interpolation in case of nonequidistant data) for getting each data point's value. |
| New Axis Description | The description of the target Numerical Data Array's coordinate can be set here. |
| New Axis Physical Property of Axis | The physical property of the target Numerical Data Array's coordinate can be set here. |
| New Interpolation Method | The interpolation method of the 1D target array can be set here. |
| New Data Description | The data description of the resulting array. |
| New Coordinate Positioning | The mode for calculating the coordinates in the 1D target array has to be defined here. <br> - Center Around Zero will calculate the new coordinates in a way that zero will be exactly in the center. <br> - Center Around Zero Node is the same in case of an odd number of resulting data points, but in case of an even number, the data point at the left of the exact center of the coordinate range will get the coordinate zero. <br> - The mode Start Coordinate allows you to define the value of the start / the lowest coordinate. |
| New Coordinate Positioning > Equals minimum boundary of first interval | If the mode Start Coordinate is chosen, the target interpolation method is set to Nearest Neighbor, and this option is set, the given coordinate will refer to the minimum boundary of the first data point. If not set, it refers to the center of the first nearest neighbor interval. |
| New Coordinate Positioning > New Sampling Distance | The sampling distance of the new coordinate axis. |

### 24.15 Miscellaneous

The ribbon menu Manipulations > Miscellaneous contains various special manipulations e.g. to smooth data or to introduce discrete value levels.

### 24.15.1 Savitzky-Golay Filter

The Savitzky-Golay filter is a commonly used filter to remove noise from measured data while retaining information like the position of the extrema as good as possible. It is a special moving window filter where a window of given size $k$ is moved over the data and the data point in the center is then replaced by the value of a polynomial of order $n$ fitted to the data in the window. The implementation in VirtualLab Fusion supports both one- and two-dimensional data.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Window Size | The window size $k$. If it is even, internally 1 is added to ensure that there is <br> always a data point in the center of the window. For two-dimensional data the <br> same window size is used for $x$ - and y-direction. |
| Order | The order $n$ of the polynomials to fit. For $k=0$ you obtain a moving average <br> filter. If $n \geq k-1$ the fitted polynomial reproduces exactly the data points in <br> the window and thus no smoothing is done. |

### 24.15.2 Temporal Sampling of Real Part

This manipulation is only available for Numerical Data Arrays that contain a single subset.

This operation considers the input being static data which will be transformed into time dependent data. The input will be treated either as being the complex amplitude of a harmonic electric field or just as numerical data without electromagnetic meaning.
The calculation is done for different time indices within one period and the resulting sampled values are stored within a numerical data array with a number of subsets, one for each point of time.
The following options are available:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sampling Count of T | Number of equidistant points of time $n$ within the temporal period $T=2 \pi / \omega_{0}$. The real part will be extracted at $t=\frac{1}{n} T, \frac{2}{n} T, \ldots, T$. |
| Treat the Data as Electric Field | If true, the input will be considered being the complex amplitude of a harmonic electric field $E(r)$ and the result will be calculated to $E(r, t)=$ $2 \operatorname{Re}\left(\boldsymbol{E}(\boldsymbol{r}) \exp \left(-i \omega_{0} t\right)\right)$. Physical unities and interpolation method will be taken into account in this case. <br> If false, the input will be considered being just numerical data $f_{c}(\boldsymbol{r})$ and the result will be calculated to $g(\boldsymbol{r}, t)=\operatorname{Re}\left(f_{c}(\boldsymbol{r}) \exp \left(-i \omega_{0} t\right)\right)$. |

With harmonic field data, this operation can be used to get the field components of the electric or the magnetic field at different points of time.
After conversion of the result into an animation (via Manipulations > 唱 Create Animation), one can visualize the temporal field sampling in a movie.
Note, this operation is available only with data arrays with one subset. However, you can always extract a subset from a data array with multiple subsets via Manipulations > 噵 Change Subset Parameters > Remove Subset(s) ( $\hookrightarrow$ Sec. 24.5.3).

### 24.15.3 Quantization

The quantization of a Numerical Data Array means to introduce discrete value levels for real-valued data as well as discrete amplitude and phase levels for complex-valued data. The following entries are available at Manipulations > Miscellaneous > Quantization:

| ITEM | DESCRIPTION |
| :--- | :--- | :--- |
| Hard Quantization | This calls the Hard Quantization algorithm described in Sec. 22.11.2. |
| Soft Quantization | This calls the Soft Quantization algorithm described in Sec. 22.11.3. |
| Floyd-Steinberg Quanti- This calls the Floyd-Steinberg Quantization algorithm described in <br> zation Sec. 22.11.4. |  |

### 24.16 Editing Single Data Points

It is possible to edit the value of a single data point in a Numerical Data Array. In order to open the dialog shown in Fig. 180, either the context menu in the Table panel ( $\hookrightarrow$ Sec. 13.5.2) or the Edit Data Point button in the Value at $(x, y)$ panel ( $\hookrightarrow$ Sec. 13.5.3) has to be used.

| Enter the New Data $\times$ |  |  |
| :---: | :---: | :---: |
| Data point (42; 42) is edited. Real / Imaginary Part <br> - Amplitude / Phase |  |  |
| Subset | Amplitude of Value | Phase of Value |
| Sample A | 2 | 0 rad |
| Sample B | 3 | 1 rad |
|  | OK Cancel | Help |

Figure 180. Dialog for editing the value(s) of a single data point.

For complex data, the representation of the complex values (Real / Imaginary Part vs. Amplitude / Phase) can be chosen. Each table row contains the value of one subset for the data point to be edited.

### 24.17 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

### 24.18 Fourier Transform

For a detailed discussion of Fourier transforms $\hookrightarrow$ Sec. 31 .

### 24.19 Graphics Add-on

For a detailed discussion of graphics add-ons $\hookrightarrow$ Sec. 32.

### 24.20 Expert Mode

ONLY FOR DATA ARRAYS WITH FIXED PHYSICAL MEANING.

Usually, only a few manipulations are available for data arrays with a fixed physical meaning ( $\hookrightarrow$ Sec. 24.1.4). In case more manipulations are needed, activating the Expert Mode ${ }^{7}$ allows to access a lot more operations on the contained sampled data.

## 25 Manipulation of Chromatic Fields Sets

### 25.1 Selection Related Operations

ITEM
DESCRIPTION

| Extract Equidistant 1D Data Along Selected Line | Only for two-dimensional Chromatic Fields Sets with a visible pro- |
| :---: | :---: |
|  | This operation works as described in Sec. 24.14.1 with the difference that it is not possible to change the interpolation settings for the extraction. Can be accessed via Manipulations > 㹃 Array Size Manipulations and via Manipulations > 椔 Selection Related Operations. |

### 25.2 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

### 25.3 Graphics Add-on

For a detailed discussion of graphics add-ons $\hookrightarrow$ Sec. 32 .

### 25.4 Expert Mode

Usually, only a few manipulations are available for chromatic fields sets. In case more manipulations are needed, activating the Expert Mode allows to access a lot more operations on the contained sampled data.

## 26 Manipulations of Pulse and Field Components

### 26.1 Array Size Manipulations

ITEM
DESCRIPTION
Change Array Size (Pixel Available for equidistantly sampled data only.
Dimensions) Changes the number of data points. If the number of data points is increased then the array is embedded, that means the newly created surrounding data points are filled with zero values. Otherwise, i. e. if the number of data points is decreased then the new array is extracted. Embedding as well as extracting is done centered. Can be accessed via Manipulations > 峰 Array Size Manipulations.
A pulse in time domain is usually sampled equidistantly and thus this operation can be used to increase the sampling within the frequency domain. See Sec. 31.2 for the conversion from frequency to time domain and vice versa.

### 26.2 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

### 26.3 Fourier Transform

For a detailed discussion of Fourier transforms $\hookrightarrow$ Sec. 31 .

### 26.4 Graphics Add-on

For a detailed discussion of graphics add-ons $\hookrightarrow$ Sec. 32 .

## 27 Manipulation of Order Collections

### 27.1 Selection Related Operations

## ITEM

DESCRIPTION

| Extract 1D Data Along | Extracts all data points of the currently shown Gridless Data Array which lie |
| :--- | :--- |
| Selected Line | exactly on the line marker $(\leftrightarrows$ Sec. 11.3) to a separate one-dimensional, non- |
|  | equidistant data array. The order numbers are added as labels to the resulting |
|  | data array. |
|  | Can be accessed via Manipulations $>$ Selection Related Operations. |

### 27.2 Conversions

For a detailed discussion of all possible conversions $\hookrightarrow$ Sec. 30 .

## 28 Manipulations of Regions

### 28.1 Edit Region

The edit of an existing region can be done using the dialogs which will open via Manipulations > $\mathbf{n}$ / Edit Region and which are described in Sec. 21.

### 28.2 Selection Related Operations

AVAILABLE FOR SAMPLED REGIoNs only.

All operations in the ribbon menu Manipulations >组 Selection Related Operations affect the selected area of the region. These are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| N Fill Selection | Sets the data points within the selection to being 'inside' the actual region. |
| $X$ Clear Selection | Sets the data points within the selection to being 'outside' the actual region. |
| Clear Inverse Selection | Sets the data points outside the selection to being 'outside' the actual region. |
| Extract Selection | Creates a new region object which contains only the selected portion of the <br> current region. |

### 28.3 Conversions

For a detailed discussion of all possible conversions $\leftrightarrows$ Sec. 30 .

## 29 Manipulation of Sets of Data Arrays

### 29.1 Selection Related Operations

ITEM
DESCRIPTION
Extract 1D Data Along
Only for sets of Gridless Data Arrays
Selected Line
Extracts all data points of the currently shown Gridless Data Array which lie exactly on the line marker ( $\leftrightarrows$ Sec. 11.3) to a separate one-dimensional, nonequidistant data array.
Can be accessed via Manipulations > Selection Related Operations.

### 29.2 Conversions

For a detailed discussion of all possible conversions $\leftrightarrows$ Sec. 30 .

### 29.3 Graphics Add-on

For a detailed discussion of graphics add-ons $\leftrightarrows$ Sec. 32 .

## 30 Conversions

Conversions are manipulations whose result is of another document type than the input document.

### 30.1 Conversions for Complex Amplitude Documents

Complex Amplitude Documents, namely Harmonic Fields and Jones Matrix Transmissions, allow the following conversions, which can be found in the ribbon group Manipulations > Conversions.

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\rightarrow$ Create Numerical Data Array | Converts the document to a Numerical Data Array. $\hookrightarrow$ Sec. 30.1.1, Shortcut: F3 |
| $\rightarrow$ Create Harmonic Field | Only for Jones Matrix Transmissions Converts the document to a Harmonic Field. |
| $\vec{\square}$ Create Transmission | Only for globally polarized Harmonic Fields Converts the document to a Jones Matrix Transmission. |
| $\square_{\text {¢ }}$ Create Sampled Region | Converts the document to a sampled region ( $\leftrightarrows$ Sec. 21). You are asked for a relative threshold and all values having a squared amplitude larger than the maximum squared amplitude times this value are regarded as being 'inside' the region. |
| ag Create Harmonic Fields Set | Only for Harmonic Fields <br> Converts the harmonic field to a harmonic fields set with one member field. Then you can add further member fields as required ( $\lrcorner$ Sec. 23.3). |
| $\overline{x-k}$ Convert to Spectral Coordinates / Convert to Spatial Coordinates | Converts the coordinate axes from Length to Wave Number and vice versa according to the formulas given at the end of Sec. 135.5.1.1. <br> As a stored analytical spherical phase is not allowed for spectral fields, you are asked whether you want to sample or remove that spherical phase factor prior to converting to spectral coordinates. |
| tor Dimension Separation | The operations in this menu convert between one- and two-dimensional fields. $\hookrightarrow$ Sec. 30.3.5 |

To convert globally polarized fields into locally polarized ones and vice versa use Manipulations > folarization Change ( $\hookrightarrow$ Sec. 22.10).

### 30.1.1 Conversion to Numerical Data Arrays

If a Harmonic Field, a Transmission, or a Harmonic Fields Set is to be converted to a Numerical Data Array then the dialog shown in Fig. 181 is used to determine the conversion parameters. For Harmonic Fields Set all member fields are interpolated to a common sampling using the "Sinc Interpolation (Fourier Transform)". The common sampling is derived from the largest field size and the smallest sampling distance of all member fields.


Figure 181. Dialog for the parameters needed for converting a Harmonic Field or a Transmission into a Numerical Data Array.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component | For locally polarized Harmonic Fields, here can be chosen whether the vec- <br> torial component $E_{x}$ or $E_{y}$ or both of them are to be converted to a subset <br> in the new Numerical Data Array. For globally polarized fields, as well as for <br> Transmissions, this choice is not provided. |
| Complex Conversion | If checked, the whole complex information will be converted to a complex <br> Numerical Data Array. If not, a Field Quantity has to be chosen which will be <br> extracted into a real valued Data Array. |
| Field Quantity | For a non-complex conversion, here the field quantity has to be selected that <br> shall be extracted for the Numerical Data Array. |
| Interpolation Method for $\mathbf{X}$ | The interpolation method for the X direction in the Numerical Data Array to be <br> created is set here. |
| Direction | Interpolation Method for $\mathbf{Y}$  <br> Direction Despite the synchronization of the interpolation methods for X and Y direction, <br> the interpolation method for the latter is given here for the sake of complete- |

### 30.2 Conversions for Harmonic Fields Sets

The ribbon group Manipulations > Conversions of Harmonic Fields Sets has the following entries.

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\rightrightarrows$ Create Numerical Data | Converts the document to a Numerical Data Array. $\hookrightarrow$ Sec. 30.1.1, Shortcut: |
| Array | F3 |
| $\rightrightarrows$ Create Animation | Converts the document to an Animation. Then, each member of the Harmonic |
|  | Fields Set becomes one frame in the animation. |
|  | It works in the same way as the corresponding Combined Output |
|  | $(\hookrightarrow$ Sec. 44.5.1.3). |

### 30.3 Conversions for Data Arrays

The ribbon group Manipulations > Conversions of Data Arrays has the following entries.

| ITEM | DESCRIPTION |
| :---: | :---: |
| 唱 Create Animation | VirtualLab Fusion allows you to convert the subsets of a two－dimensional Data Array into the frames of an animation．$\hookrightarrow$ Sec．30．3．1 |
| $\exists$ Create Numerical Data Array | Sometimes a Data Array document is not a Numerical Data Array but has a physical meaning，for example if you apply the Electric Field detector $(\hookrightarrow$ Sec．75．3．1）on a Harmonic Field．Then the caption of the document dif－ fers（ $\hookrightarrow$ Fig．182）．This manipulation can be used to convert such a document to a Numerical Data Array．Shortcut：F3 |
| $\rightarrow$ Create Harmonic Field | Converts the data array to a Harmonic Field．$\hookrightarrow$ Sec．30．3．2，Shortcut：F3 |
| 绿 Dimension Reduction <br> $>$ 䍐 $\downarrow$ Extract All Rows | ONLY FOR TWO－DIMENSIONAL DATA ARRAYS WITH EXACTLY ONE SUBSET． Each data row becomes one subset of a one－dimensional data array． |
| 经 Dimension Reduction ＞苗 Extract All Columns | OnLY FOR TWO－DIMENSIONAL DATA ARRAYS WITH EXACTLY ONE SUBSET． <br> Each data column becomes one subset of a one－dimensional data array． |
| 都 Dimension Reduction <br> $>$ 央く Extract Cross Profile <br> at Point | OnLY FOR TWO－DIMENSIONAL DATA ARRAYS WITH VISIBLE POINT MARKER． <br> Out of the current position of the point marker，two one－dimensional cross sections are extracted：one along the x－position of the marker and one along the y－position of the marker．The two cross sections are shown as separate data arrays． |
| $\vec{*}$ Create 2D Data Array | ONLY FOR ONE－DIMENSIONAL DATA ARRAYS WITH MORE THAN ONE SUBSET． Creates a two－dimensional data array out of the subsets of a one－dimensional data array．$\hookrightarrow$ Sec．30．3．3 |
| Extrude to 2D Data Ar－ ray | ONLY FOR ONE－DIMENSIONAL DATA ARRAYS． <br> Creates a two－dimensional data array via extruding a one－dimensional data array．The result will contain the same number of subsets as the original． $\rightarrow$ Sec．30．3．4 |
| for Dimension Separation | The operations in this menu convert between one－and two－dimensional fields．$\hookrightarrow$ Sec．30．3．5 |



Figure 182．Sample captions for a Data Array with physical meaning（top and center）and for a Numerical Data Array （bottom）．

## 30．3．1 Create Animation from Numerical Data Arrays

ONLY FOR TWO－DIMENSIONAL GRIDDED OR GRIDLESS DATA ARRAYS．
This conversion creates one bitmap from each subset of the currently used data array or set of data arrays． This bitmap contains the data as shown in the diagram panel（ $\hookrightarrow$ Sec．13．5．1），it does not contain the axes，the legend and other additional information．Especially the following settings from the current configuration of the diagram panel influence the generated bitmaps：
－the color table（ $\hookrightarrow$ Sec．11．2．4）
－the field quantity（ $\hookrightarrow$ Sec． 11.1 ）
－whether the view is interpolated（for gridded data arrays，$\hookrightarrow$ Sec．11．2．1）

- the dot size in pixels (for gridless data arrays, $\hookrightarrow$ Sec. 13.5.1.4)
- whether triangles are shown (for gridless data arrays, $\hookrightarrow$ Sec. 11.2.3)


Figure 183. The settings for the conversion to an animation.

There is an edit dialog for this conversion where you can set the bitmap size and the data scaling ( $\hookrightarrow$ Fig. 183). It has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Aspect Ratio | The aspect ratio of the resulting animation is determined in different ways: <br> - True to Physical Scale: The aspect ratio is determined from the ratio of the $x$-axis range of the data array to its $y$-axis range. This option is not available if the two coordinate axes have different physical properties. <br> - User-Defined: If you choose this option you can define a suitable aspect ratio. For example you can use 16:9 to ensure that the animation (and a video possibly generated out of it via File > Export) looks nicely on matching monitors or projectors. For gridded data arrays the default user-defined aspect ratio is calculated from the number of data points in the data array. <br> - Free: You can set Width and Height of the single bitmaps as you want. |
| Width / Height | The width and height of the resulting bitmaps. If the Aspect Ratio is not Free and you change one dimension, then the other dimension is always changed automatically. |
| Scale Frames to | - Common Value Range: The global minimum and maximum value of all subsets is used to scale the color table. As a result you can see in which subsets there are smaller values then in others. <br> - Individual Value Range: The color table for each frame is adapted to the minimum and maximum value of the individual data. As a result all subsets use all colors of the color table. |

If True To Physical Scale is set in the View ribbon of the data array, then True to Physical Scale is set as default. Otherwise User-Defined is the default.
For sets of data arrays the overall extension, i.e. the union of the ranges of all included data arrays, is shown in the resulting animation. Subsets from data arrays which have a smaller extension are filled up with black pixels accordingly.

### 30.3.2 Conversion of Numerical Data Arrays to Harmonic Fields

The data of a Data Array can be used for creating a new Harmonic Field of course. This can be done via Manipulations > $\quad \rightarrow \mathbf{a}$ Create Harmonic Field.
Since some of the parameters have to be specified additionally, the conversion dialog shown in Fig. 184 will open.


Figure 184. Dialog for the parameters needed for creating a Harmonic Field from a Numerical Data Array.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Polarization Mode | The resulting field can be Globally Polarized or Locally Polarized. <br> In case of a Globally Polarized resulting field, the Data Array's subset to be <br> used as lateral field distribution U can be chosen here. <br> In case of a Locally Polarized resulting field, the Data Array's subset to be <br> used as lateral field distribution of the component Ex/Ey can be chosen here. |
| Subset for Ex/Ey | The wavelength of the Harmonic Field to be created. |
| Wavelength | In case of a Globally Polarized resulting field, the currently set Jones vector <br> is shown here. It can be changed via the button Set Jones Vector. |
| Jones Vector J | The Jones vector for a Globally Polarized resulting field can be set via a dia- <br> log, that opens when this button is pressed. |
| Set Jones Vector | VirtualLab Fusion will check the Numerical Data Array for valid physical units <br> for the stored data and its coordinates. Valid means: Electric field strength as <br> unit for the data and a length or reciprocal length for the coordinates. How- <br> Show Warnings in Case of, if this option is unchecked, no warnings will be displayed in case of <br> Wrong Physical Units |

### 30.3.3 Create 2D Data Array from 1D

If it makes sense to order all subsets of a one-dimensional Numerical Data Array on another dimension, a two-dimensional Numerical Data Array can be created from that data. For this, the new dimension has to be defined using the dialog shown in Fig. 185. The subsets will be concatenated along this new dimension, then.


Figure 185. Dialog for defining a new dimension for creating a 2D Numerical Data Array from 1D data.
The following parameters are necessary in order to define the second dimension:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Direction of New Axis | Determines whether the new dimension shall be in x or y. |
| Description | The meaning of the new dimension. This will be the label for the new axis of <br> the resulting Numerical Data Array. |
| Physical Property | The physical property of the new dimension's coordinate. |
| Sampling Distance | The distance of two adjacent 1D subsets on the new dimension. |
| First Coordinate | The coordinate which corresponds to the first 1D subset on the new dimen- <br> sion. |

### 30.3.4 Extrude 2D Data Array from 1D

Besides creating a 2D data array from a 1D data array by concatenating its subsets ( $\rightarrow$ Sec. 30.3.3), there exists another possibility of adding another dimension. The dialog shown in Fig. 186 can be used for extruding the 1D data along a new coordinate axis.

| Extrude 1D Data Array to 2D |  |  |
| :---: | :---: | :---: |
| Direction of New Axis | $y$-Axis | $\checkmark$ |
| Number of Points |  | $5 \div$ |
| Parameter of Axis |  |  |
| Description | Index |  |
| Physical Property | Length | $\checkmark$ |
| Sampling Distance |  | 1 mm |
| First Coordinate |  | 0 mm |
| OK | Cancel | Help |

Figure 186. Dialog for defining an extrusion of 1D data for creating a 2D Numerical Data Array.
The following parameters are necessary in order to define the extrusion:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Direction of New Axis | Determines whether the new dimension shall be in x or y. |
| Number of Points | To what number of new data points shall the result be extruded (along the <br> Direction of New Axis)? |
| Description | The meaning of the new dimension. This will be the label for the new axis of <br> the resulting Numerical Data Array. |
| Physical Property | The physical property of the new dimension's coordinate. |
| Sampling Distance | The distance of two adjacent sampling points on the new dimension. |
| First Coordinate | The coordinate which corresponds to the first data point on the new dimen- <br> sion. |

### 30.3.5 Dimension Separation

The ribbon menu Manipulations > Dimension Separation offers the option to separate a two-dimensional complex array or to recombine the parts of a previously separated array. A two-dimensional separable array $u_{\text {sep }}(x, y)$ fulfills the property

$$
\begin{equation*}
u_{\text {sep }}(x, y)=u_{x}(x) u_{y}(y) \tag{30.1}
\end{equation*}
$$

with the one-dimensional arrays $u_{x}$ and $u_{y}$ which are calculated from the (not necessarily separable) current array $u(x, y)$ by

$$
\begin{align*}
& u_{x}(x)=f_{x} u_{x}^{\prime}(x),  \tag{30.2}\\
& u_{y}(y)=f_{y} u_{y}^{\prime}(y) \tag{30.3}
\end{align*}
$$

with

$$
\begin{align*}
& u_{x}^{\prime}(x)=\sum_{j=0}^{N_{y}-1} u\left(x, y_{j}\right),  \tag{30.4}\\
& u_{y}^{\prime}(y)=\sum_{i=0}^{N_{x}-1} u\left(x_{i}, y\right) \tag{30.5}
\end{align*}
$$

and

$$
\begin{align*}
& f_{x}=\sqrt{f_{0} \frac{N_{x}}{N_{y}}},  \tag{30.6}\\
& f_{y}=\sqrt{f_{0} \frac{N_{y}}{N_{x}}}, \tag{30.7}
\end{align*}
$$

where $N_{x}$ and $N_{y}$ denote the number of sampling points and $f_{0}$ is calculated as

$$
\begin{equation*}
f_{0}=\frac{\sum_{j=0}^{N_{y}-1} \sum_{i=0}^{N_{x}-1} u\left(x_{i}, y_{j}\right) \overline{u_{x}\left(x_{i}\right) u_{y}\left(y_{j}\right)}}{\sum_{j=0}^{N_{y}-1} \sum_{i=0}^{N_{x}-1}\left\|u_{x}\left(x_{i}\right) u_{y}\left(y_{j}\right)\right\|^{2}} \tag{30.8}
\end{equation*}
$$

| ITEM | DESCRIPTION |
| :--- | :--- |
| Make Field Separable | Works similar to Separate into $x$ - and y -Direction (see below) with the excep- <br> tion that the output of this operation is the two-dimensional separable array <br> $u(x, y)$ which is calculated according to Eq. (30.1). |
| Separate into $\mathbf{x - a n d} \mathbf{y -}$ - | Constructs two one-dimensional arrays $u_{x}$ and $u_{y}$, with the goal that the array <br> $u_{\text {sep }}(x, y)$ according to Eq. (30.1) differs as little as possible from the current <br> one. The error criterion is to minimize the squared amplitude sum of the dif- <br> ference between the original and the approximated array. The arrays $u_{x}$ and <br> $u_{y}$ are calculated by integrating the current array in Y or X direction, respec- <br> tively (see Eqs. (30.4)-(30.5)). Afterwards a rescaling factor is applied to $u_{x}$ <br> and $u_{y}$, respectively (according to Eqs. (30.6)-(30.8)). <br> Constructs a two-dimensional separable array according to Eq. (30.1) from <br> the two given one-dimensional arrays. |

### 30.4 Conversion for Chromatic Fields Sets

ITEM DESCRIPTION
$\rightarrow$ Create Numerical Data Extracts the underlying Data Array ( $\rightarrow$ Sec. 13) and displays it as separate Array document. Shortcut: F3

### 30.5 Conversions for Pulse and Field Components

| ITEM | DESCRIPTION |
| :---: | :---: |
| 召 Create Animation | ONLY FOR TWO-DIMENSIONAL DOCUMENTS WITH MORE THAN ONE SUBSET, I. E. for Pulse Component and Field Vector Component. <br> VirtualLab Fusion allows to convert the subsets of a Pulse and Field Component document into the frames of an animation. The current view settings Field Quantity and Color Table will be used for the conversion. |
| $\rightarrow$ Create Numerical Data Array | Extracts the underlying Data Array ( $\varsigma$ Sec. 13) and displays it as separate document. Shortcut: $\square$ |

### 30.6 Conversion for Order Collections

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\Rightarrow$ Convert to Equidistant Data Array | Converts all information (coordinates, efficiencies, and Rayleigh coefficients) into distinct subsets of an equidistant data array, plotted versus order numbers. Shortcut: F3 |
| Extract Current Grating Efficiencies | Extracts the currently visible grating efficiencies diagram into a gridless data array ( $\leftrightarrows$ Sec. 13) and displays it as separate document. Shortcut: Shift + F3 |

### 30.7 Conversion for Regions

## ITEM DESCRIPTION

$\rightarrow$ Convert to Sampled Re- Only available for non-sampled regions.
gion Opens a dialog for sampling the current region ( $\rightarrow$ Sec. 30.7.1).
$\rightarrow$ Create Numerical Data Only available for sampled regions.
Array Extracts the underlying Data Array ( $\hookrightarrow$ Sec. 13) and displays it as separate document. Shortcut: F3

### 30.7.1 Conversion to Sampled Regions

Converting non-sampled into sampled regions require input of the sampling parameters. This has to be done via the dialog shown in Fig. 187.


Figure 187. Dialog for defining the sampling parameters for converting a non-sampled region into a sampled one.
The sampling parameters are the following:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Points | The number of sampling points to be used in the respective dimension. |
| Sampling Distance | The sampling distance to be used in the respective dimension. <br> Center Around Zero |
| If checked, the result will be zero centered in the respective dimension. In <br> order to achieve this, the data will be embedded if necessary. |  |
| Array Size | Information about the resulting array size. |

### 30.8 Conversions for Sets of Data Arrays

| ITEM | DESCRIPTION |
| :---: | :---: |
| 㕷 Create Animation | Only for Data Arrays 2D and Data Arrays Gridless <br> VirtualLab Fusion allows you to convert all subsets of a two-dimensional Set of Data Arrays into the frames of an animation. In the resulting animation first come the subsets of the first data array, then the subsets of the second data array and so on. The edit dialog for this conversion is described in Sec. 30.3.1. |
| $\nexists$ Convert to Single Data Array | Only for Data Arrays 1D and Data Arrays 2D <br> Converts the Set of Data Arrays into a single data array containing all subsets. If necessary, the data is resampled to a common grid. Shortcut: F3 |
| 霊 Extract Current Numerical Data Ar- ray/Electromagnetic Field/... | Extracts the currently visible Data Array ( $\hookrightarrow$ Sec. 13) and displays it as separate document. Shortcut: Shift + F3 |

## 31 Fourier Transforms

### 31.1 Fourier Transform (Space)

The Fourier transform has many applications in wave-optical simulations. Examples are the usage in free space propagation operators ( $\hookrightarrow$ Sec. 93) and the simulation of Fourier transforming optical setups ( $\hookrightarrow$ Sec. 31.1.1). It is available via various ribbon items in the ribbon group Manipulations > Fourier Transform (Space):

- Manipulations >FF Forward: $\mathrm{x} \rightarrow \mathrm{k}$,
- Manipulations $>\boldsymbol{F}$ Backward: $\mathrm{k} \rightarrow \mathrm{x}$,
- Manipulations $>\boldsymbol{F}$ Numerical FFT $>\boldsymbol{F}$ Forward: $\boldsymbol{x} \rightarrow \mathrm{k}$, and
- Manipulations $>\boldsymbol{F}$ Numerical FFT $\boldsymbol{F}$ Backward: $\mathrm{k} \rightarrow \mathrm{x}$

The numerical and the "normal" or physical Fourier transform differ in their scaling: The numerical variants ensure that the summed norm of the field ( $\hookrightarrow$ Sec. 75.4.7) is not changed by the transform. This leads to the effect that if you embed the Fourier transform of a field in a zeroized frame and then perform the backward transform, the power and maximum amplitude of the field has changed. This is circumvented if you use the physical transforms.
The Fourier transform cannot handle fields having a stored analytical spherical phase. Thus in this case you are asked whether you want to sample or remove that spherical phase factor prior to the actual Fourier transform. The used equations are given in Sec. 135.5.1. The Fourier transform can also be done using a focusing lens ( $\hookrightarrow$ Sec. 31.1.1).

### 31.1.1 Fourier Setups

## Availability

Toolboxes: All

## Accessible:

- Harmonic Field, Harmonic Fields Set, or Jones Matrix Transmission: Manipulations > 1f) 1f-Setup and Manipulations > 2f) 2f-Setup
- Harmonic Field and Harmonic Fields Set: Propagations > 1f)) 1 f -Setup and Propagations > 2f)) 2f-Setup
- Optical Setup: Ideal Components > Special Components >1f-Setup and Ideal Components > Special Components > 2f-Setup

A Fourier transform can be done experimentally with an (ideal) focusing lens. The principal setup is shown in Fig. 188. It is mainly used for optical filtering problems like high-pass and low-pass filters. In the output plane, the Fourier plane, a filter to truncate high or low frequencies can be placed.

A Far Field Propagation of a paraxial field can also be used to create experimentally the Fourier transform.


Figure 188. Principal setup for a Fourier transform with a focusing lens. $f$ is the "Focal Length" of the lens and $d$ is the "Distance to Lens".

If the Distance to Lens $d$ equals the Focal Length $f$, the setup is called $2 f$-Setup. In this case the phase in the output plane vanishes. The other special case, if $d$ is nearly zero, is called 1 f -Setup.

| Distance to Lens | 0 mm |
| :--- | ---: |
| Focal Length | 100 mm |
|  |  |

$\square$ Simulate Pixelation Exactly
Figure 189. Control for editing the 1 -setup function.

Both special cases are available as operators in VirtualLab Fusion. These two operators have nearly identical dialogs ( $\hookrightarrow$ Fig. 189) with the following parameters:


If these operators are used in the Optical Setup, the control shown in Fig. 189 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 31.2 Fourier Transform (Temporal)

### 31.2.1 Inverse Temporal Fourier Transform

The ribbon item Manipulations $>\mathscr{F}_{t}^{\prime \prime}$ Inverse Temporal Fourier Transform can be used to calculate the pulse form of the underlying data field. This transformation is only possible if the active document contains a data field which is defined in the frequency domain. In VirtualLab Fusion these fields can be functions of the frequencies $v$ or the wavelengths $\lambda$. The resulting function in the time domain will be displayed in a new document.
The edit dialog of the Inverse Temporal Fourier Transform allows you to configure the exclusion of the time shift within the inverse temporal Fourier Transform. Also the increase of the time window can be specified. Additionally the user can define an accuracy factor which will influence the sampling in the time domain.


Figure 190. Dialog for the settings of the inverse temporal Fourier transform.
Fig. 190 shows the edit dialog of the Inverse Temporal Fourier Transform. The following parameters can be specified:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Exclude Time Shift of | You can exclude the time shift by the inverse temporal Fourier transform. The position in time of the pulse can be evaluated with the Optical Path Length Analyzer ( $\hookrightarrow$ Sec. 82). |
| Extend Time Window by Factor | For pulse evaluation VirtualLab Fusion implements a smart algorithm to extend the time window during the inverse temporal Fourier Transform. Therefor the Optical Path Length Analyzer has to be used. The residuals of the fitted linear phase function and the correct phase function can be used for the interpolation of the underlying data set. A larger time window can be realized by increasing the Oversampling Factor (Frequencies) of the Optical Path Length Analyzer $(\hookrightarrow$ Sec. 82). The resulting residual function has to be set into the edit dialog of the Inverse Temporal Fourier Transform. This can be done by clicking on the Set button in the dialog. The accuracy of the selected residual function defines the time window extension factor. This factor is displayed and cannot be edited directly by the user. |
| Oversampling Factor | Uses $n$ times the number of preset sampling points, where $n$ is the given Oversampling Factor. |

### 31.2.2 Temporal Fourier Transform

By clicking on the ribbon item Manipulations $>\mathcal{F}_{t}$ Temporal Fourier Transform a temporal Fourier transform of the underlying data field is performed. This operation is only available for fields which are defined in the time domain. The result of this operation is the field in the frequency domain. This field is displayed as function over $v$ and also as function over $\lambda$.

### 31.2.3 Envelope to Real Function Converter

If the pulse is displayed in time domain, you can show the real field instead of the envelope using the ribbon item Manipulations > Envelope to Real Function Converter.

## 32 Graphics Add-Ons

The manipulations in the category Graphic Add-Ons do not cause changes to the actual data but add some more graphical information to the view of the currently active object instead.

### 32.1 Add Region

The ribbon button Manipulations $>$ Add Region allows to select any open region object as source for a region to be drawn to the currently active view.
In case there is more than one subset present in the current object, an additional dialog will ask for the subsets to apply the add-on to.

### 32.2 Add Point Cloud

ONLY FOR TWO-DIMENSIONAL VIEWS.

The ribbon button Manipulations > Add Region allows to select any open gridless data array or ray distribution as source for a point cloud to be drawn to the currently active view.
In case there is more than one subset present in the current object, an additional dialog will ask for the subsets to apply the add-on to.

### 32.3 Add Polarization Ellipses

ONLY FOR ELECTRIC OR ELECTROMAGNETIC FIELDS.
The ribbon button Manipulations > Add Polarization Ellipses allows you to calculate polarization ellipses for Electric or Electromagnetic Fields ( $\hookrightarrow$ Sec. 13.1) either if none were calculated by the Universal Detector ( $\hookrightarrow$ Sec. 74.4) or if the ellipses shall be calculated anew for whatever reason.
The dialog shown in Fig. 191 will open in order to allow the specification of the calculation of the ellipses.


Figure 191. Dialog for the settings the parameters for calculating polarization ellipses for an existing electric or electromagnetic field.

The following parameters are to be specified:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Field / Data Array | ONLY FOR FIELDS WITH MORE THAN ONE MODE / WAVELENGTH. <br> The (sub)field for which the ellipses shall be calculated can be selected here. |
| Subsets | Each Electric or Electromagnetic Field contains one or more subsets representing the contained vectorial component. This column lists all available components with names. |
| Vectorial Component (Exactly Two Needed) | In this column, exactly two vectorial components have to be selected to be used for calculating the ellipses. Possible combinations are $E_{x} / E_{y}, E_{x} / E_{z}$, $E_{y} / E_{z}$. |
| Accessible in View | Shall the ellipses be available for the view of the respective component? If so, the visibility of the ellipses can be toggled anyway. |
| Ignore Vanishing Jones Vectors | If checked, no polarization ellipses will be calculated at positions where the amplitudes of both of the Jones vector's components are below a certain fraction (given be Threshold) of the maximum field amplitude (see also Sec. 11.8). |
| Threshold | Only available if Ignore Vanishing Jones Vectors is checked. The threshold for identifying vanishing Jones vectors. |
| Configure Ellipses | Pressing this button opens the dialog for configuring the appearance of the polarization ellipses ( $\hookrightarrow$ Sec. 11.7.3). |

### 32.4 Edit List

Since more than one graphics add-on may be associated with a data array (or data array based object), there is a list of it which can be edited via Manipulations > Edit List.

The dialog shown in Fig. 192 allows this editing.


Figure 192. Dialog for editing the list of graphics add-ons.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index | The layer index. Index \#1 corresponds to the bottom layer which is drawn <br> above the data first. The row with the highest index will be the upmost layer <br> which is drawn at last. |
| Up/Down | Moves the add-on up or down in the layer order. |
| Name | Name of the add-on. |
| Subsets | Shows for which subsets the add-on is available. |
| Delete | Deletes the add-on in this row. |

## V Catalogs



The figure above shows the Catalogs ribbon tab. As you can see, catalogs are available for

- boundary responses ( $\rightarrow$ Sec. 41)
- coatings ( $\leftrightarrows$ Sec. 36)
- components ( $\leftrightarrows$ Part IX)
- detectors ( $\leftrightarrows$ Part XI)
- light sources ( $\leftrightarrows$ Part VIII)
- materials ( $\rightarrow$ Sec. 38)
- media ( $\rightarrow$ Sec. 37)
- stacks ( $\rightarrow$ Sec. 39) and
- surfaces ( $\leftrightarrows$ Sec. 35)

These catalogs are accessible via the dialog described in Sec. 33. It serves for adding, viewing, editing, or removing of catalog entries, or for the selection of an entry. Sec. 34 describes the controls which open that dialog so that you can apply catalog entries where needed.

## 33 Catalog Dialog



Figure 193. The main form for VirtualLab Fusion catalogs.
Fig. 193 shows the main form for catalogs. It contains the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition Type | There are three definition types <br> 1. Templates: Catalog entries with either unspecified parameters or pa- <br> rameters with default values. These entries are read-only. <br> 2.LightTrans Defined: <br> structure (e.g. the material "Gold"). These entries are read-only. <br>  <br> 3. User Defined: The place where the user can store own entries. These <br> entries are saved in the path for user settings specified in the Global <br> Options dialog (Sec. 6.17). |
| Filter by... | If you enter text in this text box, only catalog entries are shown whose name <br> contains this text. The filter is not case sensitive, i.e. "glass", "Glass", and <br> "GLASS" yield the same results. It is possible to search for multiple words <br> and word groups embraced by quotation marks. |
| Shows the categories and entries of the currently selected Definition Type. <br> Each catalog entry must be within at least one category. If you have opened <br> the catalog via a Load button, double-clicking on a catalog entry loads this <br> entry. |  |


| \{Preview\} | Shows a preview of the currently selected catalog entry. The corresponding previews are as follows: <br> - Boundary Responses: $\hookrightarrow$ Sec. 41.2 <br> - Coatings: $\hookrightarrow$ Sec. 36.3 <br> - Components: 3D view as described in Sec. 5.15 <br> - Detectors: a description of the detector <br> - Light Sources: a Chromatic Fields Set View ( $\leftrightarrows$ Sec. 14) of the resulting light <br> - Materials: $\hookrightarrow$ Sec. 38.3 <br> - Media: $\hookrightarrow$ Sec. 37.2 <br> - Stacks: a read-only version of the edit dialog ( $\leftrightarrows$ Sec. 39.2) <br> - Surfaces: $\hookrightarrow$ Sec. 35.3 |
| :---: | :---: |
| Q / 3 2 View | Shows the preview as separate resizable dialog. Not available for the detectors catalog. |
| $\checkmark$ Edit | Opens the edit dialog of the currently selected catalog entry. If you edit a template or a LightTrans defined entry, you are asked to specify name and categories for saving the entry as user defined entry ( $\varsigma$ Sec. 33.1). User defined entries can be either overwritten or saved under a new name and or category. |
| $\times$ Remove | Removes a user defined catalog entry. |
| Tools | The following catalog tools are available: <br> - View, Edit, Remove (see above) <br> - Rename, Edit Categories (available for user defined catalog entries only. $\hookrightarrow$ Sec. 33.1) <br> - Export to Catalog File ( $\hookrightarrow$ Sec. 33.2) / Import from Catalog File ( $\hookrightarrow$ Sec. 33.3) <br> - Import VirtualLab <4.5 Materials / Coatings (available within the material or coating catalog only. $\hookrightarrow$ Sec. 33.4) <br> - Import Zemax OpticStudio® Glass Catalog (available within the material catalog only. $\hookrightarrow$ Sec. 129) <br> - Import Macleod Coating Data (available within the coating catalog only. $\hookrightarrow$ Sec. 128) <br> - Extract Material(s) from Medium/Coating into Catalog (available within the medium or coating catalog only. $\hookrightarrow$ Sec. 33.5) <br> - Reload from Hard Disc: If the saved catalogs have changed (e.g. by another instance of VirtualLab Fusion), you can reload them with this catalog tool. Also saving new entries sometimes requires a reload. |
| Show Preview | For performance reasons you can disable the preview with this checkbox. |
| Keep View Range (If Medium Changed) | Only available for the Media catalog and if Show Preview is actiVATED. <br> If checked, changing the shown medium will not change the displayed view range. In this case, the medium's own default view range will be ignored and the media views can be better compared. |

### 33.1 Specify Name and Categories



Figure 194. Dialog for specifying the name and the categories of a catalog entry.
The dialog shown in Fig. 194 opens if you want to save a new catalog entry, rename an existing catalog entry or change its categories. It has the following entries, whereas some of them might be disabled due to the actual purpose of the dialog.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Name | Shows the name of the catalog entry and allows you to enter a new name. <br> Each name must be unique for one type of building block (e.g. only one user <br> defined surface can have the name "Cylindrical Surface".) |
| Check | Checks whether the name is unique. This check is also done if you press Ok <br> - if the name is not unique, the dialog does not close. <br> Shows a list of all categories the catalog entry is sorted into. |
| New Category | Asks for the name of the new category and adds it to the list of Categories. <br> Two categories with the same name are merged. |
| $\times$ Remove Category | Removes the currently selected category from the list of Categories. At least <br> one category must be in this list. |

### 33.2 Export to Catalog File

You can export selected entries from the User Defined catalog to a separate catalog file which can then be imported ( $\varsigma$ Sec. 33.3) on other computers. This tool first opens a dialog ( $\leftrightarrows$ Fig. 195) where you can select which entries to export and give them other names if you like. But the names in the exported file must be unique, otherwise they are marked red and the dialog becomes invalid. The dialog also offers two Selection Tools to Select All or Unselect All entries.


Figure 195. Dialog for exporting selected entries to another catalog file. Two selected entries have the same name and thus the dialog cannot be closed with OK.

After closing this dialog with OK you can then specify path and name of the new catalog file.

### 33.3 Import from Catalog File

You can import selected entries from any catalog file (*.ctlg) into the User Defined catalog. This tool first opens a dialog where you can specify path and name of the catalog file to be imported. In the subsequent dialog ( $\hookrightarrow$ Fig. 196) you can then select which entries to import and assign additional categories to them.


Figure 196. Dialog for importing selected entries from another catalog file.
This dialog has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- | :--- |
| \{Table of Catalog Entries\} |  | | This table has the following columns: |
| :--- |
| - Import: Allows you to select which entries of the file shall be imported. |
| Entries whose name is not unique, already present in the user defined |
| catalog, or empty cannot be imported. If such an entry is selected the |
| corresponding row is marked red. Otherwise, it is marked green and |
| "OK" is shown in the Status column. |
| - Name: Shows the name of the entry and allows you to change it. |
| - Status: Shows error messages for those entries that cannot be im- |
| ported. Entries that can be imported have the status "not selected" |
| ("OK" if marked for import). |

### 33.4 Import of Catalogs of Older VirtualLab Fusion Versions

Via the Catalog Tools of the catalog main form ( $\hookrightarrow$ Sec. 33) you can Import VirtualLab <4.5 Materials / Coatings (created with VirtualLab Fusion 4.2.1 or less) into the user defined materials / coatings catalog. The following file types can be imported:

| ITEM | DESCRIPTION |
| :--- | :--- |
| ${ }^{*}$. .mtr | File containing a single material. |
| ${ }^{*}$. ctg | File containing a single coating. |
| ${ }^{*}$. mct | Materials catalog, created with or for a VirtualLab Fusion version before 4.5. |
| ${ }^{*} . \mathbf{c c t}$ | Coatings catalog, created with or for a VirtualLab Fusion version before 4.5. |



Figure 197. Import dialog for an old material catalog with some inconsistent entries.

This catalog tool first shows the standard Windows dialog for opening one or more files with matching file extensions. The selected files are then imported with the dialog shown in Fig. 197. In the upper part of this dialog there is a table with the following columns:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Import | Allows you to select which entries of the file shall be imported. Entries whose <br> name is not unique, already present in the user defined catalog, or empty <br> cannot be imported. If such an entry is selected the corresponding row is <br> marked red. Otherwise, it is marked green and "OK" is shown in the Status <br> column. <br> Shows the name of the entry and allows you to change it. |
| Name | Prior to VirtualLab Fusion 4.5, materials had no state of matter. Thus you can <br> State of Matter <br> (Only for materials) |
| Status | Shows error messages for those entries that cannot be imported. Entries that <br> can be imported have the status "not selected" ("OK" if marked for import). |

By clicking on a column caption, you can sort by this column.
The Selection Tools allow you to either Select All entries in the table or to Unselect All.
The lower part of the catalog defines the categories into which all entries are stored. You can add a new category with the -button and remove a category with the X -button.

### 33.5 Extraction of Materials stored in Media or Coatings

Optical Media as well as thin film Coatings usually contain materials. If, for any reason, such a material is not stored in the materials catalog yet, the tool Catalog Tools > Extract Material(s) from Medium/Coating into Catalog allows to extract it. It will be stored into the user defined materials catalog.
The tool will examine the selected medium or coating which contains the desired material. Then the dialog
shown in Fig. 197 will appear. Select the material(s) to extract here (for a detailed description see Sec. 33.4 please) and press OK. The chosen materials will be saved to the user defined materials catalog.

## 34 Application of Catalog Entries

The following sections describe the controls which are used to access and apply catalog entries in order to build up superordinate building blocks or real components.

### 34.1 Load and Edit of Catalog Entries

The controls shown in Fig. 198 are e.g. used for the definition of optical surfaces, media, stacks, and/or boundary operators of real components ( $\hookrightarrow$ Part IX).
These controls are also used within table cells (for example in the table defining the surfaces within a Lens System component). Then they are compactified as shown in Fig. 199 and shown only if the user enters that row.
Furthermore there is a "one line version" as shown in Fig. 200.


Figure 198. Control for loading, editing and viewing optical surfaces (above) and media (below).

```
Plane Interface
```

$3 \%$ Q
Figure 199. Control for loading, editing and viewing building blocks within a table.

SurroundingMedium: "Air in Homogeneous Medi... Load Edit Qiew
Figure 200. One line version of the control for loading, editing and viewing building blocks

| ITEM | DESCRIPTION |
| :--- | :--- |
| Load | Load an entry form the corresponding dialog. In the moment, this not possible <br> for boundary operators. |
| Edit | Edit the current entry. |
| / Shew View | Shows the currently set entry. |

### 34.2 Application of Coatings

Optical surfaces may be coated in order to change their reflection and transmission behavior. So each edit dialog for a surface allows to define such a coating via the coating panel, shown in Fig. 201.


Figure 201. The control for loading, viewing and removing of coatings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Name | Name of the currently set coating. |
| Load | Load a coating from the coating catalog. |
| Q View | Edit the currently set coating. |
| $\times$ Remove | Shows the currently set coating. |

### 34.3 Application of Materials

Each medium contains at least one material. So whenever a medium is to be specified, a material has to be set. This is done via the control shown in Fig. 202.


Figure 202. The control for loading or defining and viewing of materials. Left side: Accessing a catalog material. Right side: Defining a material with constant refractive index.

This control ( $\hookrightarrow$ Fig. 202) allows you to either load a material from the catalog or to define a material with constant refractive index directly. It contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Name | Shows the name of the current material. |
| Q View | Shows the view of the currently set material. |
| Catalog Material ${ }^{[\mathrm{PE}}$ / <br> Defined by Constant Refractive Index | If you set this combo box to Catalog Material, the materials catalog is shown where you can select the material. The $\qquad$ button opens the materials catalog again. With the button you can edit the material. <br> In contrast, if you set the combo box to Defined by Constant Refractive Index you can enter the real refractive index directly. |
| \{Value ${ }^{\text {PV }}$ | Available only if Defined by Constant Refractive Index is selected. The constant value of the real refractive index. It is defined absolutely (i.e. referring to vacuum) and applies for a wavelength range of $10 \mathrm{pm} . . .0 .1 \mathrm{~m}$. |
| State of Matter | Shows the state of matter of the current material. If the material is Defined by Constant Refractive Index, you can change this entry. This information is needed for the orientation of coatings on surfaces. |

## VI Building Blocks: Media, Materials, Surfaces, ...

Complex optical components are built up from simple Building Blocks:

- Optical Surfaces ( $\leftrightarrows$ Sec. 35)
- Coatings ( $\leftrightarrows$ Sec. 36)
- Media ( $\rightarrow$ Sec. 37)
- Materials ( $\leftrightarrows$ Sec. 38)
- Stacks ( $\rightarrow$ Sec. 39)
- Surface Layouts ( $\leftrightarrows$ Sec. 40)
- Boundary Responses ( $\leftrightarrows$ Sec. 41) and
- Surface Regions ( $\leftrightarrows$ Sec. 42)

Some types of Optical Building Blocks contain other Building Blocks (e. g. a medium contains materials). In VirtualLab Fusion most Building Block categories have their own catalog. The general catalog concept is explained in Part V .

## 35 Optical Surfaces

Optical Surfaces separate two optical media ( $\hookrightarrow$ Sec. 37) and represent the borders of real optical components ( $\hookrightarrow$ Part IX). Every Optical Surface can be provided with an optical thin film coating ( $\hookrightarrow$ Sec. 36). There is a Surface Catalog, storing several predefined Optical Surfaces as well as a variety of templates of different surface types.
Please note: If you save a coated Optical Surface to the catalog, the coating will not be saved.
The following (template) types of Optical Surfaces are available in VirtualLab Fusion.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Anamorphic Asphere Surface | A biconic surface with additional coefficients describing a deviation in radial and azimuthal direction. $\hookrightarrow$ Sec. 35.2.1 |
| Aspherical Surface | Allows you to define a rotational symmetric surface using asphere parameters. $\hookrightarrow$ Sec. 35.2.2 |
| Combined Surface | Allows you to combine the height profiles of two distinct surface. $\hookrightarrow$ Sec. 35.2.3 |
| Conical Surface | A surface that can be described as a rotating conic section. $\hookrightarrow$ Sec. 35.2.4 |
| Cylindrical Surface | Allows you to define a axially symmetric surface using asphere parameters. $\rightarrow$ Sec. 35.2.5 |
| Plane Surface | Describes a plane surface which can be tilted around the $x$-axis and the $y$ axis. $\hookrightarrow$ Sec. 35.2.7 |
| Polynomial Surface | A conical surface which is modulated by a polynomial separable in $x$ - and y-direction. $\hookrightarrow$ Sec. 35.2.8 |
| Programmable Surface | Allows you to enter the height profile as a formula. $\hookrightarrow$ Sec. 35.2.9 |
| Q-Type Asphere Surface | An asphere described by the polynomials proposed in [For07]. $\hookrightarrow$ Sec. 35.2.10 |
| Sampled Surface | Allows you to set an arbitrary height profile. $\hookrightarrow$ Sec. 35.2.11. |
| Toroidal Asphere Surface | An aspherical cross section rotated about the y-axis. $¢$ Sec. 35.2.12 |
| Transition Point List Surface | This surface allows you to define arbitrary heights at arbitrary positions along a line. $\hookrightarrow$ Sec. 35.2.13 |
| Zernike Standard Surface | Defines an surface by Zernike polynomials $Z_{i}(\rho, \phi)$ using polar coordinates $(\rho, \phi) . \hookrightarrow$ Sec. 35.2.14 |
| Grating Surfaces | $\hookrightarrow$ Sec. 35.2.6. Rectangular gratings ( $\hookrightarrow$ Sec. 35.2.6.1), sawtooth gratings ( $\leftrightarrows$ Sec. 35.2.6.2), sinusoidal gratings ( $\hookrightarrow$ Sec. 35.2.6.3), and triangular gratings ( $\hookrightarrow$ Sec. 35.2.6.4) are available. |

### 35.1 Edit Dialog for Optical Surfaces



Figure 203. Edit dialog for an optical surface (here: plane surface)
The edit dialogs for all surface types (see for example Fig. 203) have the following controls in common:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Definition Area | $\hookrightarrow$ Sec. 35.1.1.1. |
| 39] View | Shows a 3D view of the surface as described in Sec. 35.3. |
| HSave | Saves the surface to the catalog ( $\hookrightarrow$ Sec. 33). Not visible if the edit dialog is shown from within the surfaces catalog. |
| Tools | $\hookrightarrow$ Sec. 35.1.3. |
| Validity Indicator | The parameters of a surface must fulfill some complex constraints. For example the conical constant of a surface determines its maximum definition area. If any of these constraints is breached, the green check mark $\sigma$ on the bottom of the surface dialog turns into a red diagonal cross $\boldsymbol{\otimes}$. If you click on the -button to the right, an info dialog is shown which lists all error messages. For constraints concerning the definition area and periodization, this dialog offers a link to a visualization of the current (approximated) function domain, the definition areas and the period of the surface ( $\hookrightarrow$ Sec. 35.1.1) . |
| Coating tab | The controls on the Coating ${ }^{[\operatorname{PE}}$ tab are explained in Sec. 34.2. Not visible if the edit dialog is shown from within the Surfaces Catalog or from within a stack ( $\rightarrow$ Sec. 39) . |
| Discretization tab | $\hookrightarrow$ Sec. 35.1.2 |
| Scaling tab | $\hookrightarrow$ Sec. 35.1.2 |
| Periodization tab | $\hookrightarrow$ Sec. 35.1.1.2 |

### 35.1.1 Definition Area and Periodization

A surface can be set to be periodical. In the non-periodical case you can set up the (Inner) Definition Area ${ }^{\text {P® }}$ of the surface. This means that you define the Size and Shape of the definition area and how it behaves Outside of the definition area. The corresponding control is described in more detail in Sec. 35.1.1.1.
The specified definition area should lie completely within the Approximated Function Domain ( $\hookrightarrow$ Sec. 133.1.1) which depends on the type and the parameters of the actual surface. If this constraint is breached, it is shown as ! in the Validity indicator. It is ensured that a definition area exceeding the function domain yields still a valid surface, but possibly with sharp "bends" or very large height values. For example the function domain of a spherical surface is a circle with a radius equal to its radius of curvature. But for a toroidal surface only an approximated function domain can be calculated numerically.
On the Periodization tab you can define whether to Use Periodization and if yes, what Period ${ }^{[\mathrm{PV}}$ the surface has. In this case the height profile as defined in the Structure tab is replicated periodically whereas only rectangular "elementary cells" are supported. If the inner definition area is smaller than the period, the surface does not fill the whole elementary cell.
The Outer Definition Area ${ }^{[\mathrm{PE}}$ which can be also set up on the Periodization tab ( $\hookrightarrow$ Sec. 35.1.1.2) defines the overall size of the surface. Fig. 204 shows an example for a periodical surface.
The inner definition must not be larger than the period and the period must not be larger than the outer definition area. This is also shown by the Validity indicator.


Figure 204. Definition of Inner and Outer Definition Area, Period and Approximated Function Domain using the example of a periodical conical surface. Left: 3D view. Right: Section

Grating surfaces are always periodical and have an inner definition which is always equal to the period.

### 35.1.1.1 Definition Area Control



Figure 205. Definition area control used for setup of definition areas of optical surfaces.

This control ( $\hookrightarrow$ Fig. 205) lets you specify Size and Shape of the definition area of a surface and how it behaves outside, i. e. the Effect on Field Outside of Definition Area.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Shape ${ }^{\text {PE }}$ | You can choose whether the actual definition area of the control has a Rectangular or an Elliptical shape. |
| Size ${ }^{\text {PV }}$ | Specify $x$ - and $y$-extension of the actual definition area. With a double-click on either the $x$ - or the $y$-extension box you can turn the definition area into a circular or quadratic one, respectively. |
| Effect on Field Outside of Definition Area | Outside of the definition area always a plane surface is added. This plane surface either behaves as normal surface (i.e. Field Passes Plane Surface) or as completely absorbing surface (i. e. Field is Absorbed). |
| Position of Surrounding Absorbing Plane / <br> Position of Surrounding Surface Plane | The value z-Position gives the position of the plane that surrounds the definition area and which either absorbs the field or lets it pass, depending on the setting of Effect on Field Outside of Definition Area. A value of 0 m is identical to the surface's location at the lateral position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ). If the Specification Mode is set to User Defined, you can set an arbitrary value. For the other specification modes, the height is determined automatically, see below. |
| Specification Mode | The mode to specify the Position of Surrounding Surface / Absorbing Plane. This can be equal to one of the following positions, that are also shown in Fig. 206: <br> - The maximum height value in the definition area (Area Maximum), <br> - the minimum height value in the definition area (Area Minimum), <br> - the maximum height value along the boundary of the definition area (Boundary Maximum), or <br> - the minimum height value along the boundary of the definition area (Boundary Minimum). |



Figure 206. The different specification modes for the position of that plane which surrounds the definition area of a surface.

### 35.1.1.2 Periodization



Figure 207. The periodization tab of the edit dialog for surfaces.

This tab ( $\hookrightarrow$ Fig. 207) allows you to specify the parameters for the periodization of optical surfaces.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Period ${ }^{\text {PV] }}$ | Specify $x$ - and y -extension of the period. |
| Shape | You can choose whether the outer definition area of the control has a Rectangular or an Elliptical shape. |
|  | Specify $x$ - and $y$-extension of the outer definition area. |
| Effect on Field Outside of Definition Area | Outside of the definition area always a plane surface is added. This plane surface either behaves as normal surface (i. e. Field Passes Plane Surface) or as completely absorbing surface (i. e. Field is Absorbed). |
| Position of Surrounding Absorbing Plane / Position of Surrounding Surface Plane | The value z-Position gives the position of the plane that surrounds the definition area and which either absorbs the field or lets it pass, depending on the setting of Effect on Field Outside of Definition Area. A value of 0 m is identical to the surfaces location at the lateral position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ). If the Specification Mode is set to User Defined, you can set an arbitrary value. For the other specification modes, the height is determined automatically, see below. |
| Specification Mode | The mode to specify the Position of Surrounding/Surface Absorbing Plane. This can be equal to one of the following positions, that are also shown in Fig. 206: <br> - The maximum height value in the definition area (Area Maximum), <br> - the minimum height value in the definition area (Area Minimum), <br> - the maximum height value along the boundary of the definition area (Boundary Maximum), or <br> - the minimum height value along the boundary of the definition area (Boundary Minimum). |
| Edit Inner Definition Area | This link is a shortcut to the Structure tab, where you can set the Inner Definition Area as described above in Sec. 35.1.1.1. |

### 35.1.2 Height Discontinuities and Rescaling of Surfaces

VirtualLab Fusion allows to scale any surface in $x$-, $y$-, and $z$-direction, respectively. Furthermore, VirtualLab Fusion offers three mathematical operations which introduce height discontinuities into the height profile of an optical surface.

1. Pixelation introduces rectangular pixels. The height within one pixel remains constant. $\hookrightarrow$ Sec. 35.1.2.1.
2. Height Quantization introduces a limited number of equidistant discrete height levels. The height at a certain position is set to the nearest height level. $\hookrightarrow$ Sec. 35.1.2.2.
3. Using Fresnel zones, the height profile is wrapped so that all height values lie within a certain interval. $\hookrightarrow$ Sec. 35.1.2.3.
The following equation shows how and in which order these surface manipulations are applied.

$$
\begin{equation*}
h(x, y)=\mathcal{Q}\left(\zeta \mathcal{R}\left(h^{\prime}\left[\mathcal{P}\left(\frac{x}{\tilde{\xi}}\right), \mathcal{P}\left(\frac{y}{\eta}\right)\right]\right)\right) \tag{35.1}
\end{equation*}
$$

$h^{\prime}(x, y)$ is the original height profile, e.g. that of a conical surface. $h(x, y)$ is the height profile after applying the aforementioned manipulations. $\xi, \eta$ and $\zeta$ represent a Scaling in $x$-Direction, Scaling in $y$-Direction, and Scaling in z-Direction, respectively. These settings can be found on the Scaling tab of a surface dialog ( $\hookrightarrow$ Fig. 208). Obviously, the Scaling in x-Direction and the Scaling in y-Direction effect the Approximated Function Domain ( $\hookrightarrow$ Sec. 35.1.1). The Scaling in z-Direction must not be zero, a negative Scaling in z-Direction means that the height profile is inverted.
$\mathcal{P}(a)$ refers to the pixelation operator ( $\hookrightarrow$ Sec. 35.1.2.1), $\mathcal{Q}(h)$ to the quantization operator ( $\hookrightarrow$ Sec. 35.1.2.2), $\mathcal{R}(h)$ to the fresnelization operator ( $\hookrightarrow$ Sec. 35.1.2.3).


Figure 208. The Scaling tab of the edit dialog for surfaces.

### 35.1.2.1 Pixelation

The pixelation function $p(a)$ introduces discrete rectangular pixels in the height profile and is defined as

$$
p(a)= \begin{cases}\operatorname{round}\left(\frac{a}{\Delta a}\right) \Delta a & ; \text { if Use Pixelation is set. }  \tag{35.2}\\ a & ; \text { else }\end{cases}
$$

$\Delta a$ represents the Pixel Size ${ }^{\mathbb{P V}}$ along the x - or y -axis. The pixel size is in general different along both axes. Note, according to Eq. (35.1), the resulting pixelation effect (the size of a region for which the height is constant) is influenced by the scaling parameters $\beta$ (scaling in x-direction) and $\gamma$ (scaling in y-direction). Use Pixelation and the Pixel Size can be set on the Height Discontinuities tab of a surface dialog ( $\hookrightarrow$ Fig. 209).


Figure 209. The pixelation settings for a surface which can be found on the Height Discontinuities tab of its edit dialog.

The Sampled Surface contains discrete, equidistantly sampled height values with sampling distances $\delta x$ and $\delta y$ along the $x$ - and $y$-axis, respectively. An additional interpolation method creates a continuous surface profile from these sampling points. If a user selects Nearest Neighbor as Interpolation Method in the sampled surface, rectangular pixels will always appear. Hence pixelation cannot be disabled then and the pixel sizes are fixed to $\delta x \cdot \delta y$.

### 35.1.2.2 Use Discrete Height Levels (Height Quantization)

The function $q(h)$ introduces discrete height levels in an optical surface and is defined as

$$
q(h)=\left\{\begin{array}{ll}
h & \text { if Use Discrete Height Levels (Height Quantization) is not set. }  \tag{35.3}\\
q_{\min } & \text { if } h_{\min } \leq h<q_{\min } . \\
q_{\max } & \text { if } q_{\max }<h \leq h_{\max } . \\
\text { round }\left(\frac{h-q_{\min }}{\Delta h}\right) \Delta h+q_{\min } & \text { else }
\end{array} .\right.
$$

$q_{\text {min }}$ and $q_{\text {max }}$ are the minimum and the maximum height level of the discretized height profile, respectively. $\Delta h$ is the height difference between two consecutive height levels and is defined as

$$
\begin{equation*}
\Delta h=\frac{q_{\max }-q_{\min }}{n-1} \tag{35.4}
\end{equation*}
$$

$h_{\text {min }}$ represents the minimum height of the original non-discretized surface and $h_{\text {max }}$ its maximum height. $n$ is the Number of Discrete Height Levels between and including $q_{\min }$ and $q_{\text {max }}$. The function round $(x)$ returns the integer value closest to $x$.
VirtualLab Fusion offers three quantization modes differing in the choice of $q_{\text {min }}$ and $q_{\text {max }}$.


Mathematical details can be found in Sec. 133.1.2.2.
The quantization of a surface can be configured on the Height Discontinuities tab of its dialog. The corresponding controls are shown in Fig. 210 and described below.


Figure 210. The controls which can be used to configure the quantization of a surface.

ITEM DESCRIPTION
Use Discrete Height Lev- Switches the height quantization of a surface on and off.
els (Height Quantization) els (Height Quantization)
Number of Discrete Height The number $n$ of discrete height levels. Must not exceed 4096.
Levels ${ }^{[P V}$

| Quantization Mode | Allows you to select any of the three quantization modes explained in <br> Sec. 133.1.2.2 (Min-Max-Tread, Min-Max-Riser, or User Defined Min- and <br>  <br> Max-Levels). |
| :--- | :--- |
| Minimum / | Allows you to set $h_{\mathrm{q}, \min }$ and $h_{\mathrm{q}, \text { max }}$, if in user defined mode. The dialog en- |
| Maximum | sures that $q_{\min }<q_{\max }$. Note that according to Eq. (35.1), the allowed values <br> for $q_{\min }$ and $q_{\max }$ are influenced by the Scaling in z-Direction. |

### 35.1.2.3 Fresnel Zones



Figure 211. The controls for configuring the Fresnel zones of a surface. They can be found on the Height Discontinuities tab of a surface edit dialog.

The following table describes the controls ( $\hookrightarrow$ Fig. 211) which can be used to introduce Fresnel zones. A mathematical description and some explaining figures are given below.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Fresnel Zones | "Folds" the height profile so that the resulting surface contains so-called Fres- <br> nel zones. |
| Fresnel Height ${ }^{[\text {PV }}$ | The difference between the maximum and the minimum height values in the <br> surface after Fresnel zones have been introduced. |
| Relative Position on $\mathbf{z -}$ <br> Axis | The size of the innermost Fresnel zone can be adjusted by the Relative Po- <br> sition on z-Axis. |

If you Use Fresnel Zones the height profile is "folded" so that all height values lie in the interval $-p \cdot h_{\mathrm{t}} \ldots(1-$ p) $h_{\mathrm{t}}$. $h_{\mathrm{t}}$ refers to the Fresnel Height and $p$ refers to the Relative Position on z-Axis.

Thus, if the Relative Position on z-Axis is set to $0 \%$ the height values range from 0 to $+h_{\mathrm{t}}$. This is the recommended setting for a height profile containing only positive height values (e.g. a conical surface with positive radius of curvature).
Vice versa, a Relative Position on z-Axis of $100 \%$ is recommended for surfaces with only negative height values as then the height values are in the range $-h_{\mathrm{t}} \ldots 0$.
Any intermediate relative position is of course also feasible. Fig. 212 shows an example for the effect of the relative position.


Figure 212. Cross section of a cylindrical surface with positive radius of curvature and Fresnel zones. The subfigures illustrate the effect of different values for the Relative Position on z-Axis $p$.
Top: $p=0 \%$. Height values range from 0 to 2 mm . Middle: $p=50 \%$. Height values range from -1 to 1 mm . Bottom: $p=99.99 \%$. Height values range from (nearly) -2 to (nearly) 0 mm .

Note that the Scaling in z-Direction is applied after introducing the Fresnel zones. Thus the scaling in z-direction does not influence the positions of the Fresnel "jumps" but the total profile height of a surface with Fresnel "jumps" is the scaling factor $\alpha$ times the set Fresnel Height.

### 35.1.3 Surface Tools

The Tools-button opens a menu containing the following items:

| ITEM | DESCRIPTION |
| :---: | :---: |
| 國 View Surface | Shows the surface in the dialog described in Sec. 35.3. |
| Hell Save to Catalog | Saves the surface to the catalog ( $\leftrightarrows$ Sec. 33). Not visible if the edit dialog is shown from within the surfaces catalog. |
| Tlimport | In the moment, this item is only available for the sampled surface $(\leftrightarrows$ Sec. 35.2.11): Either GDSII, CIF, text or bitmap data can be imported if a parameter summary file is provided in the XML format explained in Sec. 127.4. |
| $]^{3}$ Export | Exports the surface to various text and binary formats. $\leftrightarrows$ Sec. 127.1. |

### 35.2 Surface Types

In this section, the types of Optical Surfaces provided by VirtualLab Fusion are described. They can be accessed as templates in the Surface Catalog.

### 35.2.1 Anamorphic Asphere Surface

This surface is a biconic surface with additional coefficients describing a deviation in radial and azimuthal direction.
Its height function is defined by

$$
\begin{equation*}
h(x, y)=\frac{c_{x}^{2}+c_{y}^{2}}{1+\sqrt{1-\left(1+\kappa_{x}\right) c_{x}^{2} x^{2}-\left(1+\kappa_{y}\right) c_{y}^{2} y^{2}}}+\sum_{i=2}^{n} a_{\mathrm{r}, i}\left(\left(1-a_{\mathrm{p}, i}\right) x^{2}+\left(1+a_{\mathrm{p}, i}\right) y^{2}\right)^{i} \tag{35.5}
\end{equation*}
$$

$c_{x}$ and $c_{y}$ are the curvatures in $x$ - and $y$-direction, respectively, with

$$
\begin{equation*}
c_{x}=\frac{1}{R_{x}} \quad \text { and } \quad c_{y}=\frac{1}{R_{y}} \tag{35.6}
\end{equation*}
$$

$R_{x}$ and $R_{y}$ are the radii of curvature of the surface and $\kappa_{x}$ and $\kappa_{y}$ the conical constants in $x$ and $y$ direction. $a_{r, i}$ are the radial and $a_{\mathrm{p}, i}$ the azimuthal coefficients of the surface.


Figure 213. Dialog for defining an anamorphic asphere surface.
Fig. 213 shows the edit dialog where the specific parameters of the anamorphic asphere surface can be set.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Radius of Curvature ${ }^{\text {PV }}$ | The radii of curvature $R_{x}$ and $R_{y}(\hookrightarrow$ Eq. (35.6)) of the surface in meters. |
| Conical Constant ${ }^{[\mathrm{PV}]}$ | The conical constants $\kappa_{x}$ and $\kappa_{y} . \hookrightarrow$ Eq. (35.5); see also Sec. 35.2.4 |
| Maximum Order | The maximum order $2 n$ of the additional polynomial. $\hookrightarrow$ Eq. (35.5) |
| \{Coefficients Table\} | In this table you can specify the radial coefficient $a_{r, i}{ }^{\text {PVV }}$ and the azimuthal co- <br> efficients $a_{r, i}{ }^{[\mathbb{P V}}$ of each order $2 i$. Its physical units are given in square brackets <br> in the column headers. $\hookrightarrow$ Eq. (35.5) |

Via the context menu of the table you can copy and paste the parameter list.
The remaining controls are explained in Sec. 35.1.

### 35.2.2 Aspherical Surface

The profile height $h(x, y)$ of an aspherical surface is defined by an expression of the form

$$
\begin{equation*}
h(x, y)=\underbrace{\frac{c r^{2}}{1+\sqrt{1-(1+\kappa) c^{2} r^{2}}}}_{\hookrightarrow \text { Sec. 35.2.4 }}+a_{1} r+a_{2} r^{2}+a_{3} r^{3}+\ldots+a_{n} r^{n} \tag{35.7}
\end{equation*}
$$

where the first part is the height function of a conical surface which is explained in detail in Sec. 35.2.4. $r=$ $\sqrt{x^{2}+y^{2}} ; a_{1} \ldots a_{n}$ are the additional asphere parameters.
Fig. 214 shows the edit dialog where the specific parameters of the aspherical surface can be set.


Figure 214. Dialog for defining an aspherical surface.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Radius of Curvature ${ }^{\text {PV }}$ | The radius of curvature $R(\hookrightarrow$ Sec. 35.2.4) of the surface in metric units. |
| Conical Constant ${ }^{\text {[V] }}$ | The conical constant $\kappa$ ( $\checkmark$ Sec. 35.2.4) |
| Number of Orders | The number $n$ of the additional Aspherical Parameters ${ }^{\boxed{P V}} a_{i}$. The length of the table for entering these parameters depends on this number. |
| Order | The order $i$ of the asphere parameter $a_{i}$, that is specified by Parameter Value. Its physical unit is given in square brackets: [unit]. |
| Parameter Value | Value of the asphere parameter $a_{i}(\hookrightarrow$ Eq. (35.7)), whereas $i$ is given by Order. |

Via the context menu of the table you can copy and paste the parameter list.
The remaining controls are explained in Sec. 35.1.

### 35.2.3 Combined Surface

A combined surface is the result of adding the profile heights of two sub-surfaces. As an example, sophisticated optical surfaces can be achieved by combining an asphere with a sampled surface.
Fig. 215 shows the Edit dialog, where the specific parameters of the combined surface can be set.


Figure 215. Dialog for defining a combined surface.

ITEM
Surface 1/2 ${ }^{\text {四 }}$

DESCRIPTION
The surfaces which shall be combined can be specified by standard catalog access ${ }^{1}$ in VirtualLab Fusion. The user can also edit and view the selected surfaces. For these surfaces, always Field Passes Plane Surface is selected as Effect on Field Outside of Definition Area - an addition of an absorbing and a transparent height profile is not well defined.

The remaining controls are explained in Sec. 35.1.

### 35.2.4 Conical Surface

Conical surfaces are a special kind of second order surfaces, that can be described as rotating conic sections. They are also well known as hyperboloid, paraboloid, ellipsoid and sphere and are defined by

$$
\begin{equation*}
h(x, y)=\frac{c r^{2}}{1+\sqrt{1-(1+\kappa) c^{2} r^{2}}} \tag{35.8}
\end{equation*}
$$

where $c$ denotes the curvature, $\kappa$ the conical constant and $r=\sqrt{x^{2}+y^{2}}$ the lateral distance to the optical axis. The value of the conical constant determines the type of the surface, i.e. $\kappa<-1$ gives a hyperboloid, $\kappa=-1$ a paraboloid, $-1<\kappa<0$ gives a prolate ellipsoid, $\kappa=0$ a sphere and $\kappa>0$ an oblate ellipsoid.
The curvature is connected to the radius of a sphere ( $R=\sqrt{x^{2}+y^{2}+z^{2}}$ ) or to the vertex radius of a paraboloid ( $R=\left(x^{2}+y^{2}\right) /(2 z)$ ) by $c=1 / R$. This radius is also called Radius of Curvature.
For an ellipsoid or a hyperboloid the parameters $c$ and $k$ can be calculated from its semi axes $a$ and $b$ using the relationships

$$
\begin{equation*}
\frac{1}{c}= \pm \frac{b^{2}}{a} \text { and } \kappa=-\frac{\left(a^{2}-b^{2}\right)}{a^{2}} \tag{35.9}
\end{equation*}
$$

The intersection points of the light and the surface are calculated analytically.

[^5]Fig. 216 shows the Edit dialog, where the required values to define a conical surface can be entered.


Figure 216. Dialog for defining a conical surface.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Radius of Curvature ${ }^{\text {PV }}$ | The radius of curvature (in the vertex) $r(\hookrightarrow$ Eq. (35.8)) of the conical surface <br> in metric units. |
| ${\text { Conical Constant }{ }^{[\mathrm{Pv}}} \quad$ The conical constant $\kappa . \hookrightarrow$ Eq. (35.8). |  |

The remaining controls are explained in Sec. 35.1.

### 35.2.5 Cylindrical Surface

The only difference between the Cylindrical and the Aspherical Surface is the symmetry. While the last one is circular symmetric, the first one has one prime axis (axis of symmetry). So the surface is defined by Eq. (35.7) too, but with the substitution $r=|x \cos (\alpha)+y \sin (\alpha)|$, where $\alpha$ denotes the rotation angle of the axis of symmetry relative to the $y$-axis ( $\hookrightarrow$ Fig. 217). Please note that there is a refraction effect perpendicular to the axis of symmetry only, i. e. parallel to the direction given by $\alpha$.
Fig. 218 shows the edit dialog, where the specific parameters of the cylindrical surface can be set.


Figure 217. Sketch of a cylindrical surface, rotated by an angle $\alpha$.


Figure 218. Dialog for defining a cylindrical surface.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Radius of Curvature ${ }^{\text {PV }}$ | The radius of curvature $r$ ( $\leftrightarrows$ Eq. (35.7)) of the cylindrical surface in metric units. |
| Conical Constant ${ }^{\text {PV }}$ | The conical constant $\kappa$. ↔Eq. (35.7); see also Sec. 35.2.4 |
| Number of Orders | The number of orders, i. e. the number of the additional Aspherical Parameters ${ }^{\mathbb{P V}]} a_{n}$. The length of the table for entering these parameters depends on this number. |
| Order | The order $n$ of the asphere parameter $a_{n}$, that is specified by Parameter Value. Its physical unit is given in square brackets: [unit]. |
| Parameter Value | Value of the asphere parameter $a_{n}(\hookrightarrow \mathrm{Eq} .(35.7))$, whereas $n$ is given by Order. |
| Rotation Angle ${ }^{\text {[V] }}$ | The angle ( $\alpha$ in Fig. 217) between the axis of symmetry $y$ ' and the $y$-axis. The rotation is done in the $x-y$-plane and is defined as positive rotation about the z-axis. |

Via the context menu of the table you can copy and paste the parameter list.
The remaining controls are explained in Sec. 35.1.

### 35.2.6 Grating Surfaces

To simulate the optical behavior of gratings, it is possible to use different types of one-dimensional and periodically varying profiles. All of these have some basic values in common:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Grating Period ${ }^{\text {PV }}$ | The period of the surface's height profile in metric units. |
| Modulation Depth ${ }^{\text {[VV }}$ | The amplitude of the height modulation. Please see also the "Note on quantization" below. |
| Lateral Shift ${ }^{\text {PV }}$ | A shift of the surface in the direction of the modulation. Please pay attention: Usually this lateral shift will also cause a change of the surface position on the optical axis (which means a change in the distances to other surfaces too). This is due to the definition of the object position as the intersection point of the surface with the optical axis. |
| Rotation Angle ${ }^{\text {PV }}$ | Per default, the periodical modulation is defined along the x-axis. By using this parameter, the modulation direction can be changed by rotation about the $z$-axis. |

Grating surfaces are always periodical and have an inner definition area which is always equal to the period. The Period on the Periodization tab is always determined from the Grating Period and Rotation Angle.
The remaining controls are explained in Sec. 35.1.
As an example Fig. 219 shows the Edit dialog for a sinusoidal grating surface.


Figure 219. Edit dialog for a sinusoidal grating surface showing the basic grating parameters.

### 35.2.6.1 Rectangular Grating Surface

A rectangular grating surface is shaped as shown in Fig. 220.


Figure 220. Shape of an unshifted rectangular modulated grating surface.

The user can either specify the Slit Width ${ }^{\mathbb{P V}}$ in meters or the Relative Slit Width ${ }^{[\mathrm{PV}}$ as fraction of the period ( $\hookrightarrow$ Fig. 221). For the basic grating surface parameters see Sec. 35.2.6, for the general surface dialog see Sec. 35.1.


Figure 221. Control for defining the rectangular grating surface parameters.

### 35.2.6.2 Sawtooth Grating Surface

The surface has a shape as shown in Fig. 222.


Figure 222. Shape of an unshifted sawtooth grating surface.
For the basic grating surface parameters see Sec. 35.2.6, additionally the inclination of the plane surface sections has to be specified ( $\hookrightarrow$ Fig. 223).

```
Special Sawtooth Grating Values
Inclination O Height Increases with x O Height Decreases with x
```

Figure 223. Radio buttons for defining the inclination (orientation) of a sawtooth grating.

### 35.2.6.3 Sinusoidal Grating Surface

Such kinds of grating surfaces have a sinusoidal height profile ( $\hookrightarrow$ Fig. 224).


Figure 224. Shape of an unshifted sinusoidal grating surface.

There are no further parameters needed to specify this surface, for the basic grating surface parameters see Sec. 35.2.6, for the general surface dialog see Sec. 35.1.

### 35.2.6.4 Triangular Grating Surface



Figure 225. Controls for defining the specific settings for a triangular grating surface.

A Triangular Grating Surface can be defined by either the Projected Side Ratio $\mathbb{D V}=\mathrm{b} / \mathrm{a}$ or the angle Alpha ( $\hookrightarrow$ Fig. 225). The angle Beta is just given as information.
For the basic grating surface parameters see Sec. 35.2.6, for the general surface dialog see Sec. 35.1.

### 35.2.7 Plane Surface

The profile height $h(x, y)$ of a plane surface, which may be tilted with respect to the optical axis, is calculated by

$$
\begin{equation*}
h(x, y)=m_{x} x+m_{y} y \tag{35.10}
\end{equation*}
$$

where $x$ and $y$ indicate the lateral position and $m_{x}$ and $m_{y}$ represent the inclinations of the surface in the specific directions.
The intersection points of the light and the surface are calculated using an analytical formula.
Fig. 226 shows the edit dialog, where the parameters for a plane surface can be entered.


Figure 226. Dialog for defining a plane surface.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Alpha $^{\text {PV }}$ | Angle of the plane surface, measured from the x-axis, representing a rotation <br> about the y-axis. $m_{y}=\tan$ Alpha. $\hookrightarrow$ Eq. $(35.10)$ |
| Beta $^{\text {PV }}$ | Angle of the plane surface, measured from the y-axis, representing a rotation <br> about the $x$-axis. $m_{x}=\tan$ Beta. $\hookrightarrow$ Eq. $(35.10)$ |

The remaining controls are explained in Sec. 35.1.

### 35.2.8 Polynomial Surface

Defines a surface consisting of a rotationally symmetric conical base surface and an additional two-dimensional polynomial. It is defined by the equation:

$$
\begin{equation*}
h(x, y)=\underbrace{\frac{c r^{2}}{1+\sqrt{1-(1+\kappa) c^{2} r^{2}}}}_{\hookrightarrow \text { Sec. 35.2.4 }}+\sum_{i=0}^{m} \sum_{j=0}^{n} a_{i j} x^{i} y^{j} \quad \text { with } \quad r=\sqrt{x^{2}+y^{2}} \tag{35.11}
\end{equation*}
$$

where the first part is the height function of a conical surface which is explained in detail in Sec. 35.2.4.
Fig. 227 shows the edit dialog where the specific parameters of the polynomial surface can be set.


Figure 227. The edit dialog for polynomial surfaces.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Radius of Curvature ${ }^{[\mathrm{PV}}$ | The radius of curvature $R(\hookrightarrow$ Sec. 35.2.4) of the surface in metric units. |
| Conical Constant ${ }^{[\mathrm{PV}}$ | The conical constant $\kappa(\hookrightarrow$ Sec. 35.2.4). |
| Number of Orders | The number $m \times n$ of the additional Polynomial Parameters ${ }^{[\operatorname{PV}} a_{i j}$. The length <br> of the table for entering these parameters depends on this number. |
| Use Absolute Values of <br> Coordinates <br> Order | When you check this option, $\|x\|^{i}\|y\|^{j}$ are used in Eq. (35.11). |
| Parameter Value | The order $(i, j)$ of the polynomial parameter $a_{i j}$, that is specified by Parameter <br> Value. Its physical unit is given in square brackets: [unit]. <br> Value of the polynomial parameter $a_{i j}(\hookrightarrow$ Eq. (35.11)), whereas $i$ and $j$ are <br> given by Order. |

Via the context menu of the table you can copy and paste the parameter list.
The remaining controls are explained in Sec. 35.1.

### 35.2.9 Programmable Surface



Figure 228. Sample edit dialog for a programmable surface.

The programmable surface allows you to define your own surface. The Structure tab of its edit dialog ( $\hookrightarrow$ Fig. 228) contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Snippet for Height Profile | Allows you to program a little code snippet defining the height (in meters) at a certain position $(x ; y)$ (in meters). Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ) to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Numerical Gradient Calculation | For visualization and some propagation operators, not just the height profile but also its gradient is needed. If this option is selected, the gradient is calculated numerically with a given Accuracy Factor. |
| User-Defined Gradient Calculation | If this option is selected, you can program the gradient in dependency from a certain position ( $x ; y$ ) (in meters). Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ) to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Parameters ${ }^{\text {PE] }}$ | The controls in this group box allow you to set the values of the global parameters of the snippet(s). $\hookrightarrow$ Sec. 7.4 |

The remaining controls are explained in Sec. 35.1. General information about programming in VirtualLab Fusion can be found in Sec. 7.

### 35.2.10 Q-Type Asphere Surface

A Q-Type Asphere Surface is the combination of a conical surface ( $\leftrightarrows$ Sec. 35.2.4) and so-called Q-polynomials proposed in [For07]. There are two sets of such polynomials: the $Q^{\text {con }}$ describing strong deviations from a conical surface and the $Q^{\text {bfs }}$ describing mild deviations from a spherical surface. The coefficients of these polynomials give the deviation directly as a length.


Figure 229. The edit dialog for a Q-Type Asphere Surface.

The edit dialog for this surface ( $\hookrightarrow$ Fig. 229) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Define Mild Asphere ${ }^{\text {[®E }}$ | Defines whether the $Q^{\text {bfs }}$ for mild aspheres or the $Q^{\text {con }}$ for strong aspheres are used. |
| Unit Radius ${ }^{\text {PV }}$ | The polynomials are polynomials in $\rho / \rho_{\max }$ with $\rho=\sqrt{x^{2}+y^{2}}$ and $\rho_{\max }$ being the Unit Radius. Within the unit radius the z-extension of the surface is in the range defined by the coefficients. Outside of the unit radius it can become much larger. |
| Radius of Curvature ${ }^{\text {PV }}$ | The radius of curvature $R(\hookrightarrow$ Sec. 35.2.4) of the surface in metric units. |
| Conical Constant ${ }^{[\mathrm{PV}]}$ | The conical constant $\kappa(\hookrightarrow$ Sec. 35.2.4). Always zero for mild aspheres which describe the deviation from a sphere. |
| Number of Orders | The number of monomials used, starting with the constant term. The length of the table for entering these parameters depends on this number. |
| Order | The order $n$ of the Q-polynomial. Note that because of the convention $h(0 \mathrm{~m} ; 0 \mathrm{~m})=0 \mathrm{~m}$, the first order has no effect for strong aspheres (but for mild aspheres). |
| Coefficient ${ }^{[\mathrm{PV}]}$ | Coefficient of the $n$-th monomial of the Q-polynomial in meters. |

The remaining controls are explained in Sec. 35.1.

### 35.2.11 Sampled Surface

A sampled surface is defined by a height profile $h(x, y)$ that represents discrete sampling points. These sampling points can be interpreted as rectangular pixels or they can be interpolated using different interpolation methods.
Fig. 230 shows the Edit dialog, where the specifications for the chosen sampled surface can be set.


Figure 230. Dialog for defining a sampled surface.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Set | Offers you three ways to set a data array describing the height profile (see below). It is assumed that the height profile is centered around the optical axis. The data array must contain only one real-valued, equidistantly sampled subset where both the coordinates and the data have the unit length. The definition area is set to the coordinate extent of the data and the interpolation according to the interpolation of the data array. See also the chapter about interpolation methods ( $\hookrightarrow$ Sec. 131.4) for reference. <br> The settings on the Periodization tab are reset. If you set a one-dimensional profile it is assumed to be unmodulated in the $y$-direction. |
| Set $>$ Load | Loads a data array from a .da file. |
| Set > Import | Imports a data array from a bitmap or text file by means of the import wizard described in Sec. 121.2. |
| Set > Select from Documents | Allows you to select an already open data array. |
| Set > Reset | Resets the height profile to its default (a plane surface sampled with $5 \times 5$ sampling points). |
| Show | Shows the currently set height profile as data array. The height in the center $(0 \mathrm{~m} ; 0 \mathrm{~m})$ is always zero as this is the way the height profile is interpreted by VirtualLab Fusion. |
| Interpolation Method | The four available interpolation methods determine how the height data is interpreted. <br> - Nearest Neighbor: If the data represents a pixelated surface. On the Height Discontinuities tab, Use Pixelation is always true and the Pixel Size is equal to the sampling distance of the imported diagram. <br> - Linear: If the surface consists of areas with constant slope. <br> - Cubic 8 Point: If the data represents a smooth surface. <br> - Fresnel: This interpolation method avoids interpolation artifacts at Fresnel jumps and is thus only to be used for a smooth surface which contains Fresnel zones. If you select this interpolation method, Use Fresnel Zones on the Height Discontinuities tab is always checked and you can enter the Fresnel Height directly below the interpolation selection. |
| Import 筧 | Either GDSII, text or bitmap data can be imported if a parameter summary file is provided in the XML format explained in Sec. 127.4. |

The remaining controls are explained in Sec. 35.1.
If the Interpolation Method is not set to Nearest Neighbor there is an additional surface tool ( $\hookrightarrow$ Sec. 35.1.3) for fitting a smooth surface to the given data. This tool is described in Sec. 35.2.11.1.

### 35.2.11.1 Fit Smooth Surface

VirtualLab Fusion allows you to fit a polynomial to a sampled height profile resulting in either a Cylindrical Surface ( $\hookrightarrow$ Sec. 35.2.5), Aspherical Surface ( $\hookrightarrow$ Sec. 35.2.2), or Polynomial Surface ( $\hookrightarrow$ Sec. 35.2.8). The dialog shown in Fig. 231 allows you to set the options for this fit. The resulting surface is stored in the user-defined surface catalog ( $\hookrightarrow$ Sec. 33) .


Figure 231. The edit dialog for the fit smooth surface tool if the surface type is set to cylindrical surface.

For all surface types you can specify Radius of Curvature and Conical Constant as these parameters are not handled by the fitting algorithm. However, if the number of fitted polynomial orders is sufficiently large a reasonably good fit can be achieved, even if these parameters are the default values.
The Fitting Parameters allow you to set the minimum and the maximum orders taken into account for the polynomial fit. Depending on the selected Surface Type, the actual layout of this group box varies. For the fit of a cylindrical surface you can also preset the Rotation Angle.

### 35.2.12 Toroidal Asphere Surface

This surface originates from an aspherical cross section rotated about the y-axis which results in a section of a torus ( $\hookrightarrow$ Fig. 232).


Figure 232. Principle of a Toroidal Asphere Surface.
Mathematically the cross section with the y-z-plane is described by the asphere formula:

$$
\begin{equation*}
h_{\text {Asp }}(y)=\underbrace{\frac{c y^{2}}{1+\sqrt{1-(1+\kappa) c^{2} y^{2}}}}_{\hookrightarrow \text { Sec. 35.2.4 }}+a_{1} y+a_{2} y^{2}+a_{3} y^{3}+\ldots+a_{n} y^{n} \tag{35.12}
\end{equation*}
$$

whereas $c$ is the inverse Radius of Curvature and $\kappa$ the Conical Constant.
This height profile is shifted by the Toroidal Radius $r_{\top}$ in z-direction and then rotated about the y-axis. The so-generated surface of revolution is shifted back by $-r_{\mathrm{T}}$ in z-direction, so that $h(0 \mathrm{~m} ; 0 \mathrm{~m})=0 \mathrm{~m}$.
$h(x, y)$ can be described by the following formulas and parameters:

$$
\begin{align*}
h_{\text {Asp }}^{\prime}(y) & =r_{\mathrm{T}}-h_{\text {Asp }}(y)  \tag{35.13}\\
h^{\prime}(x, y) & =\sqrt{h_{\text {Asp }}^{\prime 2}(y)-x^{2}}  \tag{35.14}\\
h(x, y) & =r_{\mathrm{T}}-\operatorname{sgn}\left(r_{\mathrm{T}}\right) \cdot h^{\prime}(x, y) \tag{35.15}
\end{align*}
$$



Figure 233. The edit dialog for a Toroidal Asphere Surface.
Its edit dialog ( $\hookrightarrow$ Fig. 233) has the following parameters.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Torus Radius | The toroidal radius $r_{\text {T }}$. |
| Radius of Curvature ${ }^{\text {PV }}$ | The radius of curvature $R$ of the aspherical height profile $h_{\text {Asp }}(y)$. $\rightarrow$ Sec. 35.2.4. |
| Conical Constant ${ }^{\text {PV] }}$ | The conical constant $\kappa$ of the aspherical height profile $h_{\text {Asp }}(y) . \hookrightarrow$ Sec. 35.2.4 |
| Number of Orders | The number $n$ of the additional Polynomial Orders $a_{i}$. The length of the table for entering these parameters depends on this number. |
| Order | The order $i$ of the asphere parameter $a_{i}$. Its physical unit is given in square brackets. |
| Parameter Value ${ }^{\text {PV }}$ | Value of the asphere parameter $a_{n}$ ( $\hookrightarrow$ Eq. (35.12)) with the Order $n$. |

The remaining controls are explained in Sec. 35.1.
35.2.13 Transition Point List Surface


Figure 234. Example for a Transition Point List Surface where the data points (marked by crosses) are distributed nonequidistantly. Between the x-positions that give the height values, the Constant Interval interpolation method is used here.


Figure 235. The edit dialog for a transition point list surface.
The Transition Points List Surface is defined by one-dimensional data specifying the Height ${ }^{[\mathbb{P V}}$ at certain $x$ Positions ${ }^{\text {TVD }}$. That data are not necessarily equidistant (see Fig. 234 for an example). If the x-positions are varied in the parameter run, the data is always considered as non-equidistant.

The Approximated Function Domain ( $\hookrightarrow$ Sec. 35.1.1) of a Transition Point List Surface corresponds to the range of given values, possibly extrapolated by the current Interpolation Method. See also the chapter about interpolation methods Sec. 13.2 for reference.
The dialog is shown in Fig. 235, while the control for the input of the data points is described in Sec. 5.9 in detail.
There are two additional buttons specific for this surface:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Invert Heights | $h(x)$ is replaced by $-h(x)$. |
| Shift Positions | Opens a dialog where you can enter a shift $s$. Each x -position $x$ is then re- <br> placed by $x+s$. |

Furthermore there is an additional surface tool, namely Set Period to Doubled Upper Limit. Before using this tool you should check that your data fills the range $-\chi \ldots+\chi$ as in VirtualLab Fusion periods are always centered around the position $(0 ; 0)$. If this is not the case you might use Shift Positions prior to using this surface tool. This tool is a short cut for doing the following steps:

1. Set the definition area in $x$-direction to twice the Upper Limit $+\chi$.
2. Make the surface periodical and set the x-period to twice the Upper Limit.
3. Set the outer definition area in x-direction to six times the Upper Limit.

The remaining controls are explained in Sec. 35.1.
If you optimize the positions within the parametric optimization ( $\hookrightarrow$ Sec. 102), there is a general Minimum Feature Size constraint. The value of this constraint becomes negative if the order of the transition points changes. Thus you can use this constraint to enforce an unchanged order of the transition points. Features in a periodic surface where one part of the feature is on the beginning of the period and one part is on the end of the period are correctly considered as one feature.

### 35.2.14 Zernike \& Seidel Surface

Zernike fringe, Zernike standard, and Seidel aberrations are often used to describe aberrations within an imaging optical system. The corresponding formulas are given in Sec. 134.2.


Figure 236. The edit dialog for a Zernike \& Seidel Surface in Zernike Standard Aberrations mode.
The Structure tab of the Zernike \& Seidel Surface ( $\hookrightarrow$ Fig. 236) allows the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Unit Radius | Radius which refers to the value $\rho=1$ in the Zernike polynomial. |
| Mode | You can choose between Zernike Fringe Aberrations, Zernike Standard Aber- <br> rations, and Seidel Aberrations. |
| Polynomial Degree | OnLY FOR ZERNIKE STANDARD ABERRATIONS <br> Allows you to set the maximum polynomial degree of the used Zernike terms, <br> and thus indirectly the number of coefficients. |
| \{Coefficients Table\} | Allows you to enter the coefficients of the polynomial describing the aberra- <br> tions. Via the context menu of the table you can copy and paste the parameter <br> list. |
| Reset Tabular | Resets all table entries to 0. |

The remaining controls are explained in Sec. 35.1.

### 35.3 Surface View



Figure 237. Sample surface view.

The surface view ( $\hookrightarrow$ Fig. 237) contains the 3D view control described in Sec. 5.15. On the bottom of the view the z-extension of the surface is shown. Furthermore the Minimum and Maximum Height of the surface are given, whereas a height of zero means the height at the lateral position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ).

## 36 Optical Coatings

For plenty of practical applications of optical systems it is important to have optical coatings on the setup's surfaces at one's disposal. Usually, there are two kinds of effects intended that shall be caused by coatings, which are suppression of reflection on the one hand and maximum reflectivity on the other. For these purposes, a coating is built in the production process by one or more thin films of materials of defined thickness and index of refraction. The necessary combination of the layer parameters is determined by the wavelength the desired effect shall be maximized for. For further information please read [Her90], [Mac01], or [Ran96].
In order to give the user the possibility to work with correct values of reflectance and transmittance of coated elements, there is the Building Block type Coating, which can be applied to most of the surfaces.
Inside the edit dialog of an Optical Surface, a coating can be selected from the catalog as described in Sec. 34.2. While propagating through the system, any type of propagation operator will regard the coating when crossing the surface - provided that the operator is able to consider Fresnel effects.

### 36.1 Types of Optical Coatings

VirtualLab Fusion provides two different kinds of coatings. The first type contains layers of homogeneous, isotropic media only. Processing data which influence the layer thickness in dependence on some process parameters ( $\hookrightarrow$ Sec. 36.2.2) can be defined as well. The regarding template can be found in the coatings catalog as 'Standard Coating'. The other type of coating may contain layers of homogeneous isotropic as well
as anisotropic media. However, processing parameters cannot be specified here. The template for this kind of coating can be found as 'Anisotropic Layer Stack' in the catalog.

|  | Standard Coating | Anisotropic Layer Stack |
| :--- | :---: | :---: |
| Inhomogeneous Layer Media | $\mathbf{x}$ | $\boldsymbol{x}$ |
| Anisotropic Layer Media | $\mathbf{x}$ | $\boldsymbol{\nu}$ |
| Isotropic Layer Media | $\boldsymbol{v}$ | $\boldsymbol{\checkmark}$ |
| Processing Parameters | $\boldsymbol{v}$ | $\boldsymbol{x}$ |

### 36.2 Defining and Editing Optical Coatings

If a new coating is to be created, the coating template (which is part of the Coatings Catalog) has to be provided with a layer system of different media and thicknesses.
In case of Standard Coatings, the edit dialog consists of two panels, the Layer Definition Panel and the Process Data Panel, both described in the following sections. While the layer definition is very similar for both types of coatings, there is no process data definition for Anisotropic Layer Stacks.
Regardless of the type of coating, the following buttons can be found on the bottom of the dialog:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Q | Shows the coating view. $\hookrightarrow$ Sec. 36.3 |
| the | Saves the coating to the catalog. Not available if the coating is edited from <br> within the catalog. |
|  | In case of Standard Coatings, an import for Macleod Coating Data $\hookrightarrow$ Sec. 128 <br> is called by this button. <br> In case of Anisotropic Layer Stacks, a Standard Coating can be imported (i.e. <br> converted) by this button. |

### 36.2.1 Layer Definition

The definition of coatings as stacks of thin layers is done via the edit dialogs shown in Fig. 238.


Figure 238. Layer definition controls of the edit dialog for coatings. Left: The layer definition control for a Standard Coating. Right: The layer definition control for an Anisotropic Layer Stack.

There are two important differences in the definition of Standard Coatings on the one hand and Anisotropic Layer Stacks on the other hand: Since a Standard Coating allows isotropic homogeneous media only, its layer media can always be defined by a single material ( $\varsigma \mathrm{Sec} .38$ ), respectively. Anisotropic Layer Stacks, in contrast, need an Optical Medium ( $\leftrightarrows$ Sec. 37) specification for each layer. The other difference is the need for a definition of the anisotropic medium's orientation in case of an Anisotropic Layer Stack.
All layer definition parameters are described in the following:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index | Index of the layer, counted from the substrate. That means: the higher the <br> index, the higher is the distance of the layer to the substrate's surface. |
| Thickness ${ }^{\text {PV }}$ | Thickness of the layer. For a Standard Coating, this is the initial thickness <br> before applying any process parameters to the coating. |
| Distance | Distance of the upper border of the layer to the substrate. This value can not <br> be changed and is calculated from all thicknesses of the layers with a smaller <br> index. |
| Material ${ }^{[P E}$ | STANDARD CoATINGs onLY. <br>  <br> The material the layer consists of is to be set here. It can be loaded from a <br> catalog, edited or shown via the buttons <br> the table cell when the corresponding row is active. |
| Medium which appear inside |  |

### 36.2.1.1 Repeated Appending of Layer Sequences

Especially high reflection coatings consist of many thin film layers. The stack is built of a replication of the same elementary layer sequence, like for instance $\mathrm{SiO}_{2}-\mathrm{TiO}_{2}-\mathrm{SiO}_{2}-\mathrm{TiO}_{2}-\cdots-\mathrm{SiO}_{2}-\mathrm{TiO}_{2}$.
In order to make the definition of that kind of coatings easier, VirtualLab Fusion provides a tool for the replication of layer sequences (Layer Tools > Append Repeated Layer Sequence). Its configuration dialog is shown in Fig. 239.


Figure 239. Configuration of the Append Repeated Layer Sequence tool.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index of First Layer | Index of that layer, the sequence to append shall start with. |
| Index of Last Layer | Index of that layer, the sequence to append shall end with. |
| No. of Replications | Number of replications of the defined sequence to be appended to the current <br> stack. |

### 36.2.2 Process Data

## Only for Standard Coatings

The properties of a real coating naturally depend on the conditions of the process it was produced in. First of all, its thickness depends on the deposition parameters, like the flow direction of the material. Therefore VirtualLab Fusion allows to specify some of these parameters in case of Standard Coatings. The modeling is done according to the Hertz-Knudsen-Law ( $\hookrightarrow$ Sec. 133.2).


Figure 240. Process data panel of the edit dialog of coatings.

The panel shown in Fig. 240 contains the parameters to adapt the simulated coating to its processing. They are summarized in the following table.

ITEM
DESCRIPTION

| Coating Thickness De- <br> pends on Normal Vector <br> of Substrate Surface | If checked, consider the normal vector of the surface, i.e. the surface of the |
| :--- | :--- |
| substrate, for the calculation of the coating thickness. |  |



Figure 241. Sketch of the meaning of the processing parameters of coatings.

### 36.3 Coating View

The view for coatings is shown in Fig. 242 (Diagram tab) and Fig. 243 (Coefficients Calculator tab).
Please note: Even if the same view is used for Standard Coatings and Anisotropic Layer Stacks, the shown values and the diagram are only of limited value in case of the latter. There are two reasons for this restriction: At first, The incident wave is always assumed to lie in the x-z-plane. Secondly, only the main diagonal values of the complete Fresnel matrix are used for the view. So, in case of Anisotropic Layer Stacks, the view should only be used cautiously.


Figure 242. Example for a coating view, showing the dependence of the transmittance on the wavelength for an angle of incidence of $50^{\circ}$ for TE and TM polarization.


Figure 243. Example for the coating coefficients calculator.

Besides the name of the coating and the categories it belongs to, the document always shows the wavelength range, the coating data are defined for:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Min. Wavelength | The minimum vacuum wavelength the materials in the coating layers are de- <br> fined for. |
| Max. Wavelength | The maximum vacuum wavelength the materials in the coating layers are <br> defined for. |

TE and/or TM polarization. The diagram view can be configured via a configuration dialog ( $\hookrightarrow$ Sec. 36.3.1) which is called by the button Configure Diagram.
The Coefficient Calculator tab allows calculating reflectance and transmittance for a given wavelength and angle of incidence:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vacuum Wavelength | Wavelength to calculate reflectance $R$ and transmittance $T$ of this coating for. |
| Angle of Incidence | Angle of incidence to calculate reflectance $R$ and transmittance $T$ of this coat- <br> ing for. |
| Reflectance | Reflectance for the Vacuum Wavelength and the Angle of Incidence. |
| Transmittance | Transmittance for the Vacuum Wavelength and the Angle of Incidence. |

### 36.3.1 Configuration of the Coating View

The dialog for the coating diagram configuration is described in the following sections.

### 36.3.1.1 Parameter Selection Panel



Figure 244. The panel for the selection of the parameters to be drawn.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength $/$ Incidence <br> Angle | Choose whether the dependency on the wavelength or the angle of incidence <br> shall be drawn. |
| Constant Incidence Angle | The incidence angle to show the diagram for, if dependency on Wavelength <br> is chosen. |
| Constant Wavelength | The wavelength to show the diagram for, if dependency on Incidence Angle <br> is chosen. |
| Reflectance / Transmit- <br> tance | Choose whether the reflectance or the transmittance shall be shown. |
| Show TE Coefficient | THIS CAN BE SELECTED ONLY FOR AN ANGLE OF INCIDENCE WHICH IS DIFFER- <br> ENT FROM 0. |
| If selected, one curve for TE polarization is plotted. |  |

### 36.3.1.2 Materials Panel



Figure 245. The panel for the definition of the materials to be used for the calculation.

| ITEM | DESCRIPTION |
| :--- | :--- |
| First Material | Set the material on the incidence side. $\hookrightarrow$ Sec. 34.3 |
| Second Material | Set the material on the transmitting side. $\hookrightarrow$ Sec. 34.3 |
| Coating Orientation <br> Substrate | Defines the orientation of the coating. $\hookrightarrow$ Sec. 34.2 |

### 36.3.1.3 Axes Panel



Figure 246. The panel for the configuration of the axes.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Scale Y-Range Automati- <br> cally. | If selected, the range for the $y$ axis is calculated automatically. |
| Minimum | If Automatic Detection is not chosen, the minimum of the $y$-axis range can be <br> set here. |
| Maximum | If Automatic Detection is not chosen, the maximum of the y-axis range can <br> be set here. |

### 36.3.1.4 Colors

The colors of the curves can be set via this control. Only the color of those curves can be set, which have been selected in the Parameter Selection panel ( $\leftrightarrows$ Sec. 36.3.1.1).


Figure 247. The panel for the curve colors.

## 37 Optical Media

The structural information of an optical system can be understood as a sequence of different homogeneous or inhomogeneous media, separated by optical surfaces ( $\hookrightarrow$ Sec. 35). The first medium in the system is always defined in connection with the light source.
VirtualLab Fusion supports different types of optical media: homogeneous, isotropic media ( $\hookrightarrow$ Sec. 37.3.1) as well as different kinds of inhomogeneous (but isotropic) or anisotropic (but homogeneous) media (Sec. 37.3.2 - Sec. 37.3.14). Homogeneous, isotropic media consist of exactly one material ( $\hookrightarrow$ Sec. 38), while inhomogeneous, isotropic media usually are defined either by several, spatially distributed materials or by one material and a function that gives the spatial variation of the refractive index. The anisotropic, homogeneous media are defined either by two materials (uniaxial crystals), three materials (biaxial crystals) or by two wavelength dependent tensors for permittivity and permeability (general anisotropic media).
The application of media is described in Sec. 34.1.

### 37.1 Common Controls for Editing Inhomogeneous Optical Media

All inhomogeneous optical media have their edit dialog divided into three tab pages. The Basic Parameters tab is specific for the particular medium ( $\hookrightarrow$ Sec. 37.3).


Figure 248. The edit dialog of optical media showing the scaling tab.

The Scaling tab ( $\hookrightarrow$ Fig. 248) has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Scaling in $x$-Direction ${ }^{[\mathbb{P V}}$ | The scaling factor for $x$-direction as defined in Sec. 133.3.1. |
| Scaling in y-Direction ${ }^{[\mathbb{P V}}$ | The scaling factor for $y$-direction as defined in Sec. 133.3.1. |
| Scaling in z-Direction ${ }^{[\mathbb{P V}}$ | The scaling factor for $z$-direction as defined in Sec. 133.3.1. |

These three factors must be larger than zero.


Figure 249. The edit dialog of optical media showing the periodization tab.
The Periodization tab ( $\hookrightarrow$ Fig. 249) has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Periodization | If checked, a period for $x$-, $y$-, and / or z-direction can be set. If you do not <br> want periodization for a certain direction, you can set the period to infinity for <br> that direction. |
| Period in x-Direction ${ }^{[\operatorname{PV}}$ | The period $P_{x}$ as defined in Sec. 133.3.1. |
| Period in y-Direction ${ }^{[\mathbb{P V}}$ | The period $P_{y}$ as defined in Sec. 133.3.1. |
| Period in z-Direction ${ }^{[\mathbb{P V}]}$ | The period $P_{z}$ as defined in Sec. 133.3.1. |

The aforementioned controls are disabled if a medium cannot be modulated in the corresponding direction. For example a Sampled Medium ( $\hookrightarrow$ Sec. 37.3.11) can never be modulated in z-direction and thus Scaling in zDirection and Period in z-Direction are disabled and cannot be changed by the user. Furthermore, if a medium is always periodically, its period is calculated from the specific medium parameters and the scaling factors. In this case, all periodization controls are disabled. This affects Pillar Medium (z-Independent) ( $\hookrightarrow$ Sec. 37.3.9) and the Volume Grating Medium ( $\hookrightarrow$ Sec. 37.3.14).
Additionally the edit dialog has a $Q_{\text {-button to show the medium preview ( } \hookrightarrow \text { Sec. } 37.2 \text { ) and alllbuth to save }}$ the medium to the medium catalog.

### 37.2 Medium View

Different types of media need different kinds of views. The next sections will describe these different views.

### 37.2.1 View for Inhomogeneous, Isotropic Media

This medium view ( $\hookrightarrow$ Fig. 250) shows a cross section through the spatial distribution of the refractive index of a medium.

 ( $\hookrightarrow$ Sec. 37.3.6).

Please note: Since optical media are inherently unlimited (spatial limits in modeled optical setups are always defined by surfaces, $\hookrightarrow$ Sec. 35), the view allows unlimited zoom and scrolling as well. That's why the scroll bars behave somewhat unusual: They always jump back to the center position after scrolling and they don't change their size during zooming as well.

### 37.2.1.1 Context Menu

| ITEM | DESCRIPTION |
| :--- | :--- |
| Aspect Ratio | The aspect ratio of the diagram can be changed here ( $\hookrightarrow$ Sec. 11.5). |
| Zoom | These items allow to zoom in or out or into a marked rectangular selection <br> $(\hookrightarrow$ Sec. 11.4). |
| Selection Mode | This option allows to define what happens if mouse clicking or drawing in the <br> diagram is done ( $\hookrightarrow$ Sec. 11.3$).$ |
|  | The rectangular marker can be used for defining a zoom window. The line <br> marker allows to define an arbitrary section plane (see Sec. 37.2 .1 .2 be- <br> low). The point marker is useful for reading medium data at a certain point <br> ( $\leftrightarrows$ Sec. 37.2.1.4). |
| A selection which markers (( $\hookrightarrow$ Sec. 11.3)) are to be visible can be done. |  |

### 37.2.1.2 Panel 'Content'

The Content panel allows to specify what medium data are to be shown in the diagram.


Figure 251. Panel for the configuration of the view content.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Wavelength | Wavelength to be used for calculating refractive index or absorption data. |
| Refractive Index $\mathbf{n}$ / <br> Absorption Coefficient $\alpha$ I <br> Absorption Index $\kappa$ | Which quantity shall be shown? |
| Environment | Only visible if Refractive Index $N$ is selected. <br> Opens a small dialog for defining temperature and pressure for refractive index calculation. |
| Section Plane | The plane to be intersected with the medium is to be selected here. Arbitrary refers to the last plane which has been created via From Marker Line. |
| From Marker Line | Only enabled if a Line Marker is shown. (To be activated via context MENU, $\hookrightarrow$ SEC. 37.2.1.1) <br> An arbitrary section plane can be created by pressing this button. The plane is defined by the current marker line and the normal direction to the currently visible plane. The new view range to be shown is determined by the length of the line marker which will be used as horizontal and vertical extension resp. |
| ```View Range > Default View``` | Only available if Section Plane is different from Arbitrary. (Re-)Sets the visible view range to default values. |
| View Range > Multiple Periods | Only available if the medium is periodically defined. <br> Opens a dialog where the numbers of horizontal and vertical periods to be shown can be defined. If Section Plane is set to Arbitrary, the view range will be approximated. |
| View Range > Free Range Definition | Opens a dialog ( $\hookrightarrow$ Sec. 11.3.1.2) for direct editing of the view range to be shown. |
| $x-/ y-/ z-P o s i t i o n ~ o f ~ S e c t i o n ~$ Plane | Allows to set the position for the section plane along its own normal direction. If Section Plane is set to Arbitrary, the normal and the starting point for the measurement is written to an informational label. |

### 37.2.1.3 Panel 'Appearance'

The Appearance panel allows to specify the color scaling of the diagram.


Figure 252. The panel for the configuration of the color scaling.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Scaling | If checked, the diagram's value range will be adapted automatically to the <br> range of the currently selected quantity to be shown. |
| Minimum | OnLy visible IF AUTOMATIC SCALING IS NOT SELECTED. <br>  <br> The minimum of the selected quantity to be shown. |
| Maximum | ONLY VISIBLE IF AUTOMATIC SCALING IS NOT SELECTED. |
|  | The maximum of the selected quantity to be shown. |

### 37.2.1.4 Panel 'Value at ( $x, y, z$ )'

This panel allows reading all stored media information at one given position $(x, y, z)$ in space.


Figure 253. Panel for reading.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Position X/Y/Z | The position $(x, y, z)$ to read all quantities for. |
| Refractive Index $\mathbf{n} /$ | The real valued refractive index $n$, the absorption coefficient $\alpha$, and the ab- |
| Absorption Coefficient $\alpha$ I | sorption index $\kappa$ for the position $(x, y, z)$. |
| Absorption Index $\kappa$ |  |

The reading position $(x, y, z)$ can be selected by setting the point marker within the diagram. If the position is defined via text-boxes, the marker will be visualized in the diagram. If the position happens to lie outside the shown section plane, the user will be asked whether or not it should be projected onto the plane. Independently from the user's choice, the extracted quantities refer to the given position $(x, y, z)$.

### 37.2.2 View for Anisotropic, Homogeneous Media

This medium view ( $\hookrightarrow$ Fig. 254) shows the index ellipsoid which represent the dependency of the refractive index on the wave direction through an anisotropic medium.


Figure 254. The View for Homogeneous, Anisotropic Media.

The view contains the 3D view control described in Sec. 5.15. The display can be configured with the parameters described in the following sections.

### 37.2.2.1 Content



Figure 255. The panel for the configuration of the content of the view.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | The vacuum wavelength to show the ellipsoid for. |
| Index Ellipsoid / Velocity <br> Ellipsoid | Either the refractive index ellipsoid or the velocity ellipsoid can be shown. <br> Optical Axis / Axes |
|  | If selected, the single optical axis of a uniaxial crystal or the two optical axes <br> of a biaxial crystal are drawn. The circular ellipsoid section each of the axes <br> is perpendicular to is drawn and labeled (with the refractive index which cor- <br> responds to the effect of traveling parallel to the axis) as well. |
| Wave Direction \& Eigen In-  <br> dices If selected, an arbitrary wave direction can be set via Set Direction. It will be <br> visualized in the ellipsoid in conjunction with the elliptical ellipsoid section the <br> direction is perpendicular to. The effective refractive Eigen indices are given <br> as well. <br> Set Direction In case Wave Direction \& Eigen Indices are selected, the wave direction can <br> be set via a dialog (described in Sec. 5.5 ) opening when this button is pressed. |  |

If neither Optical Axes nor Wave Direction \& Eigen Indices are shown, the ellipsoid's principal semi-axes are drawn and labeled.

### 37.2.2.2 Appearance



Figure 256. The panel for the configuration of the appearance of the view.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wireframe | If selected, the ellipsoid will be drawn as wireframe. |
| Density | if Wireframe has been selected, the density of the lines can be set here. |
| Digits | The number of digits to be used for all labels inside the view. |

### 37.2.3 View for Homogeneous, Isotropic Media

For homogeneous, isotropic media, the user can choose whether to visualize the homogeneity or the isotropy of the medium.


Figure 257. The tabs for choosing between visualizing the homogeneity or the isotropy of the medium.

Using the control shown in Fig. 257, the user may select the view described in Sec. 37.2.1 or the one described in Sec. 37.2.2.

### 37.3 Optical Media Types

In this section, the types of Optical Media provided by VirtualLab Fusion are described. They can be accessed as templates in the Media Catalog.

### 37.3.1 Homogeneous Medium

Homogeneous media (which, for the sake of completeness, should be called 'homogeneous and isotropic media') are media which are completely defined by a single Materia/ ${ }^{\text {PE. }}$. Thus their refractive index is independent from the spatial position as well as from the wave direction through the medium. The control for setting this material for the medium is described in Sec. 34.3. The remaining controls are explained in Sec. 37.1.


Figure 258. Dialog for setting up a homogeneous medium.

### 37.3.2 Aperture Medium

The aperture medium consists of two different materials arranged in a way that the lateral cross section looks like an aperture. That means the Outer Material envelops the elliptically or rectangularly shaped Inner Material. For detailed information about materials please see Sec. 38.
The edit dialog of this type of media is shown in Fig. 259.


Figure 259. Dialog for the specification of an aperture medium.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Inner Material $^{[\mathrm{PE}}$ | Control which defines the material inside the aperture. $\hookrightarrow$ Sec. 34.3 |
| Outer Material $^{[\mathrm{PE}]}$ | Control which defines the material outside the aperture. $\hookrightarrow$ Sec. 34.3 |
| Shape | Shape of the Inner Material in a cross section lateral to the optical axis. |
| Diameter ${ }^{[\mathrm{Pv}}$ | Determines the diameter of the Inner Material in $x$ - and y-direction. |

The remaining controls are explained in Sec. 37.1.

### 37.3.3 Biaxial Crystal

Biaxial crystals are anisotropic media which are specified by three principal refractive indices.


Figure 260. Dialog for the specification of a biaxial crystal.

The edit dialog for this kind of medium (shown in Fig. 260) needs the following parameters:
ITEM DESCRIPTION

Material of Principal Index The dispersion relations for the three principal indices $\alpha, \beta$, and $\gamma$ are repre$\alpha / \beta / \gamma \quad$ sented by three materials. The control for setting a material is described in Sec. 34.3.

### 37.3.4 Fiber Medium

| Edit Fiber Medium $\times$ |  |  |
| :---: | :---: | :---: |
| Basic Parameters Scaling | Periodization |  |
| Core Medium GRIN Medium |  |  |
|  |  |  |
| $\square$ Load | / Edit | Q View |
| Cladding Material |  |  |
| Name Fused_Silica |  | $Q$ |
| Catalog Material |  | (1) |
| State of Matter | Solid | $\checkmark$ |
| Core Diameter | $100 \mu \mathrm{~m}$ | $100 \mu \mathrm{~m}$ |
| 9 - | OK | Help |

Figure 261. Dialog for the specification of a fiber medium.

A fiber can be described as a round core (made of an arbitrary medium) which is surrounded by a cladding (made of a homogeneous medium).
The edit dialog of this medium ( $\hookrightarrow$ Fig. 261) has thus the following parameters.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Core Medium | Here you can define the medium of the core using the control described in <br> Sec. 34.1. |
| Cladding Material | Allows you to define the material of the homogeneous cladding medium. This <br> control is described in Sec. 34.3. |
| Core diameter | The diameter of the core. If you enter different values for the x- and y- <br> direction, you can define an elliptical core. Double-clicking into one of the <br> two text boxes inserts the value from the other text box. |

The remaining controls are explained in Sec. 37.1.

### 37.3.5 General Anisotropic Medium

If some anisotropic medium has to be described which cannot be considered being an uniaxial or biaxial crystal, a General Anisotropic Medium can be defined. It is not based on different materials (describing dispersion relations for different principal directions) but provides wavelength dependencies for the permittivity tensor and permeability tensor instead.


Figure 262. Dialog for the specification of a general anisotropic medium.
The edit dialog for this kind of medium (shown in Fig. 262) works with the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Snippet for Permittivity / | The wavelength dependency of the permittivity and permeability tensor has to |
| Permeability Tensor | be programmed by code snippets, resp. Edit opens the Source Code Editor <br> $(\hookrightarrow$ Sec. 7.3$)$ to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10$)$ shows <br> whether this snippet is consistent. |
| Valid Vacuum Wavelength | The wavelength range the defined tensors hold valid for is to be defined via <br> Range |

### 37.3.6 GRIN Medium

A GRIN medium is described by a base material and an analytical formula which alters the (complex-valued) refractive index $n_{0}$ of this base material.


Figure 263. Dialog for editing a GRIN medium.
The edit dialog ( $\hookrightarrow$ Fig. 263) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Base Material ${ }^{\text {PEE }}$ | Defines the base material of the GRIN medium. For a detailed description of the controls within this group box see Sec. 34.3. |
| Rotational Symmetry / Cylindrical Symmetry | You can define a GRIN lens with either Rotational Symmetry (modulation along the radius $r=\sqrt{x^{2}+y^{2}}$ ) or with Cylindrical Symmetry (modulation only along one direction). In the latter case you can additionally set the Rotation Angle ${ }^{\text {PV }} \alpha . \alpha=0^{\circ}$ refers to modulation in x-direction only and $\alpha=90^{\circ}$ refers to modulation in y-direction only. |
| \{Formula\} | This list box lets you choose the equation used for the calculation of the refractive index modulation. The available formulas are described in Sec. 133.3.2. Each equation has different parameters and thus different input controls. |
| Maximum Order $\mathbf{N}$ | Only for the equations Polynomial and Square Root of Polynomial The maximum order $N$ of the polynomial. |
| \{Table ${ }^{[/ \mathrm{PV}}$ | For all equations but Power Law Index Profile Allows you the enter the parameters of the polynomial. |
| Invalidity Substitute ${ }^{\text {PVV }}$ | The resulting refractive index is equal to the Invalidity Substitute in case the actual formula yields zero or negative values (or roots of negative values in case of Square Root of Polynomial). |
| Calculate $g$ from GRIN Lens Parameters | Only for the equation Approximation of sech(s) <br> Opens a dialog where you can calculate the gradient constant $g$ from the so-called pitch $P$ of a GRIN lens and its length $z$. |
| Decrease $\Delta^{[\mathrm{PV}]}$ <br> Outside Value $\mathrm{n}_{1}{ }^{\text {[PV }}$ | Only for the equation Power Law Index Profile <br> The decrease $\Delta$ describes how much the refractive index is decreased till the border $b$. Alternatively you can directly enter the refractive index $n_{1}$ at and outside of the border. The two values are related via $n_{1}=n_{0} \sqrt{1-2 \Delta}$. |
| Border $\mathrm{b}^{\text {PV }}$ | Only for the equation Power Law Index Profile <br> The Power Law Index Profile is usually used to describe an optical fiber with a GRIN profile. In this case, the border $b$ is equal to the core radius of the fiber. |
|  | Only for the equation Power Law Index Profile The (positive) exponent $p$ of the equation is usually close to 2 for GRIN fibers and infinity for step-index fibers. |

The remaining controls are explained in Sec. 37.1.

### 37.3.7 Medium with Inclusions

In the base material of a Medium with Inclusions, spherical ${ }^{1}$ inclusions of another material are embedded. These inclusions are placed at random positions in the elementary cell of the medium ( $\checkmark$ Sec. 133.3.1). Thus, the Medium with Inclusions must always be periodical, which is ensured by its edit dialog. Both the positions and the radii of the inclusions follow a uniform random distribution.

[^6]

Figure 264．Dialog for editing a Medium with Inclusions．
The edit dialog（ $\hookrightarrow$ Fig．264）contains the following controls：

| ITEM | DESCRIPTION |
| :---: | :---: |
| Base Material ${ }^{\text {固 }}$ | Defines the material the inclusions are embedded within．For a detailed de－ scription of the controls within this group box see Sec．34．3． |
| Material within Inclu－ sions ${ }^{\text {国 }}$ | Defines the material the inclusions consist of．For a detailed description of the controls within this group box see Sec．34．3． |
| Diameter Range of Inclu－ sions | Allows to specify the Minimum Inc／usion Diameter ${ }^{[\mathrm{DV}}$ and the Maximum Inclu－ sion Diameter ${ }^{\text {『V }}$ for the diameter random distribution．Both values may be equal in case no size variation is needed． |
| Density of Inclusions ${ }^{\text {®V }}$ | The mean density $\rho$ of the inclusions． <br> The number of inclusions $N$ within the elementary cell is $N=\rho \cdot V$ ，with $V$ being the volume of the elementary cell．Note that even if the medium is Invariant in $y$－Direction，the media period in $y$－direction influences the volume $V$ and thus the number of inclusions． <br> A warning is shown in case <br> －the desired density is so low that less than 0.5 inclusions are to be placed in the elementary cell． <br> －the desired density cannot be achieved due to a too high density or a too small media period． |
| Invariant in y－Direction | If this option is checked，the centers of all inclusions are placed at $y=0$ so the positions vary in the $x$－z－plane only． |
| Seed for Random Genera－ tor ${ }^{\text {PV }}$ | A value which is needed for the generation of the random distribution of the inclusions：With the same value and the same physical settings listed above always the same refractive index distribution will be generated． |

## Create Inclusions <br> Pressing this button will start the generation of the inclusions. Please note: Every parameter change (except for changed materials) requires a new creation in order to become effective!

The remaining controls are explained in Sec. 37.1.

### 37.3.8 Pillar Medium (General)

The Pillar Medium (General) is a periodical medium consisting of a base material with periodically distributed pillars of another material ( $\hookrightarrow$ Sec. 38). In contrast to the Pillar Medium (z-Independent) it supports parameter variation, slanted pillars and round edges; but not elliptical pillars.
An arbitrary amount of pillars can be freely distributed, each with its own lateral extension. The pillars must be well-separated. This means that refractive indices are determined only by the nearest pillar, if at all.


Figure 265. The parameters defining the geometry of a single (circular) pillar.


Figure 266. Basic Parameters tab of the Pillar Medium (General).
The Basic Parameters tab ( $\hookrightarrow$ Fig. 266) has the controls explained below. The other tab pages are explained in Sec. 37.1.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Embedding Material ${ }^{\text {PEE }}$ | Allows the user to define the material outside the pillars by means of the control described in Sec. 34.3. |
| Pillar Material ${ }^{\text {PEE }}$ | Allows the user to define the material inside the pillars by means of the control described in Sec. 34.3. |
| Pillar Geometry | This tab page contains settings for the geometry of all pillars. They are explained in a separate table below. |
| Pillar Distribution | The table on this tab page allows you to define $x$-Position, $y$-Position, and Side Length I Diameter D of each pillar. <br> There are several Table Tools which help you to set up the table (for example add or remove rows). They are explained in a separate table. <br> Furthermore this tab page contains the Import Diameter Data button which allows you to import diameter values on an equidistant grid from a twodimensional data array or (via Import...) from a bitmap or text file by means of the import wizard described in Sec. 121.2. |
| Validity | Indicates problems with the current configuration of the medium by means of the control explained in Sec. 5.10. |

On the Pillar Geometry sub-tab there are the following settings for the geometry of all pillars.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Height ${ }^{\text {PV }}$ | The height $H$ of all pillars. |
| Side Wall Slope Angle ${ }^{\text {PVV }}$ | The angle $\alpha$ defining the slope of the side walls. As you can see in Fig. 265 an angle between $0^{\circ}$ and $90^{\circ}$ means that the side length / diameter of a pillar becomes larger with increasing $z$, and an angle between $90^{\circ}$ and $180^{\circ}$ means that the side length / diameter of a pillar becomes smaller with increasing $z$. |
| Shape ${ }^{\text {® }}$ | A pillar can either have a Squared or Circular shape. In the former case you define the side lengths of the pillars, in the latter the diameters. |
| Definition Mode of Side Lengths / Diameters ${ }^{[\text {PE }}$ | Only if the Side Wall Slope Angle is not $90^{\circ}$, i. e. if the side walls are NOT PERPENDICULAR. <br> As shown in Fig. 265 there are three possible heights where the side length / diameter D can be measured: at the Bottom, the Half Height, or the Top. In case of perpendicular side walls all three values are the same. |
| Round Edges | Only for CIRCULAR PILLARS. <br> Allows you to define round edges at the top and the bottom, respectively, of the side wall. |
| Rounding via Diameter Percentage | Only for Round Edges. <br> If this option is checked, the edge radii are defined relatively to the diameter $D$ of each pillar. Otherwise they are defined absolutely. |
| Edge Radius (Bottom) ${ }^{\text {[/VV }}$ | Only for Round Edges. <br> The edge radius $R_{\text {bottom }}$. Note that this radius can also be negative to define an overhanging pillar. |
| Edge Radius (Top) ${ }^{[\sqrt{\mathbb{V}}}$ | Only for Round Edges. <br> The edge radius $R_{\text {top }}$. Note that this radius can also be negative to define an overhang. |

The following table tools are available:

| TOOL | DESCRIPTION |
| :--- | :--- |
| Add Pillar... | Opens a separate dialog where you can enter Position and Side Length I <br> Diameter of a new pillar which is the added to the end of the table. |
| Remove Current Pillar | Removes the currently selected pillar. The same can be done by pressing <br> the Del key while the table is has the input focus. |
| Reset Table | Resets the table to its initial state (one pillar at position (0 m; 0 m) with a side <br> length / diameter of 100 nm$).$ |
| Add Equidistant Pillars... | Opens a separate dialog where you can enter the Number of Pillars and their <br> Center-to-Center Distance as well as their Side Length / Diameter. <br> If you check Overwrite Existing Data the table contains only these new pillars <br> after you close the dialog with OK. Otherwise the new pillars are simply added <br> to the table. |
| Set Common Side Length | Sets the side length / diameter of all already defined pillars to the same value. |
| Diameter... | Defines how the values in the table are made available for Parameter Extrac- <br> tion. $\hookrightarrow$ Sec. 37.3.8.1 |
| Configure Parameter Vari- |  |
| ation... |  |

### 37.3.8.1 Parameter Variation

There are several ways how the positions and side lengths / diameters of the pillars can be made available for Parameter Extraction ( $\hookrightarrow$ Sec. 43.5).

- Original Values: The values defined in the table are directly made available for parameter extraction. This means that for each pillar Position X, Position Y, and Side Length / Diameter can be varied e.g. in the Parameter Run.
- Deviation of Original Values: For each pillar you can vary the deviation from the original values defined in the table. For example you then can make the side length / diameter of the first pillar 5 nm smaller and the side length / diameter of the first pillar 5 nm smaller.
- Scaling of all Values: The values of all pillars are multiplied with the same scaling factor, whereas there is one Scaling Factor for Positions and one Scaling Factor for Side Lengths / Diameters.

The table tool Configure Parameter Variation... allows you to set this separately for the pillar positions and the pillar side lengths / diameters.
To increase performance in case of very many pillars ( $>1000$ ), consider choosing Scaling of all Values instead of the other two options, especially if Parameter Extraction is not needed for the positions or side lengths / diameters. You can also exclude these parameters completely from Parameter Extraction via an Optical Setup Tool ( $\hookrightarrow$ Sec. 43.5).

### 37.3.9 Pillar Medium (z-Independent)

The Pillar Medium (z-Independent) is a periodical medium consisting of a base material with periodically distributed pillars of another material ( $\hookrightarrow$ Sec. 38). In contrast to the Pillar Medium (General) it supports elliptical pillars; but not parameter variation, slanted pillars and round edges.
The position and shape of the pillars are z-independent. That means that all $x-y$ cross sections through the medium are equal. The shape all pillars of the $x-y$ cross section is either rectangular or elliptical. The pillars are distributed periodically on the $x-y$ cross section. They are grouped in equal rows (along $x$-direction), whereas two consecutive rows can be $x$-shifted to each other, but every other row has the same $x$-shift ( $\hookrightarrow$ Fig. 267).


Figure 267. $x-y$ cross section through a Pillar Medium (z-Independent) with all parameters that can be edited.
Via the edit dialog ( $\hookrightarrow$ Fig. 268) the materials and the geometrical parameters of the medium can be adjusted.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Base Material ${ }^{\text {PEE }}$ | There the user can define the base material ( $\hookrightarrow$ Fig. 268). It is loadable from a material catalog (if Catalog Material is selected) or can be defined by a constant refractive index (if Defined by Constant Refractive Index is selected). |
| Pillar Material ${ }^{\text {PE] }}$ | The pillar material ( $\hookrightarrow$ Fig. 268) is adjustable in the same manner as the base material. |
| Pillar Size and Shape | The size and shape of pillars in the $x-y$ cross section of the medium can be defined there. The pillar cross sections can be of Elliptical or Rectangular shape. The Diameter ${ }^{[\mathrm{PV}}$ is adjustable in x - and y -direction. |
| Horizontal Pillar Distance ${ }^{\text {PV }}$ | $x$-distance between two consecutive pillars within a row of pillars in the $x-y$ cross section ( $\hookrightarrow$ Fig. 268) |
| Vertical Pillar Distance ${ }^{\text {PV }}$ | $y$-distance between two consecutive rows of pillars in the $x-y$ cross section ( $\hookrightarrow$ Fig. 268) |
| Row Shift ${ }^{\text {PV }}$ | Via this parameter the x-shift between two consecutive rows of pillars ( $\hookrightarrow$ Fig. 268) can be adjusted. Any real value can be entered there, but it is internally transformed to the smallest equivalent positive value (smaller than the period in x-direction. |
| Period | The size of a 2D periodical $x-y$-section through the medium can not be entered directly but is calculated from the other geometrical parameters. Both values ( $x$ and $y$ ) are updated after each parameter change. |

The remaining controls are explained in Sec. 37.1.


Figure 268. Dialog for the specification of a Pillar Medium (z-Independent).

### 37.3.10 Programmable Medium

The programmable medium allows you to define an arbitrary, complex-valued refractive index distribution $\widetilde{n}(x, y, z)$ by writing its formula into a little code snippet. If the medium is set to periodic, you can use the variables MediaPeriodX, MediaPeriod $Y$, and MediaPeriodZ in your snippet.


Figure 269. Sample edit dialog for the programmable medium.
The corresponding edit dialog ( $\hookrightarrow$ Fig. 269) contains:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Base Material ${ }^{\text {PE] }}$ | $\hookrightarrow$ Sec. 34.3 <br> The refractive index of the Base Material is always added to the function defined by the snippet if the snippet defines Index Modulation.It is also taken into account for the optical path length calculated by the Optical Path Length Analyzer ( $\hookrightarrow$ Sec. 82). |
| Snippet defines... | If you select Index Modulation the refractive index of the Base Material is always added to the function defined by the snippet. Otherwise you directly define the refractive index distribution $\widetilde{n}(x, y, z)$. |
| Definition | This group box allows you to program the actual code snippet. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3) to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Parameters ${ }^{\text {PEE }}$ | The controls in this group box allow you to set the values of the global parameters of the snippet. $\hookrightarrow$ Sec. 7.4 |

General information about programming in VirtualLab Fusion can be found in Sec. 7. The remaining controls are explained in Sec. 37.1.

### 37.3.11 Sampled Medium

This medium allows you to set a 1D or 2D data array ( $\hookrightarrow$ Sec. 13) with a sampled refractive index profile.
The edit dialog of this optical medium is shown in Fig. 270.


Figure 270. Dialog for the specification of a sampled medium.

The following options can be entered:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sampled data defines | Defines whether the sampled refractive index profile is interpreted as Index Modulation, i. e. it is added to the refractive index defined by the Base Material. Or it can be interpreted as Index Distribution, i. e. the values in the data array are directly the final refractive indices. |
| Base Material ${ }^{\text {[PE] }}$ | Only for Index Modulation <br> The controls in this group box are explained in Sec. 34.3. They define the complex refractive index added to the refractive index profile. |
| Set | Offers you three ways to set a data array with the refractive index modulation (see below). The data array must contain exactly one subset where the coordinates have the unit length and the data have no unit. |
| Set > Load | Loads a data array from a .da file. |
| Set > Import | Imports a data array from a bitmap or text file by means of the import wizard described in Sec. 121.2. |
| Set > Select from Documents | Allows you to select an already open data array. |
| Show | Shows the currently set refractive index definition / modulation as separate document. |
| \{Interpretation of 1D Data\} | When you set 1D data, you can define whether the coordinates are interpreted as being $x$ - or $y$-values. When the data contain only positive values, the coordinates can additionally be interpreted as $\rho=\sqrt{x^{2}+y^{2}}$ yielding rotationally symmetric refractive indices. |


| Interpolation Method | Lets you select the Interpolation Method Equidistant and/or the Interpolation |
| :--- | :--- |
|  | Method Non-equidistant, dependent on the data. $\leftrightarrows$ Sec. 13.2 |
| Extrapolation | Lets you select how coordinates outside of the coordinate range of the given |
|  | data are interpreted ( $\lrcorner$ Sec. 13.3). |
|  | In particular, you can select periodic extrapolation. This is in the very |
|  | most cases more suitable then choosing the normal medium periodization |
|  | $(\leftrightarrows$ Sec. 133.3.1) - where periods have to be entered by the user and are re- |
|  | stricted to be always centered around the coordinate origin which might yield |
|  | unexpected results. |

The remaining controls are explained in Sec. 37.1.

### 37.3.12 Slanted Grating Medium

This kind of medium represents a periodic grating with ridges. A ridge has two flanks which both are slanted with respect to the vertical by a certain angle. A coating with a single layer can be applied to the flanks, the bottom, and the top of the grating.


Figure 271. Dialog for the specification of a Slanted Grating Medium.

The edit dialog of this medium（ $\rightarrow$ Fig．271）has the following options：

| ITEM | DESCRIPTION |
| :---: | :---: |
| Grating Material ${ }^{\text {同 }}$ | The material of the grating ridges．Also used to fill the area in front of the modulated region．The controls in this group box are explained in Sec．34．3． |
| Groove Material ${ }^{\text {限 }}$ | The material of the grating grooves．Also used to fill the area behind the modulated region．The controls in this group box are explained in Sec．34．3． |
| Fill Factor ${ }^{\text {［V］}}$ | The ratio of the grating ridges to the period in $x$－direction of the medium．If the slant angles of the flanks differ，the width of the ridges changes with $z$ ．In this case it makes a difference whether the fill factor Refers to ．．．the bottom （ $z=0$ ）or the top（ $z=z$－Extension）of the grating． |
| z－Extension ${ }^{\text {『V }}$ | The extension of the ridges（without coating）in z－direction．Note that if a Slanted Grating Medium is used within an Optical Stack（ $\leftrightarrows$ Sec．39），its z－ extension（with coating）determines the thickness of the stack layer where it is placed in．Thus you cannot set the $z$－．Distance of the subsequent layer． |
| Slant Angle Left ${ }^{[\mathbb{V}]}$ | The angle to the vertical of the left flank．＂Left＂refers to the flank with the smaller x－position． |
| $\neq 1=$ | If you click on the $\neq$ button it turns into $\mathrm{a}=$ button which means that the two slant angles are always the same，even during e．g．Parametric Optimization （ $\leftrightarrows$ Sec．102）．Clicking on this button again allows you to set different angles again． |
| Slant Angle Right ${ }^{\text {『V }}$ | The angle to the vertical of the right flank．＂Right＂refers to the flank with the larger x－position． |
| Apply Coating | If you click this check box the dialog extends so that you can apply a coating （consisting of a single material）on the grating． |
| Coating Material ${ }^{\text {可 }}$ | Only visible if Apply Coating is checked． <br> The material in the coating layer．The controls in this group box are explained in Sec．34．3． |
| Coating Thickness ${ }^{\text {®V］}}$ | Only visible if Apply Coating is checked． <br> Allows you to set the thickness of the coating layer on the flanks，the bottom， and the top of the grating（measured along $x$－and $z$－direction，respectively）． |

## 37．3．13 Uniaxial Crystal

Uniaxial crystals are anisotropic media which can be described by two different refractive indices．


Figure 272. Dialog for the specification of a uniaxial crystal.
The edit dialog for this kind of medium (shown in Fig. 272) needs the following parameters:
ITEM DESCRIPTION
Material of Ordinary/Ex- The dispersion relations for the two refractive indices are represented by two traordinary Refractive In- materials. The control for setting a material is described in Sec. 34.3. dex

### 37.3.14 Volume Grating Medium

The volume grating medium is designed for analyzing interferograms recorded into a photosensitive Holographic Material ${ }^{\text {禺 }}$. In VirtualLab Fusion the interferograms can be synthesized by the superposition of an arbitrary number of plane waves. See Sec. 133.3.3 for the implemented formulas.
The angles of incidence and the wavelengths of the superposing plane waves can be freely defined by the user. It is assumed that only waves of exactly the same wavelength will interfere with each other.


Figure 273. The edit dialog for a volume grating medium.
The Basic Parameters tab of the edit dialog ( $\hookrightarrow$ Fig. 273) comprises a control for specifying the Holographic Material which is explained in Sec. 34.3 and two sub-tab pages which are explained in the following subsections. The remaining controls are explained in Sec. 37.1.

### 37.3.14.1 Interferogram

The main part of the Interferogram panel is a table showing relative power, direction and wavelength of all superposing plane waves (Fig. 274). Both the vacuum wavelength and the medium wavelength, which refers to the Holographic Material, are displayed.
You can specify whether the direction of these waves is defined in Vacuum or in the Holographic Material. Furthermore, via Representation of Direction you can specify whether the angles are displayed as Cartesian Angles, Wave Numbers, or Spatial Frequencies.


Figure 274. The Interferogram tab for a volume grating medium.

The arrows in the table indicate whether the wave comes from positive or negative z-direction.

The Append button adds a new default wave, the Delete button deletes the currently selected plane wave. If you double click on a plane wave or press Edit, the dialog explained in subsection (a) opens.
The Limit Period specifies the maximum possible period in $x$ - and $y$-direction, as large periods heavily increase the numerical effort for the Fourier Modal Method ( $\varsigma$ Sec. 96.3). On the downside, it introduces a quantization of the specified angles. Mathematical details can be found in Sec. 133.3.3.

## (a) Editing the Interfering Plane Waves



Figure 275. The dialog for setting up the interfering plane waves.
The dialog for editing one of the interfering plane waves ( $\hookrightarrow$ Fig. 275) has the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Weight ${ }^{\text {PE }}$ | Specifies the relative squared amplitude of the wave. See Eq. (133.14) for <br> details. |
| Wavelength ${ }^{\text {PE }}$ | The vacuum wavelength of the plane wave. |
| Direction ${ }^{\text {阬 }}$ | The direction of the plane wave. You can choose whether you want to enter <br>  <br> Cartesian Angles, Wave Numbers, or Spatial Frequencies. Angles must be <br> in the range $-90^{\circ} \ldots+90^{\circ}$. An angle out of this range would mean that the <br> wave comes from the positive half-space and propagates backwards. In this <br> case you have to switch off Positive z-Direction. |

### 37.3.14.2 Index Modulation



Figure 276. The Index Modulation tab of the volume grating dialog.


Figure 277. Example structure if direct refractive index modulation is used.
This panel specifies how the local electrical field density $\bar{w}(x, y, z)(\hookrightarrow$ Eq. (133.13)) is converted into a change of the refractive index. The volume grating medium offers three different modes therefor:

## (a) Direct

In this case you just specify the desired Refractive Index Modulation ${ }^{\mathbb{P V}} \Delta n$ and the Relative Refractive Index Offset $R$. The refractive index $n(x, y, z)$ at a certain position is then calculated via

$$
\begin{equation*}
n(x, y, z)=n_{\text {holo }}+\left(\frac{\bar{w}(x, y, z)}{w_{\max }}+\frac{R-1}{2}\right) \cdot \Delta n \tag{37.1}
\end{equation*}
$$

$w_{\text {max }}$ can be an arbitrary value, as it cancels out in this case (see Eqs. (133.13)-(133.14)). $n_{\text {holo }}$ is the refractive index of the Holographic Material.
For $R=+100 \%$ the refractive index modulation is added to $n_{\text {holo }}$, for $R=-100 \%$ it is subtracted from $n_{\text {holo }}$ and for intermediate values it is something in between. In particular the case $R=0$ means that the refractive indices range from $n_{\text {holo }}-\frac{\Delta n}{2}$ to $n_{\text {holo }}+\frac{\Delta n}{2}$.


Figure 278. Example structure if asymptotic dose to refractive index modulation is used with slight over-exposure.

## (b) Simulate Exposition Process

In this case you simulate the real exposition process. This means you can set up the overall Power Density ${ }^{[\mathrm{DV}}$ $P$ of all superposing waves, the Exposure Time ${ }^{\mathbb{T V}} t_{\text {exp }}$ and the Material Response.

Then, the overall energy density is calculated as follows:

$$
\begin{equation*}
w_{\max }=P \cdot t_{\exp } \tag{37.2}
\end{equation*}
$$

On the left side of the panel you can choose between three equations how the Dose to Refractive Index Modulation is modeled:

| MODEL | EQUATION | PARAMETERS |
| :---: | :---: | :---: |
| Linear | $n(x, y, z)=n_{\text {holo }}+l \bar{w}(x, y, z)+C$ | l: Linear Factor <br> C: refractive index offset, see below |
| Quadratic | $n(x, y, z)=n_{\text {holo }}+l \bar{w}(x, y, z)+p \bar{w}(x, y, z)^{2}+C$ | $l$ : Linear Factor <br> p: Squared Factor <br> $C$ : refractive index offset, see below |
| Asymptotic | $n(x, y, z)=n_{\text {holo }}+\Delta n-\frac{\Delta n}{1+\left(\bar{w}(x, y, z) / w_{0}\right)^{\gamma}}+C$ | $\Delta n$ : Refractive Index Modulation <br> $w_{0}$ : Average Energy Density <br> $\gamma$ : Modulation Exponent <br> $C$ : refractive index offset, see below <br> $\hookrightarrow$ Fig. 279 |



Figure 279. The refractive indices $n(w)$ if asymptotic dose to refractive index modulation is chosen. The blue curve has the smallest modulation exponent and the red curve the largest.

The Relative Refractive Index Offset $R$ allows you to define whether the refractive index modulation is added to $n_{\text {holo }}$ (for $R=+100 \%$ ), subtracted from $n_{\text {holo }}$ (for $R=-100 \%$ ) or something in between. In particular the case $R=0$ means that the refractive indices range from $n_{\text {holo }}-\frac{\Delta n}{2}$ to $n_{\text {holo }}+\frac{\Delta n}{2}$ where $\Delta n$ is the overall refractive index modulation. This is achieved by adding $C=\frac{R-1}{2} \Delta n$ to the formulas given above.

## (c) Photonic Crystals

In this case it is assumed that above a certain energy density $w_{\mathrm{t}}$ the original Holographic Material is replaced by a Second Material. In VirtualLab Fusion you enter the relative Threshold ${ }^{\mathbb{W V},}$, i. e. $\frac{w_{t}}{w_{\text {max }}}$.


Figure 280. Example structure if refractive index modulation for photonic crystals is used.

## 38 Materials

### 38.1 Using Materials

Materials are used for defining Optical Media ( $\leftrightarrows \mathrm{Sec} .37$ ). They hold all relevant optical material data, as described in the following.

### 38.1.1 Material Data

The complex refractive index $\hat{n}$ of a material can be expressed as

$$
\begin{equation*}
\hat{n}=n+i \kappa, \tag{38.1}
\end{equation*}
$$

where $n$ is the (real part of the complex) refractive index, and $\kappa$ the absorption index. Here the absorption index $\kappa$ must not be mixed up with the absorption coefficient $\alpha$ which is stored in the Material and that is related to $\kappa$ by

$$
\begin{equation*}
\alpha=\frac{4 \pi \kappa}{\lambda_{0}}=2 k_{0} \kappa . \tag{38.2}
\end{equation*}
$$

In Eq. (38.2) $\lambda_{0}$ represents the vacuum wavelength and $k_{0}$ the wave number in vacuum. The absorption coefficient $\alpha$ is introduced in Beer's law, which is denoted as

$$
\begin{equation*}
I=I_{0} \cdot \mathrm{e}^{-\alpha \Delta z} \tag{38.3}
\end{equation*}
$$

where $I$ is the intensity after a propagation distance $\Delta z$ through an absorbing material.
The dependency of the two parameters $n$ and $\alpha$ on the wavelength are stored in each Material and can be given as sampled data or as one constant value. Additionally, the real refractive index $n$ can be specified by some parameters that are related to a certain selected dispersion formula.

### 38.2 Defining and Editing Materials

Materials can be created or edited from the dialog of the Materials Catalog ( $\checkmark$ Sec. 33). Additional the user can modify a material where it is needed. The edit dialog is described in detail now. Besides the panels Refractive Index, Absorption, and Additional Information described below, it contains the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Usable Vacuum <br> length Range | Wave- |
| The intersection of the wavelength ranges of the absorption coefficient, the |  |
| real refractive index and, if given, the reference material's real refractive in- |  |
| dex. |  |$\quad$| Opens the view of the current material. |  |
| :--- | :--- |
| Tools $>$ Reset All Data | Saves the current material into the material catalog. <br> Discards all changes made in this dialog and resets to the previous state of <br> the material. |
| Validity | This control $(\hookrightarrow$ Sec. 5.10$)$ indicates whether there are issues with the current <br> configuration. If this is the case you can click on the 图-button for further <br> information. |

If both the real refractive indices and the absorption coefficients are defined via a Programmable function, they share the same set of Global Parameters.

### 38.2.1 Refractive Index Panel



Figure 281. The panel for the input of the real refractive index, dependent from wavelength.

The real refractive index dependency from wavelength is defined in the panel Refractive Index which is shown in Fig. 281. It has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Dispersion Formulas | After choosing this option, the user can select one of the dispersion formulas <br> summarized in Sec. 133.4. Then the corresponding formula is shown to the <br> right. And the lower part of the refractive index panel shows a table where you <br> can enter the values <br>  <br> micrometers. |
| Sam the parameters, scaled for the wavelength given in |  |

### 38.2.2 Absorption Panel

If the absorption properties of a material are unknown, you can try to use it anyhow by setting the absorption coefficient to $\alpha=0=$ constant.

The absorption coefficient dependency from wavelength is defined in the panel Absorption which is shown in Fig. 282.


Figure 282. The panel for the input of the absorption coefficient in Sampled mode.

There are three different quantities describing the absorption which can be entered in three different modes:

| Mode | Absorption Coefficient | Internal Transmittance | Absorption Index |
| :---: | :---: | :---: | :---: |
| Sampled | $\boldsymbol{\nu}$ | $\boldsymbol{\nu}$ | $\boldsymbol{\nu}$ |
| Constant | $\boldsymbol{\nu}$ | $\boldsymbol{\nu}$ | $\boldsymbol{x}$ |
| Programmable | $\boldsymbol{\nu}$ | $\boldsymbol{x}$ | $\boldsymbol{x}$ |

The three quantities Absorption Coefficient, Absorption Index and Internal Transmittance are defined as $\alpha, \kappa$ and $I / I_{0}$ in the equations 38.1 to 38.3 respectively. The latter requires to enter some additional reference Thickness.
The three modes for entering are the following:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sampled Absorption | If you check this option, the lower part of the panel shows a table control where you can enter pairs of wavelengths and the respective absorption quantity. For details see Sec. 5.9. If VirtualLab Fusion needs an absorption coefficient for a wavelength value which lies between two of the stored ones, a cubic 6 -point interpolation is used for equidistant sampling, while linear interpolation is used for non-equidistant sampling. |
| Constant | Choosing this option means to define a single Constant Absorption Coefficient ${ }^{\mathbb{T V}}$ or a Constant Internal Transmittance for the whole Wavelength Range. |
| Programmable | The Definition group box allows to program an arbitrary formula for the absorption coefficient $\alpha(\lambda)$ with a code snippet. Edit opens the Source Code Editor ( $\leftrightarrows$ Sec. 7.3) to edit this snippet, and a validity indicator ( $\leftrightarrows$ Sec. 5.10) shows whether this snippet is consistent. The Parameters ${ }^{\text {国 }}$ group box is explained in Sec. 7.4. |

The following control is visible independently from these three modes:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength Range | The minimum and maximum wavelength for which the absorption coefficient <br> data are valid. In case of Sampled Absorption these values are determined <br> automatically from the sampled data. |

### 38.2.3 Additional Information

In this panel the State of Matter for the material can be set.


Figure 283. The panel for the additional information.

| ITEM | DESCRIPTION |
| :--- | :--- |
| State of Matter | The state of matter of this material can be Solid, Liquid, or Gas or Vacuum. |
| Origin of the Data | The data source can be entered here (if unlocked $\boldsymbol{\delta}$ ). |
| I $/ \boldsymbol{f}$ | This button toggles the locked state of the textbox for Origin of the Data. The <br> box is locked by default. |

### 38.2.4 Temperature Data



Figure 284. The panel to specify the temperature data.
The parameters which determine the temperature dependence of the real part of the refractive index can be defined here.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Reference Temperature | This is the temperature $T_{0}$ (in ${ }^{\circ} \mathrm{C}$ ) the refractive index measurement has been done at. |
| D0 [1/K] | The parameter $D_{0}$ as used in Eq. (38.4). |
| D1 [1/K ${ }^{2}$ ] | The parameter $D_{1}$ as used in Eq. (38.4). |
| D2 [1/K ${ }^{3}$ ] | The parameter $D_{2}$ as used in Eq. (38.4). |
| E0 [1/K] | The parameter $E_{0}$ as used in Eq. (38.4). |
| E1 [1/K ${ }^{2}$ ] | The parameter $E_{1}$ as used in Eq. (38.4). |
| $\lambda_{\text {_TK }}$ | The parameter $\lambda_{T K}$ as used in Eq. (38.4). |

The change of the real part of the refractive index which is caused by its temperature dependence is calculated by

$$
\begin{equation*}
\Delta n(\lambda, T)=\frac{n^{2}(\lambda, T)-1}{2 \cdot n\left(\lambda, T_{0}\right)} \cdot\left(D_{0} \cdot \Delta T+D_{1} \cdot \Delta T^{2}+D_{2} \cdot \Delta T^{3}+\frac{E_{0} \cdot \Delta T+E_{1} \cdot \Delta T^{2}}{\lambda^{2}-\lambda_{T K}^{2}}\right) \tag{38.4}
\end{equation*}
$$

The value $n$ is the real valued refractive index of the material as measured at the reference temperature $T_{0}$. If the calculation shall be done for a temperature $T$ and for a vacuum wavelength $\lambda$, the temperature difference $\Delta T=T-T_{0}$ has to be put into the equation. The refractive index as modified by the different temperature is

$$
\begin{equation*}
n(\lambda, T)=n\left(\lambda, T_{0}\right)+\Delta n(\lambda, T) \tag{38.5}
\end{equation*}
$$

All these relations can be found in [SCH08].

### 38.3 Material View

The material view consists of three pages, Diagram, Additional Information, and Calculator. Besides the name of the material and the categories it belongs to, the dialog always shows the wavelength range the material's data are defined for:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Min. Wavelength | The minimum vacuum wavelength which the real refractive index as well as <br> the absorption data are known for. |
| Max. Wavelength | The maximum vacuum wavelength which the real refractive index as well as <br> the absorption data are known for. |

### 38.3.1 Diagram



Figure 285. The Diagram tab of the Material View.

The Diagram tab shows the wavelength dependency of the real refractive index $n$ and/or the dependency of the absorption coefficient $\alpha$ or the absorption index $\kappa$. The diagram view can be configured via a configuration dialog ( $\hookrightarrow$ Sec. 38.3.1.1) which is called by the button Configure Diagram.
If Shift is pressed while the mouse is moved over the diagram, the values of the displayed curve(s) at the cursor position are shown near the mouse cursor.

### 38.3.1.1 Configuring the Material Diagram

The dialog shown in Fig. 286 is used to configure the diagram of the wavelength dependent material data.


Figure 286. The Edit dialog for configuring the material's diagram.
It contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Show Energy Dependence Instead of Wavelength Dependence | If chosen, the diagram will show the dependence of the optical data from the photon energy $E$ which is related to the vacuum wavelength $\lambda_{\text {vac }}$ via $E=h_{\lambda_{\text {vac }}}$ with $h$ being Planck's constant and $c$ being the vacuum speed of light. |
| Show Refractive Index | Shall the refractive indices be drawn in the diagram? |
| Relative | THIS OPTION IS AVAILABLE FOR RELATIVELY DEFINED REFRACTIVE INDEX DATA. Show the real refractive index relative to the reference material. |
| Absolute | THIS OPTION IS AVAILABLE FOR RELATIVELY DEFINED REFRACTIVE INDEX DATA. Show the absolute real refractive index. |
| Show Absorption | Shall absorption data be drawn in the diagram? |
| Coefficient $\alpha$ | If chosen, the wavelength dependency of the absorption coefficient is drawn in the diagram. |
| Index $\kappa$ | If chosen, the wavelength dependency of the absorption index is drawn in the diagram. |
| Use Intersection of Valid Wavelength Ranges | If true, only the wavelength range that can be used during the simulation in VirtualLab Fusion is displayed. Otherwise the conjunction of the wavelength ranges of $n$ and $\alpha / \kappa$ is displayed. |
| Line Color <br> Show Symbols for Data Points | Sets the color of the drawn line. <br> This can be chosen only if the data are defined as sampled dispersion OR ABSORPTION. <br> Shall symbols, marking the actual data points, be shown additionally to the line? |
| Significant Digits | Number of digits used for the axis labels. |
| Axes are Colored Like Graphs | If checked, the diagram's $y$-axes are colored like the corresponding curve. |
| Line Thickness | The thickness the curves will be drawn with. |

### 38.3.2 Additional Information



Figure 287. The Additional Information of the Material View.

The Additional Information tab gives some important parameters of the material:

| ITEM | DESCRIPTION |
| :--- | :--- |
| State of Matter | The state of matter of the material. This is important for the usage with optical <br> coatings $(\hookrightarrow$ Sec. 36$)$. |
| Definition Range for Re- <br> fractive Index | The vacuum wavelength range for which the real refractive index $n$ is known. |
| Definition Range for Ab- <br> sorption | The vacuum wavelength range for which the absorption coefficient $\alpha$ and the <br> absorption index $\kappa$ are known. |
| Reference Material | The name of the reference material, if the real part of the refractive index is <br> defined relatively. |
| Abbe Number | The Abbe number $v_{d}$ and the Abbe number $v_{e}$ for a temperature of $20^{\circ} \mathrm{C}$ and <br> an air pressure of 101325 Pa. |
| Origin of the Data | The source of the material's data. |

### 38.3.3 Calculator

The calculator can be used in order to get refractive index and absorption information for a given vacuum wavelength and at a given temperature.


Figure 288. The Calculator of the Material View.
The input and output parameters of the calculator are the following:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Test Wavelength | Wavelength to calculate $n, \alpha, \kappa$ and the Relative Transmittance of this material <br> for. |
| Test Temperature | Temperature to calculate $n$ of this material for. |
| Test Air Pressure | THIS PARAMETER APPLIES TO MATERIALS wHICH USE THE EDLÉN EQUATION <br> FOR THE REFRACTIVE INDEX OF AIR ONLY. <br> The air pressure to calculate $n$ of this material for. |
| $\mathbf{n}$ | Calculated refractive index of the material. |
| Absolute | THIS OPTION IS AVAILABLE FOR RELATIVELY DEFINED REFRACTIVE INDEX DATA. <br> If checked, the absolute real refractive index is calculated, otherwise the re- <br> fractive index relative to the material's reference material will be given. |
| $\boldsymbol{\alpha}$ | Calculated absorption coefficient of the material. |
| $\boldsymbol{\kappa}$ | Calculated absorption index of the material. |
| Thickness | Thickness of the material to calculate the Relative Transmittance for. |
| Relative Transmittance for | Calculated relative transmittance of the material for the given Thickness. |
| $\boldsymbol{a}$ Thickness of ... |  |

### 38.4 Material Data Sources

A large variety of different materials are delivered with VirtualLab Fusion. This includes a number of glass types as well as some other substances often used in optics. All materials can be found in the Materials Catalog. The data for the refractive indices and absorption coefficients used in the Material Documents that are provided by VirtualLab Fusion are taken from several publications.

WARNING: There may be errors in the data, e.g. due to measurement, publishing, or transcription. So please verify these data, especially if you are considering to fabricate the optics designed with VirtualLab Fusion.

The information for the glass catalogs CDGM_..., Corning, Dow_..., Heraeus, Hikari_..., Hoya_..., LZOS_..., Ohara_..., Schott_...and Sumita_...were given by the manufacturers. The sources of the other catalogs are listed in Sec. A.4.5.

## 39 Optical Stacks

On the boundaries of a solid (called base block), stacks of micro-structured surfaces and media can be applied. Stacks are assumed to be periodically and they are orientated "outwards", i.e. the solid is always at $z=0$ and the embedding medium starts at $z=d$, where $d$ is the $z$-extension of the stack.
A stack can consist of an arbitrary number of so-called "stack segments". Each segment consists of an optical surface and a subsequent medium.

### 39.1 Usage Principle of Optical Stacks

Using a new optical stack needs two independent steps. At first, a new stack has to be built. Secondly, the stack is attached to a plane optical surface which serves as boundary of a solid base block. These two steps don't have to be done separately in each case of use, e.g. it is possible to edit a stack already attached to an optical surface. But in principle, the stack definition is independent from its application to a base block boundary, so there exists a catalog of stacks, storing defined stacks that can be (re-)used any time.

### 39.1.1 Defining an Optical Stack

Any stack consists of an alternating sequence of a number of indexed optical surfaces and optical media. These are positioned on one single axis. This is identical to the $z$-axis of the stack's own coordinate system. So the positions of the single optical surfaces are determined by a distance value, measured on the stack's z-axis. The origin of the stack coordinate system is the point $(0 ; 0)$ of the first surface, so this one has always a z-position of zero. This convention is shown in Fig. 289.


Figure 289. Positioning of optical surfaces inside an optical stack.

### 39.1.2 Application of an Optical Stack

If a defined optical stack has to be attached to the boundary surface of a base block, the following considerations are important.
A stack is attached to a base block in a way, that the first optical surface of the stack touches the block without entering it. The medium of the base block fills possible gaps between the base block boundary and the first stack surface. Furthermore, stacks are always orientated "outwards". Fig. 290 shows these relationships.


Figure 290. Positioning of an optical stack relative to the base block's boundary.

1) Stack on the back side of a base block.
2) Stack on the front side of a base block.

For each side of the base block (front side and back side) there are two possible orientations for the stack. It can be rotated by $180^{\circ}$ about the z-axis or be used unrotated, respectively. These two orientations are shown in Fig. 291 and Fig. 292.


Figure 291. Orientation of an optical stack on the front side of a base block.

1) Unrotated.
2) Rotated about z-axis by $180^{\circ}$.


Figure 292. Orientation of an optical stack on the back side of a base block.

1) Unrotated.
2) Rotated about $z$-axis by $180^{\circ}$.

### 39.2 Edit Dialog for Stacks



Figure 293. The edit dialog for stacks. Note that the base block is only shown in the upper part if Use Component Coordinate System for Stack Preview is checked in the Global Options dialog ( $\hookrightarrow$ Sec. 6.2). The Validity control shows a warning because the period of the surface with Index 1 has actually a period of infinity in $y$-direction.

The edit dialog for stacks ( $\rightarrow$ Fig. 293) comprises three parts: The upper part shows an intersection of the surface media sequence of the stack ( $\leftrightarrows$ Sec. 5.14). The middle part is a table listing the stack segments. The topmost entry is closest to the solid, the bottommost entry is closest to the embedding medium. This table has the following columns:

| COLUMN | DESCRIPTION |
| :---: | :---: |
| Index | The index of the segment. |
| z-Distance ${ }^{\text {PVV }}$ | Allows to enter the distance of the surface to the previous surface. It is measured in positive z-direction. |
| z-Position | Display of the absolute z-position of the surface in the stack. |
| Surface ${ }^{\text {PE }}$ | Edit control for the surface in the segment ( 4 Sec. 34.1). |
| Subsequent Medium ${ }^{\text {[同 }}$ | Edit control for the medium in the segment ( $\hookrightarrow$ Sec. 34.1). |
| Comment | One can enter a descriptive comment for each segment. |

The Index and the z-Position column are always read-only. Also, the z-Distance of the first segment and the Subsequent Medium of the last segment are fixed.
The lower part of the edit dialog contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Validity | This control ( $\leftrightarrows$ Sec. 5.10) indicates whether the currently defined stack is valid, i. e. whether it contains a least one surface and whether it has an extension greater zero. |
| Add | Adds a new stack segment to the end of the table. The surface catalog is opened automatically to define the surface of the segment. |
| Insert | Inserts a new stack segment before the currently selected table row, indicated by a triangle in the first column. The surface catalog is opened automatically to define the surface of the segment. |
| Delete | Deletes all currently selected table rows. |
| Period | Defines the stack period. <br> The stack period can be either taken from a certain surface or medium within the stack. If this reference is not periodical or has a period of infinity in one direction, a period of 100 pm is assumed instead and a warning is shown in the validity control. This way the calculation of an infinite number of orders is avoided. <br> If the stack period is Independent from Surface/Media Period, the user can set the Stack Period ${ }^{[\mathrm{PV}}$ by oneself. |
| (2] (View) | Displays a preview of the stack. |
| H (Save To Catalog) | Saves the stack to the user-defined stack catalog. |
| Stack Tools | Several tools are available to modify the stack in a user-friendly way. More information can be found in Sec. 39.3. |

When the stack is used from within a Light Guide ( $\varsigma$ Sec. 57.2), the edit dialog has an extra tab page Additional Parameters. There you can define parameters you might need if you want to use you own custom Fourier Modal Method ( $\leftrightarrows$ Sec. 96.4), using the control described in Sec. 7.3.2.

### 39.3 Stack Tools

There are stack tools implemented in VirtualLab Fusion to give the user a comfortable way for configuring a stack.

### 39.3.1 Insert Coating Tool

The Insert Coating Tool can be used to insert a coating (loaded from the Coating Catalog) on a user-specified position. The coating is translated into a surface sequence. This surface sequence is inserted into the stack. Note: The set up process data is ignored for the insert algorithm into the stack. Only the coating layers are converted.


Figure 294. The edit dialog for configuring the Insert Coating Tool

This tool can be found at Tools > Insert Coating. Fig. 294 shows its edit dialog which has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Insert Coating $\quad$ Behind | Defines the index of the surface within the stack on which the coating shall <br> Stack Surface No. |
| be set. Only visible if the stack contains at least one surface. |  |

### 39.3.2 Insert Stack Tool

The Insert Stack Tool can be used to insert a stack (loaded from the Stack Catalog) on a user-specified position.


Figure 295. The edit dialog for configuring the Insert Stack Tool
This tool can be found at Tools > Insert Stack. Fig. 295 shows its edit dialog which has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Insert Stack Behind Stack | Defines the index of the surface within the stack after which the stack shall |
| Surface No. | be set. Only visible if the stack contains at least one surface. |
| Stack To Insert | The user can select a stack from the catalog, which shall be added. |

### 39.3.3 Reduce Definition Area to Stack Periods

Via the stack period you define the region of each surface (and medium) which is evaluated. However, if the definition area ( $\hookrightarrow$ Sec. 35.1.1) of a surface is much larger than the stack period, the z-extension of the surface might be larger than expected leading to a seemingly too thick stack ( $\hookrightarrow$ Fig. 296).
Thus the Reduce Definition Area to Stack Periods tool allows you to limit the definition area of all surfaces to the stack period, whereas the following rules apply:

- For grating surfaces the inner definition area, and the outer definition area are adapted. Setting the period would change the structure definition.
- For all other periodical surfaces the inner definition area, the period, and the outer definition area are adapted.
- The definition areas are set to a rectangular shape.
- If the definition area (or period) of the surface was set by the user to a value smaller than the stack period, it is kept unchanged. This check is done separately for $x$ - and $y$-dimension.
- For stacks of 1D-periodic grating surfaces the definition area (or period) in y-direction is set to $10 \%$ of the stack period. In this way a nice-looking stack preview is ensured.


Figure 296. Left: A conical surface in a $2 D$ stack having a definition area twice the size of the stack period. The maximum z-extension is reached outside of the stack period. Right: The same surface after the Reduce Definition Area to Stack Periods tool has been applied.

### 39.3.4 Change External Name

When stacks are used within other controls ( $\hookrightarrow$ Sec. 34.1), their (external) name is shown to easier identify them. With this tool you can simply change this name, e.g. if you have changed the sinusoidal grating surface within a stack to a triangular one.

## 40 Surface Layouts

On the surfaces of a solid, VirtualLab Fusion offers the possibility to specify surface layouts, which consist of several regions on an Optical Surface ( $\hookrightarrow$ Sec. 35 ) behaving differently than just a plain surface. Each type of surface layout usually provides its own algorithm to propagate light through it, a so-called boundary operator. A boundary operator can change the position, the direction and the complex value of the incident wave and even generate new modes (e.g. multiple grating orders).

### 40.1 Cells Arrays

A Cells Array boundary operator consists of a set of cells. All cells have the same size. Every cell has a specific optical function defined by a small set of parameters.
Two types of cells arrays are available:

1. Grating Cells Array $\hookrightarrow$ Sec. 40.1.1
2. Prism Cells Array $\hookrightarrow$ Sec. 40.1.2

Sec. 40.1.3 explains how a cells arrays can be configured.

### 40.1.1 Grating Cells Array

The Grating Cells Array (GCA) boundary operator consists of a set of grating cells arranged in an equidistant grid. In every cell a grating function can be specified by the following parameters:

- Period
- Rotation Angle
- Lateral Shift

The boundary operator uses the local grating parameters to change the parameters of the incident wave. The rotation angle and the period directly influence the direction of the incident wave. The lateral shift defines an additional phase shift which shall be applied to the specific grating cell.
The way how the grating parameters of the individual cells can be configured is described in Sec. 40.1.3.

### 40.1.2 Prism Cells Array

The Prism Cells Array (PCA) consists of cells arranged in an equidistant grid. In each cell there is a slanted plane surface defined by the following three parameters:

| PARAMETER | DESCRIPTION |
| :--- | :--- |
| Tilt Angle | The spherical angle $\theta(\hookrightarrow$ Sec. 139.2.1) describing the tilt of the plane surface. |
| Rotation Angle | The spherical angle $\phi(\hookrightarrow$ Sec. 139.2.1) describing the rotation of the plane <br> surface in the $x-y$-plane. |
| Offset Height | The height of the plane surface at the center of the cell (relative to the surface <br> the boundary operator is placed on). Introduces an additional phase shift. |

If a Prism Cells Array is used in reflection it is referred to as Mirror Cells Array (MCA).
The way how the surface parameters of the individual cells can be configured is described in Sec. 40.1.3.

### 40.1.3 Configuring a Cells Array

Fig. 297 shows the edit dialog of the Prism Cells Array with the controls that all types of Cells Arrays have in common.


Figure 297. The edit dialog of the Prism Cells Array boundary operator

The dialog enables the user to configure
ITEM DESCRIPTION

Number of Grating/ Prism Cells

Cell Size

The number of cells within the Cells Array can be specified. After changing the number of cells within the boundary operator a Refresh button appears and has to be clicked to trigger the resizing of the cell array.
The user can specify the size of the cells in $x$ - and $y$-dimension. All cells have the same size.

In the middle part of the dialog the cells parameters of the boundary operator can be changed. The following possibilities can be used to specify the cells parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set | The set button can be used to set an open data array, which contains the <br> cells parameters in different subsets. This option can be very helpful to use <br> an already designed Cells Array function within a new boundary operator. |
| Get | By clicking the Get button, the cells parameters of the Cells Array operator are <br> extracted into a data array. The extracted data array is displayed within the <br> VirtualLab Fusion main window and can be used for post processing steps <br> (like usage in another boundary operator, or graphical evaluation of the pa- <br> rameter distribution). |
| \{Table\} | Additionally VirtualLab Fusion offers to directly edit the cells parameters within <br> the table at the bottom of the edit dialog. |

If the mouse hovers over the Statistics 1 icon a tooltip is shown which gives the minimum and maximum of each parameter in the cells array and the corresponding locations. For grating cells also the minimum and maximum period in $x$ - and $y$-direction is given for reference.
By pressing the Table Tools button the user can select Vary Grating Cells/ Vary Prism Cells. Fig. 298 shows the dialog to configure this tool. The button allows you to export the cells data ( $\hookrightarrow$ Sec. 126) .


Figure 298. The dialog for the Vary Grating Cells table tool. The dialog for the Vary Prism Cells tool is the same but uses different cells parameters.

The Vary Grating Parameters / Vary Prism Cells tool can be used to vary the parameters within the Cells Array systematically. The user can specify whether he likes to set a parameter to a special value or whether he likes to make a random distribution of a parameter in a user-defined value range. The user can edit the following options for each available cells parameter:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set | The column Set can be used to select the parameters which shall be speci- <br> fied /varied. After selecting the Set option within the table the Value and the <br> Vary column will be enabled. |
| Value | In this column the user can specify the value of the parameter which shall be <br> set. This column is only enabled if the Set option is selected. |
| Vary | The option Vary can be used if the parameter shall be varied in a specific user <br> range. The variation will be randomly. The Vary option is only available if the <br> Set option is selected. |
| Minimum | Defines the minimum of the value range if the parameter shall be varied. This <br> option is only available if the Vary option is set. |
| Defines the maximum of the value range if the parameter shall be varied. This <br> option is only available if the Vary option is set. |  |

### 40.1.3.1 Order Configuration

The Order Configuration tab page allows the user to specify which orders of the grating cells shall be considered during the simulation of the Grating Cells Arrays.
Fig. 299 shows the page to set up the order configuration for the simulation.


Figure 299. The orders to consider during the simulation can be specified within the Grating Cells Array edit dialog on the Order Configuration tab page.

The design of a Grating Cells Array only uses the first order to generate the target pattern. The other orders are not considered in the design but in the analysis of the system.

The user can specify the following parameters on the Order Configuration tab page:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Minimum | The user can specify the Minimum order to be considered during the simula- <br> tion of the Grating Cells Array. |
| Maximum | The user can specify the Maximum order to be considered during the simu- <br> lation of the Grating Cells Array. |
| Method to evaluate | It is possible to specify different complex weights for the orders to consider. |
| Rayleigh Coefficients | VirtualLab Fusion offers three different ways to specify the order weighting. <br> The following possibilities are available: Constant Weight ( $\leftrightarrows$ Sec. (a)), Sim- <br> ple Lookup Table for Coefficients ( $\leftrightarrows$ Sec. (b)) or Rigorous Lookup Table for <br> Coefficients ( $\leftrightarrows$ Sec. (c)) |

## (a) Constant Coefficient

The user can select the Constant Coefficient method to evaluate the weights for each order. The weights of all specified orders within the simulation are set to 1 . This could be used for a first approximation of the GCA function.

## (b) Simple Lookup Table for Coefficients

The Simple Lookup Table for Coefficients option allows the user to configure the real valued weight for each order. Fig. 300 shows the table to configure the amplitude weights for each order.


Figure 300. The Simple Lookup Table for Coefficients option enables the user to specify the amplitude weight for each order

The table contains two columns. The following settings can be viewed / edited:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Order | This column shows the order for which the weight can be specified. It is not <br> editable. The orders to consider within the simulation are specified above <br> within the dialog. |
| Amplitude Weight ${ }^{[\operatorname{PV}]}$ | In the Amplitude Weight column the user can enter the real valued amplitude <br> weight for the specific order. |

Note: Changing the numbers of Orders To Consider will reset the table - all weights will be set to 1 .

## (c) Rigorous Lookup Table for Coefficients

The evaluation of the efficiencies/Rayleigh coefficients requires VirtualLab Fusion Advanced which might not be available on the computer where the cells array simulation is done. Therefor the user needs to trigger the Local Linear Grating Approximation Analyzer ( $\leftrightarrows$ Sec. 90) within the Light Shaping Optical Setup. This analyzer uses the current configuration of the GCA boundary operator to generate a LLGA Results Generator ( $\checkmark$ Sec. 45). This generator can then be used to calculate efficiencies /Rayleigh coefficients rigorously for each wavelength, period, rotation angle, and incident direction occurring in your Light Shaping Optical Setup, possibly on another computer. Finally the generator with the calculated results can be set into the Order Configuration tab ( $\rightarrow$ Fig. 301).


Figure 301. The Rigorous Lookup Table for Coefficients option enables the usage of rigorously calculated Rayleigh coefficients.

The user can modify the Rigorous Lookup Table for Coefficients by the following options:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Set | By clicking on the Set button an open LLGA Results Generator document can be selected and set as the rigorous lookup table for the simulation. |
| Load | The Load button can be used to load an XML file which is a possible output of the LLGA Results Generator. The XML file contains all necessary information for the lookup table. |
| Save | The user can save the lookup table information to an XML file by clicking on the Save button. This option is helpful to extract the lookup table information for some post processing steps. |
| \{Lookup Table Information\} | In the bottom part of the dialog some information about the lookup table is shown. The user can see <br> - the number of wavelengths which are represented within the lookup table <br> - the total number of results where at least one Rayleigh coefficient of one order has been calculated. <br> - the minimum and maximum order of the specified lookup table <br> - the information whether the lookup table is valid for transmission or for reflection |

After specifying the Rigorous Lookup Table for Coefficients the simulation uses the lookup table data for the evaluation of the considered orders. If no valid lookup table entry is found for a specific parameter set, the simulation stops with an error message.

### 40.2 Arbitrary Surface Layouts

Light guide components ( $\lrcorner$ Sec. 57.2) can have surface layouts consisting of an arbitrary number of regions of arbitrary shape filled with an idealized or real grating. ${ }^{1}$


Figure 302. The edit dialog for surface layouts.
These surface layouts can be edited with the dialog shown in Fig. 302, which contains the following controls:

[^7]| ITEM | DESCRIPTION |
| :---: | :---: |
| \{Layout Overview\} | A specially configured 3D view ( $\leftrightarrows$ Sec. 17.1) which gives an overview of all regions in the surface layout. The region currently selected in the table is marked red. |
| \{Overview Table\} | Table that provides an overview of all regions in the layout, including the unique index (column \#), Name of Region, Region Type, and Period. |
| Edit | Allows to edit the currently selected surface region using the dialog described in Sec. 42.1. |
| Add | Adds a new surface region to the layout. The new region has to be defined via the dialog described in Sec. 42.1 first. |
| Remove | Removes the currently selected region from the layout. Shortcut: Del |
| Duplicate | Duplicates the currently selected region. |
| Gridded Segmentation | Available for rectangular and simple polygon regions only. <br> This button opens a dialog which allows to segment the currently selected region into several new regions by defining a segmentation grid. The dialog is described in Sec. 40.2.1. |
| Edit Vertex Couplings | AVAILABLE ONLY FOR SIMPLE POLYGON REGIONS WHICH SHARE COUPLED VERtices with at least another polygon. <br> The coupling of vertices of two or more polygons can be edited using the dialog described in Sec. 40.2.2. |
| Apply Absorption Outside of Region on Surface | If checked, the parts of the surface which are not covered by grating regions will absorb the light. If unchecked, the non-grating surface parts will transmit and reflect the light depending on the optical properties of the involved materials. |

### 40.2.1 Gridded Segmentation of Regions



Figure 303. Dialog for doing a gridded region segmentation.
Rectangular or polygonal grating regions may be decomposed into smaller regions by applying an equidistant grid of $n \times m$ tiles to the original region, using the dialog shown in Fig. 303. The result will be $n \times m$ new segments of the type 'simple polygon region'. The following parameters define the segmentation:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of Tiles | The axis aligned bounding box of the original region will be segmented into $n$ <br> $x m$ tiles. These numbers of the $x$ - and y-segments can be defined here. |
| Prefix for the Segment | A prefix for the automatically generated names of the new regions can be <br> given here. The names of the new segments will be "\{prefix\} \#\{index\}". |
| Segmentation Angle | The segmentation doesn't have to be axis aligned. A rotation angle which de- <br> termines the direction of horizontal and vertical segmentation can be defined <br> here instead. |
| Align With Sides | OnLY AVAILABLE FOR RECTANGULAR REGIONs. <br> Since a rectangular region may be rotated itself, pushing this button will pre- <br> select the rotation angle of the segmentation in a way which results in a side <br> alignment. So the resulting rectangles after the segmentation will have the <br> same orientation as the original rectangle. |
| Preview | This view shows the result of the segmentation process using the currently <br> set parameters. The new region indices are given within the view as well. |
| Smallest Region Index | Since all region indices inside the edited surface layout (including the new <br> regions after segmentation) has to be unique, the new indices will never start <br> with \#1. The smallest new region index is given here instead. |

### 40.2.1.1 Segmentation of Regions with a Real Grating Structure

If a region is to be decomposed which contains a real grating structure, the parameters of the gratings of the new segments may vary. That's why there will be a Next > button at the bottom of the dialog which allows to select grating parameters for variation after the tiles have been specified. After selecting the variation parameters, the parameter values can be set for each of the new segments on the last page of the dialog.

### 40.2.2 Changing Polygon Vertex Couplings

The vertices of adjacent simple polygon regions may be coupled if they share the same coordinates. 'Coupling' means that a change in the coordinates of the vertex in one polygon will change the coordinates of the coupled vertex in the other polygon as well. This is shown in Fig. 304.


Figure 304. The principle of vertex coupling. The left picture shows the polygons before editing the coordinates of the vertex in the red circle. The right picture shows how editing its coordinates change the shape of the left as well as that of the right polygon at once.

Whenever the editing of the vertex of one polygon results in identical coordinates to that of another polygon, the user will be asked whether to activate coupling.
If a coupling is not needed anymore, it can be changed by the dialog shown in Fig. 305.


Figure 305. Dialog for decoupling one or more vertices from each other.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Coupling \# | The index of the coupling that shall be edited. |
| Coordinates $\mathbf{( x , y )}$ | The coordinates of the coupling to be currently edited. |
| Region | The region the vertex in the column Vertex Name belongs to. |
| Vertex Name | The name of the selected vertex. |
| Decouple Vertex | When pressed, the selected vertex will be removed from the current coupling. <br> If there are no more than two vertices then the coupling will be completely <br> dissolved. |
| Dissolve Coupling | When pressed, the current coupling will be completely dissolved, no matter <br> how many vertices are coupled at this coordinates. |

## 41 Boundary Responses

A Boundary Response is described by a complex-valued function $\mathcal{B}=f(x, y, \lambda, n(\lambda))$ which is applied to an incoming field.

$$
\begin{equation*}
E_{x y}^{\text {out }}(x, y)=\mathcal{B} E_{x y}^{\text {in }}(x, y) \tag{41.1}
\end{equation*}
$$

$(x ; y)$ is the lateral position, $\lambda$ is the wavelength of the incoming field and $n(\lambda)$ is the complex refractive index of the homogeneous medium associated with the boundary response.

### 41.1 Edit Dialog for Boundary Responses



Figure 306. The edit dialog for Boundary responses showing the Basic Parameters if Single Function with Aperture is selected.

The edit dialogs for all boundary responses ( $\hookrightarrow$ Fig. 306) have the following controls in common:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Associated Medium | The homogeneous medium associated with the boundary response. This is <br> from which refractive indices are being calculated if required by the function <br> B. |
| Parameters | This box contains two tab pages. The Basic Parameters allows you to select <br> one out of three Construction Methods. Depending on the selected Construc- <br> tion Method this tab page changes, which is explained below in more detail. <br> The Physical Parameters tab is specific for the distinct types of boundary re- <br> sponses ( $\lrcorner$ Sec. 41.3). |
| Q View | Shows the boundary response view. $\lrcorner$ Sec. 41.2 <br> Save |

The following Construction Methods are available:

| CONSTRUCTION METHOD | DESCRIPTION |
| :---: | :---: |
| Single Function without Aperture | Not available for Aperture and Zernike Fringe / Seidel Aberrations BOUNDARY RESPONSE. <br> There are no specific controls for this construction method. |
| Single Function with Aperture | The aperture is applied by multiplying the actual function value $f$ by 1 inside and by 0 outside the specified aperture. The edge of the aperture can be defined smooth, then the values don't "jump" from 1 to 0 but follow a Gaussian function (decreasing to a value of 0.01) as shown in Fig. 307. <br> The controls to setup the aperture are explained in a separate table below. In case of an Aperture boundary response, this option is named just Single Function. |
| Periodic Function | Not available for Zernike Fringe / Seidel Aberrations boundary reSPONSE. <br> In this case you can set the Period ${ }^{[\mathrm{PV}}$ of the function. |



Figure 307. Definition of the edge width of an aperture.
The following controls ( $\hookrightarrow$ Fig. 306) are specific for the Single Function with Aperture construction method:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Setting | If checked, a reasonable size of the aperture for the boundary response is de- <br> termined automatically. This option is available for some boundary responses <br> only, e. g. exponentially decreasing ones. |
| Manual Setting | If checked, the aperture size is to be entered by the user. |
| Shape | The aperture may be Rectangularly or Elliptically shaped. |
| Diameter ${ }^{[\text {PV }}$ | Size of the aperture. |
| Relative Edge Width | The width of the aperture edge, defined relatively to the (smaller of the both <br> values of) diameter. |
| Absolute Edge Width | The width of the aperture edge, defined in physical units. See Fig. 307. |

For an Aperture boundary response, a separate aperture cannot be set on the Basic Parameters tab. For a Zernike Fringe / Seidel Aberrations boundary response, only circular apertures are allowed.


Figure 308. Tab page for setting the Basic Parameters of a boundary response with the construction method Periodic Function

The following controls ( $\rightarrow$ Fig. 308) are specific for the Single Function with Aperture construction method:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Period ${ }^{\text {If }}$ Periodic Function was chosen as Construction Method, here the length of |  |
| the period for the replication is set. The first value is used for replication in |  |
|  | -direction, the second one for the $y$-direction. |
|  | Specific for grating boundary responses: For gratings, the Period will be <br> determined automatically from the Grating Period and the Rotation Angle, <br> both to be specified at the Physical Parameters panel. |

### 41.2 Boundary Response View



Figure 309. The preview dialog for boundary responses
The view for boundary responses ( $\varsigma$ Fig. 309) shows the complex values of the function $\mathcal{B}$ within the specified View Range. A data array view ( $\leftrightarrows$ Sec. 13.5) is used to this end. In particular, the view has the same context menu which allows you to change the shown field quantity ( $\varsigma$ Sec. 11.1) to e.g. imaginary part, change the aspect ratio ( $\leftrightarrows$ Sec. 11.5) or the color table ( $\leftrightarrows$ Sec. 11.2.4).

The following controls can be used to configure the data array view:

| ITEM | DESCRIPTION |
| :---: | :---: |
| View Range | The extension of the shown region, which is centered around the position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ). |
| Show Complete Aperture | If this option is checked, the View Range is set to the aperture size of the boundary response. Obviously, this option is only enabled if the boundary response uses the construction method Single Function with Aperture. |
| Wavelength | If the boundary response depends on the wavelength, you can set the wavelength used to calculate the preview here. If the boundary response does not depend on the wavelength, an information label is shown instead. |
| Accuracy Factor | The preview shows $(A \cdot 200 ; A \cdot 200)$ sampling points, where $A$ is the Accuracy Factor. |
| Re | If pressed, the real part of the complex boundary response is shown in the preview. |
| Im | If pressed, the imaginary part of the complex boundary response is shown in the preview. |
| A | If pressed, the amplitude of the complex boundary response is shown in the preview. |
| $\varphi$ | If pressed, the phase of the complex boundary response is shown in the preview. |
| $A^{2}$ | If pressed, the squared amplitude of the complex boundary response is shown in the preview. |
| 回 | Shows the diagram as separate data array document ( $\neg$ Sec. 13.5) which can be saved for later use. |

### 41.3 Types of Boundary Responses

### 41.3.1 Aperture

This boundary response allows to apply a rectangular or elliptical aperture on the incoming field. An aperture function has the value 1 inside and 0 outside the defined Diameter. The edge of the "hole" can be defined smooth, then the values don't "jump" from 1 (inside the aperture) to 0 (outside the aperture). Instead they follow a Gaussian function (starting at 1 and cut off at a value of 0.01 ) as shown in Fig. 310.


Figure 310. Definition of the edge width of an aperture. The aperture is at the left part of the graph.

The panel to enter the parameters for the boundary response is shown in Fig. 311.


Figure 311. Physical Parameters for the Aperture boundary response.
The parameters are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Shape | Possible options for the aperture shape are Rectangular and Elliptical. |
| Diameter $^{[\operatorname{PV}]}$ | Determines the diameter of the aperture in $x$ - and y-direction. |
| Relative Edge Width | The width of the aperture edge, defined relatively to the (smaller of the both <br> values of) Diameter. |
| Absolute Edge Width | The width of the aperture edge, defined in physical units. $\hookrightarrow$ Fig. 310. |

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.2 Grating Boundary Responses



Figure 312. Example for the Physical Parameters tab of a grating boundary response (here Sinusoidal Grating which has no specific parameters).

There are four boundary responses which represent a periodic grating invariant in y-direction: Rectangular Grating ( $\lrcorner$ Sec. 41.3.2.1), Sawtooth Grating ( $\hookrightarrow$ Sec. 41.3.2.2), Sinusoidal Grating ( $\hookrightarrow$ Sec. 41.3.2.3), and Triangular Grating ( $\hookrightarrow$ Sec. 41.3.2.4). Their Physical Parameters tab ( $\hookrightarrow$ Fig. 312) always has the following parameters.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Modulate Amplitude / Phase | Shall the amplitude or the phase be modulated? |
| Period ${ }^{\text {PV] }}$ | The period $P$ of the modulation. |
| Modulation Depth ${ }^{[\operatorname{PV}]}$ <br> Lateral Shift ${ }^{\text {PV }}$ | Range of the modulation $D$. Please see also 'Note on Phase quantization' below. A shift of the zero point of the modulation $\Delta x$ in the direction of Rotation Angle. |
| Rotation Angle ${ }^{\text {PV }}$ | The direction of the modulation will be rotated by this angle $\theta$ about the z-axis. |
| Achromatic / Chromatic | In the case of phase modulation the user can choose here whether the transmission shall work in the same way for all wavelengths (Achromatic) or if the defined Modulation Depth $D_{0}$ shall be considered as defined for one reference wavelength $\lambda_{0}$ (Chromatic), so the modulation depth $D$ applied with a field of wavelength $\lambda$ is calculated by $D=D_{0} \lambda_{0} / \lambda$. |
| Wavelength <br> Quantize Amplitude <br> / Phase | Reference wavelength $\lambda_{0}$ for the modulation depth in Chromatic mode. <br> Not for rectangular gratings. <br> If checked, the amplitude / phase is modulated discrete. Note that quantization is done in the following way: If $N$ is the number of Amplitude/Phase Levels and $\Delta h$ is the step height, then the quantization levels will be $0, \Delta h, \ldots,(N-1) \cdot \Delta h$. Please see also 'Note on Phase quantization' below. |
| Amplitude / Phase Levels | Not for rectangular gratings. <br> The number of discrete height steps (if Quantize Amplitude/Phase is checked). |

## Note on Phase quantization

In most cases, a quantized phase modulated grating would have a modulation depth equal to $2 \pi$, i.e. the lowest level $(=-\pi)$ and the highest level $(=+\pi)$ would be the same. In order to preserve the number of phase levels, the following phase levels $\phi_{k}$ are used:

$$
\begin{equation*}
\phi_{k}=\frac{d_{\mathrm{m}}}{2}-k \frac{d_{\mathrm{m}}}{n} \quad \text { with } \quad k=0, \ldots, n-1 \tag{41.2}
\end{equation*}
$$

where $d_{\mathrm{m}}$ means the given modulation depth and $n$ the number of phase levels. Therefore the total phase modulation depth is just $d_{\mathrm{m}}^{\text {total }}=\phi_{0}-\phi_{n-1}=d_{\mathrm{m}} \cdot \frac{n-1}{n}$, which corresponds to the total modulation depth in a Structure Design ( $\hookrightarrow$ Sec. 98). For your information, the total modulation range is given to the right of the Modulation Depth in the dialog.

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.2.1 Rectangular Grating

The effect of a grating transmission with a rectangular phase or amplitude profile can be simulated by this boundary response. The modulated value $t\left(x^{\prime}\right)$ is computed from the modulation depth $D$ and the slit width $w$ by

$$
t\left(x^{\prime}\right)= \begin{cases}D, & \text { if } \xi-w \leq 0  \tag{41.3}\\ 0, & \text { if } \xi-w>0\end{cases}
$$

for the case of amplitude modulation and by

$$
t\left(x^{\prime}\right)= \begin{cases}\exp (i D / 2), & \text { if } \xi-w \leq 0  \tag{41.4}\\ \exp (-i D / 2), & \text { if } \xi-w>0\end{cases}
$$

for modulation of the phase.
With $\xi=x^{\prime}-P\left\lfloor\frac{x^{\prime}}{P}\right\rfloor . P$ is the grating period and $x^{\prime}$ is the shifted and rotated position $x^{\prime}=x \cos \theta+y \sin \theta-\Delta x$ (with the lateral position $(x ; y)$, the rotation angle $\theta$, and the lateral shift $\Delta x$ ).

```
Special Rectangular Grating Value
Slit Width 20 \mum
```

Figure 313. Special Rectangular Grating Value for a Rectangular Grating boundary response.

## ITEM

DESCRIPTION
Slit Width ${ }^{\text {IVV }}$ The width $w$ of the slits within the grating.

The Common Grating Values are explained in Sec. 41.3.2, the other tab pages in Sec. 41.1.

### 41.3.2.2 Sawtooth Grating

The effect of a sawtooth like phase or amplitude profile can be simulated with this boundary response. The modulated value $t\left(x^{\prime}\right)$ is computed from the modulation depth $D$ and the grating period $P$ by

$$
t\left(x^{\prime}\right)= \begin{cases}D \xi / P, & \text { if Amplitude / Phase Increases with } x  \tag{41.5}\\ D(P-\xi) / P, & \text { if Amplitude / Phase Decreases with } x\end{cases}
$$

for the case of amplitude modulation and by

$$
t\left(x^{\prime}\right)= \begin{cases}\exp [i D \xi /(2 P)], & \text { if Amplitude / Phase Increases with } x  \tag{41.6}\\ \exp [i D(P-\xi) /(2 P)], & \text { if Amplitude / Phase Decreases with } x\end{cases}
$$

for modulation of the phase.
With $\xi=x^{\prime}-P\left\lfloor\frac{x^{\prime}}{P}\right\rfloor . P$ is the grating period and $x^{\prime}$ is the shifted and rotated position $x^{\prime}=x \cos \theta+y \sin \theta-\Delta x$ (with the lateral position $(x ; y)$, the rotation angle $\theta$, and the lateral shift $\Delta x$ ).

```
Special Sawtooth Grating Value
Inclination Amplitude Decreases with x Amplitude Increases with x
```

Figure 314. Special Sawtooth Grating Value for a Sawtooth Grating boundary response.

## DESCRIPTION

Amplitude / Phase If checked, the amplitude / phase of the unrotated grating transmission descends in Decreases with $x \quad$ positive $x$-direction.

Amplitude / Phase If checked, the amplitude / phase of the unrotated grating transmission ascends in Increases with $\mathbf{x}$ positive x-direction.

The Common Grating Values are explained in Sec. 41.3.2, the other tab pages in Sec. 41.1.

### 41.3.2.3 Sinusoidal Grating

The effect of a sinusoidal modulated phase or amplitude can be simulated with this boundary response. The modulated value $t\left(x^{\prime}\right)$ is computed from modulation depth $D$, grating period $P$, and lateral shift $\Delta x$ by

$$
\begin{equation*}
t\left(x^{\prime}\right)=D / 2\left(\sin \left(2 \pi\left(x^{\prime}-\Delta x\right) / P\right)+1\right) \tag{41.7}
\end{equation*}
$$

for the case of amplitude modulation and by

$$
\begin{equation*}
t\left(x^{\prime}\right)=\exp \left[i D / 2 \sin \left(2 \pi\left(x^{\prime}-\Delta x\right) / P\right)\right] \tag{41.8}
\end{equation*}
$$

for modulation of the phase.
$x^{\prime}$ is calculated from the lateral position $(x ; y)$ and the rotation angle $\theta$ via $x^{\prime}=x \cos \theta+y \sin \theta$.
This grating boundary response has no specific parameters. The Common Grating Values are explained in Sec. 41.3.2, the other tab pages in Sec. 41.1.

### 41.3.2.4 Triangular Grating

In a triangular phase or amplitude profile the modulation increases linearly along a certain part $a$ of the grating period $P$ and then decreases linearly to the original value along $b=P-a$. The modulated value $t\left(x^{\prime}\right)$ is computed from the modulation depth $D$, the period $P$ and the triangle side ratio $\sigma=b / a$ by

$$
t\left(x^{\prime}\right)= \begin{cases}D \xi(1+\sigma) / P, & \text { if } x^{\prime}<P /(1+\sigma)  \tag{41.9}\\ D(P-\xi)(1+\sigma) /(\sigma P), & \text { if } x^{\prime} \geq P /(1+\sigma)\end{cases}
$$

for the case of amplitude modulation and by

$$
t\left(x^{\prime}\right)= \begin{cases}\exp [i D \xi(1+\sigma) /(2 P)], & \text { if } x^{\prime}<P /(1+\sigma)  \tag{41.10}\\ \exp [i D(P-\xi)(1+\sigma) /(\sigma 2 P)], & \text { if } x^{\prime} \geq P /(1+\sigma)\end{cases}
$$

for modulation of the phase.
With $\xi=x^{\prime}-P\left\lfloor\frac{x^{\prime}}{P}\right\rfloor . P$ is the grating period and $x^{\prime}$ is the shifted and rotated position $x^{\prime}=x \cos \theta+y \sin \theta-\Delta x$ (with the lateral position $(x ; y)$, the rotation angle $\theta$, and the lateral shift $\Delta x$ ).

```
Special Triangular Grating Value
Triangle Side Ratio
```

Figure 315. Special Triangular Grating Value for a Triangular Grating boundary response.

## DESCRIPTION

Triangle Side Ratio ${ }^{\mathrm{PV}} \quad$ Ratio $\sigma$ of the projections of the sides of the triangle on its baseline.

The Common Grating Values are explained in Sec. 41.3.2, the other tab pages in Sec. 41.1.

### 41.3.3 Ideal Lens

This boundary response applies the effect of a thin lens with the Focal Length ${ }^{\mathbb{D V} /} f$ to the incoming field. One has to distinguish between a paraxial and the more general non-paraxial application. The first case is given by

$$
\begin{equation*}
t_{\mathrm{par}}(x, y)=\exp \left[-i k\left(\frac{\left(x-x_{0}\right)^{2}}{2 f_{x}}+\frac{\left(y-y_{0}\right)^{2}}{2 f_{y}}\right)\right] \tag{41.11}
\end{equation*}
$$

while the non-paraxial relation is described by

$$
\begin{equation*}
t(x, y)=\exp [i k r] \tag{41.12}
\end{equation*}
$$

with

$$
\begin{equation*}
r=-\sqrt{\left(x-x_{0}\right)^{2}+\left(y-y_{0}\right)^{2}+f^{2}} \tag{41.13}
\end{equation*}
$$

The wave number $k$ is defined by

$$
\begin{equation*}
k=\frac{2 \pi n}{\lambda} \tag{41.14}
\end{equation*}
$$

The Lateral Offset relative to the optical axis is represented by $\left(x_{0}, y_{0}\right)$.


Figure 316. Physical Parameters for an Ideal Lens transmission.

These parameters have to be entered to the dialog shown in Fig. 316 and are listed in the following table:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Paraxial Lens Function | If checked, the paraxial equation Eq. (41.11) is used, otherwise the nonparaxial Eq. (41.12). |
| Focal Length ${ }^{\text {PV }}$ | Corresponds to $f$ in Eq. (41.12) and to $f_{x}$ and $f_{y}$ in Eq. (41.11) respectively. It represents the focal length of a real lens. It can differ in $x$ - and $y$-direction in the case of a Paraxial Lens Function, which represents different curvature radii in a real lens. |
| Lateral Offset ${ }^{\text {PV }}$ | Corresponds to $x_{0}$ and $y_{0}$ in Eq. (41.11) and Eq. (41.13). It determines the displacement of the radial symmetric function, perpendicular to the optical axis. |
| Achromatic Function/ Chromatic Function | If the function is defined as achromatic, then the wavelength $\lambda$ used in Eq. (41.14) is always the wavelength of the incoming (member) field and thus the effect of the ideal lens function is always the same. <br> In contrast, in chromatic mode, the Wavelength $\lambda$ used in Eq. (41.14) is set to a fixed value in the tab page. This is closer to the behavior of a real lens. |
| Wavelength | The fixed wavelength used for Chromatic Function mode. Only for this wavelength the chromatic lens has exactly the entered Focal Length. |

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.4 Linear Phase

By using a linear phase boundary response, a wave can be deflected by a certain angle.
The direction of the linear phase can be entered as Cartesian Angles, Spherical Angles, Wave Number Vector, and Spatial Frequency.
The lateral transmission function is defined by:

$$
\begin{equation*}
t(x, y)=\exp \left[i\left(k_{x} x+k_{y} y\right)\right] \tag{41.15}
\end{equation*}
$$

Here you can find the Wave Number Vector $\boldsymbol{k}=\left(k_{x}, k_{y}, k_{z}\right)^{T}$, which has the length

$$
\begin{equation*}
k=\frac{2 \pi}{\lambda}=\sqrt{k_{x}^{2}+k_{y}^{2}+k_{z}^{2}} \tag{41.16}
\end{equation*}
$$

The Cartesian Angles $\alpha$ and $\beta$ (Alpha and Beta) are related to $k_{x}$ and $k_{y}$ by

$$
\begin{align*}
& \tan \alpha=\frac{k_{x}}{k_{z}}  \tag{41.17}\\
& \tan \beta=\frac{k_{y}}{k_{z}} \tag{41.18}
\end{align*}
$$

whereas the Spherical Angles $\phi$ and $\theta$ (Phi and Theta) are related to the wave number coordinates $k_{x}$ and $k_{y}$ by

$$
\begin{equation*}
k_{x}=k \cos \phi \sin \theta \tag{41.20}
\end{equation*}
$$

and

$$
\begin{equation*}
k_{y}=k \sin \phi \sin \theta \tag{41.21}
\end{equation*}
$$

In case of Spatial Frequency the given parameters $u$ and $v$ are related to $k_{x}$ and $k_{y}$ by

$$
\begin{equation*}
u=k_{x} /(2 \pi) \tag{41.22}
\end{equation*}
$$

and

$$
\begin{equation*}
v=k_{y} /(2 \pi) . \tag{41.23}
\end{equation*}
$$



Figure 317. Physical Parameters for a Linear Phase boundary response.
The following physical parameters are available for a Linear Phase boundary response ( $\hookrightarrow$ Fig. 317):

| ITEM | DESCRIPTION |
| :---: | :---: |
| Cartesian Angles | Defines the tilt angles $\alpha$ and $\beta$ (Alpha $a^{[V V}$ and Beta $\left.{ }^{[V V}\right)$ of the linear phase. The angle unit is degrees. For the definition see Eq. (41.17) and Eq. (41.18). |
| Spherical Angles | Defines the tilt angles in spherical coordinates $\phi$ and $\theta$ (Phi and Theta). The angle unit is degrees. For the definition see Eq. (41.20) and Eq. (41.21). |
| Wave Number Vector | Defines the direction of the linear phase in terms of the components $k_{x}$ and $k_{y}$ of the wave number vector $k$. For the physical meaning on it see Eq. (41.15). |
| Spatial Frequency | Defines the direction of the plane wave in spatial frequencies $u$ and $v$ for $x$ and y-direction, in units of $1 / \mathrm{m}$ (see Eq. (41.22) and Eq. (41.23)). |
| Achromatic Function / Chromatic Function | If the function is defined as achromatic, then the wavelength $\lambda$ used in Eq. (41.16) is always the wavelength of the incoming (member) field and thus the deflection is always the same. <br> In contrast, in chromatic mode, the Wavelength $\lambda$ used in Eq. (41.16) is set to a fixed value in the tab page. As you can see from Eq. (41.15), Eq. (41.22), and Eq. (41.23), setting the wavelength has no effect if the linear phase is defined by Wave Number Vector or Spatial Frequency. Thus, the group box Wavelength Dependency is not visible in these cases. |
| Wavelength | The wavelength the Cartesian Angles and the Spherical Angles refer to in Chromatic Function mode. |

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.5 Programmable Function



Figure 318. Physical Parameters for a programmable boundary response.
The programmable function allows you to define your own boundary response. This means you write a little code snippet defining the function $\mathcal{B}=f(x, y, \lambda, n(\lambda))$. The Physical Parameters tab ( $\rightarrow$ Fig. 318) contains:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition | This group box allows you to program the actual code snippet. Edit opens the <br>  <br>  <br>  <br> Source Code Editor $(\leftrightarrows$ Sec. 7.3$)$ to edit this snippet, and a validity indicator <br> $(\leftrightarrows$ Sec. 5.10$)$ shows whether this snippet is consistent. |
| Parameters ${ }^{\text {国 }}$ | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\leftrightarrows$ Sec. 7.4 |

General information about programming in VirtualLab Fusion can be found in Sec. 7. The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.6 Single Phase Dislocation

This boundary response can be used to simulate the effect of a special type of phase dislocations. Around phase dislocations the phase distribution of a field has a shape like a spiral staircase (see example in Fig. 319). A circle integral over the phase around a single phase dislocation results in a multiple of $2 \pi$.
The boundary response function $\boldsymbol{\mathcal { B }}(x, y)$ of the generated type of phase dislocations is given by

$$
\begin{equation*}
\mathcal{B}(x, y)=1 \cdot \exp (\mathrm{i} \cdot c \varphi)=1 \cdot \exp \left(\mathrm{i} \cdot c \arctan \frac{y-y_{0}}{x-x_{0}}\right), \tag{41.24}
\end{equation*}
$$

where $c$ denotes the Charge of the phase dislocation and $\left(x_{0}, y_{0}\right)$ marks its Position.


Figure 319. Two examples of a single phase dislocation transmission with a charge cof -5 (left) and +5 (right).


Figure 320. Physical Parameters for a Single Phase Dislocation boundary response.
The following physical parameters are available for a Single Phase Dislocation boundary response ( $\hookrightarrow$ Fig. 320):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Position | Corresponds to $x_{0}$ and $y_{0}$ in Eq. (41.24). It defines the lateral displacement <br> of the phase dislocation in physical coordinates with respect to the center of <br> the field. |
| Charge $^{\text {PV }}$ | Determines the charge $c$ of the phase dislocation ( $\hookrightarrow$ Eq. (41.24)). It gives <br> the number of $2 \pi$ jumps. Its sign specifies whether the phase increases or <br> decreases with angle $\varphi(\hookrightarrow$ Fig. 319$)$. |

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.7 Spherical Phase

A radially converging or diverging wave has a spherical phase, which can be simulated by using this boundary response. It is defined by

$$
\begin{equation*}
t(x, y)=\exp [i k r] \tag{41.25}
\end{equation*}
$$

with

$$
\begin{equation*}
r=\sqrt{\left(x-x_{0}\right)^{2}+\left(y-y_{0}\right)^{2}+z^{2}} \tag{41.26}
\end{equation*}
$$

and the wave number

$$
\begin{equation*}
k=\frac{2 \pi n}{\lambda} \tag{41.27}
\end{equation*}
$$

$n$ is the refractive index of the embedding medium.

The Lateral Offset $\left(x_{0}, y_{0}\right)$ relative to the optical axis as well as the Distance to Source Plane $z$ has to be entered in the Physical Parameters tab ( $\hookrightarrow$ Fig. 321).


Figure 321. Physical Parameters for a Spherical Phase boundary response.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Distance from Source Plane ${ }^{\text {PV }}$ | Corresponds to $z$ in Eq. (41.26). A wave, propagating in positive z-direction, would have the desired spherical phase if it is this distance (measured on the optical axis) away from its (point) source. |
| Lateral Offset ${ }^{\text {PV }}$ | Corresponds to $x_{0}$ and $y_{0}$ in Eq. (41.26). It determines the displacement of the radial symmetric transmission function, perpendicular to the optical axis. |
| Achromatic Function / Chromatic Function | If the function is defined as achromatic, then the wavelength $\lambda$ used in Eq. (41.27) is always the wavelength of the incoming (member) field and thus the effect of the spherical phase function is always the same. <br> In contrast, in chromatic mode, the Wavelength $\lambda$ used in Eq. (41.27) is set to a fixed value in the tab page. |
| Wavelength | The fixed wavelength used for Chromatic Function mode. Only for this wavelength a plane wave having a spherical phase as defined by Eqs. (41.25)-(41.27) would be completely focused if propagated a distance of $-z$. |

### 41.3.8 Stop

This boundary response allows you to apply a rectangular or elliptical stop function on the incoming field. Such a function has the value 0 inside and 1 outside the defined Diameter. The edge of the stop can be defined smooth, then the values don't "jump" from 1 (outside of the stop) to 0 (the blocking stop). Instead they follow a Gaussian function (starting at 1 and cut off at a value of 0.01 ) as shown in Fig. 322.


Figure 322. Definition of the edge width of a stop. The stop is at the right part of the graph.
The panel to enter the parameters for the boundary response is shown in Fig. 323.


Figure 323. Physical Parameters for the Stop boundary response.
The parameters are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Shape | Possible options for the aperture shape are Rectangular and Elliptical. |
| Diameter $^{[\operatorname{PV}}$ | Determines the diameter of the stop in $x$ - and y-direction. |
| Relative Edge Width | The width of the aperture edge, defined relatively to the (smaller of the both <br> values of) diameter. |
| Absolute Edge Width | The width of the aperture edge, defined in physical units. $\hookrightarrow$ Fig. 322. |

The controls that all boundary responses have in common are described in Sec. 41.1.

### 41.3.9 Zernike \& Seidel Aberrations

Zernike fringe, Zernike standard, and Seidel aberrations are often used to describe aberrations within an imaging optical system. The corresponding formulas are given in Sec. 134.2.


Figure 324. Parameters for a Zernike Standard Aberrations boundary response.

| Mode |  | Seidel Aberrations | $\checkmark$ |
| :---: | :---: | :---: | :---: |
| n | Name | Magnitude [ $\lambda$ ] | Angle |
| 1 | Piston | 0 |  |
| 2 | Distortion | 0 | $0^{\circ}$ |
| 3 | Field Curvature | 0 |  |
| 4 | Astigmatism | 0 | $0^{\circ}$ |
| 5 | Coma | 0 | $0^{\circ}$ |
| 6 | Spherical Aberration | 0 |  |
| Maxi | mum Radial Extent | $150 \mu \mathrm{~m}$ | Reset Tabular |

Figure 325. Parameters for a Seidel Aberrations boundary response.
The Physical Parameters tab (see Fig. 324 and Fig. 325) allows the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Mode | You can choose between Zernike Fringe Aberrations, Zernike Standard Aber- <br> rations, and Seidel Aberrations. |
| Polynomial Degree | OnLY FOR ZERNIKE STANDARD ABERRATIONS <br> Allows you to set the maximum polynomial degree of the used Zernike terms, <br> and thus indirectly the number of coefficients. |
| \{Coefficients Table\} | Allows you to enter the coefficients of the polynomial describing the aberra- <br> tions. They refer to wavelengths. For example a Zernike fringe tilt of 1 leads <br> to phase values in the range $-1 \lambda(=-2 \pi) \ldots+1 \lambda(=+2 \pi)$. <br> Via the context menu of the table you can copy and paste the parameter list. |
| Maximum Radial Extent | The radii $r=\sqrt{x^{2}+y^{2}}$ are divided by this value. It is equal to half the Di- <br> ameter plus the Absolute Edge Width as set up in the Basic Parameters tab. <br> This parameter is sometimes also referred to as maximum radius, radius of <br> unit pupil, or radius of unit disc. |
| Reset Tabular | Resets all table entries to 0. |

### 41.3.10 Stored Function

By using the Stored Function it is possible to include an arbitrary sampled transmission function into an optical system. Fig. 326 shows the dialog where the transmission and the other parameters can be set.


Figure 326. Parameters of a stored function.

All parameters of the dialog are listed in the following table:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Type of Transmission Function | The chosen type determines which interpolation is used to retrieve function values at a certain position and what scale errors can be simulated. A Continuous function uses Cubic 8 Point Interpolation, while Pixelated or Quantized transmissions use Nearest Neighbor. Details on these interpolations can be found in Sec. 13.2.2. <br> Furthermore a Phase-Only function allows to apply a linear scale factor on the phase. A Regularly Quantized Phase-Only Transmission assumes $2^{n}$ equidistant phase levels with distances of $2 \pi / 2^{n}$. In this case one can assume a binary mask fabrication process and apply an error to each mask. Note that any Phase-Only option will not cause any amplitude modulation that may be present to be ignored. |
| Set | Sets the desired Jones Matrix Transmission. When you click on this button you can do the following: <br> - Load a Jones Matrix Transmission from a .ca2 file. Note that the Jones matrix of that transmission is ignored. <br> - Select from Documents allows you to select an already open Jones Matrix Transmission. <br> - Reset the data to the default transmission. |
| Show | Shows the Complex Amplitude containing the currently set transmission as separate document. |
| Sampling | Gives information about the number of sampling points, the sampling distance, and the diameter of the currently set transmission. |
| Pixelation Factor ${ }^{\text {PV }}$ | If these factors $\left(F_{x} ; F_{y}\right)$ are larger than one, every pixel in the original transmission is replaced by $F_{x} \times F_{y}$ pixels with the same value. This ensures that a pixelated transmission is really simulated as pixelated. |


| Impose Linear Scale Error <br> by Scale Factor | Takes a specific scale error into account, the Linear Scale Factor ${ }^{\text {VV }}$. It is <br> considered by |
| :--- | :--- |
| $\qquad$$T_{\text {new }}(x, y)=\exp \left(i \phi_{\text {new }}(x, y)\right)=\exp \left(i \phi_{\text {old }}(x, y) f\right), \quad(41.28)$ |  |
| whereby $f$ denotes the Linear Scale Factor. |  |

## 42 Surface Regions

Surface Regions are regions on a surface ( $\leftrightarrows$ Sec. 35) which behave differently than just a plain surface. As such they consist of the actual geometric region and the functionality to be applied in that region. In the moment only surface regions with an idealized or real grating are implemented. These grating regions are described in Sec. 42.1.
Multiple regions on a surface form a so-called Surface Layout ( $\varsigma$ Sec. 40).

### 42.1 Grating Regions

Grating Regions describe the effect of an idealized or real grating within a certain geometric region.
The edit dialog for grating regions has the following three tab pages:

| TAB PAGE | DESCRIPTION |
| :---: | :---: |
| Shape | Describes the actual geometric region in which the grating is located. $\rightarrow$ Sec. 42.1.1 |
| Region Channels | Allows you to define which propagation channels are used for this region. The names of the channels refer to the sign the $z$-component of the direction vector the incident and outgoing light has, respectively. Plus-Plus-Direction for example refers to transmitted light going along the optical axis while Minus-Plus-Direction refers to reflected light going initially against the optical axis. Note that this settings might be overwritten by the settings on the Channel Configuration tab ( $\varsigma$ Sec. 43.9) of the parent component. |
| Grating | Describes the idealized or real grating. $\leftrightarrows$ Sec. 42.1.2 |

Additionally it has a validity indicator ( $\leftrightarrows$ Sec. 5.10 ) in the bottom-left corner.

### 42.1.1 Shape Tab



Figure 327. Shape tab of a grating region.
In the top of this tab ( $\hookrightarrow$ Fig. 327) there are the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| 4 | Creates a new geometric region, which can be either a New Rectangular Region ( $\rightarrow$ Sec. 21.1.1), New Elliptic Region ( $\rightarrow$ Sec. 21.1.2), New Simple Polygon Region ( $\leftrightarrows$ Sec. 21.1.3), New Sampled Region ( $\leftrightarrows$ Sec. 21.1.4), or New Composed Region ( $\rightarrow$ Sec. 21.1.5). |
| 3 | If you click on this button you can do the following: <br> - Load a region document ( $\varsigma$ Sec. 21) from a .rgn file. <br> - Select from Documents allows you to select an already open region document. |
| Herlor | Saves the current region definition as region document. |
| Q | Displays the current region definition as separate region view ( $\checkmark$ Sec. 21.3). |
| Region Name | You can give the region an arbitrary name which for example identifies this region in the edit dialog of the parent surface layout. |
| Spectral Domain / Region Type | These two controls provide useful information about the current region. |

In the lower part there are controls specific to the current Region Type (see sections given above for details) and a preview of the region.

### 42.1.2 Grating Tab



Figure 328. Order Selection tab of a grating region.
On this tab ( $\hookrightarrow$ Fig. 328) you first specify the general parameters of the grating.

| ITEM | DESCRIPTION |
| :--- | :--- |
| 1D-Periodic (Lamellar) / | Determines the periodicity of the grating. Influences some controls on this <br> tab page and in the end also the computational effort. |
| Grating Period ${ }^{\text {PV }}$ | The period of the grating. |
| Orientation ${ }^{\text {PV }}$ | Rotates the whole grating around the z-axis and so determines into which <br> direction the grating orders go. |

Furthermore this tab contains two sub-tabs. On the Order Selection tab ( $\hookrightarrow$ Sec. 42.1.2.1) you define which orders shall be used for the simulation. On the Efficiencies tab ( $\leftrightarrows$ Sec. 42.1.2.2) you either specify the efficiencies directly or via a snippet or you define a real grating whose efficiencies are used.

### 42.1.2.1 Order Selection Tab



Figure 329. Order Selection tab of a grating region with a 2D-Periodic grating.
This tab page ( $\hookrightarrow$ Fig. 329) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Propagating Orders | There are three ways how the orders specified by the user are taken into account during the simulation of the optical setup. <br> - All Orders: All orders are taken into account, independent from the user specification. <br> - Specified Orders: Only the orders specified by the user are taken into account. <br> - All but Specified Orders: Only the orders not specified by the user are taken into account. |
| From Front Side | Table with all propagating orders if the grating is illuminated from the front side, i.e. with light whose z-component of the direction vector has a positive sign. $\hookrightarrow$ Sec. 5.12 |
| From Back Side | Table with all propagating orders if the grating is illuminated from the back side, i. e. with light whose z-component of the direction vector has a negative sign. $\hookrightarrow$ Sec. 5.12 |

### 42.1.2.2 Efficiencies Tab

This tab offers you three ways how the efficiencies of the distinct orders are determined:

- Constant: The efficiencies of an idealized grating are specified via a table. $\hookrightarrow$ Sec. (a)
- Programmable: The efficiencies of an idealized grating are specified via a snippet in dependency from e. g. direction or wavelength. $\hookrightarrow$ Sec. (b)
- From Real Grating: The efficiencies are calculated from a real grating stack. In this case the Grating Period and the period of the stack defining the real grating are synchronized so that they are always the same. $\hookrightarrow$ Sec. (c)

If you switch from a real grating to an idealized grating you are asked whether the Grating Period shall be the period of the stack or the value you last entered as Grating Period.
(a) Constant Efficiencies


Figure 330. The Efficiencies tab of a grating region if Constant efficiencies are specified.

For Constant Efficiencies there are the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Overall Transmission / For consistency the sum of all grating orders must not be larger than $100 \%$. <br> Overall Reflection With these controls you can divide this $100 \%$ between transmission and re- <br> flection. If then the sum of the efficiencies for either the transmitted or the re-  <br> flected orders exceeds the specified limit, the validity indicator ( $\hookrightarrow$ Sec. 5.10)  <br> of the dialog indicates a warning.  |  |
| From Front Side / | Table where you can enter efficiencies |
| From for all orders specified in the From |  |
|  | Front Side / From Back Side table of the Order Selection tab. If All Orders <br> or All but Specified Orders was set on this tab, then all entered efficiencies <br> are subtracted from the overall transmission / reflection efficiency and this <br> remaining efficiency is then distributed evenly among the unspecified orders. |
|  |  |

## Example

You have specified that the order " $\mathrm{T}+1$ " for the light coming from the front side has an efficiency of $50 \%$ whereas the overall transmission is $80 \%$. You have set to use All Orders and the orders "T-1", "T0", and "T+1" are propagating ones. Thus the remaining $30 \%$ are distributed evenly among "T-1" and "T0" and thus both orders have $15 \%$ efficiency.

## (b) Programmable Efficiencies



Figure 331. The Efficiencies tab of a grating region if Programmable efficiencies are specified. The snippet is valid and some general parameters are available.

For Programmable Efficiencies you can program a snippet returning a list of order numbers and corresponding efficiencies in dependency from e.g. wavelength, direction of the incident light and whether the light is reflected or transmitted. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3) to edit this snippet, and a validity indicator $(\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. Below these two controls you can edit the values of the global parameters of the snippet ( $\hookrightarrow$ Sec. 7.4).

## (c) Efficiencies From Real Gratings

The efficiencies can also be calculated from a real grating stack ( $\hookrightarrow$ Sec. 39). The efficiencies of this stack are then calculated rigorously with the Fourier Modal Method (FMM, $\hookrightarrow$ Sec. 96.3) when the Grating Channel Analyzer ( $\hookrightarrow$ Sec. 91) is used. Alternatively you can load an already calculated lookup table with efficiencies from file.
Note that in case of a $2 D$ Grating only a one-dimensional section of the orders is used. I.e. only orders are taken into account having an order number of zero in y-direction (of the unrotated grating).


Figure 332. The Efficiencies tab of a grating region if the efficiencies are calculated From Real Gratings.

For Efficiencies From Real Gratings there are the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Use Modulated Grating Parameters within Region | Switches to a mode where not a well-defined grating is used but a grating where parameters vary over the region. This mode is explained in Sec. 42.1.3. |
| \{Actual Grating Stack ${ }^{\text {[ }}{ }^{\text {E }}$ | Control for loading a stack with a grating from catalog, for editing and viewing it. $\hookrightarrow$ Sec. 34.1 |
| On Front Side of Base Surface | If checked it is assumed that the stack is placed on the front side of the base surface. This means that in comparison to its normal orientation it is rotated by $180^{\circ}$ about the $y$-axis and thus points against the optical axis. Sec. 39.1.2 shows an example. |
| On Back Side of Base Surface | If checked it is assumed that the stack is placed on the back side of the base surface. This means that it is used in its normal orientation. |
|  | The FMM does not evaluate the real grating but an approximated structure decomposed into layers and transition points. By clicking on the Configure button you can adjust and preview this decomposition and set the number of calculated orders. $\rightarrow$ Sec. 96.3.1 |
| Lookup Table | Normally the lookup table with the efficiencies is filled by the LUT Result Generator ( $\leftrightarrows$ Sec. 46). But the controls in this section allow you to Save a lookup table into a file so that you can Load it into other grating regions. Or you can Remove the lookup table to enforce a new calculation by the Grating Channel Analyzer ( $\leftrightarrows$ Sec. 91) / LUT Result Generator. A label gives you some additional information about the current lookup table - or informs you that no lookup table is set. The button right to it shows all wavelengths and directions for which the lookup table contains Rayleigh coefficients. |

### 42.1.3 Modulated Grating Parameters

If Use Modulated Grating Parameters within Region is checked the parameters of the grating used within the region are modulated. Currently we support the 1D or 2D variation for grating parameters (reason for this is the usage of a 1D or 2D data array to store the Rayleigh matrices in dependency of the grating parameters which are varied). In order to use a modulated grating within a region, two things need to be specified:

1. The function how the grating parameter is changed inside the region in dependency of the lateral position $(x ; y)$.
2. The lookup tables which define the grating effect in dependency of the grating parameters. (note: the grating effect is defined by a complex $2 \times 2$ matrix (Rayleigh matrix) per grating parameter, so all polarization effects are included, because we do not deal "only" with efficiencies.

The lookup tables should typically be filled by using the Footprint and Grating Analysis tool ( $\hookrightarrow$ Sec. 101.1).
Fig. 333 shows the edit dialog for activated Use Modulated Grating Parameters within Region.


Figure 333. The Efficiencies tab of a grating region if the efficiencies are calculated From Real Gratings with modulated grating parameters.

The following options are available in this section of the region edit dialog:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Grating Stack | The grating stack which is associated with this region. In modulated parameter mode the grating stack cannot be edited and also won't be used during propagation, because all required information is given in the lookup tables. The stack can only be displayed. |
| Grating Parameter Modulation Function | In this group box several information about the configured modulation function is displayed (like number of parameters that are defined for the modulation, name of the parameter(s) and type of modulation, e.g. sampled or programmable. In addition the user can edit the grating parameter modulation function by clicking on the Edit button ( $\leftrightarrows$ Sec. 42.1.3.1). It is also possible to display the parameter variation function in the region. This is triggered by clicking on the View button ( $\hookrightarrow$ Sec. (a)). |
| Lookup Table | The effect of the modulated grating is defined by a special lookup table concept. Here the Rayleigh matrices per grating parameter is stored. The user can edit the lookup tables by clicking on the corresponding Edit button ( $\varsigma$ Sec. 42.1.3.2). |

### 42.1.3.1 Edit Grating Parameter Modulation Function

The grating parameter modulation function defines the dependency of the grating parameter(s) in dependency of the lateral position in the grating region. Currently we support that one or two grating parameters can be varied.
Fig. 334 shows the edit dialog of the grating parameter modulation function.


Figure 334. The dialog to edit the grating parameter modulation function.
In the top part of the dialog the following options can be configured by the user:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Define Grating Parameter Function for Two Grating Parameters | Currently we allow the definition for one or two grating parameters that are varied. By checking this option the variation of two parameters is enabled. If the option is unchecked only one parameter is available for modulation. |
| Settings for Grating Parameter \#1 | The user needs to specify several information for parameter \#1 that shall be used for parameter variation: <br> - The name of the parameter (string format) <br> - The physical property of the parameter (selection by a drop-down list) <br> - Minimum and maximum of the parameter <br> This information is used within the display of the grating parameter function and within the parameter extraction in case of sampled function definition. |
| Settings for Grating Parameter \#2 | The user needs to specify several information for parameter \#2 that shall be used for parameter variation: <br> - The name of the parameter (string format) <br> - The physical property of the parameter (selection by drop-down list) <br> - Minimum and maximum of the parameter <br> This information is used within the display of the grating parameter function and within the parameter extraction in case of sampled function definition. |

VirtualLab Fusion provides two options for the specification of the grating parameter dependency from $\mathrm{x}-\mathrm{y}$ coordinates:

1. Programmable Function: The user has to implement a snippet which returns an array of parameters in
dependency of the position. If only one parameter is to be varied the length of the array is 1 , otherwise it is 2. The configuration of the snippet can be done by the standard input methods provided by VirtualLab Fusion ( $\hookrightarrow$ Sec. 7.3).
2. Sampled Data: A table is displayed where the coordinates of the data points and the corresponding values are listed. This table can be edited by several tools, which can be accessed by clicking on the corresponding buttons on the right side of the table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Edit Data Point | By clicking this button a dialog will be displayed which contains the parame- <br> ters of the currently selected row. The user can modify the coordinate of the <br> data points as well as the value(s) at the coordinate. |
| Add Data Point | To add a new data point, click this button. A dialog will be displayed where <br> you can enter the coordinate as well as the value(s) at the coordinate. Af- <br> ter pressing OK the data point will be added to the list and the table will be <br> updated. |
| Remove Data Point | By clicking on the Remove Data Point button the currently selected data point <br> will be deleted from the list of coordinates. Afterward the table will be updated. |
| Load from Data Array | In addition to the previously mentioned options it is also possible to load data <br> points from a gridless data array. This operation will delete all present data <br> points and add all data points from the selected data array. Note: this oper- <br> ation is essential if you like to transfer for example a programmable grating <br> parameter modulation function into a sampled one, or you like to increase or <br> decrease the resolution of the data points. This tool is especially helpful in <br> combination with the tool described in Sec. (b). |

The information of the discrete data points has to be converted into a continuous function by interpolation. For this purpose we offer here the interpolation by

- Spline interpolation
- Nearest neighbor interpolation (in non-equidistant case this is also known as Voronoi interpolation) The interpolation method can be selected by checking the corresponding option on the bottom of the dialog.


## (a) Show Grating Parameter Variation Function

On the bottom of the dialog shown in Fig. 334 the user can click on View to visualize the grating parameter modulation function. A dialog is shown, in which the user can select the (varied) grating parameter to be displayed. Below the drop-down list for selection of the parameter to show, a graph is displayed which visualizes the grating parameter variation within the region. The Minimum and Maximum value configured for the selected grating parameter are used here also for visualization.
Fig. 335 shows the output of the grating parameter modulation function visualization tool (in this example the parameter modulation function was defined by a snippet which represents a linear modulation in dependency of the positions).


Figure 335. Visualization of the grating parameter modulation for a linear parameter dependency.

## (b) Show Grating Parameter Modulation Values As Data Array

Additionally to the visualization tool, the user can also extract the parameters for the grating parameter modulation function as data array. By clicking on the corresponding button at the bottom a dialog is shown which offers several options for the extraction.
Fig. 336 shows the edit dialog which can be used to define the parameters for the sample selection for the extraction into a data array.


Figure 336. The dialog to define the sample selection.
The following parameters can be configured for extraction:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Samples of Present <br> Sampled Modulation | If this option is checked the original data points are used for extraction. This <br> option is only available if the modulation is defined by sampled data. It is re- <br> commended to use this option to transfer the parameters from one modulation <br> function to another one. |
| Add Data Point | If Use Samples of Present Sampled Modulation is false, the user can define <br> the number of sampling points manually. Then VirtualLab Fusion will use the <br> extension of the underlying region and perform an equidistant evaluation of <br> the grating parameter modulation function according to the number of data <br> points defined in the dialog. |

parameter modulation function. In addition it can be also applied to change the resolution of the sampled grating parameter modulation function.

### 42.1.3.2 Edit Lookup Tables

In addition to the configuration of the grating parameter modulation function also the specification of the lookup tables to use is necessary to enable the simulation of a region with modulated grating parameters. This is done within the dialog displayed in Fig. 337.
The definition of the lookup tables for the modulated grating region is typically done automatically by the footprint and grating analysis tool ( $\hookrightarrow$ Sec. 101.1). In case you need to adapt the lookup table data manually the tools described below can be used.


Figure 337. Edit dialog to configure the lookup tables for the modulated grating region.

The following information is displayed in the table inside the edit dialog of the lookup tables per entry:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index | The index of the lookup table entry within the configuration. |
| Direction | The incident direction associated with the lookup table entry. The incident direction is <br> given in the grating coordinate system (including the rotation of the grating along z-direction <br> relative to the grating region). |
| Wavelength | The wavelength for which the lookup table is defined. |
| Order | The order information for which the lookup table entry is defined. In combination with the <br> sign of the incident direction we have a full 4-channel definition (including transmission and <br> reflection from front and behind). The order number in general is two-dimensional. In case <br> of 1D-periodic gratings the second value of the order index will be always zero. |
| Show | The lookup table entry is stored as a data array (1D data array for variation of one grating <br> parameter and 2D data array for two parameters). By clicking on the Show button the <br> lookup table is displayed as data array in VirtualLab Fusion. |
| The lookup table entry is stored as data array (1D data array for variation of one grating <br> parameter and 2D data array for two parameters). It has to have four subsets, due to the <br> fact that for each grating parameter a complex $2 \times 2$ matrix (Rayleigh matrix) has to be <br> stored. The subsets represent the entries of the Rayleigh matrix ( $R_{x x}, R_{x y}, R_{y x}$ and $R_{y y}$ ). <br> By clicking the Set button, the user can select a data array from the VirtualLab Fusion <br> main window and define it as underlying data for the corresponding lookup table entry. <br> VirtualLab Fusion will check the validity of the data to be set. |  |

Several additional tools are available to modify the lookup table data defined in the dialog. These tools can be accessed by clicking on the corresponding buttons on the right side of the table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Add Lookup Table Entry | By clicking on this button a dialog is shown, where the user can enter all <br> necessary information for one lookup table entry. The options available within <br> the edit dialog are described in Sec. (a). |
| Load from Hard Disc | Additionally the user has the option to load the lookup table data (all entries) <br> from hard disc. Therefor a folder has to be selected where all lookup tables <br> to load are stored. The file names of the da-files within the folder encode all <br> necessary information. Usually these files will be created by the footprint and <br> grating analysis tool ( $\hookrightarrow$ Sec. 101.1.2), where the calculated lookup table data <br> is automatically stored on hard disc. |
| Remove Lookup Table En- | By clicking on this button the selected lookup table entry will be removed from <br> the underlying data set. |
| try | To remove all lookup tables, press the Remove All button. |
| Remove All |  |

## (a) Add Lookup Table Entry

Fig. 338 shows the edit dialog to add a new lookup table entry to the grating region with modulated grating parameters.


Figure 338. Edit dialog to add a new lookup table entry.

The user has to define the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | The wavelength for which the lookup table to add will be used. |
| Direction | Normalized direction vector in the grating coordinate system. It is possible to <br> enter an arbitrary 3D vector and afterward perform normalization by pressing <br> on the update button (3). |
| Is Transmission | Boolean flag whether the lookup table entry is defined in transmission (true) <br> or reflection (false). The illumination from in front or behind is encoded in the <br> sign of $s_{z}$. |
| Order Number | The user needs to define the order number associated with the lookup table <br> entry. |
| The lookup table entry is stored as data array (1D data array for variation of <br> one grating parameter and 2D data array for two parameters). It has to have <br> four subsets, due to the fact that for each grating parameter a complex $2 \times 2$ <br> matrix (Rayleigh matrix) has to be stored. The subsets represent the entries <br> of the Rayleigh matrix $\left(R_{x x}, R_{x y}, R_{y x}\right.$ and $\left.R_{y y}\right)$. By pressing on the Set button <br> a data array which fulfills these restrictions can be set. |  |

After clicking the OK button, the entered data will be checked for validity (to ensure unique entries) and the input will be added to the lookup tables of the grating region.

## VII Optical Systems

In VirtualLab Fusion optical systems are defined using the Optical Setup document ( $\leftrightarrows$ Sec. 43). The parameters of an optical setup can be varied using the Parameter Run ( $\leftrightarrows$ Sec. 44). Session Editors ( $\leftrightarrows$ Sec. 47) are a special way how optical setups can be created.

## 43 Optical Setup

In VirtualLab Fusion optical systems are defined using the Optical Setup document. It can contain different Optical Setup Elements (light sources, components, detectors, and so on) which are linked to define an execution sequence.
This document is represented by two document windows. The Optical Setup View ( $\hookrightarrow$ Sec. 43.1) contains a two-dimensional flowchart where the user can add, place and link the Optical Setup Elements. The Optical Setup Editor window ( $\leftrightarrows$ Sec. 43.2) allows to configure the linkages, start the simulation and change various settings.
Closing one of both documents will close the other window automatically, so the associated Optical Setup is no longer available.
A sample Optical Setup is shown in Fig. 339.


Figure 339. A sample Optical Setup.

### 43.1 Optical Setup View

The Optical Setup View ( $\hookrightarrow$ Fig. 340) is one of the two document windows in VirtualLab Fusion which is used for configuring an Optical Setup.
The window is divided into two areas. On the left side a tree view with all available types of Optical Setup Elements is displayed, sorted into categories (light sources, components, detectors, and so on). Which categories and Optical Setup Elements are available depends on the type of the Optical Setup ( $\hookrightarrow$ Sec. 43.11). Above the tree there is a text box where you can enter a filter string. Only elements containing the given string or being in a category matching the given string are shown. The matching is case insensitive. It is possible to search for multiple words and word groups embraced by quotation marks.
The right side is used for showing the two-dimensional flowchart which visualizes the current optical setup.


Figure 340. The Optical Setup View.

In order to add a new element to the Optical Setup, the user simply drags the Optical Setup Element from the tree view on the left side and drops it onto the flowchart area on the right side. Alternatively, the user can double click an item in the tree view. After doing this, the selected element's symbol will be added to a default position on the flowchart.
While adding an element to the Optical Setup, a unique index is assigned. Therefor the following rules are used:

- The active light source always gets the index 0 .
- There is always only one active light source at the same time. If there is more than one light source in an Optical Setup, the non-active sources get indices of 500 and higher.
- All ideal and real components are enumerated with indices between 1 and 499.
- The indices of detectors start at 600 and are increased till 799.
- Indices higher than 799 are reserved for indexing analyzers in the Optical Setup.

After adding an Optical Setup Element, its properties can be edited by double clicking the associated symbol in the Optical Setup View.


Figure 341. The button in the Optical Setup View to toggle to the Optical Setup Editor.

The following tools for the Optical Setup View are available in its bottom right corner:

| ITEM | DESCRIPTION |
| :--- | :--- |
| 目 | Shows a resizable panel on the bottom of the form where you can enter ar－ <br> bitrary notes，e．g．for documentation purposes．Clicking on this button again <br> hides this panel again．An orange background of this button indicates the <br> presence of notes． |
| The notes panel can have two modes：One（with gray background）shows |  |
| the text in a formatted，but read－only way．The other mode（with white back－ |  |
| ground）allows you to edit the text and format it using HTML（and CSS）syntax． |  |
| For example you can use＜b＞．．．＜b／＞to make some text bold and＜i＞．．．＜i／＞to |  |
| make it italic．You can toggle between these two modes with the $/$ button． |  |
| In both modes you can change the displayed font size by pressing Ctrl and |  |
| scrolling with the mouse wheel． |  |

To toggle between the Optical Setup View window and the Optical Setup Editor window，the button in the upper right corner of the Optical Setup View can be used．（ $\hookrightarrow$ Fig．341）

## 43．1．1 Customizing the Optical Setup View

For a good visualization elements in the flowchart area can be arranged by using drag and drop．
Important：The positions of the Optical Setup Element symbols in the flowchart have nothing to do with the locations of the elements in the actual optical setup．This position is set via the edit dialog of each element or by clicking the Positioning Control．Details about positioning can be found in Sec．43．8．2．

The Positioning Control is available for all（real）Components，Ideal Components，and Detectors．Light Sources and Analyzers don＇t have a position to configure．For grating components illuminated by an ideal plane wave， the position cannot be changed．
Furthermore，each Optical Setup Element has a Comment Control where you can enter an arbitrary comment to describe the corresponding element．You can extend this control by clicking on the $⿴ 囗 十 \rightarrow$ button and minimize it again by clicking $\boxminus$ ．To change the comment simply click on its text．A small T．．．next to the $⿴ 囗 十$ indicates that the comment has been changed，i．e．that it is not the default comment．
The caption of each Optical Setup Element can be changed．
Sometimes（e．g．for presentations）it is helpful to hide the Positioning Controls and／or the Comment Controls． This can be done via the context menu of the flowchart．This context menu contains the following items：

| ITEM | DESCRIPTION |
| :--- | :--- |
| Show Comments | This toggles the visibility of the Comment Controls. |
| Paste Optical Setup Ele- <br> ments | Allows to paste Optical Setup Elements from the Windows ${ }^{\text {TM }}$ clipboard to the <br> current position of the mouse cursor. You can copy one or more Optical Setup <br> Elements to the Windows ${ }^{\text {TM }}$ clipboard by selecting them and then using the <br> context menu entry Copy Selected Optical Setup Elements. |
| Improve Node Locations | The locations of the flowchart nodes, i.e. the symbols of the Optical Setup <br> Element, are reset automatically. |
| Show Position Controls | The visibility of the positioning controls can be set here. |
| Show Only z-Positions | If checked, only the z-Positions of the elements are shown. This menu item is <br> a shortcut to the more detailed advanced option described in Sec. 43.8.2.4. |
| Advanced Position Con- | Opens a sub-menu for advanced configuring of the Positioning Controls. It is <br> described in Sec. 43.8.2.4. |

You can change the zoom factor (i.e. the size of all symbols and fonts) by pressing and holding Ctrl and scrolling via mouse wheel.

### 43.1.2 Mouse and Keyboard Interactions

The following list summarizes all actions that can be done with mouse and keyboard:

- Drag an item from the tree view to the flowchart: Adds a new element to the Optical Setup View.
- Drag an item in the flow chart: Moves the element in the flowchart (Does not affect its real position!).
- Click on an Optical Setup Element or linkage: Selects this element or linkage.
- Click on 田 / : Extends / minimizes a comment.
- Click on an element caption: Makes the element caption editable.
- Click on a comment: Makes the comment editable.
- Double click on an Optical Setup Element: Opens the corresponding edit dialog.
- Double click on a linkage: Switches the linkage on or off. An off linkage is not executed during simulation of the Optical Setup and is indicated by a dashed line.
- Double click on a Position Control: Opens a dialog to edit the position of the Optical Setup Element in the optical setup ( $\hookrightarrow$ Sec. 43.8.2.4).
- Click and drag: Selects multiple Optical Setup Elements and linkages.
- Ctrll + A: Selects all Optical Setup Elements and linkages.
- Del: Removes the currently selected Optical Setup Element(s) and linkage(s) from the optical setup. If a removed element was connected with other Optical Setup Elements the according linkages are deleted too.
- Ctrl+C: Copies the currently selected Optical Setup Elements to the clipboard, to paste them into the same or another Optical Setup View.
- Ctrl+V: Pastes the Optical Setup Element(s) which are currently in the clipboard to the current mouse position (to the upper left corner if the mouse is outside the flowchart).
- Ctrl+D: Opens a dialog to select a result window with a rectangular marker ( $\hookrightarrow$ Sec. 11.3). For each selected detector the size of this marker is then set as Window Size and its (central) position is set as Center Position. $\hookrightarrow$ Sec. 74.1.1
- Scrolling with the mouse wheel: Moves the currently visible region of the Optical Setup View up and down.
- Shift and scrolling with the mouse wheel: Moves the currently visible region of the Optical Setup View left and right.
- Ctrl and scrolling with the mouse wheel: Changes the zoom factor (i.e. the size of all symbols and fonts).
- Click with the right mouse button on an Optical Setup Element: Copies this element to the clipboard via a context menu. Some real and ideal components have in this context menu additional entries for converting this component to another type ( $\hookrightarrow$ Sec. 55).
Detectors have one entry to copy window size and position ( $\hookrightarrow$ Sec. 74.1.1) from a result window with a rectangle marker and one entry to copy certain settings from another detector ( $\hookrightarrow$ Sec. 74.2).
- Click with the right mouse button on an unoccupied region of the flowchart: Opens a context menu to configure the Optical Setup View and to paste elements from the clipboard to the current position.
"Click" or "double click" means always clicking with the left mouse button unless otherwise noted.
The following elements can be neither deleted nor copied:
- all elements but analyzers in a Grating Optical Setup
- the Eigenmode Analyzer

The symbol of each Optical Setup Element which is not a light source or analyzer has one gray input connector triangle at its left side representing its input. Vice versa, each symbol of an Optical Setup Element which is not a detector or analyzer has one gray output connector at its right side, representing its output. Linkages always go from an output connector to an input connector triangle of another Optical Setup Element. Note that all Optical Setup Elements but detectors can have only one incoming linkage. If you click and drag from one connector triangle to another free connector triangle, you can create a new linkage. A selected linkage has two green diamonds with which you can move the start or end of this linkage to another free connector triangle of the same type (input or output triangle, respectively). Fig. 342 shows an example.


Figure 342. Figure a) shows how to create a new linkage by clicking on the (output) connector triangle of Stop \#1 followed by dragging the line to the left (input) connector triangle of the Stop \#2 symbol.
Figure b) shows an activated linkage, indicated by two green diamonds. Clicking on one of these and dragging the lose end of the line to another connector triangle allows to change the linkage.

### 43.2 Optical Setup Editor

The Optical Setup Editor is the window for configuring the linkages and other simulation settings. The most essential parts of this window are the different tables for displaying the linkages between Optical Setup Ele-
ments. The main navigation in the Optical Setup Editor is done by the four buttons at the top of the window. By clicking the button Path, a table with all linkages is shown ( $\hookrightarrow$ Sec. 43.2.1) which define the execution order of the elements. All linkages which end at a detector can be listed by clicking the Detectors button ( $\hookrightarrow$ Sec. 43.2.2). The button Analyzers displays a list of all analyzers in the Optical Setup ( $\varsigma$ Sec. 43.2.3). There is an additional Logging button ( $\hookrightarrow$ Sec. 43.2.4), showing the single steps done during a simulation.

### 43.2.1 Path Table

The Path table in the Optical Setup Editor can be used for configuring the connections between Optical Setup Elements except for connections to detectors. (This handling is done by the Detectors table $\hookrightarrow$ Sec. 43.2.2.) Every row in the Path table represents one connection in the Optical Setup. Fig. 343 shows a typical example of the Path table.


Figure 343. The linkages between Optical Setup Elements are displayed in the Path table of the Optical Setup Editor.
The Path table is organized in three regions, differentiated by three different background colors. On the left side, all necessary information of the start element of a linkage is available. The middle part of the table enables the user to configure the end element of the linkages, while on the right side several linkage settings can be done.
The following columns are available:

| REGION | COLUMN | DESCRIPTION |
| :---: | :---: | :---: |
| Start Element | Index | The index of the start element of the linkage. |
|  | Element <br> Name | The name of the start element of the linkage. By double clicking on this cell, the settings of the selected Optical Setup Element can be edited. |
|  | Ref. Type | The type of the reference output coordinate system where the linkage starts. Typically (but not in every case), the transmission type $T$ and the reflection type $R$ are available. Sources have the reference output CS type "-" only. Several Ideal Components have specific reference output coordinate systems. ( $\hookrightarrow$ Part X.) |
|  | Medium ${ }^{\text {PE }}$ | The embedding medium behind the Optical Setup Element. It can be changed via double clicking in the specific cell ( $\hookrightarrow$ Sec. 37.3.1). |
| Target Element | Index | The index of the end element of the linkage. |
|  | Element <br> Name | The name of the end element of the linkage. By double clicking on this cell the settings of the selected Optical Setup Element can be edited. |
| Linkage | Propagation Method | The propagation method used for propagating through the free space between the start and the target element. If Classic Field Tracing is used and the propagation method is not None, you can open the edit dialog of the used propagation operator ( $\hookrightarrow$ Sec. 93) by double clicking on a cell in this column. |
|  | On/Off | By toggling the entry in the On/Off column, the linkage is turned on/off. If the linkage state is switched to off, it is not simulated when simulating the Optical Setup. |
|  | Color | The color of the arrow in the Optical Setup View. It can be changed by double clicking on the Color cell. |

> Important: Every Optical Setup Element has only one referring input coordinate system. So, a specific element can be set as end element of one single linkage only. Detectors are excluded from that rule, their position are handled as "virtual", so detectors can be end elements of more than one linkage (see Sec. 43.2 .2 for details).

In order to create a linkage, the start element has to be selected at first. This can be done by clicking in the column Index in the region Start Element. VirtualLab Fusion shows a list of all Optical Setup Elements which are available as start elements. After the user's selection VirtualLab Fusion inserts all other available information in the Start Element region automatically. To define the end element, the index of the end element has to be chosen by clicking in the column Index in the region Target Element. If Start and Target Element are configured, the link is created and drawn in the Optical Setup View.
Linkages can be deleted by selecting the corresponding row in the Path Table and pressing Del on the keyboard.

### 43.2.2 Detector Table

The Detectors table in the Optical Setup Editor is used for configuring the linkages from Optical Setup Elements to detectors. Fig. 344 shows the Detectors table of a sample Optical Setup.


Figure 344. The linkages between Optical Setup Elements and detectors are configured and listed in the Detectors table of the Optical Setup Editor.

In VirtualLab Fusion, Detectors are regarded as kind of "virtual". That means that the assignment of a detector does not cause any loss of energy in the further Optical Setup simulation. Detectors can also be set as end elements of more than one linkage. Thus they don't have a defined absolute position ( $\hookrightarrow$ Sec. 43.8).

Because Detectors can be configured as end elements of multiple linkages, the configuration of detector linkages is done in the Detectors table, containing the following columns:

| REGION | COLUMN | DESCRIPTION |
| :---: | :---: | :---: |
| Detector | Index | The index of the detector of the linkage. |
|  | Element <br> Name | The name of the detector to be linked. By double clicking a cell in this column, the settings of the selected detector can be edited. |
| Last Optical Setup Element | Index | The index of the start element of the linkage. |
|  | Element <br> Name | The name of the start element of the linkage. By double clicking a cell in this column, the settings of the selected Optical Setup Element can be edited. |
|  | Ref. Type | The name of the reference output coordinate system where the linkage starts. Typically (but not in every case), the transmission type $T$ and the reflection type $R$ are available. Sources have the reference output CS type "-" only. Several Ideal Components have specific reference output coordinate systems. ( $\hookrightarrow$ Part X.) |
|  | Medium | The embedding medium which is behind the Optical Setup Element. The medium cannot be changed in the Detectors table. This has to be done in the Path table or the element's edit dialog. |
| Linkage | Sum | Shall this linkage be simulated in summation mode? This mode is a special feature of detectors. By enabling the summation mode, the detector collects the input signals of all linkages where the summation is activated. Then the detector function is applied to the coherent addition of all incoming fields. |


| Propagation <br> Method | The propagation method to use for simulating the linkage. If Classic <br> Field Tracing is used and the propagation method is not None, you can <br> open the edit dialog of the used propagation operator ( $\lrcorner$ Sec. 93) by <br> double clicking on a cell in this column. |
| :--- | :--- |
| On/Off | By toggling the entry in the On/Off column, the linkage is turned on/off. <br> If the linkage state is switched to off, it is not simulated when running <br> the Optical Setup. |
| Color | The color of the arrow in the Optical Setup View. It can be changed by <br> double clicking on the Color cell. |

Important: If a detector is added to the Optical Setup via the Optical Setup View, a new row, filled with default values, is automatically inserted in the Detector Table. The user simply has to select the element which shall be the start element for the linkage to the detector. If a linkage is established, a new row is added to the detector section and can be configured for additional linkages to this detector.

Detector linkages can be deleted by selecting the corresponding row in the Detectors Table and press Del key on the keyboard. If all linkages to a detector are erased, an empty row will be displayed in the table. It can be used to set new linkages to the detector.

### 43.2.3 Analyzer Table

The Analyzers table contains a list of all analyzers in the current Optical Setup. Analyzers cannot be connected with other Optical Setup Elements. They are used for analyzing parts of the system or the whole system. More information about analyzers can be found in Part XII.
Fig. 345 shows the Analyzers table of a sample Optical Setup.


Figure 345. All analyzers included in the Optical Setup are listed in the Analyzers table.
The Analyzers table provides the following information:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Index | The index of the analyzer. Unlike the other tables in the Optical Setup Edi- <br> tor, the user cannot choose which analyzers shall be shown in the Analyzers <br> table; it always contains all analyzers in the Optical Setup. |
| Element Name | The name of the analyzer. By double clicking on this cell, the selected ana- <br> lyzer can be edited. |
| Comment | A short description of the function of the Analyzer. For detailed information <br> about available analyzers in VirtualLab Fusion please see Part XII. |

The Analyzers table is mainly for information about but not for editing of the Optical Setup. The user has only the possibility to edit the properties of the analyzer by double clicking in the Type column.

### 43.2.4 Process Logging

There is an additional Logging button in the top row of the Optical Setup Editor. It shows the single steps done during simulating the optical setup and thus helps you to identify problems within your setup. Fig. 346 shows an example.


Figure 346. Sample output of the process logging.

The actual logging panel has a context menu where you can

- Copy the currently selected text to the Windows ${ }^{\text {TM }}$ Clipboard,
- Select All logging information,
- delete all logging information using the Clear Logging item or
- Set Tab Width in pixels according to your liking

If you start a new simulation, the logging information is deleted so that the Logging only shows information about the most recent simulation run.
The detail level of the logging can be set in the Other Settings > System tab of the Profile Editor dialog $(\hookrightarrow$ Sec. (a)), in the Property Browser of the Optical Setup or in the side panel (see table below). The default level for new Optical Setups can be set in the Global Options ( $\hookrightarrow$ Sec. 6.1.4).
There is also a side panel with the following additional settings. Unless otherwise noted, the options are only available if there is no simulation in progress.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Suspend Logging | ONLY IF A SIMULATION IS RUNNING. <br> If you check this option, logging is suspended which means that no new mes- <br> sages are added until you uncheck this option again. This allows you to read <br> and search the current messages undisturbedly. |
| Search | ONLY IF THERE IS NO sIMULATION IN PROGRESS OR IF LOGGING IS suSPENDED. <br> Searches for the given word or word group. The matching is case insensitive. <br> Clicking on $\rightarrow$ marks the (next) occurrence of the entered word group. |
| Hide Time Stamps | Each message in the logging starts with the exact time when this message <br> was created. While this allows performance analysis, it can make reading and <br> comparing different loggings more complicated. Thus you can hide these time <br> stamps with this option. |
| \{Logging Level\} | Defines how much details you want to see during logging - or whether you <br> want to completely disable logging. |

### 43.3 Optical Setup Ribbon

The Profile Editing \& Run group can be used to perform and configure the simulation of the active optical setup. For the configuration of the simulation settings VirtualLab Fusion provides a variety of tools which are also available in the Profile Editing \& Run ribbon group.
The ribbon has the following main categories:

- Execution: In this section you can select the modeling profile you like to process. VirtualLab Fusion has two build-in modeling profiles: Ray Results Profile and the General Profile. VirtualLab Fusion performs in all modeling profiles physical optics simulation. The Ray Results Profile allow the access to results the user knows from typical ray tracing software. There are several limitations of the Ray Results Profile, which are explained in more detail in Sec. 43.4.3. In addition to the selection, which modeling profile shall be used, the user can start a simulation by clicking on the Go! button. If a simulation is running the Go! button will become a Stop button, which enables the cancellation of a running simulation.
- Settings: In the Settings section VirtualLab Fusion provides a set of tools to configure the underlying optical setup. The center of the modeling configuration is the Profile Editor. It enable the configuration of modeling and geometry parameters in a systematic and structured way. Detailed information on the Profile Editor can be found in Sec. 43.4.1. Next to the profile editor VirtualLab Fusion also offers the Parameter Overview, which enable the access of all numerical parameters of the underlying system in table format ( $\varsigma$ Sec. 43.6.1). The last entry in the category Settings is the tool for parameter coupling. This tool enables the user of VirtualLab Fusion to define parameter dependencies. A detailed explanation of Parameter Coupling can be found it Sec. 43.10. By clicking on Use Parameter Coupling the parameter coupling is activated. The parameter coupling can be edited by clicking on the gear symbol next to the User Parameter Coupling button.
- Result Visualization: In this section the user needs to select the result visualization type. Depending on the profile different type are available. If the user select the Ray Results Profile he can select whether to use System: 3D or Detectors as result output. In case the user selects the General Profile can define to use Detectors or the Modeling Analyzer as the result visualization output. The result visualization can be configured alternatively in the Profile Editor. Details on the Result Visualization can be found in Sec. (a).
- Light Path Finder: VirtualLab Fusion provides several options to determine which paths the light will go
through the configured optical setup. These path are determined by the Light Path Finder. A more detailed discussion of the options of the Light Path Finder can be found in Sec. 43.3.1.
- Profile Editing Tools: In this section the user can find a variety of tools for a user-friendly configuration of modeling parameters. The tools are described in more detail in Sec. 43.3.2.
- Parameter Variation: In the section Parameter Variation the user triggers the generation of New Parameter Run documents, New Parametric Optimization documents or select to perform a system optimization using optiSlang. The starting point for all these parameter variation documents is always the active system. You can find detailed information for the New Parameter Run in Sec. 44. For the Parametric Optimization please check Sec. 102. The optimization using optiSlang is described in detail within Sec. 124.1.1.
- View: By clicking on the button View System in the section View the user can trigger VirtualLab Fusion to generate a 3D view of the underlying optical setup within a dialog. This can be used for visualization and as a check of the system geometry configuration.

Fig. 347 shows the Profile Editing \& Run, which is visible if the active document is an optical setup.


Figure 347. The Profile Editing \& Go! which enable the user to perform the simulation, select the modeling profile and it parameters and enable a set of tools for a user-friendly configuration of system parameters.

### 43.3.1 Light Path Finder

One major tool to perform optical simulations is the Light Path Finder. It enables the evaluation of the paths that light will go through the optical setup. In general we differ between two general configurations: Pre-Selected and Manual Channel Configuration. In practice this means that for Pre-Selected configuration the surface channels of the components are defined by VirtualLab Fusion directly and the user can not change the detailed channel configuration. In case Manual channel configuration is selected, the user has the option to define at each surface in each component, which channels should be active.
The section Light Path Finder in the Profile Editing \& Go! enable the selection of the channel configuration and the corresponding detail settings.
Fig. 348 shows section Light Path Finder in the Profile Editing \& Go!.

```
    \(\stackrel{\square}{4}\)
    Pre-Selected
Configuration *
Light Path Finder
```

Figure 348. The ribbon entries to select the channel configuration and to edit the detailed parameters within the section Light Path Finder.

In the ribbon section the user can directly switch between Pre-Selected Configuration and Manual Configuration. In addition he can click on the small gear button to open the edit dialog for the detailed specification of the Light Path Finder.

Fig. 349 show edit dialog to configure the parameter of the Light Path Finder.


Figure 349. The edit dialog to configure the parameters of the Light Path Finder.

The following settings can be done within the edit dialog of the Light Path Finder:
ITEM DESCRIPTION

Channel Configuration The user can select the channel configuration. The user can select between Option

Settings for Manual Channel Configuration Manual and Pre-Selected channel configuration. In case of Manual channel configuration the user can specify several advanced options for the Light Path Finder in the group Settings for Manual Channel Configuration.
If the user selects Manual channel configuration, several advanced configuration options can be configured. These settings are available in the section Settings for Manual Channel Configuration. The detailed explanation of these settings can be found below.

The following advanced configuration options for Manual channel configuration are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Energy Threshold | In Manual channel configuration the light path finder evaluated all paths <br> through the optical setup according to the manually configured channel con- <br> figuration. The Energy Threshold is used to define which path shall be <br> aborted. VirtualLab Fusion evaluates the energy which should be traced. <br> If it is below the specified threshold the path will not followed further. |
| Maximum Level | Additionally to the Energy Threshold there is another criteria to stop a light <br> path if a certain level is reached. Each interaction with a surface will increase <br> the current level. If the level is larger the the Maximum Level the light path <br> will not be followed further. |
| Channel Resolution Accu- | If light hits a surface, which contains surface regions, VirtualLab Fusion will <br> check which regions are hit. Therefore the user can define the Channel Res- <br> racy |
| olution Accuracy. In case a surface region is not resolved by the light path <br> finder, you need to increase the Channel Resolution Accuracy. |  |
| Show Only Paths That Hit | To enable the user more insides of the light path finder result, the option Show <br> Only Paths That Hit a Detector in $3 D$ View can be deactivated. |

### 43.3.2 Profile Editing Tools

Within the ribbon section Profile Editing Tools VirtualLab Fusion provides several tools which enable a userfriendly configuration of modeling and geometry parameters within the active optical setup.
Fig. 350 show the ribbon section Profile Editing Tools within Profile Editing \& Go!.


Figure 350. The ribbon section to access the Profile Editing Tools within the Profile Editing \& Go!.
The following tools for the configuration and analysis of the parameters of the underlying optical setup are available in this section

| ITEM | DESCRIPTION |
| :--- | :--- |
| Source to Component | The tool Source to Component has two general functions: (1) Analysis of |
| the current settings for the propagation settings from source to components |  |
|  | and (2) Fast access to configure/synchronize the settings for the propagation |
| from source to components. If case the user configured the propagation to be |  |
|  | pointwise the caption of the button will be changed to Source to Component: |
|  | Pointwise and the corresponding icon is adapted to visualize the pointwise |
|  | setting. In case the optical system is configured to select the Fourier trans- |
|  | forms automatically for the propagation from the source to the components |
| the caption of the ribbon button will be changed to Source to Component: |  |
|  | Automatic and the icon is adapted to mark the automatic settings. There |
|  | might be also settings which are not pointwise and not automatic but some |
| intermediate setting. In Addition it is possible that the settings for different |  |
| components is different. In these cases the icon will be also adapted and the |  |
| caption will be Source to Component: State = N/A. |  |



Figure 351. The different states of the ribbon buttons to analyze the settings for propagation from source to components. The propagation between components and to detector follow the same logic.

It shall be mentioned at this point, that the settings for free space propagation (and also geometry) can be configured per component/detector. The Profile Editing Tools enables an alternative way for a fast configuration and analysis of these parameters.

### 43.3.2.1 Profile Editing Tool: Paraxial Assumptions

With the profile editing tool Paraxial Assumptions the user gets a fast access to the parameters for paraxial assumptions for field component evaluation within all Universal Detectors within your optical setup. In addition to the option for synchronizing the settings for all Universal Detectors, the edit dialog of the Paraxial Assumptions tool provides an analysis of the actual settings of these parameters for all Universal Detectors within the optical setup.


Figure 352. The edit dialog of the profile editing tool Paraxial Assumptions.
Fig. 352 shows the edit dialog to configure and analyze the settings for Paraxial Assumptions. On the right side of the dialog the user can make the definition of the parameters he likes to be configured by the Paraxial Assumption profile editing tool. The group box on the left side is used to get an overview of the current parameter configuration within the underlying system (which can be configured inside this tool). The user can see here whether the setting is currently set to all (identified by the green bubble in the All column), none (identified by the red bubble in the None column) or some elements (the yellow bubble in the Some column). Some means that for different detectors different settings are currently configured.
The following parameters can be done by the Paraxial Assumptions tool:
ITEM
DESCRIPTION
Apply Paraxial Approximation (Transversal Field Components Only)

The Universal Detector allows to use paraxial approximations for the calculation of field components at its input. This will easy up the calculation of the field components (Ez, Hx, Hy and Hz ) because no additional Fourier transforms will be use for their calculation, but simplified formulas. This will speed up your simulation.

After the configuration of the desired parameters the Paraxial Assumptions tool can be applied by clicking on the Apply button at the bottom of the dialog or by clicking on the OK button. By clicking on Apply the tool is applied, the dialog will be kept open and the actual settings will be analyzed again and the corresponding status is displayed on the right side of the dialog. By clicking on OK the dialog will be closed and the tool will be applied.

### 43.3.2.2 Profile Editing Tool: Speed vs. Accuracy

The configuration of several parameters which affect the accuracy and speed behavior of the free space propagation the user can make several settings per component/detector. As an alternative he can also use the profile editing tool Speed vs. Accuracy to define some selected parameter and trigger their setting for all components and detectors at once.
The Speed vs. Accuracy tool has again two main sections: (1) on the right side the user can specify the parameters for the tool before it is applied and (2) on the left side we provide the analysis of the actual settings analyzed from the underlying system.


Figure 353. The edit dialog of the profile editing tool Speed vs. Accuracy.
The edit dialog of the tool is shown in Fig. 353 and provides the following parameters to configure:

## ITEM

DESCRIPTION

Accuracy Level Nyquist Period Evaluation

For the conversion of gridless to gridded data format VirtualLab Fusion will apply an automatic sampling algorithm which internally determines the bandwidth of field. For the sampling estimation algorithm the user can configure the Accuracy Level Nyquist Period Evaluation. Detailed information can be found in Sec. 43.4.2.2. The analysis tool on the right side will show you the current setting of the accuracy level for all components. If there is a nonunique specification of the accuracy level we will show the information about the range of the accuracy levels configured within your system.
Gridless Sampling Factor The number of gridless samples to used within the simulation can be controlled by the Gridless Sampling Factor. The higher the factor the more points will be used. Detailed information on gridless sampling can be found in Sec. 43.4.2.3. The analysis tool in the right side shows again the range of Gridless Sampling Factor values for all components and detectors within your system. In case a unique setting is used for all elements the value for it will be displayed.

Enforce Pointwise Fourier Transform Beyond XXXX² Sampling Values

To ensure that the numerical effort is not to high to perform an integral Fourier transform, the user can activate the option Enforce Pointwise Fourier Transform Beyond $X X X X^{2}$ Sampling Values. If the numerical effort during the simulation for an integral Fourier transform is higher than the limit and the user activated this option VirtualLab Fusion will automatically use a pointwise Fourier transform instead of the integral one. For further details you can check Sec. 43.4.2.1.
Limit Gridded Sampling to Maximum of $\mathrm{XXXX}^{2}$ Sampling Values

For automatic sampling estimation VirtualLab Fusion can be configured to use not more than $x x x x^{2}$ sampling points. This option can be used for the activation and configuration of this option. Additional details can be found in Sec. 43.4.2.2.

After the configuration of the desired parameters the Speed vs. Accuracy tool can be applied by clicking on the Apply button at the bottom of the dialog or by clicking on the OK button. By clicking on Apply the tool is applied, the dialog will be kept open and the actual settings will be analyzed again and the corresponding status is displayed on the right side of the dialog. By clicking on OK the dialog will be closed and the tool will be applied.

### 43.3.2.3 Profile Editing Tool: Pointwise vs. Integral

The profile editing tool Pointwise vs. Integral can be used to configure the the Fourier transform selection for all components/detectors within your optical setup simultaneous. These settings can be also done individually per component or detector, but in case the user likes to define a synchronized configuration the Pointwise vs. Integral can be used in a user-friendly way.
Fig. 354 shows the edit dialog of the Pointwise vs. Integral tool.


Figure 354. The edit dialog of the profile editing tool Pointwise vs. Integral.
On the top of the dialog the user can select the selection mode for the Fourier transforms. The following selection modes are available

| ITEM | DESCRIPTION |
| :--- | :--- |
| Individual | In Individual mode the settings can be defined directly in the matrix on the <br> central part of the dialog. The user can select between Pointwise, Integral <br> and Automatic Selection for all combinations between source, components <br> and detectors. |
| All Pointwise | If All Pointwise is selected as selection mode, the controls for the configu- <br> ration of the detailed Fourier transform are deactivated and set to be in all <br> combinations to Pointwise. |
| All Automatic | If All Automatic is selected as selection mode, the controls for the configu- <br> ration of the detailed Fourier transform are deactivated and set to be in all <br> combinations to Automatic Selection. |
| All Integral | If All Integral is selected as selection mode, the controls for the configuration <br> of the detailed Fourier transform are deactivated and set to be in all combi- <br> nations to Integral. |

In case the user selected Individual selection mode the control in the center of the dialog are editable. The configuration of the Fourier transforms can be done for

- From Source To Component
- From Source To Detector
- From Component To Component
- From Component To Detector
- Inside Component

For each of these scenarios the user can select between

| ITEM | DESCRIPTION |
| :--- | :--- |
| Pointwise | If the user select Pointwise only the pointwise Fourier transform (PFT) will be <br> used for forward and inverse Fourier transform. There will be no selection <br> between different Fourier transforms. |
| Integral | In case the user defines Integral, VirtualLab Fusion will configure for the sce- <br> nario (source/component/detector) to use for Fourier selection only to use <br> fast Fourier transform (FFT) or semi-analytical Fourier transform (SFT). The <br> pointwise Fourier transform will be not be used as an option for the free space <br> propagation. |
| Automatic Selection | By selecting Automatic Selection the free space propagation will be config- <br> ured to select freely between PFT, FFT or SFT. The selection is based on an <br> automatic algorithm based on mathematical decision criteria. |

After the configuration of the desired parameters the Pointwise vs. Integral tool can be applied by clicking on the Apply button at the bottom of the dialog or by clicking on the OK button. By clicking on Apply the tool is applied and the dialog will be kept open. By clicking on OK the dialog will be closed and the tool will be applied.

### 43.4 Propagating Through an Optical Setup

VirtualLab Fusion enables the simulation of optical systems by physical optics. By default an optical system comes with two modeling profiles: Ray Results Profile and General. The Ray Results Profile has several limitations and can be used to generate typical results the user are used to if they use traditional ray tracing software. The limitation of the Ray Result Profile are described in Sec. 43.4.3. Within the General Profile there are no limitations regarding the specification of the freespace propagation parameters (especially the selection of Fourier transform to be used). For the profile the user needs to select the result visualization to be used. For the Ray Results Profile can select whether he like to evaluate the information as System: 3D output or as Detectors output. For the System: 3D result the user can specify the sampling for gridless points as well as view options for the 3D result visualization. Detailed information about its configuration can be found in Sec. 43.4.5. In case of Detectors output within the Ray Results Profile the user need also to specify the sampling for gridless data and some selected view properties for the detector outputs.
For the General Profile the user can select between Detectors output and Modeling Analyzer. In case of Detectors the visualization/evaluation options are configured directly in the detectors within the underlying optical setup. The Modeling Analyzer offers the user the access to intermediate field information within the system simulation. Detailed information about the Modeling Analyzer can be found in Sec. 43.4.6.
In general the parameters for propagation through the optical setup can be made via the edit dialogs of the different elements (components, detector, ect.) within your optical system. Alternatively, we provide also an options to edit the parameter in a more organized form via the Profile Editor. The graphical user interface of the profile editor is described on Sec. 43.4.1
In addition to the innovative concept of modeling profiles we provide also the simulation of optical systems by Classic Field Tracing which is the first version of our implementation to do physical optics. The Classic Field Tracing is already working good for paraxial optical setups. In addition every Analyzer can be used as Simulation Engine because Analyzers process Optical Setups in their own special way.


Figure 355. Starting a simulation from the Optical Setup Editor. By selecting the Simulation Engine the user specifies how the source field should be traced through the complete Optical Setup, or whether only a certain analyzer shall be evaluated.

In the bottom-right corner of the Optical Setup Editor ( $\hookrightarrow$ Fig. 355) you can choose which Simulation Engine is to be used and start a new simulation.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Simulation Engine | The Simulation Engine (or Analyzer) to be used. The selected Simulation En- <br>  <br>  <br>  <br> gine also influences the available settings in the edit dialogs of Components <br> $(\hookrightarrow$ Sec. 54$)$, Ideal Components ( $\hookrightarrow$ Sec. 66), and Detectors ( $\hookrightarrow$ Sec. 74.1). |
| Go! | Starts the simulation of the Optical Setup. Shortcut F5. <br>  <br>  <br>  <br>  <br>  <br> During a simulation the Go! button turns into a Stop button to stop the <br> simulation. Shortcut Shift + F5.. |

For the modeling profiles there are several tools available which analyze the underlying configuration (on the fly or on demand) and that can be used to realize a fast reconfiguration of the modeling settings. Detailed information can be found in Sec. 43.3.

### 43.4.1 Profile Editor

The Profile Editor can be used to configure the optical setup in an alternative way. In former versions it was only possible to edit most of the configuration parameter (structural parameters as well as modeling parameters) via the edit dialogs of the sources/components/detectors within the optical setup. With the Profile Editor the configuration of all important parameter is provided in a more structured way.
The dialog of the Profile Editor is separated in four main sections:

- Source: The Sources section of the dialog contain all parameters regarding the active light source. For a detailed explanation please check Sec. 43.4.1.2.
- Components \& Solvers: In the section Components \& Solvers you may find all parameters for (real and ideal) component that are connected to the active light source within the underlying system. Detailed information can be found in Sec. 43.4.1.3.
- Visualization \& Detectors: Under Visualization \& Detectors you can find the parameters for detectors and also for the visualization type that shall be used for evaluation. A detailed description of the parameters to configured can be found in Sec. 43.4.1.4.
- Other Settings: Finally a collection of all other important parameters can be found under Other Settings. These settings are explained in detail in Sec. 43.4.1.5.

Fig. 356 shows the edit dialog of the Profile Editor.


Figure 356. Dialog of the Profile Editor.
For the configuration of parameters we use some standard techniques. These common techniques are explained in the next sections. Afterward the detailed configuration options for the different section of the Profile Editor are explained in detail.

### 43.4.1.1 Profile Editor: Common User Controls

For the specification of parameters and their configuration options we support different standard techniques, which shall be explained next. The following user interface concepts will be discussed in detail

- Parameter Overview Tables: Is a table which provides an overview of all numerical parameters of the connected elements within the underlying optical system.
- Table Layout/Tree View: VirtualLab Fusion provides a innovative concept to show for selected parameters (e.g. Fourier Transforms for Free Space Propagation. The configuration is done also via different types of controls. Detailed information can be found in Sec. (b).
- Master-Client-Individual (MCI) Configuration: The configuration of parameters could be quite complex. So VirtualLab Fusion supports the selection of a master configuration, which can be use to serve other configuration that are configured as Client. A detailed discussion on the MCl concept can be found in Sec. (c).


## (a) Parameter Overview Tables

One universal user interface concept that is used within the Profile Editor are the Parameter Overview Tables. Fig. 357 shows such a table for the configuration of parameters for Components and Solvers.

| Filter by... |  |  | $\times$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $12 \cdot$ | Object | Category | Parameter | Value | $\wedge$ |
| - | 'Zernike \& Seidel Aberrations" (\# 1) | Basal Positioning (Relative) | Distance Before | 0 mm |  |
|  |  |  | Lateral Shift X | 0 mm |  |
|  |  |  | Lateral Shift Y | 0 mm |  |
|  |  |  | Spherical Angle Theta | $0^{\circ}$ |  |
|  |  |  | Spherical Angle Phi | $0^{\circ}$ |  |
|  |  |  | Angle Zeta | $0^{\circ}$ |  |
|  |  |  | Initial Number of Gridless Sampling Values | 1100 |  |
|  |  |  | Control Factor of Gridless Sampling Values | 1 |  |
|  |  |  | Accuracy Nyquist Period Evaluation | 0 |  |
|  |  | Free Space Propagation (Profile Physical Optics) | Oversampling Factor Gridded Data | 1 |  |
|  |  |  | PFT Selection Accuracy Level | 0 |  |
|  |  |  | Sampling Limit to Enforce Pointwise Fourier Transfor... | 10000 |  |
|  |  |  | Threshold for Semi-Analytical Fourier Transform | 2 |  |
| $G$ |  |  | Diameter X | $250 \mu \mathrm{~m}$ |  |
|  |  | Aperture | Diameter Y | $250 \mu \mathrm{~m}$ |  |
|  |  |  | Relative Edge Width | 10\% |  |
|  |  |  | Accuracy Factor | 1 |  |
|  |  |  | Piston | 0 |  |
|  |  |  | Tilt Y | 0 |  |
|  |  |  | Tilt X | 0 |  |
|  |  |  | Astigmatism Y | 0 |  |
|  |  |  | Defocus | 0 |  |
|  |  |  | Astigmatism X | 0 |  |
|  |  |  | Trefoil Y | 0 |  |
|  |  |  | Coma Y | 0 |  |
|  |  |  | Coma X | 0 |  |
|  |  |  | Trefoil X | 0 | $\checkmark$ |

Figure 357. A typical Parameter Overview Table used for the showing all parameters of the components in the underlying optical system.

This tables display all numerical parameters of the sources/components/detectors and allow its modification directly in the table. The table has the following columns:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Object | In this column you will find the name of the source/component/detector for <br> which the parameters are given. There are typically more than one parameter <br> per element, so the cells are merged together for a better graphical overview. <br> By double clicking in the cell within the Object column the edit dialog of the <br> element will be opened and the parameters can also entered in the edit dialog <br> instead of the Parameter Overview Table. |
| Category | Due to the complexity of parameters within a single optical setup, the pa- <br> rameters are categorized. This categorization is done on one hierarchy level <br> only. |
| In the column Parameter the name of the parameter is listed. By that you can |  |
| identify the parameter you like to modify or investigate. |  |

Due to the fact that such overview lists can be quite long, VirtualLab Fusion offers a user friendly way to apply a filter on the table. By entering a string value into the Filter by ... text box a full text search in the table will be applied on the table (full text search on all but not the entries in the Value column).

## (b) Table Layout/Tree View

The Parameter Overview Tables enable the systematic display and modification of all numerical parameters within the optical systems. For important parameter sets VirtualLab Fusion provides an alternative approach to
configure them using the Table Layout／Tree View．Fig． 358 shows a sample for Table Layout／Tree View．Here the Table Layout configuration is selected，which is the standard when you open the Profile Editor the first time．

| Filter Controls by．．． |  | $\times$ | 囲 | － |
| :---: | :---: | :---: | :---: | :---: |
| Component | Settings |  |  |  |
| ＂Single Phase Dislocation＂（\＃2） | $\begin{array}{lll} \bigcirc & \bigcirc & O \\ M & C & 1 \end{array}$ | Automatic Sampling <br> Manual Sampling <br> Accuracy Level of Nyquist Period Evaluation <br> Power Portion for Field Size Estimation <br> Oversampling Factor with Respect to Nyquist Period <br> Limit Gridded Sampling to Maximum of Sampling Points | $\square$ <br> 99．9999 \％ <br> 1 <br> 1000 |  |
| ＇Zernike Seidel Aberrations＂（\＃3） | $\begin{array}{lll} \bigcirc & O \\ M & C & 1 \end{array}$ | Automatic Sampling <br> Accuracy Level of Nyquist Period Evaluation <br> Power Portion for Field Size Estimation <br> Oversampling Factor with Respect to Nyquist Period $\square$ Limit Gridded Sampling to Maximum of Sampling Points | $0 \div$ <br> $99.9999 \%$$\square$ <br> 1000 |  |

Figure 358．A sample Table Layout．In this example the parameters for Sampling Gridded Data within the Free Space Propagation parameters for Component are displayed

The Table Layout／Tree View contains a list of controls for specific settings．Each source（mode）／component／de－ tector comes with a set of parameters that can be configured within the corresponding control．The list of controls can be visualized in a Table Layout or as a Tree View．
Within the Table Layout VirtualLab Fusion generates a table with the following columns

| ITEM | DESCRIPTION |
| :--- | :--- |
| Source／Component／De－ <br> tector | In the first column you can find the name of the element（source／component <br> or detector）which provides the data set．By double clicking on the cell within <br> the first column the edit dialog of the element is opened and the user can <br> alternatively configure the parameters directly in the edit dialog．After closing <br> the edit dialog with Ok the parameters in the Profile Editor will be updated． |
| Settings | In the column Settings VirtualLab Fusion will place the control that is used for <br> configuration the corresponding parameter set．This control is quite different <br> for different parameter sets and explained in the later paragraphs when we <br> discuss their concrete usage within the Profile Editor． |

Alternatively to the Table Layout the user can switch to the Tree View mode．Fig． 359 shows a sample Tree View in which also the buttons are marked to switch between the view modes．

| Filter Controls by．．． |  | $\times$ | 囲 | 哑 |
| :---: | :---: | :---: | :---: | :---: |
| Component | Settings |  |  |  |
| ＊Single Phase Dislocation Zernike \＆Seidel Aberratic | $\begin{array}{lll} \bigcirc & \bigcirc & O \\ M & C & 1 \end{array}$ | O Automatic Sampling O Manual Sampling |  |  |
|  |  | Accuracy Level of Nyquist Period Evaluation | $0 \div$ |  |
|  |  | Power Portion for Field Size Estimation | 99．9999\％ |  |
|  |  | Oversampling Factor with Respect to Nyquist Period | 1 |  |
| －＞ |  | $\square$ Limit Gridded Sampling to Maximum of Sampling Points | 1000 |  |

Figure 359．A sample Tree View visualization．In this example the parameters for Sampling Gridded Data within the Free Space Propagation parameters for Component are displayed

In comparison to the Table Layout the controls are not arranged in a table, but the user can navigate through the settings of different elements by selecting the element of interest in the tree view on the left side of the component. If you double clicks on the entry within the tree on the left side, the edit dialog of the selected element will be opened and the configuration of all parameters of the element can be done this dialog.
To get a better overview for a specific parameter VirtualLab Fusion supports also the filtering of parameters. Therefore the user has to enter the filter string in the text box above the Table Layout/Tree View. After entering the the filter string VirtualLab Fusion will check, which parameter matches with the filter. The graphical user interface is adapted completely automatically. By that you can get a good overview of parameters in the system which you like to check in detail.
Fig. 360 shows a the resulting user interface after applying the filter mechanism on a sample Table Layout view.


Figure 360. A sample Table Layout visualization after filtering. In this example the parameters for Fourier Transform selection within the Free Space Propagation parameters for Component are displayed

## (c) Master-Client-Individual (MCI) Configuration

VirtualLab Fusion supports the use of a so-called Master-Client-Individual (MCI) configuration. This enables the user to select one parameter set (e.g. Sampling Gridless Data for Free Space Propagation parameters of Components) to serve as Master. If a parameter set in the same group is defined as Client it will automatically take over the parameter configuration of the Master. In each parameter set the user can select only one Master. Alternatively to the master and client selection the user can also specify that the parameter set should be configured Individually. In this case changing the Master will have no effect on the parameter set. In case that no Master is selected all settings will be handled as Individual.
Fig. 361 shows a Table Layout view in which the MCI configuration is marked by a red rectangle.


Figure 361. Table Layout view in which the selection of Master-Client-Individual (MCI) is marked.

### 43.4.1.2 Profile Editor: Sources

In the Sources section of the Profile Editor the user can find all important setting of the active source. On this tab page three sub pages are available:

- Parameter Overview: Here the user can access the all numerical parameters of the active source in a Parameter Overview Table. The user can filter the parameters he like to see. A detailed explanation of the Parameter Overview Table can be found in Sec. (a).
- Position \& Size: On this page of the Profile Editor we offer you a Table Layout/Tree View control, which contains parameters for position and size of the active sources. The parameters which can be entered here are explained below. In case a Multiple Source is active in the underlying system you will get an entry per source within the Multiple Source.
- Power Management: Here the user can define the parameters which are used for the power management of the source. The user can activate the Power Management and specify the power of the source that shall be used for the configuration. If the Power Management is not activated VirtualLab Fusion will normalize the amplitudes of the scattered fields of the active light source. In addition, the user has to specify the type of the spectrum which is used.

Fig. 362 shows the Position \& Size page for Sources within the Profile Editor.


Figure 362. The Position \& Size page for Sources. In this example the active light source is a Spherical Wave, so the Table Layout/Tree View only contains one parameter set.

The control to configure the Position \& Size parameters of a light source have the following parameters that can be configured by the user

| ITEM | DESCRIPTION |
| :---: | :---: |
| Distance to Input Plane | This value describes the distance between input plane and source plane along the $z$-axis: distance $=z_{\text {Input Plane }}-z_{\text {Source Plane }}$. <br> For some of the sources this value is fixed to zero. <br> In the case of spherical and quadratic waves this value must not be zero and the spherical phase radius is set to this value. |
| Lateral Offset | This value describes the offset between the origins of the coordinates for the source and the input plane. |
| Apply Lateral Offset to Source Field | By default, the resulting input field is centered at the position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ) in the input plane. By checking this box, the field is shifted by the Lateral Offset of the source plane ( $\leftrightarrows$ Sec. 48.2.1.1). Note, the resulting numerical array (sampled field) will still be centered at ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ), so additional zero-values will be generated. An example is given in Fig. 458 and Fig. 459. |
| Shape | You can choose whether the single modes have a Rectangular or an Elliptical shape. |
| Field Size | The size or diameter of the aperture. If the light source determines the aperture size automatically, this control is disabled. |
| Relative Edge Width | The width of the smoothing edges defined relatively to the lateral extension of the mode. If the extension in $x$ - and $y$-direction differ, the minimum of both values is taken. |
| Absolute Edge Width | The width of the smoothing edges in meters ( $\rightarrow$ Fig. 454). If the light source determines the aperture size automatically, this control is disabled. |

The Position \& Size parameters of light sources is discussed in Sec. 48.2.1.2 in more detail.
Fig. 363 show the parameter that can be configured on the tab page Power Management.


Figure 363. The Power Management page for Sources.

In the section Power Management the user can define the following parameters to configure the power of the active source:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Type of Spectrum | For the power management is done by calculation of the initial power of the <br> source, calculating a corresponding scaling factor and then adding this scal- <br> ing factor automatically into the light source. For this calculation the user <br> need to specify whether the spectrum in use is Discrete or Continuous. This <br> information is then used to calculate the integrated power over all wavelength <br> emitted by the source. |
| Activate Power Manage- | The user can activate or deactivate the power management. In case the <br> ment <br>  <br>  <br>  <br>  <br>  <br> Power Management is not activated, VirtualLab Fusion will generate the <br> source fields with normalized amplitude (which is the same flow as done in <br> previous versions). If the Power Management option is checked, VirtualLab <br> Fusion will analyze the source field before simulation, calculate a scaling fac- <br> tor by measuring the power of the normalized output field of the source and |
| apply the evaluated scaling factor within the following simulation to the source |  |
| field. Within the process logging the information about the Power Manage- |  |
| ment evaluation can be checked by the user. |  |

### 43.4.1.3 Profile Editor: Components \& Solvers

In the section Components \& Solvers all important parameters for ideal component and real components can be accessed. This section has the following tab pages in which different parameters are accessible.

- Parameter Overview: On this tab page the user can access all numerical parameters of the connected components within the underlying optical system. More information can be found in Sec. (a).
- Solver \& Functions: Each real component has an associated solver and for each ideal component comes with an associated function. On the tab page Solver \& Functions you can access the parameters for these solvers/functions. The numerical parameters of the solver/functions are communicated by a Parameter Overview Table (details can found in Sec. (a)).
- Free Space Propagation: Next to the parameters for the solvers/functions it is important to define the parameter to propagate to components through free space. These parameters are available in the page

Free Space Propagation. Sec. (b) contains a detail explanation of control to configure the free space propagation parameters.

- Channel Configuration: Within the section Channel Configuration the user gets an overview of the current surface channel settings for all components within the system. Detailed information of the controls to specify the Channel Configuration can be found in Sec. (c).

Fig. 364 shows the Component \& Solver which is accessible in the Profile Editor.


Figure 364. The Component \& Solver section of the Profile Editor.

## (a) Parameter Overview

For the display of all numerical parameters of the components within the underlying system a Parameter Overview Table is used. Detailed information on the common user interface of Parameter Overview Table can be found in Sec. (a).
Fig. 365 shows Parameter Overview tab for components within the Profile Editor.


Figure 365. The Parameter Overview of the Component \& Solver section within the Profile Editor.

In general the table list all numerical parameters for the components of the underlying optical setup. But by activating the check box Hide Modeling Parameters all modeling parameters are not included in the listing. The modeling parameters are parameters of the solver/function and parameters of the free space propagation. These parameters can be accessed in the section Solver \& Functions and Free Space Propagation in the Components \& Solvers section.

## (b) Free Space Propagation

Within this section of the Profile Editor the user can configure all parameters that are important to be used within the free space propagation from source to component, from component to component or inside components (in case that a component contains several surfaces).
Fig. 366 shows the control to configure the Free Space Propagation parameters for components.


Figure 366. The section to configure the Free Space Propagation parameters for components within the Profile Editor.
For the communication of the Free Space Propagation parameters the parameters are displayed within several Table Layout/Tree View are used. Detailed information on this common user interface can be found in Sec. (b). The section within the dialog contains a tab page for

- Fourier Transform: The controls for specification are described in Sec. 43.4.2.1.
- Sampling Gridded Data: Details on the user controls for the configuration of gridded data can be found in Sec. 43.4.2.2.
- Sampling Gridless Data: In Sec. 43.4.2.3 the controls for the configuration of gridless data are explain in detail.


## (c) Channel Configuration

In the section Channel Configuration the user can get an overview of the current surface channel settings. This configuration is done via a compact table, which has the following entries:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Name | The name of the component (including the index of the component). |
| Surface | The name of the surface within the component. If more than one surface is <br> present in one component, an additional line will be available to configure all <br> channels for the component at once to be active or inactive. |
| $\boldsymbol{+ / +}$ | Defines whether the plus-plus channel is active/open. |
| $\boldsymbol{+ / -}$ | Defines whether the plus-minus channel is active/open. |
| $\boldsymbol{- / -}$ | Defines whether the minus-minus channel is active/open. |
| $-/+$ | Defines whether the minus-plus channel is active/open. |

Fig. 367 shows the control to configure the Channel Configuration for all components of the underlying optical setup.

| Name | Surface | +/+ | +/- | \% | -/+ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| "Single Phase Dislocation" (\# 2) | Surface \# 1 (Single Phase Dislocation) | $\checkmark$ | $\square$ | $\square$ | $\square$ |
| "Zernike \& Seidel Aberrations" (\# 3) | Surface \#1 (Zernike \& Seidel Aberrations) | $\square$ | $\square$ | $\square$ | $\square$ |
| "Spherical Lens" (\# 6) | All Surfaces ('Spherical Lens* (\# 6)) | $\square$ | 回 | $\square$ | $\square$ |
|  | Surface \#1 (Plane Surface) | $\square$ | $\square$ | $\square$ | $\square$ |
|  | Surface \#2 (Conical Surface) | $\square$ | $\square$ | $\square$ | $\square$ |

Figure 367. The section to configure the Channel Configuration for components within the Profile Editor.

The Channel Configuration is read-only if the Channel Configuration Option is set to Pre-Selected. In case of Manual Channel Configuration the user can select freely which channels should be open or closed for automatic analysis the light propagation through the optical setup.

### 43.4.1.4 Profile Editor: Visualization \& Detectors

Within the section Visualization \& Detectors the user can find all settings which are accessible for detectors and general result visualization. This section has the following tab pages in which different parameters are accessible.

- Result Visualization: On this tab page the user can select the result visualization type. Depending on the selected result visualization different tab pages will be available within the section Visualization \& Detectors. A detailed information on the Result Visualization section can be found in Sec. (a).
- 3D View: This tab page is only available if the user selects System: 3D as Result Visualization. On this tab page the user can configure the number of points that shall be used for processing and also pre-configure the 3D system view. More information see in Sec. (b).
- Detector Setting: If the user selects Detectors as Result Visualization type he can use the controls within this section to specify the parameters of the detectors within the optical setup. The configuration can be done per detector. In Sec. (c) you can find a detailed description of the controls to define the parameters for the detectors.
- Modeling Analysis: VirtualLab Fusion provides access of the intermediate fields during propagation through the system. This can be done by selecting Modeling Analyzer as Result Visualization. On the tab page Modeling Analysis you configure the generation of the intermediate output. This tab is only available if Modeling Analyzer is selected. More information can be found in Sec. (d).
- Parameter Overview: This tab page provides an overview of all numerical parameters for detectors. Please check Sec. (e) for more information.
- Propagation to Detector: In this section the user can define the parameters that are used to propagate the light to the detector. A detailed explanation of all user control that are available under Propagation to Detector can be found in Sec. (f).

Fig. 368 shows the control to configure the Visualization \& Detectors settings of the underlying optical setup.


Figure 368. The section to configure the Visualization \& Detectors settings within the Profile Editor.

On the next pages we will explain the settings for Visualization \& Detectors more in detail.

## (a) Result Visualization

On the tab page Result Visualization the user can select the result visualization type that shall be used for system analysis. Fig. 369 show the content of the tab page Result Visualization.

```
System: 3D
(O) Detector Output
```

Figure 369. The user interface to select the Result Visualization type.

Depending on the selected profile the available Result Visualization type will be enabled. For the Ray Results profile VirtualLab Fusion supports the evaluation System: 3D or the Detector Output. The General Profile allows the evaluation of Detector Output or the Modeling Analyzer.
The following parameters can be configured within the user interface of the Result Visualization:

| ITEM | DESCRIPTION |
| :--- | :--- |
| System: 3D | This visualization is currently only available for the Ray Results profile. By <br> selecting this output type, performing the simulation will generate a result <br> document which contain the 3D system information including ray information. <br> By activating this option the tab page 3D View will be available for further <br> configurations. |
| Detector Output | Each detector will generate an output. The output can be in gridless and/or <br> gridded format. Within the Ray Results profile the output is restricted to be <br> gridless. The settings for the detectors can be adapted on the tab page De- <br> tector Settings. |
| Modeling Analyzer | For the Genera/ profile the visualization type Modeling Analyzer can be used. <br> This allow the access to intermediate information during propagation through <br> the optical setup. Further configuration can be done on the tab page Modeling <br> Analysis. |

## (b) 3D View

If the user selected the System: 3D as Result Visualization type the tab page 3D View becomes visible. On this tab page the user can configure all settings that are related to the System: 3D view output.
Fig. 370 shows all control which can be used to configure the parameter for System: $3 D$ view output generation.


Figure 370. The user controls to configure the visualization type System: 3D.
The parameters to configure for 3D View parameters can be found in Sec. 43.4.5. The Result Visualization type System: 3D are currently only available for the Ray Results profile.

## (c) Detector Settings

If the user selects Detectors as Result Visualization type, the tab page Detector Settings will be available. The user configure the detector output per detector. VirtualLab Fusion will use a set of Table Layout/Tree View
controls are used to provide a systematic overview of all available parameters of the Universal Detectors within the underlying system. Detailed information on this common user interface can be found in Sec. (b). Fig. 371 shows the controls to configure the Detector Settings of the detectors within the underlying system.


Figure 371. The user can configure the parameters of the Universal Detectors within the underlying system in the section Detector Settings.

The section within the Profile Editor contains a tab page for

- Field Quantities: The controls for the configuration of field values are described in Sec. 74.4.1. Within the Ray Results profile this tab page will be now shown.
- Detector Window (x-Domain): The definition of the window size and the sampling of equidistant data can be defined here. Detailed information can be found in Sec. 74.4.2.
- Detector Window (k-Domain): For the evaluation of field in $k$-domain the user can configure the size of the detector window and the resolution for equidistant data on the tab page Detector Window ( $k$-Domain). Detailed information can be found in Sec. 74.4.3.
- Gridless Data: Additional to gridded output the detector supports also the evaluation of gridless output. The parameters for the configuration of gridless data can be found in Sec. 74.4.3.
- Add-Ons: Adding, removing and the configuration of detector add-ons can be done in the section AddOns. You can find a detailed description of the user interface to configure the detector Add-Ons in Sec. 74.4.5.


## (d) Modeling Analysis

When selecting the General profile the Result Visualization type is available. This result visualization type allows the evaluation of intermediate results during propagation which enable you to get a detailed understanding what happens, when the light is propagated through the optical setup.

Fig. 372 shows the user interface to configure the Modeling Analyzer to analyze the process during propagation through the optical setup.


Figure 372. The user controls to configure the parameters of the Modeling Analyzer within the section Detector Settings.

The control to specify the settings of the Modeling Analyzer are explained in Sec. 43.4.6.

## (e) Parameter Overview

For the display of all numerical parameters of the detectors within the underlying system a Parameter Overview Table is used. Detailed information on the common user interface of Parameter Overview Table can be found in Sec. (a).
Fig. 373 shows the Parameter Overview tab for detectors within the Profile Editor.


Figure 373. The Parameter Overview of the Visualization \& Detectors section within the Profile Editor.

In general the table list all numerical parameters for the detectors of the underlying optical setup. But by activating the check box Hide Modeling Parameters all modeling parameters are not included in the listing. The modeling parameters are parameters of the free space propagation to the detectors. These parameters can be accessed in the section Propagation to Detector in the Visualization \& Detectors main section.

## (f) Propagation to Detector

Within this section of the Profile Editor the user can configure all parameters that are important to be used within the free space propagation to detectors.

Fig. 374 shows the control to configure the Propagation to Detector parameters.


Figure 374. The section to configure the Propagation to Detector within the Profile Editor.
For the communication of the Free Space Propagation parameters the parameters are displayed within several Table Layout/Tree View. Detailed information on this common user interface can be found in Sec. (b). The section within the dialog contains a tab page for

- Fourier Transform: The controls for specification are described in Sec. 43.4.2.1.
- Sampling Gridded Data: Details on the user controls for the configuration of gridded data can be found in Sec. 43.4.2.2.
- Sampling Gridless Data: In Sec. 43.4.2.3 the controls for the configuration of gridless data are explain in detail.


### 43.4.1.5 Profile Editor: Other Settings

In the section Other Settings a collection of parameters can be accessed which is valid for the complete system and not only for selected sources/components or detectors. This section is separated in the following sub sections:

- System: Here the user can enter some basic parameters like pressure and temperature which are provided as system parameters and used for system modeling. Detailed information on the System parameters can be found in Sec. (a).
- Free Space Parameters: On this tab page several global parameters are listed which are used for the propagation through homogeneous medium. These parameters are defined on system level and explained in detail in Sec. (b).
- Light Path Finder: For the evaluation of the tracing sequence through the setup, VirtualLab Fusion provides several options for determining the light paths (which paths the light goes within the system). These
parameters can be configured here. Detailed information on the Channel Configuration can be found in Sec. (c).

In the following paragraphs the controls to define the Other Settings are explained in detail.
(a) System

Fig. 375 show the content of the tab page System in the section Other Settings.


Figure 375. The system parameters which can be configured within the section Other Parameters.

The user can specify the following parameters via the controls of the tab page

| ITEM | DESCRIPTION |
| :--- | :--- |
| Process Logging Level | During the processing of an optical setup, VirtualLab Fusion provides several <br> logging information about the current step of the simulation. By selecting the <br> Process Logging Level the user can define to which detail level he like to see <br> this process information. The following levels are available: None, Normal <br> and Detailed. |
| Environment | VirtualLab Fusion supports to define the Environment parameters for the sys- <br> tem modeling. Here the user has to define the Air Pressure and the System <br>  <br>  <br>  <br>  <br>  <br> Temperature. These parameters are used to evaluate the refractive index of <br> the media within the system when propagating through it. |

## (b) Free Space Parameters

In general the Free Space Parameters are configured per component/detector. There are several settings that you can configure which are defined only once within the system. Fig. 376 show the content of the tab page Free Space Parameters in the section Other Settings.


Figure 376. The Free Space Parameters which can be configured for the complete system within the section Other Parameters.

The following settings are available for the Free Space Parameters on system level

| ITEM |  | DESCRIPTION |
| :---: | :---: | :---: |
| Wavefront dling |  | The handling of wavefront phases is a major challenge within optical simulation. Typically VirtualLab Fusion tries to handle the wavefront phase as smart as possible when propagating through an optical setup. By selecting to Extract Wavefront Phase Information from 2PI Modulo Data it is configured that VirtualLab Fusion tries to extract a smooth wavefront phase information after an integral Fourier transform. In this case the phase has to be typically sampled in 2PI modulo and after the integral Fourier transform is performed VirtualLab Fusion will apply smart unwrapping algorithms and interpolation techniques to extract a smooth wavefront from the 2PI modulo data. The default of this option is Yes. Another parameter also available in this section effect the result of a pointwise Fourier transformation. If the user defines to Use Spherical Part of Wavefront Phase for Pointwise FT Only VirtualLab Fusion will fit the spherical part before doing the PFT and use only this spherical part for the Fourier transform. This option is by default false. |
| Automatic <br> Analytical <br> form Selec | FFT/SemiFourier Transion | For the decision whether FFT or SFT is used a numerical criteria is applied. VirtualLab Fusion compares the numerical effort of the FFT and the SFT. In case of FFT a given quadratic phase of the field needs to be sampled, because it can only be handled analytically in the SFT. By defining the Threshold for Semi-Analytic Fourier Transform the user defines when to use FFT or SFT. The higher this threshold is, the later VirtualLab Fusion will use SFT. |

## (c) Light Path Finder

Within the section Light Path Finder the user can define all parameters necessary for the evaluation of light paths to be processed during the simulation. The parameters and the user interface to configure the parameters for the Light Path Finder are explained within Sec. 43.3.1.

### 43.4.2 Free Space Propagation Parameters (Modeling Profiles)

The most important step for doing fast physical optics is the free space propagation, which is used to simulate the light propagation from the output of one component (or source) to the input of another component (or detector). Therefor, VirtualLab Fusion offers a variety of parameters that can be adapted by the user for the free space propagation. These parameter can be specified per component and detector. The user can enter the configuration settings by opening the edit dialog of the component or detector and go to the tab page Free Space Propagation. Alternatively, it is possible to configure these parameter using the Profile Editor. The Profile Editor enables the user to have an overview of setting of multiple components/detectors. Detailed information on the Profile Editor can be found in Sec. 43.4.1.
The configuration of the free space propagation parameters is divided into three sections

| ITEM | DESCRIPTION |
| :--- | :--- |
| Fourier Transforms | Within this section the user can define several settings to select Fourier <br> transforms within the free space propagation. Detailed information see <br> Sec. 43.4.2.1. |
| Sampling Gridded Data | Next to the selection of Fourier transforms the specification for handling of <br> gridded data is important. Therefore the section Sampling Gridded Data can <br> be used. More information can be found in Sec. 43.4.2.2. |
| Sampling Gridless Data | Within our physical optics simulation approach we work also with gridless <br> data (e.g. to represent wavefront information). The settings for gridless data <br> can be configured in the section Sampling Gridless Data. A detailed expla- <br> nation of the controls to configure the Sampling Gridless Data can be found <br> in Sec. 43.4.2.3. |

Fig. 377 shows the Free Space Propagation page of the edit dialog of a Universal Detector. Note: the graphical user interface for the configuration of the Free Space Propagation parameters is everywhere the same (for components/detectors and also in the edit dialogs or the Profile Editor).


Figure 377. Free Space Propagation page of the edit dialog of a detector/component.

Within the following section the detailed configuration options for the Free Space Propagation parameters are explained.

### 43.4.2.1 Fourier Transforms

To enable fast physical optics it is a key technology to switch between different domains. In standard optical simulations we typically deal with x - and k -domain. This domain switching is very often done within the free space propagation.
VirtualLab Fusion comes with three different Fourier transform algorithms to enable a fast solution depending on the incident field:

- Fast Fourier Transform (FFT): The fast Fourier transform is rigorous. Lateral shift and linear phase are handled analytically.
- Semi-Analytical Fourier Transform (SFT): The semi-analytical Fourier transform is also rigorous. In addition to lateral shift of the field and linear phase it can also handle quadratic phase terms analytically. This method has numerical advantages if the quadratic phase term is significant.
- Pointwise Fourier Transform (PFT): The pointwise Fourier transform is an approximation. Here the smooth phase of the field is evaluated and a pointwise transformation into the target domain is done. Mathematically this method is derived from the stationary phase. For the pointwise Fourier transform we check initially for singular cases (plane wave and cylindrical wave) and perform regularization if a singular case appears.

Fig. 378 show controls to define the parameters for the selection of Fourier Transforms within the Free Space Propagation parameters.

| Type of Fourier Transform | Source to Detector | Component to Detector |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Forward FFT | $\square$ | $\square$ |  |  |
| Forward SFT | $\square$ | $\square$ |  |  |
| Forvard PFT | $\square$ | $\square$ |  |  |
| Inverse frt | $\square$ | $\square$ |  |  |
| Inverse SFT | $\square$ | $\square$ |  |  |
| Inverse PrT | $\square$ | $\square$ |  |  |
| Automatic Prt Selection Accuracy Level |  |  |  | $0 \%$ |
| Resulting Pointwise Transformation Index (PT) Threshold |  |  |  | 1 |
| Enforce PrT Beyond | 10000 | npling Values? | (o) Yes | Ono |
| PFT for Bijective Mapping Only? |  |  | OYes | O No |

Figure 378. The user interface to define the Fourier Transforms selection parameters.

The following parameters can be specified by the user

> Type of Fourier Trans- VirtualLab Fusion supports the automatic selection of the Fourier transform to forms use dependent on the input field for which the domain shall be changed. This algorithm evaluates the pointwise transformation index (PTI) and first decides whether to use pointwise Fourier transform or an integral Fourier transform (SFT or FFT). If an integral Fourier transform is used the numerical effort for SFT and FFT is compared and the most suitable method is used. Nevertheless, it is not untypical that the user already pre-select the types of Fourier transforms which should be used for evaluation. If the user likes to enforce the usage of pointwise Fourier transform for example, it is possible to select only the PFT for the free space propagation. This makes the decision process faster and also enable the user to have a concrete control of the effects he likes to include in the simulation (e.g. diffraction). In the section Type of Fourier Transform the user can select whether to use FFT, SFT and or PFT for the usage within the free space propagation. This selection can be done independently for the forward ( $x$ to $k$ ) and the inverse ( $k$ to $x$ ) Fourier transform. In addition we differ between the selection for Source to Component, Component to Component, Inside Components, Source to Detector and Component to Detector. In dependency whether you edit a component (single surface or multiple surfaces) or a detector, VirtualLab Fusion will offer you a matrix, which enable a full flexibility to configure the modeling according to your needs.

## Automatic PFT Selection Accuracy Level

As explained above VirtualLab Fusion evaluated how accurate the pointwise Fourier transform is in case not only PFT is marked as an option for automatic Fourier transform selection. The accuracy for this evaluation can be specified by the Automatic PFT Selection Accuracy Level. The higher the accuracy the later VirtualLab Fusion will decide to use PFT. Internally, VirtualLab Fusion calculate the pointwise transformation index (PTI), which is the relation between the size of the function after pointwise Fourier transform and the size of the function after an integral Fourier transform. The sizes for integral Fourier transform are evaluated by 1D cuts. This ratio is gauged by theoretical consideration with a factor $\epsilon$. If the $P T /$ is larger than 1 PFT is selected. By selecting the Automatic PFT Selection Accuracy Level the threshold for the PTI comparison will be changed. In the graphical user interface the user can check the resulting threshold value where VirtualLab Fusion switches between pointwise and integral Fourier transform in the box after Pointwise Transformation Index (PTI) Threshold.

Enforce PFT Beyond $\mathbf{x x x}^{2}$ VirtualLab Fusion provides also a fall-back solution to restrict the numerical Sampling Points effort of integral Fourier transforms. Therefor the option Enforce PFT Beyond $x x x^{2}$ Sampling Points is to be selected (by selecting Yes). If this option is activated VirtualLab Fusion will check the numerical effort to perform the integral Fourier transform. If it is larger than the value specified by the user, the integral Fourier transform is aborted and VirtualLab Fusion will use pointwise Fourier transform instead. This information can be seen also in the progress logging to make a transparent documentation of the decision making during propagation through the system.

PFT for Bijective Mapping The pointwise Fourier transform is typically valid only in bijective cases, which Only? means that the mesh of gridless points in x-domain and in y-domain are well sorted. Nevertheless, it can be also applied in non-bijective/surjective cases. By activating the flag PFT for Bijective Mappping Only it is ensured that the pointwise Fourier transform is not applied in surjective cases.

### 43.4.2.2 Sampling Gridded Data

If an integral Fourier transform is used VirtualLab Fusion typically needs to switch from gridless (or hybrid) data format into gridded data format. For this operation the user has several new options to be configured in the section Sampling Gridded Data.
Fig. 379 shows controls to define the parameters for the configuration of Sampling Gridded Data within the Free Space Propagation parameters.


Figure 379. The user interface to define the parameter for Sampling Gridded Data.

The following configurations can be done in the user interface for Sampling Gridded Data:

## ITEM

| Automatic Sampling/Man- | In general the user can decide whether the sampling should be evaluated <br> automatically or a manual sampling configuration shall be used. Depending <br> on the selection different options are display, e.g. only for Manual Sampling |
| :--- | :--- |
|  | the user can define Sampling Values for Gridded Data directly. |

Sampling Values for Grid- If the user selects Manual Sampling, the option to configure the Sampling ded Data Values for Gridded Data is activated in the graphical user interface. Here the user can directly configure the number of pixels to be use in x and y direction.

### 43.4.2.3 Sampling Gridless Data

As already explained before VirtualLab Fusion typically needs to handle gridless and gridded data within the simulation of an optical setup. In Sec. 43.4.2.2 the free parameters for Sampling Gridded Data were explained. In the section Sampling Gridless Data of the Free Space Propagation parameters for the sampling for gridless data can be configured.
Fig. 380 show controls to define the parameters for the configuration of Sampling Gridless Data.


Figure 380. The user interface to define the parameter for Sampling Gridless Data.
The following options can be configured by the user in this section of the user interface:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Initial Number of Gridless <br> Sampling Values | The user may enter an initial number for the gridless values to be used. <br> VirtualLab Fusion uses the specification of the shape of the source aperture <br> to generate a regular x-y mesh (in case of rectangular aperture) or a hexap- <br> olar mesh (in case of elliptical aperture). The initial number is used to define <br> the number of points in x/y direction for a regular grid or the density for a <br> hexapolar mesh. |
| Control Factor of Gridless <br> Sampling Values with Re- | The evaluated density (of hexapolar mesh) or number of sampling points in <br> x/y direction (for a regular x-y grid) can be scaled with the Control Factor of <br> Gridless Sampling Values with Respect to Initial Number. The control factor |
| is multiplied on the density or the number of sampling points in x/y direction. |  |

### 43.4.3 Restrictions of Ray Results Profile

In the current version VirtualLab Fusion comes with two build-in modeling profiles: (1) Ray Results Profile and General Profile. In both profiles VirtualLab Fusion performs physical optic simulation to obtain the results at detectors. For the Ray Results Profile several restriction are defined. This profile can be used to configure results users are typically used when using conventional ray tracing software tools. The General Profile is not restricted (beside the availability of the result visualization type System: 3D, which will be released in one of the upcoming releases). It should be stated clearly, that you can generate the same results with the General Profile as with the Ray Results Profile if you use the corresponding definition of modeling parameters.
The following restrictions are defined for the Ray Results Profile

- The Fourier transform selection for detector is fixed to be only pointwise (user interface is reduced to information of used Fourier transforms only).
- The Fourier transform selection between and inside components is fixed to be only pointwise.
- The result visualization type Modeling Analyzer is disabled.
- The Universal Detector is fixed to generate gridless data only, which contains only positions, directions and wavefront phase.
- Within the Universal Detector the user can not define the Field Quantities to be displayed.
- The Universal Detector can not configured to provide the field in k-domain. So also the tab page Detector Window ( $k$-Domain) is not visible.
- The profile editing tool Between Components: ... is disabled.
- The profile editing tool To Detectors: ... is disabled.
- The profile editing tool Speed vs. Accuracy is disabled.
- The profile editing tool Pointwise vs. Integral is disabled.

To overcome these limitations we propose that you use the General Profile with the corresponding settings.d

### 43.4.4 Ray Results Profile: Detectors

Only available in a General or a Light Shaping Optical Setup.
In case the user selects the visualization type Detectors each detector will generate a detector result. Via the editor of the visualization type the user can specify the parameters for the point selection and other global view parameters. The edit dialog can be opened by clicking on the small gear symbol next to the Detectors ribbon icon.
Fig. 381 shows the edit dialog of the Detectors visualization type for the Ray Results Profile.


Figure 381. Edit dialog of the Detectors visualization type for the Ray Results Profile.

Within the dialog the user can configure the following options

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Positions | The user needs to specify the number of samples that shall be used for the <br> result generation. Several modes of operations are provided for this config- <br> uration, which have different free parameters. The different modes and their <br> parameter are described in Sec. 43.4.4.1. |
| Unselect Points $\quad$ with <br> an Associated Energy | VirtualLab Fusion supports to apply a filter according to the maximum intensity <br> on the point selection. This filtering can be activated by checking the flag <br> Unselect Points with an Associated Energy Smaller than and definition of the <br> Smaller than |
| Use Color Table for Differ- minimum percentage value. |  |

### 43.4.4.1 Point Selection

For the Ray Result Profile one of the most important parameters to specify is the number of samples/positions to use in the pointwise processing sequence. This can be done by different modes of operations. In addition this specification is also possible for gridless data at the Universal Detector.
Fig. 382 shows the panel that is used to select the selection mode of positions and the selection dependent parameters.


Figure 382. Panel to define the sampling positions (mode of operation and parameters) for the gridless data.
Depending on the selection mode different distribution of position will be generated and are used to define the distribution of a gridless data set. Fig. 383 shows some sample distributions for different modes of operations with different (mode-dependent) parameters.


Figure 383. Left: x-y-Grid with 15 times 11 points. Middle: Hexapolar pattern with a Density of 6. Right: 100 points placed at Random positions

For each mode there are different free parameters available that can be defined by the user. The following modes are supported:
(a) $x$-y-Grid

The positions are placed on an equidistant grid.

| Number <br> Points ${ }^{[\mathrm{VV}}$ | of Sampling | The number of points in $x$ - and $y$-direction, respectively. It is ensured that the <br> numbers are odd so that there is always a ray is at the position $(0 \mathrm{~m} ; 0 \mathrm{~m})$. |
| :--- | :--- | :--- |

## (b) Hexapolar

The positions are placed on rings so that the overall structure has the symmetry of a regular hexagon. The $\mathrm{n}^{\text {th }}$ ring contains $6 \cdot n$ points. There is one additional sample in the center.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Density ${ }^{[\operatorname{DV}]}$ | The number of rings. |

## (c) Random

The positions are placed uniformly at random positions.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of <br> Points ${ }^{[\mathrm{PV}}$ | Sampling | | The overall number of sampling points. |
| :--- |
| Use Seed of |
| If you check this option the position of the samples remain the same between <br> consecutive simulations. You can change the seed value to obtain a different <br> random pattern. |
| Generate Mesh |
| If you uncheck this option no mesh information will be generated. This will in- <br> crease the performance for the random point generation, because the mesh <br> is generated by a so called Delauney triangulation, which might be time con- <br> suming for large number of sampling points. |

### 43.4.5 Ray Results Profile: 3D System

## Only available in a General or a Light Shaping Optical Setup.

The evaluation of System: 3D output is only supported in the Ray Results Profile. By performing the Ray Results Profile with selected output System: 3D a Ray Distribution 3D document ( $\hookrightarrow \mathrm{Sec} .17 .1$ ) is generated, which shows the complete optical system and how light propagates through it.
The user can edit the parameters to be used within this configuration by clicking on the small gear symbol next to the System: 3D ribbon entry. The edit dialog is divided into two tab pages which are explained in the following subsections.
Using the Copy From button you can copy the view settings from any open Ray Distribution 3D document to the dialog.

### 43.4.5.1 Ray Selection Tab



Figure 384. The edit dialog to edit the System: 3D output of the Ray Results Profile showing the Ray Selection tab.

This tab page ( $\hookrightarrow$ Fig. 384) has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Positions | The user needs to specify the number of samples that shall be used for the <br> result generation. Several modes are provided for this configuration, which <br> have different free parameters. They are described in Sec. 43.4.4.1. |
| Unselect Points with <br> an Associated Energy <br> Smaller than | VirtualLab Fusion supports to apply a filter according to the maximum intensity <br> on the point selection. This filtering can be activated by checking the flag <br> Unselect Points with an Associated Energy Smaller than and definition of the <br> desired minimum percentage value. |

### 43.4.5.2 View Settings Tab

This tab page is described in Sec. 5.15.2, the additional Rays page in Sec. 17.1.3.

### 43.4.6 General Profile: Modeling Analyzer

The Modeling Analyzer provides intermediate results of the light propagating through the Optical Setup using physical optics simulation. This helps you to understand and optimize the system modeling. As during propagation it is often switched between $x$ - and $k$-domain using a Fourier Transform, the intermediate results are stored in a Set of Data Arrays ( $\hookrightarrow$ Sec. 16) which can contain results in both domains. The evaluation of the Modeling Analyzer is only supported in the General Profile as result visualization type.


Figure 385. The edit dialog of the Modeling Analyzer.

The edit dialog of the Modeling Analyzer ( $\hookrightarrow$ Fig. 385) has the same structure as the Universal Detector. The following tab pages are available for configuration:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Field Quantities | On this tab page the user can define the field quantities and domains that shall be evaluated by the Modeling Analyzer. A detailed description of the user interface can be found in Sec. 74.4.1. Please note that in comparison to the Universal Detector, the Modeling Analyzer will always calculate Ex and Ey component in both domains, because they are provided within the system modeling. The selection of the quantities that shall be shown is done via Configure Field Data Visualization by Electromagnetic Field Quantity Add-On. The dialog to configure the field quantities to show (and their domains) and the available view options can be found in Sec. 74.4.5.1. The Modeling Analyzer provide the field information at different locations through the system. So the options for combination of modes is not provided here and the modes are shown separately. The current implementation of the Modeling Analyzer only support the evaluation of $E x$ and $E y$, so there is also not the option to use paraxial assumption for field component calculation here. |
| Detector Window Domain) | ( $\mathbf{x}$ - On the tab page Detector Window ( $x$-Domain) the user can specify the size of the detector window which shall be used in $x$-domain. In addition he can select how the field information should be sampled (in case equidistant sampled data shall be generated). More information on the Detector Window can be found in Sec. 74.4.2. |
| Detector Window Domain) | (k- On the tab page Detector Window (k-Domain) the user can specify the size of the detector window which shall be used in k-domain. In addition he can select how the field information should be sampled (in case equidistant sampled data shall be generated). More information on the Detector Window can be found in Sec. 74.4.3. |
| Gridless Data | The Modeling Analyzer can also be configured to generate the output data in gridless format. Gridless format will be only provided if it is also available within the simulation (e.g. before and after pointwise Fourier transforms). Sec. 74.4.4 gives a detailed overview of the settings for gridless data. The Modeling Analyzer does not allow to configure manual sampling for gridless data, so you can access only the gridless data that is used within the engine processing. |
| Add-Ons | The edit dialog of the Modeling Analyzer also have a tab page to configure add-ons. For the Modeling Analyzer no customized detector add-ons can be specified. Only the standard add-on to show the Electromagnetic Field Quantities is available. The edit options for the Electromagnetic Field Quantities can be found in Sec. 74.4.5.1. |

### 43.4.7 Classic Field Tracing

The Classic Field Tracing is our first implementation of to do physical optics. Its implementation is typically limited to paraxial simulations or typical Fourier optical configurations. For the propagation between components (or to detectors) well-known and established diffraction integrals can be selected, which include for example Spectrum of Plane Waves, Fresnel Integral or Far Field Integral. In comparison to Classic Field Tracing the newly implemented way to do fast physical optics using our Modeling Profile technology is a generalization of all these techniques for free space propagation.

When applying the Classic Field Tracing engine the progress of the simulation can be tracked in the Optical Setup Editor. When the simulation of a linkage in the Optical Setup starts, the symbol ${ }^{z_{i n}}$ is displayed in the very first column. When the simulation of the linkage is completed, the symbol is changed to 1 .
The Optical Setup Editor also provide the special option to Re-Use Automatic Settings if Classic Field Tracing is selected as simulation engine. Here some settings automatically calculated during a simulation with Classic Field Tracing are written to a cache, for example the location of the Input Transface. For the next simulation these settings are then not calculated anew but the value from the cache is used, which can speed up the simulation. An example for such a setting is evaluation of the input transface ( $\hookrightarrow$ Sec. 93.1 ) by the geometrical optics component propagation ( $\hookrightarrow$ Sec. 96.1).
The Re-Use checkbox indicates whether the cache is filled and can be reused. If the check box is disabled the cache is empty. If the checkbox is enabled the user can select whether or not to use the cached settings by checking or unchecking the box.
In case that more than one mode is simulated and for each mode the automatic parameters are determined the Re-Use option stays disabled. This is because the size of the cache (only one parameter set is handled for each operator). To overcome this limitation, the user can select that only one member of the fields set is used to evaluate the automatic propagation parameters ( $\hookrightarrow$ Sec. 43.4.7.1).


Figure 386. The user interface which is used to communicate the state of the cache (filled or empty. If the cache is filled, the user can decide to re-use these settings from cache, which will speed up the simulation by classicEngine.

Fig. 386 shows the option to Re-Use Automatic Settings, which is only available if Classic Field Tracing is selected as Simulation Engine.

### 43.4.7.1 Property Browser for Classic Field Tracing

Only available in a General Optical Setup.

Only for Classic Field Tracing, the following options are available in the Simulation Settings tab of the Property Browser.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Global Accuracy ${ }^{[P E}$ | To use a global Accuracy Factor for automatic operations in VirtualLab Fusion, <br> e. g. Automatic Propagation Operator, this option has to be set to True. Then <br> the specific accuracy factors of the operation in the Optical Setup are ignored <br> and the set global Accuracy Factor is used instead. |
| Accuracy Factor ${ }^{[\mathbb{P V}}$ | The Optical Setup wide accuracy factor can be defined here. The default <br> value is 1.0. |


| Use Global Deviation Threshold ${ }^{[\boxed{E}]}$ | If checked, the Deviation Threshold given here is used within each Automatic Propagation Operator present in the Optical Setup. |
| :---: | :---: |
| Deviation Threshold ${ }^{\text {PE }}$ | Threshold value being used instead of values defined locally in the operators. |
| Optimize Field Before Propagating ${ }^{\text {国 }}$ | If set to True, VirtualLab Fusion tries to optimize the field before propagating it between two subsequent Optical Setup Elements by truncating the field size and by rotating the field according to a possibly given analytical linear phase (i. e. a global direction vector). This option applies to the complete Optical Setup. The only exception, where no optimization will be tried, is the free space propagation behind a Field Size and Sampling Manipulation element. The meaning of this option for the free space propagation algorithm is shown in Fig. 387, where it is related to the first step. |
| Tilt Threshold ${ }^{\text {PEE }}$ | If there is an analytically given linear phase at the field, the field will be rotated according to this global direction vector during optimization only if the tilt angle is above this threshold. If the value is set to zero, a rotation will be done by the optimization algorithm for each direction vector which differs from $(0,0,1)$. The meaning of this option for the free space propagation algorithm is shown in Fig. 387, where it is related to the last step. |
| Pilot Ray Direction from Analytical Data Only ${ }^{\text {国 }}$ | If this option is set to True, the calculation of the local pilot ray for the free space propagation between two subsequent elements will use the analytically stored linear phase direction of the field only. There will be no consideration of the sampled phase values in this case. So the calculation time for this special algorithm will be less, especially for large fields. On the other hand, a possibly incorrect pilot ray may lead to inefficient working of the subsequent algorithms with a bad overall performance. So use this option with caution. The meaning of this option for the free space propagation algorithm is shown in Fig. 388, where it is related to the second step. |
| Analysis for One Member Only ${ }^{\text {PE }}$ | During the simulation of Optical Setups with a polychromatic or partially coherent source, several automatic operations (e. g. Automatic Propagation Operator) can be done by evaluating all sub-fields in the Harmonic Fields Set. This is very time consuming. VirtualLab Fusion enables the user to configure that these automatic operations are only done by evaluating one member of the Harmonic Fields Set. To enable this simulation mode, the user has to set this option to True. |
| Index of Analyzed Member ${ }^{\text {PE }}$ | When the user defines that the decisions of the automatic operations are done only by evaluating one member of the Harmonic Fields Set, he also has to define the index of the sub-field in the Harmonic Fields Set which shall be used for the evaluation. This is done by setting the specific index here. |



Figure 387. Sub-algorithm for the free space propagation: Optimization of the field. (The colored steps refer to entries in the table shown above.)


Figure 388. Sub-algorithm for the free space propagation: Pilot ray calculation. (The colored step refers to an entry in the table shown above.)

### 43.5 Parameter Extraction

VirtualLab Fusion allows that almost all parameters of an Optical Setup can be extracted and read out or varied externally.

- All parameters can be extracted to an XML file ( $\rightarrow$ Sec. 124.1).
- Changeable parameters are those parameters which when changed in the XML file can be re-imported into VirtualLab Fusion. This mainly affects Boolean and string variables of snippets.
- Variable parameters are those changeable parameters which in addition can be varied externally. This is only possible for integer or real values. This mechanism is the foundation for the special batch mode commands ( $\leftrightarrows$ Sec. 9), the Modulated Grating Parameters ( $\leftrightarrows$ Sec. 42.1.3), the Parameter Overview ( $\checkmark$ Sec. 43.6.1), the Parameter Overview Tree ( $\hookrightarrow$ Sec. 43.7), the Parameter Coupling ( $\hookrightarrow$ Sec. 43.10), the Parameter Run ( $\varsigma$ Sec. 44), the Light Guide Grating Design ( $\leftrightarrows$ Sec. 101.2), the Parametric Optimization ( $\varsigma$ Sec. 102), the optiSLang Bridge ( $\leftrightarrows$ Sec. 103), and the export to optiSLang projects ( $\leftrightarrows$ Sec. 124.1.1).

Variable parameters are marked in the manual with a ${ }^{[\mathrm{PV}}$ symbol, changeable but not variable parameters
 represented by more than one numerical parameter. In general, only properties which are visible and activated in the corresponding edit dialog are extracted.

## Example 1

If an optical stack（ $\checkmark$ Sec．39．2）is used for a General Grating in 1D－Periodic mode，you can edit its Period ${ }^{[\mathbb{V}]}$ in the corresponding edit dialog．This property is represented as＂Period＂in the parameter run．In contrast，if you set the grating to 2D－Periodic mode，you can set two values for the Period ${ }^{\text {［⿹V }}$ ， namely one for the x －and one for the y －direction．Thus two parameters＂Period X ＂and＂Period Y ＂are available in the parameter run．
However，if the stack period is determined from a surface or media period，it cannot be changed by the user．In this case，no＂Period＂parameter for the stack is available in the parameter run．

More complex properties can have their own sub－properties．They are marked with a ${ }^{[巴 \boxminus}$ symbol．Clicking on this symbol leads to the corresponding manual section．In this section or subsections of it the available sub－properties can be found．

## Example 2

An optical stack can comprise several surfaces ${ }^{\text {国 }}$ and subsequent media ${ }^{\text {同．}}$ ．For example the Conical Constant ${ }^{\text {VV }}$ of an Aspherical Surface ${ }^{\text {『® }}$ within an Optical Stack ${ }^{\text {狍 }}$ of a grating component ${ }^{\text {PE }}$ can be varied in the parameter run．

Parameters can be extracted from the following objects：
－The Optical Setup itself：For example the system temperature and the air pressure（ $\hookrightarrow$ Sec．（a））or the General Parameters of the Parameter Coupling snippet（ $\hookrightarrow$ Sec．43．10．1．2）．
－The Optical Setup Elements
－The linkages between the Optical Setup Elements：parameters of the rotation operators and the actual free space operators．Only for Classic Field Tracing．$\hookrightarrow$ Sec． 93
However，extraction of 10 ＇000s of objects can decrease performance of VirtualLab Fusion significantly．Thus you can disable objects which can provide that many parameters via an Optical Setup Tool（ $\hookrightarrow$ Sec．43．6）．These objects are：
－A Surface Layout（ $\hookrightarrow$ Sec．40．2）of a Light Guide with many regions．
－Coatings with many layers．
－For a Pillar Medium（General）（ $\hookrightarrow$ Sec．37．3．8）with very many pillars，the pillar distribution parameters can be excluded．

## 43．6 Tools

Besides the Profile Editing Tools（ $\lrcorner$ Sec．43．3．2）there are much more tools which help you to configure an Optical Setup to your needs．Some of them are available in the ribbon tabs of the Optical Setup document， while the full set of tools is accessible via the menu that opens by clicking the button Tools in the left bottom corner of the Optical Setup Editor window．The following tools are available：
－Parameter Overview（ $\hookrightarrow$ Sec．43．6．1）
－Configure Parameter Extraction：allows you to exclude performance critical objects from Parameter Ex－ traction（ $\hookrightarrow$ Sec．43．5）
－Optical Setup Tools which help you defining the optical setup，especially the execution sequence of the Optical Setup Elements（ $\leftrightarrows$ Sec．43．6．2）
－Component Tools operate on specific types of Optical Setup Elements（ $\hookrightarrow$ Sec．43．6．3）
－Catalog Support（ $\hookrightarrow$ Sec．43．6．4）
－Import／Export of elements（ $\hookrightarrow$ Sec．43．6．5）

- Import Parameters from XML: Imports an XML having the format described in Sec. 124.1 and sets all matching variable parameters ( $\hookrightarrow$ Sec. 43.5) to the values in the XML file
- Find Focus Position ( $\hookrightarrow$ Sec. 43.6.6)
- Optimize Detector Positions ( $\hookrightarrow$ Sec. 43.6.7)
- Show Simulation Report ( $\hookrightarrow$ Sec. 43.6.8)
- Create New Parameter Run ( $\hookrightarrow$ Sec. 43.6.9)
- Create New Parametric Optimization ( $\hookrightarrow$ Sec. 43.6.10)
- New Cells Array Design ( $\hookrightarrow$ Sec. 100)
- Remove All Lookup Tables ( $\hookrightarrow$ Sec. 43.6.11)
- Update Add-ons in Detectors ( $\hookrightarrow$ Sec. 43.6.12)


### 43.6.1 Parameter Overview

## Availability

Toolboxes: All

## Accessible:

- Main window: Optical Setup > Parameter Overview
- Optical Setup Editor: Tools > 睴 Parameter Overview


Figure 389. The parameter overview dialog which also allows you to set new values for the given parameters.
This tool opens a resizable dialog giving you an overview of most numerical parameters of all Optical Setup Elements. This dialog ( $\rightarrow$ Fig. 389) comprises a table with the following columns.

| COLUMN | DESCRIPTION |
| :--- | :--- |
| \{Unnamed \} | The first column allows you to collapse/expand all parameters of an Optical <br> Setup Element or its building blocks. Simply click on the $\exists$ and $\oplus$ symbols, <br> respectively. At the top of this column you can select to collapse all levels (1), <br> collapse only the Category level (2) or show all levels (*). |
| Object | The object to which the shown Parameters belong. |
| Category | Allows further grouping of the parameters. For example the surface or <br> medium to which the parameter belongs. |
| Parameter | Name of the parameter. |
| Value | By default the current value of the parameter is shown in this column. How- <br> ever, you can enter a new value here. It must be within the allowed Minimum <br> - Maximum range (these columns can be made visible using Show Minimum <br> and Maximum Allowed Values). Otherwise it is marked red. <br> If you click OK the new value is set for the corresponding parameter. |

Furthermore this dialog has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | Only rows containing the given string either in the Object, Category (if appli- <br> cable) or the Parameter column are shown. The matching is case insensitive. <br> It is possible to search for multiple words and word groups embraced by quo- <br> tation marks, for example: "surface \#1" scaling. |
| Show Minimum and Maxi- | If you check this option, two additional columns are displayed showing the |
| mum Allowed Values | absolute minimum and maximum values of the parameter - you must not <br> enter a value outside of this range. |

Sec. 43.7 describes a similar technique allowing you to change a single parameter without the need to open a separate dialog.
The available parameters are explained in Sec. 43.5.

### 43.6.2 Optical Setup Tools

These tools assist you in defining the optical setup, especially the execution sequence of the Optical Setup Elements, by

- generating the sequence automatically ( $\hookrightarrow$ Sec. 43.6.2.1)
- toggling the active light source ( $\hookrightarrow$ Sec. 43.6.2.2)
- inserting elements into the sequence ( $\hookrightarrow$ Sec. 43.6.2.3)
- excluding elements from the sequence ( $\hookrightarrow$ Sec. 43.6.2.4)
- exchanging one element in the sequence by another ( $\hookrightarrow$ Sec. 43.6.2.5)
- synchronizing the sampling of the detectors ( $\varsigma$ Sec. 43.6.2.6)
- converting a Grating Optical Setup into a General Optical Setup ( $\hookrightarrow$ Sec. 43.6.2.7)
- deleting all linkages ( $\hookrightarrow$ Sec. 43.6.2.8) or
- sorting the entries in the Optical Setup Editor ( $\hookrightarrow$ Sec. 43.6.2.9)


### 43.6.2.1 Generate Sequence

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools $>\rightarrow$ Complete Sequence Generation / Layout Tools $>m$ - Partial Sequence Generation
- Optical Setup Editor: Tools > Generate Sequence > $\rightarrow$ Complete Sequence Generation / Tools > Generate Sequence > -H Partial Sequence Generation

Configuring an Optical Setup requires the creation of all linkages between Optical Setup Elements which shall be simulated. This can be done manually or by using the Optical Setup Tool Generate Sequence. First the user has to drag all Optical Setup Elements to the Optical Setup View in an order which corresponds to the desired execution sequence. Then Generate Sequence can be used for creating the corresponding linkages between the Optical Setup Elements automatically.


Figure 390. The same optical setup before (top) and after (bottom) automatic sequence generation.

This algorithm uses the following rules to connect the elements in the Optical Setup:

1. The algorithm only considers the light source with index 0 , Components, and Ideal Components. Detectors are not included in the Generate Sequence algorithm, because they can be connected to more than one Optical Setup Element ( $\hookrightarrow$ Sec. 43.2.2). Analyzers cannot be linked at all.
2. The start element is the Optical Setup Element with the lowest index which is not connected to another element).
3. This start element is then connected to the element with the next larger index having a free input. Usually a transmission linkage is generated.
4. The 2 nd and 3 rd step are repeated until no element without output connection can be found anymore.

There are two options available for generating a sequence: Complete Sequence Generation means the connection of all free elements. Partial Sequence Generation allows the user to define the maximum end element of the sequence algorithm ( $\hookrightarrow$ Fig. 391).


Figure 391. If the user likes to apply the Generate Sequence algorithm only to a subset of the system, the index of the end element has to be configured in the Partial Sequence Generation dialog.

This Partial Sequence Generation can be helpful when the Optical Setup the user likes to configure is split at one specific Optical Setup Element.

### 43.6.2.2 Toggle Light Source

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools $>$ Toggle Light Source
- Optical Setup Editor: Tools $>$ Toggle Light Source

The configuration of a second light source in an Optical Setup that contains already an active light source can be helpful, e.g. to investigate the behavior of the defined optical system when another source is used for illumination. VirtualLab Fusion supports adding additional light sources to an existing Optical Setup. To ensure that only one light source is used for the simulation of the Optical Setup, the active source always gets the special index 0 . All additionally added light sources get an index of 500 or higher. In the Optical Setup only linkages from the source with the index 0 are supported. Light sources with index 500 or higher cannot be connected with other Optical Setup Elements.
To change the active light source of a configured Optical Setup, one has to use the Optical Setup Tool Toggle Light Source. If only one other light source exists in the Optical Setup, the indices between this light source and the active one are toggled. If the Optical Setup contains more than one additional light source, the user has to select the index of the light source which shall be activated. This selection is done by the dialog shown in Fig. 392.


Figure 392. Dialog for selecting the active light source.

### 43.6.2.3 Insert Element into Optical Setup

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools > 't' Insert Element
- Optical Setup Editor: Tools > 'T' Insert Element into Optical Setup

To insert a new Optical Setup Element into an already configured Optical Setup, the Path table of the Optical Setup Editor can be used to relink the corresponding connections manually. Or you can use the Optical Setup Tool Insert Element into Optical Setup which inserts a currently not linked element behind a given already linked element. The affected elements are relinked automatically. For the linkage from the precedent to the inserted element the used reference coordinate system is specified in the dialog. For the linkage from the inserted element to a possible subsequent element usually the "T" (transmission type) or "0" reference coordinate system is used. Detector linkages are not changed. Fig. 393 shows an example.


Figure 393. Example how the Insert Element into Optical Setup tool works. The left image shows the initial situation. The right image shows the setup after the Aperture \#6 has been linked to the reference coordinate system named "1" (red) of the Ideal Beam Splitter \#4. Aperture \#6 has been linked automatically to Ideal Lens \#2 which was previously the subsequent element of the Ideal Beam Splitter \#4. Therefor its reference coordinate system " $T$ " (blue) is used.


Figure 394. For inserting a new Optical Setup Element into an existing Optical Setup, the element and its position in the execution sequence can be specified.

Fig. 394 shows the edit dialog where the user can define the Optical Setup Element which shall be inserted as well as its position in the execution sequence.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Element to Insert | Select the index of the Optical Setup Element you like to insert into the existing Optical Setup. |
| Insert Behind | Select the index of the Optical Setup Element behind which the Element to Insert shall be inserted. |
| Reference Output Coordinate System | The output coordinate system of the element which is chosen as Insert Behind which will serve as reference for the Element to Insert. |
| How shall the position of the element to be inserted be handled? | If the Element to Insert has already got an absolute position / orientation, the user can decide whether it will be kept or be re-initialized. |
| Keep the Absolute Position and Orientation after Inserting | If selected, the absolute position / orientation of the Element to Insert will be kept. |
| Re-initialize Relative Position and Orientation | If selected, the relative position and orientation of the Element to Insert will be re-initialized after inserting. |
| Which of the following values shall be kept constant? | Since the position and orientation of the subsequent elements may be changed by the insert operation, the user may select the handling of these data. |
| Relative Position and Orientation of Subsequent Element | If selected, the relative positions and orientations of the subsequent elements will be kept constant. |
| Absolute Position and Orientation of Subsequent Element | If selected, the absolute positions and orientations of the subsequent elements will be kept constant. |

This Optical Setup Tool is only available if there is at least one not linked Component or Ideal Component and at least one linkage.

### 43.6.2.4 Exclude Element from Optical Setup

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools > ' $\ddagger$ Exclude Element
- Optical Setup Editor: Tools > ' $\ddagger$ Exclude Element from Optical Setup

For fast excluding of an Optical Setup Element from a configured Optical Setup without losing its validity, the Optical Setup Tool Exclude Element from Optical Setup can be used. This tool removes all linkages of a selected Optical Setup Element. Fig. 395 shows the edit dialog of this tool.


Figure 395. Dialog for selecting the index of the Optical Setup Element to exclude.

Important: The Optical Setup Element is excluded from the execution sequence only, it is not removed from the Optical Setup itself. Only all linkages which start or end at the selected Optical Setup Element are relinked and so the simulation is done without this Optical Setup Element.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Element to exclude | Select the index of Optical Setup Element you like to exclude from the Optical <br> Setup. |
| Which of the following val- <br> ues shall be kept con- <br> stant? | Since the position and orientation of the subsequent elements may be <br> changed by the exclude operation, the user may select the handling of these <br> data. |
| Relative Position and Ori- |  |
| entation of Subsequent | If selected, the relative positions and orientations of the subsequent elements <br> will bept constant. |
| Element  <br> Absolute Position and If selected, the absolute positions and orientations of the subsequent ele- <br> Orientation of Subse-  <br> quent Element will be kept constant.  |  |

VirtualLab Fusion only supports to exclude Optical Setup Elements which are the end element of one linkage and the start element of one or more linkages. If no elements which meet this conditions are available, the Optical Setup Tool Exclude Element from Optical Setup cannot be applied.

Important: Only Ideal and Real Components can be excluded from Optical Setups, because all other elements can only be the start (light sources) or end (detectors) points of light paths.

### 43.6.2.5 Exchange Elements in Optical Setup

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools> ' $\ddagger$ Exchange Elements
- Optical Setup Editor: Tools > Exchange Elements in Optical Setup

Sometimes it is helpful to exchange an Optical Setup Element in a configured Optical Setup by another more
suited element. This can be done manually by using the Path table in the Optical Setup Editor and relinking of all corresponding linkages. Alternatively, the Optical Setup Tool Exchange Elements in Optical Setup can be used to solve this task. The user has to specify the element which shall be excluded from the Optical Setup and the element to substitute. This selection is done by the dialog shown in Fig. 396

| Exchange elements in the Optical Setup |
| :--- |
| Element to Insert |
| Element to Exclude |
| Element to be Inserted |
| How shall the position of the element to be inserted be handled? |
| Keep the Absolute Position and Orientation after Inserting |
| Subsequent Elements |
| The positions of subsequent element(s) may be changed by the Position From Substituted Element |
| operation. |
| Which of the following values shall be kept constant? |
| Relative Position and Orientation of Subsequent Element |
| Absolute Position and Orientation of Subsequent Element |

Figure 396. To exchange an Optical Setup Element with a new one in an existing Optical Setup, use the Optical Setup Tool Exchange Optical Setup Elements.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Element to insert | Select the index of the Optical Setup Element you like to insert into the Optical Setup. |
| Element to exclude | Select the index of the Optical Setup Element you like to exclude from the Optical Setup. |
| How shall the position of the element to be inserted be handled? | If the Element to insert has already got an absolute position / orientation, the user can decide whether it has to be kept or be re-initialized. |
| Keep the Absolute Position and Orientation after Inserting | If selected, the absolute position / orientation of the Element to insert will be kept. |
| Copy Absolute Position From Substituted Element | If selected, the absolute position and orientation of the Element to exclude will be copied to the Element to insert after inserting. |
| Which of the following values shall be kept constant? | Since the position and orientation of the subsequent elements may be changed by the insert operation, the user may select the handling of these data. |
| Relative Position and Orientation of Subsequent Element | If selected, the relative positions and orientations of the subsequent elements will be kept constant. |
| Absolute Position and Orientation of Subsequent Element | If selected, the absolute positions and orientations of the subsequent elements will be kept constant. |

Fig. 397 shows a sample application of the Exchange Elements in Optical Setup tool.


Figure 397. An example for the usage of the Exchange Elements in Optical Setup tool. The Linear Phase Transmission with index \#3 is exchanged by the Spherical Phase Transmission with index \#2.

### 43.6.2.6 Synchronize Detector Sampling

## Availability

Toolboxes: All

## Accessible:

- Ribbon: Layout Tools > Synchronize Detector Sampling
- Optical Setup Editor: Tools > Synchronize Detector Sampling


Figure 398. The dialog for synchronizing detector window and resolution among detectors.

Using this Optical Setup Tool you can copy the detector window and resolution settings ( $\hookrightarrow$ Sec. 74.1.1) from one detector to another. This tool opens a dialog ( $\hookrightarrow$ Fig. 398) with the following settings:

## ITEM

| Detector to Copy the Set- <br> tings from | The detector from which the detector window and resolution settings are <br> copied. |
| :--- | :--- |
| Detectors to Copy the Set-  <br> tings to This section of the dialog allows you to select one or more detectors to which <br> the settings from the Detector to Copy the Settings from are copied. The <br> Selection Tools allow you to either Select All or to Unselect All detectors in <br> the list. <br> Validity This control $(\hookrightarrow$ Sec. 5.10$)$ displays a red cross if no detector to copy the set- <br> tings to is selected. |  |

### 43.6.2.7 Convert to General Optical Setup

Only for Grating Optical Setups

This tool converts a complete Grating Optical Setup ( $\hookrightarrow$ Sec. 43.11.1) into a General Optical Setup by means of the following rules:

- The Ideal Plane Wave is converted into a Plane Wave ( $\hookrightarrow$ Sec. 51.2).
- Each stack of the grating component is converted into a Grating component ( $\hookrightarrow \mathrm{Sec} .60 .3$ ).
- If the Raw Data Detectors are in Light View mode they are converted into a Camera Detector ( $\hookrightarrow$ Sec. 74.5.2). Else they are converted into an Universal Detector ( $\hookrightarrow$ Sec. 74.4).
As a result you obtain a General Optical Setup which produces nearly the same near field results as the original Grating Optical Setup. However, for all the analyzers of a Grating Optical Setup there are no equivalents in a General Optical Setup. So among others you cannot directly evaluate the efficiencies. But you can use the Efficiency detector from the LightTrans Defined Detectors Catalog ( $\hookrightarrow$ Sec. 33) to this end.


### 43.6.2.8 Delete All Linkages

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools $>\underset{x_{x}^{*}}{*}$ Delete All Linkages
- Optical Setup Editor: Tools > $\underset{\times}{\text { 焱 }}$ Delete All Linkages

This Optical Setup Tool deletes all linkages (also linkages to the detectors) in the underlying Optical Setup.

### 43.6.2.9 Sort Table Entries

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Optical Setup Editor: Tools > Sort Table Entries

This Optical Setup Tool can be used for sorting the Path table of the Optical Setup Editor in a well-defined way. This tool is very helpful if the linkages were set in a confused order, e. g. first the last two elements in the Optical Setup were connected and then the light source at the end of the light path configuration. Then this Optical

Setup Tool sorts the table entries in the Path table in the order of their execution when the Optical Setup is simulated. This tool is also automatically applied after loading a stored Optical Setup.

### 43.6.3 Component Tools

There are tools which operate on specific types of Optical Setup Elements.
The Split Component tool splits one Lens System or Light Guide component into distinct elements ( $\hookrightarrow$ Sec. 43.6.3.1). The Combine Components tools combines several consecutive Curved Surfaces, Spherical Lenses, and Lens Systems into a single Lens System ( $\hookrightarrow$ Sec. 43.6.3.2). The Turn Component tool turns a Curved Surface, Lens System, or Spherical Lens by $180^{\circ}$ about its y-axis ( $\hookrightarrow$ Sec. 43.6.3.3).

### 43.6.3.1 Split Component

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools > $\mathbb{M}$ Split Component
- Optical Setup Editor: Tools > Wplit Component...

If the user likes to evaluate a detector result within a Lens System or Light Guide component, VirtualLab Fusion provides the Optical Setup Tool Split Component to split the component after the specified surface(s). So the user can place a detector between the resulting components.


Figure 399. Edit dialog of the Split Component tool

The edit dialog of this tool ( $\hookrightarrow$ Fig. 399) has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component to Split | The index of the component to be split. Any Lens System or Light Guide with <br> at least two surfaces is available in this list. |
| Split after Each Surface | If this option is active, the selected Component to Split is split after each <br> surface, i. e. each resulting component contains exactly one surface. |
| Set Surface Rotation to EI- | ONLY IF THE SELECTED COMPONENT TO SPLIT conTAINS ANY SURFACES THAT |
| ement | ARE INCLINED / ROTATED. <br> If checked, the rotation / inclination of the surfaces will be set to the new com- <br> ponents. The single surface inside each new component will not be inclined <br> anymore, then. If not checked, the new components will have the same ori- <br> entation as the original one. The single surface inside each new component <br> will keep its inclination as before. |
| Surface Rotation at Ele- | ONLY IF SET SURFACE ROTATION TO ELEMENT IS SELECTED. <br> If checked, the rotation/inclination of the element, which has been taken from <br> ment is Isolated <br> the surface, will be set as isolated. So, subsequent elements which have a <br> relative position and orientation to the inclined element are not affected. <br> If this option is active, you can select the index of the surface after which the |
| Split after Surface | component shall be split into two. All indices of the surfaces of the selected <br> Component to Split (except that of its last surface) are available. |

After pressing the OK button of the edit dialog, the selected component is split into two or more components. The split components are connected by linkages. Fig. 400 shows an example: the resulting Optical Setup contains two Lens Systems which are connected.


Figure 400. An example for the usage of the Optical Setup Tool Split Component.

If no valid component to split is available, VirtualLab Fusion displays an error message when executing the Split Component tool.

### 43.6.3.2 Combine Components

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:



- Optical Setup Editor: Tools > [ $\mathbb{Z}]$ Combine Component...

Real Components of type Curved Surface ( $\hookrightarrow$ Sec. 58.1), Spherical Lens ( $\hookrightarrow$ Sec. 57.3), Lens System ( $\hookrightarrow$ Sec. 57.1), or Light Guide ( $\hookrightarrow$ Sec. 57.2) can be tried to be combined into new components of type Lens System. All optical surfaces inside the original components will form a new sequence if possible.
Calling this tool, the dialog shown in Fig. 401 allows to specify the operation.


Figure 401. Edit dialog of the Combine Components tool
The edit dialog of this tool provides the following settings and information:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Index and Name of Com- <br> ponent | The first column shows the indices and names of components which can be <br> combined to a new component. Adjacent rows with the same background <br> color mark those components which can be combined to the same resulting <br> Lens System. Example from Fig. 401: The elements \#9, \#10, \#11, and \#12 <br> can be combined to one Lens System, the elements \#3, \#4, and \#7 can be <br> combined to another Lens System. |
| Separation | In this column the user has to select which separations shall be kept. If a <br> combination is not possible at one place, the box is checked read-only (like <br> between \#12 and \#3 in Fig. 401). Each box which is not checked will result <br> in a combination of the components above and below the dashed line. |
| Combination | This column gives the information about the new components which would <br> result from the current selections. |
| Combination Info... | This opens a dialog that informs about the restrictions which determine what <br> components can be combined with others (see below). |

The restrictions for a Lens System component that determine the restrictions for combining existing components are the following:

- All optical surfaces have to be centered to one common optical axis.
- Optical surfaces in the sequence may not be tilted to the optical axis nor rotated about this axes in reference to the first surface in the sequence.

If it is not possible to combine any components in the current Optical Setup, an error message will be given.

### 43.6.3.3 Turn Component

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools > 愚 Turn Component
- Optical Setup Editor: Tools > Turn Component

If you execute this tool, there is first a dialog where you can select any Curved Surface, Lens System, or Spherical Lens component present in the Optical Setup. If no such component is available, an error message is shown instead.
Then this tool does the following steps on the selected component:

- Multiply the $x$ - and $z$-scaling ( $\hookrightarrow$ Sec. 35.1.2) of all surfaces with -1 . This means that they are rotated by $180^{\circ}$ about their $y$-axis.
- Invert the order of the surfaces, their corresponding distances, and media.

In effect, the whole component is turned by $180^{\circ}$ about its y-axis. Note that in contrast to rotating a component by $180^{\circ}$ via its edit dialog ( $\hookrightarrow$ Sec. 5.6 ), this tool changes through which surface light enters the component as well as the position of the internal coordinate system relative to the component.

### 43.6.4 Catalog Support

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Ribbon: Layout Tools > Catalog Support (ribbon group)
- Optical Setup Editor: Tools > Catalog Support

The menu items in this section allow you to save light sources ( $\hookrightarrow$ Part VIII), components ( $\hookrightarrow$ Part IX), and detectors ( $\hookrightarrow$ Part XI) to the corresponding catalogs.
The entries for light sources and detectors are only available for a General and a Light Guide Optical Setup.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Add Light Source from Catalog | Loads the selected item from the light sources catalog and adds it to the Optical Setup. See Sec. 33 for details on the catalog dialog. |
| Save Light Source to Catalog | Opens a dialog to select one light source. Saves the selected item to the light sources catalog after asking for name and categories ( $\hookrightarrow$ Sec. 33.1). |
| Add Component from Catalog | Loads the selected item from the components catalog and adds it to the Optical Setup. See Sec. 33 for details on the catalog dialog. |
| 절 Save Component to Catalog | Opens a dialog to select one component. Saves the selected item to the components catalog after asking for name and categories ( $\hookrightarrow$ Sec. 33.1). |
| Add Detector from Catalog | Loads the selected item from the detectors catalog and adds it to the Optical Setup. See Sec. 33 for details on the catalog dialog. |
| Save Detector to Cata$\log$ | Opens a dialog to select one detector. Saves the selected item to the components catalog after asking for name and categories ( $\hookrightarrow$ Sec. 33.1). |

### 43.6.5 Import / Export Elements

## Availability

Optical Setups: General, Laser Resonator, Light Guide, and Light Shaping Optical Setup

## Accessible:

- Optical Setup Editor: Tools > Import/Export Elements

It can be helpful to save an Optical Setup Element to hard disk. This allows you to later import them into another Optical Setup. Doing so, you can define kind of a catalog of often used Optical Setup Elements. In contrast to the Catalog Support tool ( $\hookrightarrow$ Sec. 43.6.4) this works also for light sources, Ideal Components, detectors, and analyzers. To export an Optical Setup Element from an Optical Setup, the user simply has to click the Import/Export Elements > Export Optical Setup Element item in the Tools menu. Then a dialog ( $\hookrightarrow$ Fig. 402) is shown where the index of the element to export has to be specified.


Figure 402. To export an Optical Setup Element, the index of the element to export has to specified.

VirtualLab Fusion supports only the export of one Optical Setup Element at a time. After pressing the OK button in the selection dialog, the user has to specify the file name and location to store the selected Optical Setup Element to. The Optical Setup Elements are saved with the file extension *.Ipe.
To import a previously stored Optical Setup Element from hard disk, one has to select the Import/Export Elements > Import Stored Optical Setup item in the menu for the Optical Setup Tools. Then a file open dialog is shown where the user has to specify the element to be imported. The selected file must have the file extension *.Ipe. If the import of the selected Optical Setup Element was successful, the new element is added to a default position in the flowchart area of the Optical Setup View and can subsequently be linked to other elements.

### 43.6.6 Find Focus Position

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Ribbon: Optical Setup > 病 Find Focus Position- Optical Setup Editor: Tools > 㳸 Find Focus Position

This Optical Setup Tool optimizes the position of one detector so that it is in the focus, i.e. the position where a Ray Results Profile simulation yields the smallest spot diameter. For evaluation of the size within the detector plane the RMS detector is used on the ray bundle. Only the position of detecting devices having exact one active linkage can be optimized.


Figure 403. The edit dialog of the Find Focus Position tool.
Its edit dialog ( $\hookrightarrow$ Fig. 403) has the following options

| ITEM | DESCRIPTION |
| :---: | :---: |
| Detector to Optimize | The detector whose position shall be optimized. |
| Spot Size Radial | Option for the detection of the RMS value. If this option is selected the radial size is determined by the detector. |
| Spot Size X Only | Option for the detection of the RMS value. If this option is selected only the extension in $x$-dimension is evaluated by the detector. |
| Spot Size Y Only | Option for the detection of the RMS value. If this option is selected only the extension in $y$-dimension is evaluated by the detector. |
| Spot Size Refers to Centroid | Flag whether the RMS value is measured to the centroid of the ray bundle. If this option is not selected the position of the central ray will be used as reference for the RMS calculation. |
| $\begin{array}{ll} \hline \text { Optimize } & \text { Only } \\ \text { Coordinate } \end{array}$ | The focus finder can be used to detect the 3D position of the focus. The user can select whether only the z-coordinate of the focus position shall be used in the generated or updated Optical Setup, or whether the complete 3D information shall be used. |
| Generate New Optical Setup | The user can define whether a new Optical Setup shall be generated, or whether the optimized position shall be set into the active Optical Setup. |

### 43.6.7 Optimize Detector Positions

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Ribbon: Optical Setup > Optimize Detector Positions
- Optical Setup Editor: Tools > Optimize Detector Positions

If a detector is not placed at the optimal lateral position, an embedding of the incoming field might be necessary to match it with the detector position. This Optical Setup Tool generates a new Optical Setup where the positions of all detectors of the original Optical Setup are optimized so that they are placed right in the middle of the incoming light distribution. This optimization is done using Ray Results Profile simulations. Only the position of detectors having exact one active linkage can be optimized.

In case the detector is tilted in reference to the optical axis, there are two options available. The selection is done via the dialog shown in Fig. 404.


Figure 404. Dialog for choosing an option for optimizing the position of a tilted detector.

> ITEM

DESCRIPTION
... Inside Detector Plane If chosen, the optimization will do a lateral shift of the detector in its own plane.
... Perpendicular to Opti- If chosen, the optimization will do a shift of the detector inside the plane percal Axis pendicular to the optical axis.

### 43.6.8 Show Simulation Report

## Availability

Optical Setups: General Optical Setup with Classic Field Tracing \& Light Shaping Optical Setup Accessible:

- Optical Setup Editor: Tools > Show Simulation Report

After the simulation of an Optical Setup, it is possible to view and save several information about the simulation process in VirtualLab Fusion using this Optical Setup Tool. It shows a VirtualLab Fusion document which lists all available information, $\hookrightarrow$ Fig. 405.
This document works like a web browser. The initial page Report Overview shows a list of all Optical Setup Elements (as well as their processing durations) through which the light has been propagated. If a magnifier symbol $Q$ is clicked on, a new page with the report of the associated element will be opened ( $\lrcorner$ Fig. 406).


Figure 405. Simulation report document showing a list of processed Optical Setup Elements.

Initially only a rough overview of the processing of the selected Optical Setup Element is given. More details for the report entries can be explored by clicking on the associated magnifier symbol $Q$. For any selected page except the initial page ( $\hookrightarrow$ Fig. 405) the following controls are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Full Expansion | By clicking on this button the report information is exported into a XML file as <br> described below. |
| Close Tab | If checked, the report tree expands completely, i.e. all report entries are <br> visible. |

The entire simulation report can be exported to a XML file via the ribbon item File > Export > Export as XML or the $\boldsymbol{R}^{-3}$ button on the bottom of the report window. The XML file is stored along with the style file lt_logstyle.xslt that transforms the XML to a human-readable tabular form if opened in a web browser, looking similar to the report document itself. Additionally, some CSS files for formatting the text will be saved. Finally, an XML schema file (lt_logstyle.xsd) which contains the structure definition of the logging XML file will be created in the same directory.


Figure 406. Simulation report document showing details in a new page.

Important: If the Optical Setup has not been simulated in the current VirtualLab Fusion session, the Simulation Report is not available. Reports are not stored with the Optical Setup.

### 43.6.9 Create New Parameter Run

## Availability

Toolboxes: All

## Accessible:

- Ribbon: Optical Setup > New Parameter Run
- Optical Setup Editor: Tools > Create New Parameter Run

This tool provides the simulation of an existing Optical Setup within a Parameter Run ( $\leftrightarrows$ Sec. 44). This allows the modification of one or more parameters of the optical setup and the evaluation of all included detectors in the Optical Setup.
For the generation of a Parameter Run, the Optical Setup has to be consistent.
If at least one parameter run is already open, the new parameter run obtains the view settings and (if possible) the parameter(s) to vary from the last opened parameter run.

### 43.6.10 Create New Parametric Optimization

## Availability

Optical Setups: All but Light Shaping Optical Setup

## Accessible:

- Ribbon: Optical Setup > New Parametric Optimization
- Optical Setup Editor: Tools $>\mathbb{\mathbb { E }}$ Create New Parametric Optimization

If the Optical Setup is consistent, a parametric optimization document ( $\hookrightarrow$ Sec. 102.1) can be opened using this Optical Setup Tool.

### 43.6.11 Remove All Lookup Tables

## Availability

Toolboxes: AR/VR/XR Package

## Accessible:

- Optical Setup Editor: Tools > Remove All Lookup Tables

This Optical Setup Tool deletes all lookup tables for all grating regions with real gratings ( $\hookrightarrow$ Sec. (c)) for all light guide components.

### 43.6.12 Update Add-ons in Detectors

## Availability

Optical Setups: All that contain a Universal Detector ( $\leftrightarrows$ Sec. 74.4 ) with at least one snippet based Detector Add-on ( $\hookrightarrow$ Sec. 74.4.5).

## Accessible:

- Ribbon: Layout Tools > Update Add-ons in Detectors

This tool updates all predefined Detector Add-ons in all Universal Detectors in the current Optical Setup. Predefined refers to all snippet based add-ons which have the same name as an Add-on provided by Wyrowski Photonics. Update means that the snippet is copied from the downloaded version of the add-on. It is recommended to keep the downloaded add-ons up-to-date by either clicking on the Add-ons tab a Universal Detector or by clicking Detectors > Apply Detector Add-on > Update Predefined Add-ons if a Data Array or Chromatic Fields Set is open. The values of the parameters of the add-on are kept while updating.

### 43.7 Parameter Overview Tree



Figure 407. The parameter overview tree which allows you to set new values for the given parameters.

This docking tab page ( $\hookrightarrow$ Sec. 4.3) provides you with quick access to most numerical parameters of all Optical Setup Elements. It contains the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | Only parameters containing the given string or being in a category matching <br> the given string are shown. The matching is case insensitive. It is possible <br> to search for multiple words and word groups embraced by quotation marks, <br> for example: "surface \#1" scaling. |
| \{Tree View\} | Shows all parameters matching the current filter string. You can navigate <br> through the tree with the arrow keys and Page Up and Page Down. You can <br> expand / collapse nodes using + , * and $\square$. |
| New Value | Shows the value of the currently selected parameter and allows you to change <br> it (if it is not a coupled parameter, $\hookrightarrow$ Sec. 43.10$).$ If the value is valid and <br> different from the original value, you can submit it to the Optical Setup with <br> the Enter key or the $\leftrightarrows-b u t t o n . ~$ |

You can move between the controls with the Enter key. The Optical Setup Element or linkage currently selected in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1) is highlighted.
Sec. 43.6.1 describes a similar tool which allows you to set multiple parameters at once but within a separate dialog.
The available parameters are explained in Sec. 43.5.

### 43.8 Positions

The details of the positioning concept for Optical Setups can not be presented here extensively. So this section gives a short overview but you can learn more about the concepts of coordinate systems and positioning via a supplemental file available upon request.
An Optical Setup is associated with a global coordinate system (GCS), while every Optical Setup Element (OSE) owns two or three kinds of coordinate systems (CS):

1. Internal Coordinate System (ICS): Unambiguously specified coordinate system which is related to the inner structure of the OSE. Its origin is identical to the position of the element within the global coordinate system.
2. (Referring) Input Coordinate System (InCS, components and detectors only): The z-axis of this coordinate system defines the typical input direction of light. The position of the origin and the orientation of the $x$ and $y$-axes are related to the structure of the OSE ( $\hookrightarrow$ Sec. 43.8.1).
3. Reference Output Coordinate Systems (OutCS, components and light sources only): The z-axis of an output coordinate system defines the typical direction for a special kind of output (e.g. transmission type or reflection type). The position of the origin and the orientation of the $x$ - and $y$-axes are related to the structure of the OSE ( $\hookrightarrow$ Sec. 43.8.1).

Usually, the positioning of Optical Setup Elements is done by defining the relative position and orientation of the $\operatorname{InCS}$ with reference to the output CS of the previous Element in path. This principle is shown in the sketch below ( $\hookrightarrow$ Fig. 408) and explained in Sec. 43.8.2.


Figure 408. Principle of positioning of Optical Setup Elements. The blue coordinate system is the output CS of the previous element while the green one indicates the input CS of the element to position. Its origin is translated by the axial distance $\Delta Z$ and a lateral shift $\Delta X$. Its orientation is rotated by $\eta$, which means a rotation of the OSE about the $y$-axis. The red coordinate system is the Internal CS of the element.

An alternative workflow is the positioning of Optical Setup Elements by defining the absolute position and orientation of either the InCS or the ICS with reference to the global coordinate system (GCS). The GCS is defined by the position and orientation of the currently active light source element.

### 43.8.1 Element Internal Definition of Axes, Coordinate Systems, and Reference Points

All information about the definitions of axes, coordinate systems and reference points can be got and (in some cases) set via the Coordinate Systems page ( $\hookrightarrow$ Fig. 409) of each Optical Setup Element's edit dialog.


Figure 409. Page selector for information about axes, coordinate systems and reference points of Optical Setup Elements.

### 43.8.1.1 Internal Coordinate System

The Internal Coordinate System (ICS) is related to the inner structure of the OSE. Its position and orientation relative to the geometry of the element are shown in the panel Internal Coordinate System. Furthermore, the geometrical parameters are described here. For an example see Fig. 410.
The position of the origin of the ICS in relation to the global coordinate system of the Optical Setup gives the absolute position of the element ( $\hookrightarrow$ Sec. 43.8.2).


Figure 410. Example (Spherical Lens) for the Internal Coordinate System panel with the description of the geometrical parameters.

### 43.8.1.2 Reference Points

Although the orientations of the input and output coordinate systems are either fixed or calculated automatically, the internal position (i. e. referring to the ICS) of these coordinate systems can be chosen by the user from a list of reference points in order to have a great flexibility for the relative positioning ( $\hookrightarrow$ Sec. 43.8.2). These points are distinguished points of the element's structure which could come into consideration to serve as a reference for distance measurements. For a spherical lens, for instance, these are the vertices, the intersections of the principal planes with the symmetry axis, and the center of the lens. The list of all reference points of an element is shown in the panel Reference Points. For an example see Fig. 411.

| Intemal Coordinate System | Reference Points | Reference Coordinate Systems |
| :--- | :--- | :--- |



Figure 411. Example (Spherical Lens) for the Reference Points panel with the description of all reference points.
The Programmable Component allows to define new reference points by the user, see Sec. 61.3.

### 43.8.1.3 Reference Coordinate Systems

The information of all reference coordinate systems are given in the panel Reference Coordinate Systems $(\hookrightarrow$ Fig. 412). Here you can see the orientation and meaning of the input coordinate system and of each output CS. Furthermore you can set the origin to one of the reference points.


Figure 412. Example (Spherical Lens) for the Reference Coordinate System panel with the description of the coordinate systems.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Coordinate System | Which coordinate system shall be shown? |
| Default Position of Coor-  <br> dinate System The sketch shows the position and orientation of the CS in relation to the <br> element's structure. Note: Only a sample position is shown, that means <br> there will be no update if the reference point is changed! <br> Origin <br> Point) ${ }^{\text {PE }}$$\quad$ (Reference Select the reference point which provides the position of the origin of the <br> reference CS here. For grating components illuminated by an ideal plane <br> wave, the reference point of the input coordinate system cannot be set. For <br> the grating cells diffuser component no reference points can be set at all. |  |

Note: Since the Programmable Component allows to define new reference coordinate systems, the edit control is completely different for Programmable Components ( $\rightarrow$ Sec. 61.3).

### 43.8.2 Positioning of Optical Setup Elements

All information about the position and orientation can be get and (in most cases) set via the Position / Orientation page (Fig. 413) of each Optical Setup Element's edit dialog.


Figure 413. Page selector for information about position and orientation of Optical Setup Elements.

### 43.8.2 1 Basic Principles of Positioning

There are two modes of positioning for Optical Setup Elements which can be combined:

1. Basal Positioning: The basal positioning influences the positions of all of these Optical Setup Elements whose location and orientation refer to the current element.
2. Isolated Positioning: The isolated positioning of an element has no consequences for the position of any other Optical Setup Element. It is always applied additionally (i.e. after) doing the Basal Positioning.


Figure 414. Principles of positioning.
a) The original positions of the three elements I, II and III. Element I is the reference element for element II, and at the same time, this is reference element for III.
b) If the position of II is changed by increasing $r_{1}$ to $r_{1}^{\prime}$ using Basal Positioning, the absolute position of element III is changed too. This is due to the fact that the relative distance $r_{2}$ is kept.
c) In contrast, a distance value of $\Delta r_{1}$ using Isolated Positioning shifts the element II (additionally to its basal positioning) without changing the position of the following element III.

If both modes of positioning are used for the same element, its resulting position and orientation are calculated by the consecutive application of basal positioning first, followed by the isolated positioning.
Please note: For the simulation of an Optical Setup, always the position and orientation which results from the described combination of both principles will be used.

### 43.8.2.2 Basal Positioning

The relative positioning of an Optical Setup Element is done by defining a translation and a rotation of the element's referring input coordinate system ( $\operatorname{InCS}$ ) in relation to the reference output coordinate system (OutCS) of the Optical Setup Element it is linked to ( $\hookrightarrow$ Fig. 408). The origin of the InCS is translated from the origin of the reference OutCS via a distance $\Delta Z$ on the $z$-axis of the OutCS and a lateral shift ( $\Delta X, \Delta Y$ ) perpendicular to that z-axis. This information can be entered in the control shown in Fig. 415. Furthermore, it contains a control for defining an inclination or rotation which can be used for certain types of elements and that is explained in detail in Sec. 5.6.


Figure 415. Control for determining the basal position and orientation of an Optical Setup Element.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Enter Absolute Position- <br> ing Data | Clicking this button will open an edit dialog where absolute position and ori- <br> entation for the element can be entered. |
| Reference Element | Optical Setup Element that serves as reference for positioning. It is identical <br> to the previous element in the path. |
| Reference Output Coordi- <br> nate System | The name of that output coordinate system (OutCS) of the Reference Element <br> which defines the reference for the relative distances and angles. |
| Delta Z $\mathbf{Z V}^{\text {Pv }}$ | Distance to the reference element, measured on the z-axis of the OutCS. <br> (This means the z-component of the distance vector from the OutCS origin to <br> the InCS origin.) |
| Delta $\mathbf{X}^{\text {PV }}$ | Shift of the element in x-direction, lateral to the z-axis of the OutCS. (This <br> means the x-component of the distance vector from the OutCS origin to the <br> InCS origin.) |
| Delta $Y^{\text {Pv }}$ | Shift of the element in y-direction, lateral to the z-axis of the OutCS. (This <br> means the y-component of the distance vector from the OutCS origin to the |
| InCS origin.) |  |

The absolute positioning of an Optical Setup Element is done by defining a translation and a rotation of the element's input coordinate system (InCS) or the elements internal coordinate system (ICS) in relation to the global coordinate system GCS of the Optical Setup. It can be entered after clicking the button Enter Absolute Positioning Data, which opens the dialog explained in Sec. 43.8.2.4.

### 43.8.2 $\mathbf{3}$ Orientations of Optical Setup Elements

In many cases, the orientation of an Optical Setup Element can be set freely.
There are several ways to define the orientation of an Optical Setup element which are all equivalent ( $\hookrightarrow$ Sec. 139.2). Each of these conventions uses some rotations, applied to the input coordinate system InCS, referring to the reference output coordinate system OutCS. The rotation is centered around the origin of the InCS as pivotal point, in any case. This ensures that the translation values (z-distance and lateral shift in $x$ and y) will be kept independent from the orientation.

The control for defining an orientation is described in Sec. 5.6.

### 43.8.2.4 Positioning Control

An alternative way to edit the basal position of an element is to use the positioning control of the Optical Setup Element in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1 and Fig. 416).


Figure 416. The positioning control in the Optical Setup View.
The layout of the control can be configured via the Optical Setup View's context menu. The following menu items refer to the positioning control:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Show Position Controls | The visibility of the positioning controls can be set here. |
| Show Only z-Positions | If checked, only the z-Positions of the elements are shown. This menu item is a shortcut to the more detailed advanced option described below. |
| Advanced Position Control Settings > Show Absolute Positions if Possible | If checked, absolute positions and orientations are shown if available. (Which will be not the case for detectors.) The absolute values are red colored. Relative values are blue. |
| Advanced Position Control Settings > Info for Internal CS / Info for Input CS | If Show Absolute Positions if Possible is chosen, this selection determines whether the absolute positioning information is shown for the internal coordinate system ICS or the input coordinate system InCS. |
| Advanced Position Control Settings > Include Isolated Positioning | If checked, the basal as well as the isolated positioning information will be shown. If unchecked, only the basal positioning information will be shown. In the latter case, the values will be written in an italic font. |
| Advanced Position Control Settings > z-Position Only / Position Only / Position \& Orientation / NonZero Values Only | The display mode for the control. It determines how much information will be shown. |

If one of the display modes is chosen which doesn't show all information (i.e. z-Position Only or Position Only), the control will indicate whether or not there are non-zero values hidden. If there are non-zero $x$ - or $y$-translation values which are not visible in z-Position Only mode, the symbol ${ }_{+}$indicates that there is hidden information. If there are non-zero orientation values which are not visible in z-Position Only or Position Only mode, the symbol $*$ indicates that there is hidden information.

There can also be hidden information in case of isolated positioning. Whether or not the shown values include isolated positions or orientations is indicated by the font as shown in Fig. 417.

| $X: 0 \mathrm{~m}$ <br> $Y: 0 \mathrm{~m}$ <br> $Z: 5 \mathrm{~mm}$ | $X: 0 \mathrm{~m}$ <br> $Y: 1 \mathrm{~mm}$ <br> $Z: 5 \mathrm{~mm}$ |
| :--- | :--- | | $X: 0 \mathrm{~m}$ |
| :--- |
| $Y: 0 \mathrm{~m}$ |
| $Z: 5 \mathrm{~mm}$ |

Figure 417. A regular font (left hand side example) indicates that no isolated positioning has been used. An underlined font (center example) indicates that the shown values represent the combined resulting position of isolated and basal positioning. If the font is italic (right hand side example), the basal position is shown only, despite there is an isolated positioning given and effective in the simulation.

Another indicator is shown in Fig. 418. It appears if the shown value is rounded. If so, hovering the mouse cursor over the control will open a tooltip giving the exact values. Please note: This feature has to be activated in the Global Options Dialog ( $\hookrightarrow$ Sec. 6.5).


Figure 418. The indicator for rounded values.

A single click on the positioning control opens the dialog shown in Fig. 419.


Figure 419. Dialog for editing the basal Optical Setup Element position and orientation via external position control.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition Type | This allows to define whether the position and orientation represent relative <br> or absolute measurements. |
| Measurement from | The reference coordinate system to be used. |
| ...to | The referring coordinate system to be defined here. |
| $\mathbf{X / Y / Z} \mathbf{Z}^{\text {PV }}$ | The basal translation of the element as described above (Sec. 43.8.2.2, <br> where the values are named Delta $X / Y / Z)$. |
| Reference Point to <br> Used as Center Point | The pivotal point for the rotations which specify the orientation. |
| Orientation Angles | The basal orientation of the element can be specified here, as described in |

### 43.8.3 Isolated Positioning of Optical Setup Elements

The isolated positioning of Optical Setup Elements cannot be set for Light Sources or DetecTORS.
Sometimes, one may want to vary the position or the orientation of a single Optical Setup Element without change of the absolute positions and orientations of the following elements whose distances refer to this element. In this case the variation has to be done as isolated positioning. The functionality is shown in Fig. 414c. Basal and isolated positioning may be combined. The basal one is always applied first.
There are two different kinds of isolated positioning possible: Isolated translation and isolated orientation. At first, it has to be chosen which kind of isolated positioning shall be done, this selection is made via the control shown in Fig. 420. If isolated translation and isolated orientation shall be done, here the order of these two steps can be defined too.


Figure 420. Control to activate isolated positioning.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Use Isolated Translation | If checked, isolated translation positioning is activated and the corresponding <br> parameters can be entered ( $\hookrightarrow$ Sec. 43.8.3.1). |
| Use Isolated Orientation | If checked, isolated orientation positioning is activated and the corresponding <br> parameters can be entered ( $\hookrightarrow$ Sec. 43.8.3.2). |
| Order of Steps | If set to 1: Translation $->$ 2: Orientation, isolated translation positioning is <br> done before isolated orientation positioning. If set to 1: Orientation $->$ <br> 2: |
|  | Translation, isolated orientation positioning is done before isolated translation <br> positioning. |

### 43.8.3.1 Isolated Translation

Isolated translation positioning means dislocation of the element via translation from its former position, determined by basal positioning. The translation vector is defined via the control shown in Fig. 421.


Figure 421. Control to define the isolated translation values and directions.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Axes Selection | Here the coordinate system can be selected in which the translation vector is <br> defined. The selectable entries depend on the kind of Optical Setup Element <br> which is edited. |
| Axes | Pushing this button will open an information window that displays the direc- <br> tions of the selected coordinate system axes in reference to the internal co- <br> ordinate system of the element. |
| Delta $\mathbf{X} / \mathbf{Y} / \mathbf{Z}^{[\mathbf{P V}}$ | These values define the vector which will be used for the isolated translation. |

### 43.8.3.2 Isolated Orientation

Isolated orientation positioning means dislocation of the element via rotation, referring to its former orientation, which already has been determined by basal positioning. This rotation is defined via the control shown in Fig. 422.


Figure 422. Control to define the isolated orientation values and rotation center points.

## DESCRIPTION

Reference Point to be Here the center point for the rotation that defines the isolated orientation can Used as Center Point ${ }^{[P E}$ be selected. The selectable entries depend on the kind of Optical Setup Element which is edited.

Isolated Orientation An- This control ( $\hookrightarrow$ Sec. 5.6) is used to define the angles which determine the gles ${ }^{\text {PE }}$ isolated orientation.

### 43.8.3.3 (Absolute) Position Information about an Optical Setup Element

The absolute position of an element in an Optical Setup is measured in the Global Coordinate System (GCS) of the Optical Setup. This is identical with the Internal Coordinate System of the currently active Light Source element.
All information about the absolute position and orientation of an Optical Setup Element can be found in the control shown in Fig. 423.


Figure 423. Control that shows the absolute position and orientation of an Optical Setup Element.

ITEM

## DESCRIPTION

Show Basal Position and If selected, the absolute position information is calculated from the basal posiOrientation Only tion only. So one can see the position and orientation all other referring Optical Setup Elements will use. Important: This mode is for information purpose only. Every simulation will use the combined basal and isolated positioning.

| Show Result of Basal and <br> Isolated Positioning | If selected, the absolute position information is calculated from the basal po- <br> sition as well as the subsequent isolated positioning. So one can see the <br> position and orientation as it will be used during the simulation. |
| :--- | :--- |
| Position of Origin > of In- <br> ternal CS / of Input CS | This selection determines for which CS the values $X, Y$, and $Z$ are given for. |
| Position of Origin > X/Y/Z | Position of the origin of the internal coordinate system or the input coordi- <br> nate system (depending on the corresponding selection) of the element in <br> the global coordinate system. |
| Inclination / Rotation | The orientation of the element's internal coordinate system, given via the Ori- <br> entation Definition Type currently selected. For more information about these <br> definition types and the associated angles please see Sec. 139.2.1. |

### 43.9 Channel Configuration

A surface can be illuminated from the front (along the optical axis) or from behind (against the optical axis). Furthermore light can be reflected or transmitted. In consequence there are four ways light can take on a surface:

| CHANNEL | DESCRIPTION |
| :--- | :--- |
| $\boldsymbol{+ / +}$ | Light comes from the front and is transmitted through the surface. |
| $+/-$ | Light comes from the front and is reflected at the surface. |
| $-/-$ | Light comes from behind and is transmitted through the surface. |
| -/+ | Light comes from behind and is reflected at the surface. |

As you can see the channels refer to the sign the z-component of the direction vector of the incident and outgoing light has, respectively.


Figure 424. The table for setting the propagation channels. Here light coming from the front and transmitted through the component is taken into account as well as light reflected at the respective outermost surfaces.

The Channel Configuration tab page of Real and Ideal Components contains a table ( $\hookrightarrow$ Fig. 424) where you can configure which propagation channels are taken into account in case manual channel configuration is set ( $\hookrightarrow$ Sec. 43.3.1). In this way you can avoid that unnecessary light paths are calculated and so make the simulation faster.
If there are two or more surfaces there is an additional row All Surfaces where you can change the configuration of all surfaces at once.
For certain components certain channels might be unavailable. For example ideal mirrors have no transmission channels. In case of pre-selected channel configuration, the complete table is read-only.
For a light guide component you can configure the propagation channels in more detail in the edit dialog of the grating regions ( $\hookrightarrow$ Sec. 42.1).

### 43.10 Parameter Coupling

This expert tool allows you to define dependencies of selected Optical Setup parameters on others via a snippet. Changing the independent parameter leads to a change of the value of the dependent parameters, hence referred to as coupled parameters.
For any Optical Setup, you can switch on or off this mechanism via the Optical Setup > Ese Parameter Coupling ribbon item or via the Property Browser. If parameter coupling is switched on, you can edit it via the Optical Setup > Edit Parameter Coupling ribbon item. The resulting edit dialog is explained in the subsection Sec. 43.10.1.

Note that any changes on coupled parameters in the Optical Setup are ignored as their value depends on the independent parameters. The effects of parameter coupling are explained in detail in subsection Sec. 43.10.2.

### 43.10.1 Edit Dialog for the Parameter Coupling



Figure 425. The edit dialog for parameter coupling showing the Parameter Specification page.

The edit dialog for the parameter coupling ( $\hookrightarrow$ Fig. 425) is a wizard with 4 pages:

1. The Welcome page giving you a short introduction.
2. The Parameter Specification page where you can setup the parameters to be used as input or output of the coupling snippet. ( $\hookrightarrow$ Sec. 43.10 .1 .1)
3. The Snippet Specification page where you define the snippet which does the actual parameter coupling. ( $\hookrightarrow$ Sec. 43.10.1.2)
4. The Summary Page which gives an overview of all coupled parameters you have added to the output dictionary of your snippet. Furthermore it gives for each coupled parameter the value it has if the snippet is executed with the current Optical Setup configuration.
Furthermore at the bottom of the edit dialog there is a validity control ( $\checkmark$ Sec. 5.10 ) which shows current misconfigurations (invalid snippet and alike).
This dialog is resizable.

### 43.10.1.1 Parameter Specification page

This page comprises a table with the following columns.

| COLUMN | DESCRIPTION |
| :---: | :---: |
| \{Unnamed\} | The first column allows you to collapse / expand all parameters of an Optical Setup Element or its building blocks. Simply click on the $\square$ and $\mp$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*). |
| Object | The object to which the shown Parameters belong. |
| Category | Allows further grouping of the parameters. For example the surface or medium to which the parameter belongs. |
| Parameter | Name of the parameter. |
| Use in Snippet | In this column you can select which parameters are available in the snippet - either as input or as output parameters or as both. |
| Short Name | The user can define a short name for the parameter which is used in the snippet. It can be an arbitrary non-empty string, but it must be unique. The short name proposed by VirtualLab Fusion is the Parameter name ${ }^{1}$ - or the last part of it if the parameter name contains multiple parts separated by a ' $\mid$ '. Thus the proposed short name might not be unique. |

This table contains all parameters made available by Parameter Extraction ( $\leftrightarrows$ Sec. 43.5) but integer values like the number of sampling points.
The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensitive. |
| Show Only Used Parame- <br> ters | Only rows where the Use in Snippet column is checked pass this filter. |

### 43.10.1.2 Snippet Specification page

On the Snippet Specification page you see the following controls:

[^8]| ITEM | DESCRIPTION |
| :--- | :--- |
| Edit | Opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ) to edit the actual coupling snippet. <br> The source code editor is the same as described in Sec. 7.3 with the only <br> difference that it has a additional region on its Source Code tab ( $\hookrightarrow$ Fig. 426 ) <br> where you see the short names of all parameters you have selected on the <br> Parameter Specification page. These short names can be used as keys for <br> the input and output dictionary, respectively, by double-clicking on them. |
| Validity | Shows whether the snippet is syntactically correct ( $\hookrightarrow$ Sec. 5.10 ). For exam- <br> ple if you use non-existing short names in your snippet the syntax is correct <br> and this validity indicator shows no issues. However, the snippet is never- <br> theless inconsistent and cannot be evaluated correctly. This kind of error is <br> shown by the "global validity indicator" at the bottom of the form only. <br> If you have defined Global Parameters in your snippet you can set them at <br> the bottom of this page. $\hookrightarrow$ Sec. 7.4 |
| \{Global Parameters\} |  |



Figure 426. The Source Code tab of the source code editor for Parameter Coupling. Note the list of short names in the lower right corner. Double-clicking on an entry in this list copies it to the current cursor position in your source code.

### 43.10.2 Effects of the Parameter Coupling

The parameter coupling has the following effects:

- During each simulation of the Optical Setup, the coupled parameters are calculated according to the current configuration of the Optical Setup (especially the current value of those parameters used as input of the coupling snippet).
- Changes in the Optical Setup can make the Parameter Coupling invalid, for example if you delete an element which contains a parameter used in the coupling snippet. In this case Optical Setup simulations are no longer possible, you have to first adapt the Parameter Coupling via its edit dialog - or switch it off via the ribbon item Optical Setup $>$ Ese Parameter Coupling.
- You can still edit the coupled parameters via the edit dialogs of the Optical Setup Elements and the Definition of Basal Position and Orientation dialogs ( $\rightarrow$ Sec. 43.8.2.4). However, if you close such a dialog with OK, the coupled parameters you have just changed are reset and a warning is shown. Coupled parameters in other dialogs are adapted to your changes without further notice.
- There are various places with a parameter specification table similar to that of the Parameter Coupling dialog: Parameter Overview ( $\lrcorner$ Sec. 43.6.1), Parameter Run ( $\hookrightarrow$ Sec. 44), Polarization Analyzer ( $\neg$ Sec. 87), Parametric Optimization ( $\leftrightarrows$ Sec. 102.1), and Export to optiSLang ( $\leftrightarrows$ Sec. 124.1.1).
- In all these places, coupled parameters are grayed out as their actual values are determined by the coupling snippet. You cannot change anything for them.
- In all these places but the Polarization Analyzer, the General Parameters (single values, vectors, arrays, ...) of the coupling snippet are available as additional parameters.

Fig. 427 shows an example.

- Also in the Parameter Overview Tree ( $\leftrightarrows$ Sec. 43.7) the coupled parameters are grayed out and read-only.
- Coupled Parameters are not exported to the parameters.xml file generated by the batch mode export ( $\rightarrow$ Sec. 9) or optiSLang export, respectively.
- In the result table of the Parameter Run or the Parametric Optimization, the values of the coupled parameters are logged per simulation step.

| $12 \cdot$ | Light Path Element | Category | Parameter | Value |
| :---: | :---: | :---: | :---: | :---: |
| - | Global Parameters of Coupling Snippet |  | Factor | 1 |
|  | Ideal Plane Wave \#0 |  | Wavelength (Coupled Parameter) | 532 nm |
|  |  |  | Weight | 1 |

Figure 427. The effect of Parameter Coupling in a parameter specification table (here: Parameter Overview).
First line: General Parameter of the coupling snippet
Second line: Coupled parameter (grayed out)
Third line: "Normal" parameter

### 43.11 Specific Optical Setups

Despite the General Optical Setup (which can be opened e.g. via the New button in the Start ribbon) there are some optical setups available which support specific components with specific propagation operators.
Grating, Laser Resonator, Light Guide, and Light Shaping Optical Setups require the corresponding package ( $\hookrightarrow$ Sec. 1).

### 43.11.1 Grating Optical Setup

Via the menu items below Start > Gratings you can obtain preconfigured Optical Setups containing the following Optical Setup Elements:

- Ideal Plane Wave ( $\rightarrow$ Sec. 51.7)
- A grating component ( $\varsigma$ Sec. 64). Depending on the selected menu item this grating component contains a preconfigured stack with the actual grating.
- Two Raw Data Detectors ( $\leftrightarrows$ Sec. 74.5.5) for reflected and transmitted light, respectively
- Grating Order Analyzer ( $\varsigma$ Sec. 84)

If needed, further analyzers can be added in the resulting Optical Setup View.
For the propagation to the detectors a special Rayleigh expansion propagation ( $\leftrightarrows \mathrm{Sec} .93 .8$ ) is used to adapt for the periodic nature of the gratings.
The following restrictions apply to Grating Optical Setups.

- Optical Setup Elements but the analyzers cannot be deleted. The two detectors can be switched on and off by deactivating the linkages leading to them.
- The detectors are always parallel to the grating component. Thus isolated orientation of the grating component is disabled.
- The position of the grating component cannot be changed. For detectors, only the z-position can be changed.


### 43.11.2 Laser Resonator Optical Setup

For analyzing laser resonators an Optical Setup is required. This can be generated from the main window via Start > Laser Resonators > Laser Resonator Optical Setup or via the session editor that is available from Start > Laser Resonators > Laser Resonator Session Editor.
The Optical Setup will contain already the eigenmode analyzer that is not available in other Optical Setups. In this type of Optical Setup, only this eigenmode analyzer can be processed.
It can be configured similar to other types of Optical Setups. However, an element from the section High Reflective (Start) Mirrors has to be used as first element. In that category, ideal plane and spherical mirrors, the stored mirror function, and the double surface component.

There are some restrictions for building up a valid resonator system in VirtualLab Fusion. These restrictions are:

- The last element of the resonator has to be chosen from the category Outcoupling Mirrors. This category contains an ideal plane, an ideal spherical and an ideal micro-structured mirror. Next to these mirrors the user can select a double surface component or a programmable component for the element used for out coupling.
- Reflection type reference coordinate systems are admissible for ideal plane or ideal spherical mirrors only.

A special component for a Laser Resonator Optical Setup is the Laser Crystal. The Laser Crystal can be used stand alone as start and end element in a valid system definition for a laser resonator.

[^9]Figure 428. The tree of the Optical Setup View for a Laser Resonator Optical Setup.

Detectors that are used in the Optical Setup are computed once at the end of the eigenmode computation. For that, the fundamental mode that has been computed is used.

### 43.11.3 Light Guide Optical Setup

A Light Guide Optical Setup always contains a Light Guide component ( $\leftrightarrows$ Sec. 57.2) to which you can add a restricted selection of light sources, components, and detectors. The Uniformity Detector ( $\hookrightarrow$ Sec. 74.6.8) is specific for this kind of Optical Setup.
For a Light Guide Optical Setup always manual channel configuration ( $\hookrightarrow$ Sec. 43.9) is used.

### 43.11.4 Light Shaping Optical Setup

Via the menu item Start > Light Shaping > Light Shaping Light Shaping Optical Setup with Grating / Prism / Mirror Cells you obtain a preconfigured Optical Setup containing the following Optical Setup Elements:

- Far Field Source ( $\hookrightarrow$ Sec. 52.2)
- Plate ( $\hookrightarrow$ Sec. 63) labeled as Light Shaper
- Camera Detector ( $\hookrightarrow$ Sec. 74.5.2) which can be used either for the transmission type or the reflection type reference coordinate system and
- Local Linear Grating Analyzer ( $\leftrightarrows$ Sec. 90) for grating cells light shaper

Start > Light Shaping > Light Shaping Optical Setup opens an empty Optical Setup which can be configured as Light Shaper. In any such Optical Setup the user can add any real optical component to the system, but it has to be ensured that the output of the system is always a Camera Detector which has one active connection to a light shaping component.
Light shaping component and Camera Detector must be parallel. Thus isolated orientation of the light shaping component is disabled and the Camera Detector cannot be rotated.
All Simulation Engines ( $\checkmark$ Sec. 43.4) but Classic Field Tracing can be used. For General Profile the special Cells Array Propagation ( $\hookrightarrow$ Sec. 93.9) is used to reduce the numerical effort after the light shaping component.

## 44 Parameter Run

The Parameter Run document allows you to run several Optical Setup simulations ( $\hookrightarrow$ Sec. 43), whereas for each iteration one or more parameters have a different value. The results of the distinct Optical Setup simulations are shown in a special table which allows further analyses. The variable parameters are listed in Sec. 43.5. There are three steps in using the Parameter Run document which can be performed with the Next button.

1. Define the parameter sets to be used for the distinct Optical Setup simulations ( $\hookrightarrow$ Sec. 44.2).
2. Set up the detecting devices whose results you want to analyze ( $\leftrightarrows$ Sec. 44.4).
3. Start the parameter run and analyze its results ( $\hookrightarrow$ Sec. 44.5). Only for this step the Parameter Run $>$ $\nabla$ Go! ribbon item is enabled.
The Show button shows either the original, unmodified Optical Setup or the Optical Setup with the parameters of a certain iteration step.
You can save the parameter run via the File menu or the Start ribbon tab. A newly opened parameter run derives its settings from the last activated parameter run, including the settings of the Combined Outputs ( $\hookrightarrow$ Sec. 44.5.1) and the parameter to vary if applicable.

## Handling of Obsolete Parameters

If you load a Parameter Run which has been saved in a previous version of VirtualLab Fusion, there might be some obsolete parameters still present in the parameter specification table. On the other hand, newly added parameters might not yet be available.
If no results have been calculated yet, the parameters are updated automatically. Otherwise, updating the parameters would delete the results. Then or in case the Parameter Run is in Programmable mode, only a warning is shown in both the Messages tab ( $\leftrightarrows$ Sec. 4.3) and the window title (" $\triangle$ Old Parameters ©").
If one of the varied parameters changed, the Parameter Run cannot be configured and simulated anymore. You can only analyze the results or Refresh the document via the ribbon (which deletes the results).

### 44.1 Ribbon of the Parameter Run Document

The ribbon of the Parameter Run document has the following entries:

ITEM
Go!

## DESCRIPTION

Allows you to start the actual parameter run. Only enabled if you are on the Results page of the document window. During the parameter run, the button changes into a Stop button which allows you to stop the calculation.

| After Completion | For long running parameter runs it can be useful if after completion the Parameter Run saves itself and optionally the computer shuts down. This can be defined with this option which is also available in the property browser ( $\leftrightarrows$ Sec. 4.3). <br> If the Parameter Run has not been saved before it is saved at $\{$ Path for User Settings $\} \backslash$ Autosaved Files. The Path for User Settings can be set on the Saving tab of the Global Options dialog ( $\rightarrow$ Sec. 6). Below this combo box the used file name is displayed. <br> Note that Save \& Shutdown Computer can lead to data loss if there are unsaved documents but the Parameter Run for which this option is set. |
| :---: | :---: |
| Refresh | Refreshes the document to use the current set of parameters. Note that this deletes existing results. See also the note on handling of obsolete parameters on page 501. |
| 108 Show Optical Setup | This button has two sub-entries: <br> - Show Initial Optical Setup: Shows the Optical Setup from which the Parameter Run was originally created. This can be invoked directly if the upper part of the Show Optical Setup button is clicked. <br> - Show Optical Setup for Certain Iteration Step...: Shows the Optical Setup with the parameters of a certain iteration step which can be selected in a separate dialog. |
| No Logging During Execution | If you press this button, the results of the individual iteration steps are only written after the parameter run has finished. This improves performance especially in case of many fast iteration steps. If this button is not pressed the results are written as soon as they are available. Note that this button is disabled during an ongoing parameter run and that it can also be changed via the Property Browser. |
| 庿 Create Output from Selection | If you click this button, for each table row of the current selection a combined output is generated as defined by the settings in the matching combined output box ( $\leftrightarrows$ Sec. 44.5.1). During the output creation, the button changes into a Stop Output Creation button which allows you to stop the calculation. Double clicking on a row header is a short cut for selecting this row completely and clicking 略Create Output from Selection. Similarly, double-clicking a single table cell is a short cut for selecting this row and clicking $\overrightarrow{\Delta s}$ Create Output from Selection. It is also possible to generate the combined output out of the current selection via the context menu or the $\overrightarrow{u s}_{\mathbf{s}}$ Create Output from Selection button of the results table. |
| X Delete Results | Simply deletes all already calculated results. This can be useful as Parameter Runs with results can be occupy much RAM or hard disc space. |

### 44.2 Parameter Specification Page

The table on the Parameter Specification page shows you all parameters available for the underlying Optical Setup. You can select which parameters to Vary and the corresponding value ranges.
With these settings you define a "parameter space". There are four modes how the parameter sets for the distinct iterations are determined from this parameter space.

1. Standard Mode: All selected parameters are varied equidistantly from the minimum to the maximum of the specified value range.
2. Programmable Mode: A snippet defines how the parameters are varied.
3. Scanning Mode: The parameter space is fully scanned in equidistant steps.
4. Random Mode: Uniformly distributed random combinations are used. Especially useful for Monte Carlo simulations and tolerance analysis.
Fig. 429 shows an illustration of the different modes for a two-dimensional parameter space. The combo box in the upper part of the Parameter Specification page (Fig. 430) allows you to select this Usage Mode.


Figure 429. Illustration of the different usage modes for the parameter run. A two-dimensional parameter space defined by two parameters $X_{1}$ and $X_{2}$ is shown. Red: Resulting parameter sets for the standard mode. Green: Example how the parameter sets can be generated by a snippet in the programmable mode. Blue: Resulting parameter sets for the scanning mode. Grey: Some randomly generated parameter sets.

> If you change the parameter specification page, the results table is cleared. But if applicable, results from previous runs are kept.
> Example: You start a parameter run varying a Length from 200 mm to 400 mm in 3 steps. After this run has finished you decide that you want to use 4 steps. Then the results for a Length of 200 mm and 400 mm are kept as it is not necessary that they are calculated anew.


Figure 430. The Parameter Specification Page of the Parameter Run Document in Scanning Mode.

The table lists all Parameters of all Objects which can be altered in the parameter run. Often, a Category column is available to group similar parameters.
In the Vary column you must select one or more parameters which you want to alter in the parameter run. For these parameters you can define the value range by setting the start (From) and end (To) value. The default From and To values for all parameters are their absolute minimum and maximum values - you must not enter a value outside of this range. It is possible to enter a To value which is smaller than the From value.
The Steps and the Step Size column are explained in the following subsections, as their meaning depends on the Usage Mode. For your information also the Original Values of all parameters are given.
The first column allows you to collapse / expand all parameters of an Optical Setup Element or its categories. Simply click on the $\square$ and $\ddagger$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*).
The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensi- <br> tive. It is possible to search for multiple words and word groups embraced by <br> quotation marks, for example: "surface \#1" scaling. |
| Show Only Varied Param- <br> eters | Only rows where the Vary column is checked pass this filter. |

### 44.2.1 Notes on Standard Mode

In Standard mode the number of Steps is the same for all varied parameters. The specified value ranges are split into equidistant sub-intervals. If you set Steps to 2 , it means that a simulation is done for the From value and To value, respectively. Instead of setting the number of Steps, you can alternatively set the Step Size. In case of an integer parameter, the step size can become a fractional number, too. In this case the values used for the distinct iterations are rounded to the closest integer.

### 44.2.2 Notes on Programmable Mode



Figure 431. The additional Parameter Specification page for the Programmable Mode of the Parameter Run.

If you have chosen Programmable mode on the Parameter Specification page you can customize the individual steps of the parameter run by programming a code snippet on an additional page ( $\hookrightarrow$ Fig. 431). With this snippet you define array entries parameters [i,j], which mean the value the $i^{\text {th }}$ varied parameter should have in the $j^{\text {th }}$ iteration step. Here, varied denotes a parameter where you have checked Vary on the previous page. Keep in mind that counting starts with zero: The value the second varied parameter should have in the fifth iteration step, for example, is entered in parameters [1, 4]. The following global parameters are available by default:

| ITEM | DESCRIPTION |
| :--- | :--- |
| NumberOfParameters | The number of parameters with checked Vary column on the parameter spec- <br> ification page. |
| NumberOflterations | The number of Steps set on the parameter specification page. |
| MinimumValues | The From values set on the parameter specification page. Index 0 of the array |
| represents the topmost parameter in the table. |  |
| MaximumValues | The To values set on the parameter specification page. Index 0 of the array <br> represents the topmost parameter in the table. |

This additional page has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition | This group box allows you to program the actual code snippet. Edit opens the <br>  <br> Source Code Editor $(\hookrightarrow$ Sec. 7.3$)$ to edit this snippet, and a validity indicator <br> $(\hookrightarrow$ Sec. 5.10$)$ shows whether this snippet is consistent. <br>  <br> In the lower right corner of the Source Code tab of the source code editor there <br> is an additional button Add System Parameter. It opens a dialog where you <br> can enter one or more words to search for one or more specific parameters <br> of the underlying Optical Setup. The search is not case sensitive. When you <br> then press OK, a statement is added at the current cursor position to retrieve <br> the first of the selected parameters as PhysicalValue. (If you change the <br> index in this statement, you can access others of the selected parameters <br> but the first one.) |
| Parameters The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4  |  |

More information about programming can be found in Sec. 7.
After you have set up the snippet, you can verify it on the subsequent Parameter Visualization page $(\hookrightarrow$ Sec. 44.3). It shows a table visualizing the specified parameters array in a more readable form. If you have specified an array entry whose indices are not allowed (e.g. parameters [-1,-1]), the table remains empty. If you have specified a value which is out of the allowed value range (i. e. the default From - To interval) of the corresponding parameter, this value is marked red.

### 44.2.3 Notes on Scanning Mode

In Scanning mode each parameter can be varied with its own number of Steps. The specified value ranges are split into equidistant sub-intervals. All possible parameter combinations are calculated which means that the overall number of iterations is the product of the number of steps for each parameter.
If you set Steps to 2 for a certain parameter, it means that the From value and To value, respectively, are taken into account. Instead of setting the number of Steps, you can alternatively set the Step Size.
In case of an integer parameter, the step size can become a fractional number, too. In this case the values used for the distinct iterations are rounded to the closest integer.

### 44.2.4 Notes on Random Mode



Figure 432. The available settings for the random mode

In Random mode the number of Steps is the same for all varied parameters. For this mode the following settings are available ( $\hookrightarrow$ Fig. 432):

## ITEM

## DESCRIPTION

## \{Distribution drop down\}

The values distributed randomly within the specified parameter ranges can follow one of the following distributions

- Uniform Distribution: All values of the specified parameter ranges have the same probability.
- Normal Distribution: The values follow a Gaussian normal distribution. Note that this distribution is defined for an infinite value range and thus some values might be out of the actual parameter range. How many values are out of the parameter range depends on the width of the normal distribution which can be configured with the setting The parameter range corresponds to.
- Cutoff Normal Distribution: Same as Normal Distribution with the difference that if a value would be outside the specified parameter range, a new random number within the parameter range is generated.
Fig. 433 shows an example of the various distributions.
Set Seed Manually (to) Always a fixed seed is used with which the generation of the random numbers starts. If you check this option, you see the used Seed which then you can alter if you want to use another random number distribution.

The parameter range corresponds to

Only for Normal Distribution and Cutoff Normal Distribution With this setting you can specify how broad the normal distribution is relatively to the parameter ranges defined by the user. If you keep the default value of 3 , then the parameter ranges correspond to the $3 \sigma$ interval of the normal distribution, i.e. $99.73 \%$ of all values are within the parameter ranges.


Figure 433. Histogram of 5000 values distributed randomly in the range $-1 \ldots+1$.
Left: Uniform Distribution, middle: Normal Distribution, right: Cutoff Normal Distribution. For Normal Distribution and Cutoff Normal Distribution, the range of $-1 \ldots+1$ corresponds to $-2.5 \sigma \ldots+2.5 \sigma$.

### 44.3 Parameter Visualization Page

This page simply shows the value of each varied parameter in each iteration of the Parameter Run. Invalid entries (especially resulting from wrong snippets in Programmable Mode) are marked red.
Note that if you enter this page, iterations having exactly the same varied parameters are merged into one. In this case you see fewer iteration steps than you have specified in the Parameter Specification Page $(~ \rightarrow$ Sec. 44.2) and a warning is shown. This mechanism speeds up further calculations.
With Ctrl] $+\mathbb{C}$ you can copy the currently selected cells to the Windows ${ }^{\text {TM }}$ clipboard. With the Show Physical Units option of the property browser ( $\leftrightarrows$ Sec. 4.3) you can convert all values to their respective base unit and omit all units. For example, " 1 nm " will then be shown as " $1 \mathrm{e}-9$ " and " $180^{\circ}$ " will be shown as " 3.1416 ". This simplifies using the copied values in external programs.


Figure 434. The Parameter Visualization page if three parameters are varied randomly.

### 44.4 Detecting Devices Specification



Figure 435. The Detecting Devices Specification Page of the Parameter Run Document.

On this page you can select one or more detecting devices whose results you want to analyze. It is ensured that at least one detecting device is selected. It has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Ray Results Profile | This check box allows you to check or uncheck both Detectors [Rays] and System: 3D at once. It is marked as $\square$ if only one of these two options has been selected. |
| Detectors [Rays] | If checked the detectors specified in the detector table (see below) are used for this profile. |
| System: 3D | If checked a 3D view of the rays propagating through the Optical Setup is generated for each iteration. $\hookrightarrow$ Sec. 17.1 |
| General Profile | This check box allows you to check or uncheck both Detectors [General] and Modeling Analyzer at once. It is marked as $\square$ if only one of these two options has been selected. |
| Detectors [General] | If checked the detectors specified in the detector table (see below) are used for this profile. |
| Modeling Analyzer | If checked the modeling analyzer ( $\hookrightarrow$ Sec. 43.4.6) is executed for each iteration. |
| \{Detector Table\} | Lists all available detectors ( $\hookrightarrow$ Part XI). You can select which detectors shall be evaluated. If you click on the Open button of any detector, the corresponding edit dialog is displayed. |
| \{Analyzer Table\} | Lists all available analyzers ( $\hookrightarrow$ Part XII). You can select which analyzers shall be evaluated. If you click on the Open button of any analyzer, the corresponding edit dialog is displayed. |
| Classic Field Tracing | If you check this option, the selected detectors are also analyzed with Classic Field Tracing. |
| Validity | This control ( $\hookrightarrow$ Sec. 5.10) checks that at least one detector has been selected and warns if the current configuration might be other than intended. |

Note that depending on context not all of these controls might be visible. For example the analyzer table vanishes if there are no analyzers in the Optical Setup.

If you change the Detecting Devices page, the results table is cleared.

### 44.5 Results Page



Figure 436. The layout of the results table. In this example three iteration steps were calculated where the wavelength is varied from $1 \mu \mathrm{~m}$ to $3 \mu \mathrm{~m}$ and the weight is varied from 1 to 3 at the same time.

The $\quad$ Go! button starts the parameter run. After clicking, the button changes into a $\square$ Stop button which allows you to stop the calculation. Then the Stop button becomes a $\downarrow$ Go! button again which allows you to continue the calculation later. The Parameter Run ribbon tab contains a button with the very same functionality.
In the upper right corner you can see and change the number of parallel iterations ( $\hookrightarrow$ Sec. 6.15) for this Parameter Run. In case distributed computing is activated ( $\hookrightarrow$ Sec. 8), you see the number of clients and can activate their configuration here.
The parameter run fills a table where the results of each Optical Setup simulation are shown in a separate column. Each detector is shown in a single row. If a detector consists of several sub-detectors (e.g. the beam parameters detector, $\hookrightarrow$ Sec. 74.6.1), their results are shown in separate rows. The columns are sorted ascending by iteration number and the rows are sorted numerically by the index of the detector and then alphabetically. Thus the position of a certain result can change while new results are being calculated. During calculation the table always scrolls to the most recent result. The table layout is illustrated in Fig. 436.
The varied parameters per iteration step are shown in separate rows at the top of the table.
The number of shown digits can be changed via the Number of Digits setting in the property browser. The Format of Complex Numbers can also be changed there. The default values of both settings are taken from the Global Options dialog ( $\hookrightarrow$ Sec. 6.5).
You can select a subset of all results by clicking on the column or row headers or by directly selecting a cell range. This selection can be copied to the Windows ${ }^{\text {TM }}$ clipboard via the context menu or the shortcut Ctrl + C. With the Show Physical Units option of the property browser ( $\hookrightarrow$ Sec. 4.3) you can convert all values to their respective base unit and omit all units. For example, " 1 nm " will then be shown as " $1 \mathrm{e}-9$ " and " $180^{\circ}$ " will be shown as "3.1416" (if Number of Digits is set to 5). This simplifies using the copied values in external programs. By default the rows are sorted alphanumerically by the Detector and the Subdetector. Using the Sort Rows option of the property browser ( $\hookrightarrow$ Sec. 4.3) you can ensure that the same order as on the Parameter Specification page is used.
The Combined Output column contains a control to configure the Combined Output for each row separately. This control and which combined outputs are available is explained in Sec. 44.5.1. Additionally, the following controls are available:

\begin{tabular}{|c|c|}
\hline ITEM \& DESCRIPTION <br>
\hline Create Output from Selection \& For each table row of the current selection a combined output is generated as defined by the settings in the matching combined output box ( $\rightarrow$ Sec. 44.5.1). This button has the same functionality as the corresponding ribbon button ( $\rightarrow$ Sec. 44.1). <br>
\hline Use Already Calculated Results for Next Run \& If you check this checkbox, already calculated results are kept for the next parameter run simulation. To ensure that this caching mechanism is used as often as possible, this checkbox is checked again after each simulation. <br>

\hline Filter Rows by \& | Applies a search string to the table. Only rows matching the given string are shown, whereas the following rules apply: |
| :--- |
| - The search is not case sensitive, i.e. lens, Lens, and LENS yield the same results. |
| - It is possible to search for multiple words and word groups embraced by quotation marks. Rows containing at least one of these words or word groups in any of their cells are shown. |
| - A - in front of a word or word group means 'not', e. g. -lens shows all lines not containing 'lens'. |
| - Expressions in quotation marks are searched as entered. For example ${ }^{\prime}-2.5$ ' ' searches for the number -2.5 , not for rows not containing 2.5. And '`Lens System' ' searches for rows containing directly "lens system", not for rows containing "lens" or "system". | <br>

\hline
\end{tabular}

### 44.5.1 Combined Outputs

There are different types of parameter run results (e. g. physical values, harmonic fields (sets), or data arrays). Out of a one-dimensional selection of such parameter run results (that is a table row), various combined outputs can be derived. Combined Output means that the distinct parameter run results are plotted over the iteration parameter $\xi$. Because of this the combined output has always one dimension more than the individual parameter run results. For example out of several one-dimensional results $f(x)$ a two-dimensional combined output $f(\xi, x)$ is obtained ( $\hookrightarrow$ Fig. 437). The only exception from this rule is that you can plot single physical values into two-dimensional data arrays if there are exactly two varied parameters.


Figure 437. Two-dimensional Data Array as combined output for one-dimensional fields. Here the iteration parameter is the distance behind a lens.

Usually the iteration parameter is the Iteration Step (= the column headers). But if only one parameter is varied and you do not create a combined output for this varied parameter, then the iteration parameter is the varied parameter itself. With the option Always Plot versus Iteration Step in the Property Browser you can enforce that always the Iteration Step is used as iteration parameter. In the combined output the results are sorted by the iteration parameter.
The available types of combined outputs are summarized in the following table.

| COMBINED OUTPUT | DESCRIPTION |
| :---: | :---: |
| Data Array <br> (For physical values) | Combined output where the physical values are plotted on the y-axis versus the iteration parameter on the x-axis. Does not work for single physical values. <br> If there are exactly two varied parameters you can also select other more understandable types of data arrays as output, $\hookrightarrow$ Sec. 44.5.1.1. |
| Harmonic Fields Set <br> (For harmonic fields) | All selected (member) fields (of a harmonic fields set) are simply placed into one harmonic fields set. |
| 2D Data Array <br> (For one-dimensional harmonic fields) | For each value of the varied parameter (plotted along the $x$-axis), the field values are plotted along the $y$-axis. In case of harmonic fields sets, one subset per mode is created. <br> Further information and an example for this combined output can be found in Sec. 44.5.1.2. |
| Animation <br> (For two-dimensional harmonic fields) | Either the selected field quantities or the light view of the selected twodimensional harmonic fields (sets) are shown as an animation ( $\hookrightarrow$ Sec. 20). Further information for this combined output can be found in Sec. 44.5.1.3. |
| Animation <br> (For 2D / gridless data arrays or corresponding sets of data arrays) | Shows the selected subsets of the selected data arrays as an animation ( $\leftrightarrows$ Sec. 20). <br> Further information for this combined output can be found in Sec. 44.5.1.4. |


| 1D / 2D / Gridless Data Array <br> (For 1D / 2D / gridless data arrays or corresponding sets of data arrays) | This combined output offers two modes: either all subsets are merged into a single data array which might require interpolation and embedding of the data. The other mode is that the subsets are put into different data arrays of a Set Of Data Arrays so that no interpolation is necessary. Furthermore you can choose which subsets are considered (and which data arrays for Sets of Data Arrays). <br> Further information for this combined output can be found in Sec. 44.5.1.5. |
| :---: | :---: |
| 2D Data Array <br> (For 1D data arrays) | For each value of the varied parameter (plotted along the x -axis), the values of the resulting 1D data array are plotted along the $y$-axis. Different subsets in the original data arrays become different subsets in the resulting data array. The resulting data array inherits the interpolation from the original data arrays. <br> In case the size of the original data arrays differs from iteration to iteration, the set of coordinates of the resulting array will be a union of the coordinate sets of all original arrays. The data of the source data arrays will be interpolated to this new grid. Usually, this merge mode will lead to a non-equidistant coordinate grid, but no data will be lost since all of the original data points will be kept. |
| 1D / 2D Chromatic Fields <br> Set <br> (For 1D / 2D Chromatic Fields <br> Sets) | All selected Chromatic Fields Sets are added incoherently to a new Chromatic Fields Set. |
| 2D Chromatic Fields Set <br> (For 1D Chromatic Fields Sets) | For each value of the varied parameter (plotted along the $x$-axis), the values of the resulting 1D Chromatic Fields Set are plotted along the $y$-axis. <br> All original Chromatic Fields Sets must have the same sampling which can be achieved by configuring the detector generating these Chromatic Fields Sets accordingly ( $\leftrightarrows$ Sec. 74.1.1). |
| Animation <br> (For two-dimensional Chromatic Fields Sets) | For each selected Chromatic Fields Set a bitmap is generated according to the settings in the edit dialog ( $\leftrightarrows$ Sec. 44.5.1.6) of the combined output. Each of these bitmaps then becomes one frame of the final animation. |
| Animation (For Order Collections) | For each Order Collection a bitmap is generated according to the settings in the edit dialog ( $\varsigma$ Sec. 44.5.1.7) of the combined output. Each of these bitmaps then becomes one frame of the final animation. |
| Animation (For Ray Distributions) | For each Ray Distribution a bitmap is generated which resembles the actual document view ( $\rightarrow$ Sec. 17). Each of these bitmaps then becomes one frame of the final animation. <br> You can set the view settings applied to the Ray Distribution document prior to the conversion into a bitmap using the dialog described in Sec. 17.2.3. |
| Ray Distribution (For Ray Distributions) | All Ray Distributions are merged into a single Ray Distribution as separate modes. |
| Single Documents <br> (For harmonic fields \& data arrays) | The selected documents are just shown as separate document windows. This combined output is always used if only a single document is to be shown. For harmonic fields (sets) the settings of the Raw Data Detector which generated these fields are used. |

In the Combined Output column of the results table, there is a control where you can select one of the combined outputs suitable for the results in that column. If the currently selected combined output has specific options, they can be changed via a $/$-button.

### 44.5.1.1 Data Array Combined Output for Physical Values and Two Varied Parameters.



Figure 438. The edit dialog for the combined output of physical values if exactly two parameters are varied.

If there are exactly two varied parameters plotting the physical values in a somehow two-dimensional data array is far more understandable than plotting them in a simple one-dimensional data array.
Thus in this case you can open a dialog ( $\hookrightarrow$ Fig. 438) to select the output type most appropriate for your needs.
Fig. 439 shows an example of the various output types.





Figure 439. The various output types for physical values. In this example both wavelength and polarization angle were varied for a grating and the efficiency of the zeroth transmitted order is shown. From left to right: Plot All Data on One Axis, 1D Multigraph, 2D Gridded, and 2D Gridless.

The edit dialog has the following options.

Plot All Data on One Axis / Separate Varied Parameters along 2 Dimensions

If you select Plot All Data on One Axis, the data is simply plotted versus iteration step into a one-dimensional data array. This is the kind of output you obtain if there are not exactly two varied parameters. The left-most image of Fig. 439 shows an example for this.
On the other hand, if you select Separate Varied Parameters along 2 Dimensions the data is shown in a somehow two-dimensional data array - how exactly is defined by the Data Array Type and Abscissa setting, respectively.

Data Array Type There are three possibilities how the data can be plotted along 2 Dimensions.

- 1D Multigraph: One varied parameter is taken as abscissa. The other parameter is "stacked" into several subsets. In Multigraph mode ( $\hookrightarrow$ Sec. (b)), which is the default for this output type, you see them as separate data rows. In the second image of Fig. 439 the data is plotted versus wavelength and you see one data row per polarization angle.
- 2D Gridded: The data is plotted in a two-dimensional gridded data array (one parameter plotted on the abscissa, one on the ordinate. This type is appropriate if the data is on a regular grid, i. e. if it was obtained with the scanning mode of the Parameter Run ( $\hookrightarrow$ Sec. 44.2).
- 2D Gridless: The data is plotted in a two-dimensional gridded data array (one parameter plotted on the abscissa, one on the ordinate. This type is more appropriate if the data was not obtained with the scanning mode of the Parameter Run.


#### Abstract

Abscissa Defines which of the two varied parameters is plotted on the abscissa.


If the data was not obtained with the scanning mode of the Parameter Run or not all parameter combinations have been calculated, the data may not be on a regular grid. To create gridded data arrays nevertheless, missing grid positions are filled up with NaNs (= "Not a number"). This applies to the 1D Multigraph and the 2D Gridded type, respectively. In such a case, using linear interpolation is pointless. Thus these data array types are not shown with linear interpolation by default, which you can change later on ( $\leftrightarrows \mathrm{Sec} .11 .2 .1$, Sec. 11.2.2).

### 44.5.1.2 2D Data Array Combined Output



Figure 440. Settings for the 2D Data Array combined output, here in Manual Settings mode.

This combined output creates a two-dimensional data array by plotting the varied parameter along the x-axis and the field values of one-dimensional fields along the y-axis. However, each of the fields to be combined might have its own sampling - which is not allowed for data arrays. Thus the dialog shown in Fig. 440 offers the following ways to unify the field sampling:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Inherit Field Size | All fields are shown with the default number of sampling points and stretched <br> to fill the data array window. This means that all fields are shown completely <br> even if they have very different physical extensions. |
| Manual Setting | Allows you to set Sampling Points, Sampling Distance and / or Array Size of <br> the y-dimension of the resulting data array manually. <br> Only two of these three settings can be changed at the same time. The re- <br> maining property is calculated automatically. |
| Automatic Setting | The y-extension of the resulting data array is Size Factor times the size of <br> the largest harmonic field (in physical coordinates). Size factors larger than 1 <br> just embed the result while size factors between 0 and 1 cut off a part of the <br> result. <br> By default, the default number of sampling points is used to sample the lateral <br> extension. A finer sampling with more sampling points can be defined with a <br> larger Oversampling Factor. |

The default number of sampling points is the number of sampling points as set up in the Global Options dialog (Sampling subcategory, $\hookrightarrow$ Sec. 6.12) for the x-direction.
Fig. 441 shows an example for Inherit Field Size and Automatic Setting.


Figure 441. Propagation of a divergent Gaussian beam, shown with "Automatic" (left) and "Inherit" (right) sampling. For larger beam diameters the amplitude becomes smaller. Thus the beam seems to get smaller in "Inherit" mode.

### 44.5.1.3 Animation Combined Output for Harmonic Fields

| Animation Parameters |  |  | $\times$ |
| :---: | :---: | :---: | :---: |
| View Selection | Image Options | Bitmap Resolution |  |
| View to AnimateLight ViewData View |  |  |  |

Figure 442. Edit dialog for animation combined output.

On the first tab of this dialog ( $\lrcorner$ Fig. 442) you can choose whether you want to see the Light View ( $\hookrightarrow$ Sec. 12.2.1) or the Data View ( $\hookrightarrow$ Sec. 12.2.2) of the fields in an animation. In case of Light View, the real color view is animated if each iteration has at least one visible wavelength. Otherwise the linear intensity view is animated. In case of Data View, you can configure on the Image Options ( $\hookrightarrow$ Sec. (a)) tab which field quantities are to be shown in which way.
In both cases you can adjust the sampling on the Bitmap Resolution ( $\hookrightarrow$ Sec. (b)) tab.
(a) Image Options Tab

An animation is a sequence of individual bitmap images ( $\checkmark$ Sec. 20). The controls of this tab ( $\leftrightarrows$ Fig. 443) determine how these individual bitmap images are created from the given harmonic fields.

ITEM
DESCRIPTION

| Use Twin Image Repre- <br> sentation | If checked, each bitmap image is composed of two images side by side, which <br> are created from the same field using different color mapping settings (see <br> below). |
| :--- | :--- |
| Set Options for Image | With this item, available if the check box Use Twin Image Representation is <br> enabled, the part of the image (Left or Right) can be chosen for which the <br> options shall be edited. |
| Color Mapping | The controls within this group are used for several dialogs and are therefore <br> described in Sec. 5.11 in detail. If you create an animation of a phase distri- <br> bution, an analytical spherical phase radius is ignored. |



Figure 443. Image options for animation combined output.

## (b) Bitmap Resolution Tab

This tab page ( $\hookrightarrow$ Fig. 444) determines the resolution of the resulting bitmaps. It offers three ways to define the field sampling:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Inherit Field Size | All fields are shown with the default number of sampling points and stretched <br> to fill the animation view. This means that all fields are shown completely <br> even if they have very different physical extensions. |
| Manual Setting | Allows you to set Pixels, (physical) Pixel Size and / or (physical) Bitmap Size <br> manually. <br> Only two of these three settings can be changed at the same time. The re- <br> maining property is calculated automatically. |
| Automatic Setting | The shown bitmap size is Size Factor times the size of the largest harmonic <br> field (in physical coordinates). Size factors larger than 1 just embed the result <br> while size factors between 0 and 1 cut off a part of the result. <br> By default, the default number of sampling points is used. A finer sampling <br> with more sampling points can be defined with a larger Oversampling Factor. |

The default number of sampling points is two times the number of sampling points as set up in the Global Options dialog (Sampling subcategory, $\hookrightarrow$ Sec. 6.12).

| Animation Parameters |  | $\times$ |
| :---: | :---: | :---: |
| View Selection Image Options | Bitmap Resolution |  |
| Input Mode Inherit Field Size Manual Setting Automatic Setting |  |  |
| $\square$ Pixels | $256 \times$ | 256 |
| $\square$ Pixel Size | 5 mm x | $5 \mu \mathrm{~m}$ |
| $\square$ Bitmap Size | $1.28 \mathrm{~mm} \times$ | 1.28 mm |
| Ok | Cancel | Help |

Figure 444. Bitmap resolution settings for animation combined output.

### 44.5.1.4 Animation Combined Output for Data Array and Sets of Data Arrays

This combined output allows you to show selected subsets of selected data arrays as frames of an animation ( $\leftrightarrows$ Sec. 20 ). To this end, the individual subsets are interpolated and filled up with zero values so that all subsets have the same coordinate range with the same sampling. The subsets are sorted so that all subsets of the first data array are shown first, then all subsets of the second data array and so on.


Figure 445. Settings for animation combined output.
The edit dialog of this combined output ( $\hookrightarrow$ Fig. 445) has the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| All Data Arrays / Single Data Array | Only for Sets of Data Arrays <br> With the Single Data Array option you can choose the index of one specific data array for which the animation is generated. Otherwise All Data Arrays are shown. $\hookrightarrow$ Sec. 44.5.1.5 |
| All Subsets / Single Subset | With the Single Subset option you can choose the index of one specific subset for which the animation is generated. Otherwise All Subsets are shown. $\hookrightarrow$ Sec. 44.5.1.5 |
| Field Quantity | Defines the field quantity to be shown in the resulting animation. Only has an effect if the input data arrays are complex-valued. |
| Aspect Ratio | The aspect ratio of the resulting animation is determined in different ways: <br> - True to Physical Scale: The aspect ratio is determined from the ratio of the $x$-axis range of the data array to its $y$-axis range. This option is not available if the two coordinate axes have different physical properties. <br> - User-Defined: If you choose this option you can define a suitable aspect ratio. For example you can use 16:9 to ensure that the animation (and a video possibly generated out of it via File > Export) looks nicely on matching monitors or projectors. For gridded data arrays the default user-defined aspect ratio is calculated from the number of data points in the data array. <br> - Free: You can set Width and Height of the single bitmaps as you want. |
| Width / Height | The width and height of the resulting bitmaps. If the Aspect Ratio is not Free and you change one dimension, then the other dimension is always changed automatically. |
| Scale Frames to | - Common Value Range: The global minimum and maximum value of all subsets is used to scale the color table. As a result you can see in which subsets there are smaller values then in others. <br> - Individual Value Range: The color table for each frame is adapted to the minimum and maximum value of the individual data. As a result all subsets use all colors of the color table. <br> - User-Defined Value Range: The user can enter the minimum and maximum value which is used to scale the color table. |

### 44.5.1.5 Data Arrays Combined Output for Data Array and Sets of Data Arrays

This combined output offers two modes:

1. All subsets are merged into a single data array. Because all subsets must have the same coordinate range with the same sampling, the individual subsets are interpolated and filled up with zero values if necessary. This is the same behavior as for the appending manipulation of data arrays ( $\hookrightarrow$ Sec. 24.5.2).
2. The subsets are put into different data arrays of a Set Of Data Arrays so that no interpolation is necessary. (If Sets of Data Arrays are combined, the subsets of one data array remain in one data array.)

The dialog shown in Fig. 446 also allows you to define that either one specific subset is taken from each iteration, or all subsets. In the same manner, you can define for Sets of Data Arrays that either one data array is taken from each iteration, or all data arrays.


Figure 446. The edit dialog for Sets of Data Arrays with gridded data arrays.


Figure 447. Control for entering the desired data array or subset index. With the arrow buttons you can decrease / increase the index by one. The control also shows the maximum index you can set.

| ITEM | DESCRIPTION |
| :--- | :--- |
| All Data Arrays | OnLY FOR SETS of DATA ARRAYS. <br> If you choose this option, all data arrays are used for the combined output. |
| Single Data Array | OnLY FOR SETS of DATA ARRAYS WITH THE SAME NUMBER OF DATA ARRAYS. <br> If you choose this option, one specific data array is extracted from the Set of <br> Data Arrays result of each iteration. You can set the index of the data array <br> to extract via entering it directly into the control shown in Fig. 447 or by using <br> the arrow buttons in said control. |
| All Subsets | If you choose this option, all subsets are used for the combined output. <br> OnLY IF ALL DATA ARRAYs HAVE THE SAME NUMBER of SuBSETS. <br> If you choose this option, one specific subset is extracted from each data <br> array. You can set the index of the subset to extract via entering it directly into <br> the control shown in Fig. 447 or by using the arrow buttons in said control. |
| Data Array | Not FOR GRIDLESs DATA ARRAYs <br> In this case you obtain one single Numerical Data Array as combination result <br> which contains all the data in separate subsets. The data is interpolated and <br> embedded as described in Sec. 24.5.2. The order in that data arrays is as <br> follows: First come all subsets from the first data array from the first teration, <br> then all subsets from the second data array of the first iteration and so on. |
| Set of Data Arrays | In this case you obtain one single Set of Data Arrays as combination result. <br> The first data array of this document contains all subsets from the first data <br> array from the first iteration, the second data array contains all subsets from <br> the second data array from the first iteration and so on. In this way no data <br> needs to be resampled. |

An example illustrating the effect of the settings explained above: Assume we have 7 iterations. In each iteration a Set of Data Arrays with 3 data arrays is created; each data array has 2 subsets. Then you obtain the following results.

|  | DATA ARRAY AS COMBINATION RESULT | SET OF DATA ARRAYS AS COMBINATION RESULT |
| :---: | :---: | :---: |
| All Data Arrays, All Subsets | Data Array with 42 subsets | Set of Data Arrays with 21 data arrays, each having 2 subsets |
| All Data Arrays, Single Subset | Data Array with 21 subsets | Set of Data Arrays with 21 data arrays, each having 1 subset |
| Single Data Array, <br> All Subsets | Data Array with 14 subsets | Set of Data Arrays with 7 data arrays, each having 2 subsets |
| Single Data Array, <br> Single Subset | Data Array with 7 subsets | Set of Data Arrays with 7 data arrays, each having 1 subsets |

### 44.5.1.6 Animation Combined Output for 2D Chromatic Fields Sets



Figure 448. Edit dialog of the Animation Combined Output for two-dimensional Chromatic Fields Sets.
In the edit dialog of the Animation Combined Output for two-dimensional Chromatic Fields Sets ( $\hookrightarrow$ Fig. 449) you can set the following:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Real Color / False Color | Allows you to set the color mode ( $\varsigma$ Sec. 14.2) used for the bitmap generation. <br> In Real Color wavelengths out of the visible range are shown black. |
| \{Color Table Button\} | Only for False Color mode. <br> Allows you to select the color table ( $\leftrightarrows$ Sec. 11.2.4). |
| All Wavelengths / Single Wavelength | Either All Wavelengths of the shown Chromatic Fields Up are summed in the resulting bitmap. Or you can select the index of the Single Wavelength to be shown either via the arrow buttons or by entering it directly. |
| Aspect Ratio | The aspect ratio of the resulting animation is determined in different ways: <br> - True to Physical Scale: The aspect ratio is determined from the ratio of the $x$-axis range of the data array to its $y$-axis range. This option is not available if the two coordinate axes have different physical properties. <br> - User-Defined: If you choose this option you can define a suitable aspect ratio. For example you can use 16:9 to ensure that the animation (and a video possibly generated out of it via File > Export) looks nicely on matching monitors or projectors. For gridded data arrays the default user-defined aspect ratio is calculated from the number of data points in the data array. <br> - Free: You can set Width and Height of the single bitmaps as you want. |
| Width/Height | The width and height of the resulting bitmaps. If the Aspect Ratio is not Free and you change one dimension, then the other dimension is always changed automatically. |
| Scale Frames to | - Common Value Range: The global minimum and maximum value of all subsets is used to scale the color table. As a result you can see in which subsets there are smaller values then in others. <br> - Individual Value Range: The color table for each frame is adapted to the minimum and maximum value of the individual data. As a result all subsets use all colors of the color table. <br> - User-Defined Value Range: The user can enter the minimum and maximum value which is used to scale the color table. In Real Color mode zero values always correspond to black. Thus you cannot set the minimum value. |

### 44.5.1.7 Animation Combined Output for Order Collections



Figure 449. Edit dialog of the Animation Combined Output for Order Collections.

In the upper part of the edit dialog of the Animation Combined Output for Order Collections ( $\hookrightarrow$ Fig. 449) you can define which coordinates are used to plot which data of the individual orders. In the lower part you can define properties of the resulting bitmaps.
In detail:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Coordinate Type | The coordinates versus which the individual orders are plotted: either the order numbers, the spherical angles $\theta$ and $\phi$, the Cartesian angles $\alpha$ and $\beta$, the wave vector components $k_{x}$ and $k_{y}$, or the position $(x ; y)$. |
| Data to Show | Allows to set whether the efficiencies or certain Rayleigh coefficients ( $E_{x}, E_{y}$, $\left.E_{z}, \mathrm{TE}, \mathrm{TM}\right)$ of the orders are shown. |
| Field Quantity | If you want to show Rayleigh coefficients, you must also select which part of its complex value is to be shown. |
| Selection Strategy | With this option you can restrict the shown orders. The following three strategies are available: <br> - AII: No restrictions apply <br> - Above Efficiency Threshold: Only (propagating) orders above the given Efficiency Threshold are shown. <br> - Order Range: All orders in the range between Minimum Order (inclusive) and Maximum Order (inclusive) are shown. <br> Note that evanescent orders are only shown if order numbers or wave vector components are used as Coordinate Type. |
| Largest Dimension in Pixels | Either height or width (whatever is larger) of the resulting bitmaps in pixels. |
| Dot Size <br> Scale Each Bitmap Individually | The size of the dots representing the orders in pixels. <br> If checked each bitmap uses the complete color range defined by the Color Table. Otherwise a global scaling is applied so that you can see e. g. brightness differences between different bitmaps. |
| Color Table | If you click on this button you can select the color table to be used. |
| Background Color | The color used for those regions of the bitmap where no dots are drawn. |

### 44.6 Iteration Document

The Eigenmode Analyzer ( $\hookrightarrow$ Sec. 89) generates iteration documents which simply consist of the Results page of the parameter run document ( $\hookrightarrow$ Sec. 44.5). It has the following ribbon entries:

ITEM DESCRIPTION

| $>\mathrm{Go}$ | Allows you to start the actual iteration. While the iteration is in progress, the button changes into a $\square$ Stop button which allows you to stop the calculation. |
| :---: | :---: |
| After Completion | For long running iterations it can be useful if after completion the Iteration Document saves itself and optionally the computer shuts down. This can be defined with this option which is also available in the property browser ( $\leftrightarrows$ Sec. 4.3). <br> If the Iteration Document has not been saved before it is saved at \{Path for User Settings\}\Autosaved Files. The Path for User Settings can be set on the Saving tab of the Global Options dialog ( $\rightarrow$ Sec. 6). Below this combo box the used file name is displayed. <br> Note that Save \& Shutdown Computer can lead to data loss if there are unsaved documents but the Iteration Document for which this option is set. |


| 图Show Optical Setup | Shows the Optical Setup from which the Iteration Document was originally created． |
| :---: | :---: |
| No Logging During Execution | If you press this button，the results of the individual iteration steps are only written after the complete iteration has finished．This improves performance especially in case of many fast iteration steps．If this button is not pressed the results are written as soon as they are available．Note that this button is disabled during an ongoing iteration and that it can also be changed via the Property Browser． |
| Create Output from Selection | If you click this button，for each table row of the current selection a combined output is generated as defined by the settings in the matching combined out－ put box（ $\rightarrow \mathrm{Sec} .44 .5 .1$ ）．During the output creation，the button changes into a Stop Output Creation button which allows you to stop the calculation． Double clicking on a row header is a short cut for selecting this row completely and clicking $\boldsymbol{\rightarrow} \boldsymbol{*}$ Create Output from Selection．Similarly，double－clicking a sin－ gle table cell is a short cut for selecting this row and clicking $\boldsymbol{\rightarrow} \boldsymbol{*}$ Create Output from Selection．It is also possible to generate the combined output out of the current selection via the context menu or the 路Create Output from Selection button of the results table． |

## 45 LLGA Results Generator

## Availability

Toolboxes：Grating Package
Accessible：Main Window：Start＞Grating＞LLGA Results Generator 即

The Local Linear Grating Approximation（LLGA）approach decomposes an arbitrary structure into a set of simple gratings．For such a set of simple gratings，the LLGA Results Generator can calculate rigorous results （Rayleigh coefficients per order for both $E_{x}$－and $E_{y}$－polarization）by means of the Fourier Modal Method（FMM， $\hookrightarrow$ Sec．96．3）．For each grating to analyze，the LLGA Results Generator requires period，rotation angle，and incident angle of the incoming light．Furthermore it has to know
－the wavelength of the incoming light
－the complex refractive index before and after the gratings and
－the range of diffraction orders for which results shall be calculated
A LLGA Results Generator containing this imported information can be either obtained from the Local Linear Grating Analyzer（ $\hookrightarrow$ Sec．90）or from a matching XML file via Start＞Grating＞LLGA Results Generator．
The results of the LLGA results generator are either added to the imported XML file or written in a new XML file with the same structure．


Figure 450. The document window of the LLGA Results Generator.

Some Additional Grating Parameters needed to build up the grating structure are not part of the imported information but can be specified in the document window of the LLGA Results Generator. This window has the following options.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Grating Type | The assumed type of the gratings. In the moment only sawtooth gratings are available. |
| Number of Height Levels | A continuous height profile is always converted into a quantized one for the FMM. More height levels mean a higher numerical effort of the FMM. <br> If your structure will be fabricated quantized you may enter the fabricated number of height levels. |
| Modulation Depth | The modulation depth of all gratings; i. e. the height difference between lowest and highest height level. |
| Number of Evanescent Orders | The FMM calculates all propagating orders and the specified Number of Evanescent Orders. More evanescent orders lead to more accurate results, but both calculation time and memory consumption increase. The order range specified in the imported information only defines how many orders are written into the resulting XML file. |
| Use TEA Mode for Periods larger than | The computational effort of the FMM increases not only with the number of evanescent orders but also with the number of propagating orders. Thus large periods cannot be calculated well with the FMM. However, the thin element approximation (TEA) is sufficient for large periods (roughly five times the wavelength or larger). Thus TEA instead of FMM is used for periods larger than the given threshold. |
| Keep Already Calculated Results | If the imported XML file already contains some results, you can either choose to calculate all results anew or to Keep Already Calculated Results. Note that the latter should only be used if a calculation was stopped for some reason and you restart it with exactly the same settings. |
| Go! | If clicked the calculations are started and the Go!-button turns into a Stop-button to interrupt the calculations. As the LLGA Results Generator uses a document window you can continue to work with other documents or dialogs during the calculations. |
| $\square^{2}$ (Export) | The $\Gamma^{-3}$ button at the bottom of the dialog can be used to trigger the export of the calculated lookup table into an XML file. The file contains all parameter sets of the lookup table as well as the already calculated results. Attention: For large lookup tables the XML format can result in very large files. |

The LLGA Results Generator calculates the efficiency of the grating cells array during the rigorous evaluation. This efficiency is defined by

$$
\begin{equation*}
\eta^{\text {total }}=\frac{\sum_{s} \sum_{l} \sum_{j} w_{s} \cdot\left|A_{j, l, s}^{\text {before GCA }}\right|^{2} \cdot \eta_{j, l, s}}{\sum_{s} \sum_{l} \sum_{j} w_{s} \cdot\left|A_{j, l, s}^{\text {before GCA }}\right|^{2}} \tag{45.1}
\end{equation*}
$$

using the following input variables

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\eta^{\text {total }}$ | The averaged efficiency of the grating cells array. |
| $\eta_{j, l, s}$ | The efficiency of the first order (working order) for one cell of the grating cells <br> array for one wavelength and one lateral mode. |
| $j$ | The index for all cells of the grating cells array. |
| $l$ | The index of the lateral modes. |
| $s$ | The index of the spectral modes. |
| $w_{s}$ | The weights for the specific wavelength. |
| $A_{j, l, s}$ | The field value of the electric field that hits the specific cell. |

For the evaluation of the efficiency only the first order (working order) is taken into account. The result is logged into the Detector Result tab page of the main window.

## 46 LUT Results Generator

This document type is generated by the Grating Channel Analyzer ( $\hookrightarrow \mathrm{Sec} .91$ ) if the light guides in the optical system contain channels for which rigorous results are still to be calculated. It allows you to continue your tasks while the rigorous calculations are done - or do these calculations on another computer. When the calculations are finished a copy of the original Optical Setup is generated with the calculated rigorous results set to the corresponding grating regions ( $\hookrightarrow$ Sec. 42).


Figure 451. The General tab of the document window of the LUT Results Generator.
The corresponding document window ( $\hookrightarrow$ Fig. 451) has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| \{General tab\} | On this tab you can define whether already calculated results are kept or <br> whether to Clear Lookup Tables before Calculation. Furthermore this tab <br> contains information about the Number of Lookup Tables and the progress <br> of the running calculations. |
| \{Custom  <br> Method $\}$ Fourier Modal | On this tab you can define whether you want to use your own Fourier Modal <br> Method or the one implemented in VirtualLab Fusion. See Sec. 96.4 for de- <br> tails. |
| Go! | If clicked the calculations are started and the Go!-button turns into a <br> Stop-button to interrupt the calculations. As the LUT Results Generator uses <br> a document window you can continue to work with other documents or dialogs <br> during the calculations. |

## 47 Session Editors

Session Editors are wizard documents for specific application scenarios which allow you to set up all needed documents at once. They can be found in Start > Laser Resonators and Start > Diffractive Optics, respectively. Each Session Editor generates a new VirtualLab Fusion Session. Single documents within a Session cannot be closed separately. To close a Session close the Session Editor. To avoid unintended closing of dependent documents, an inquiry dialog is displayed before closing.
If you click Finish in the Session Editor, all necessary documents are generated. If you change the settings in the Session Editor, you have to click Refresh to bring these changes into the dependent documents. It is also possible to change the dependent documents directly.
All documents of a Session can be saved separately.

### 47.1 Annotations for Session Editors in the Diffractive Optics Package

This section contains annotations for certain wizard pages of the session editors in the Diffractive Optics Package.

### 47.1.1 Effect of Coherence and the $\mathbf{M}^{2}$ Value on Beam Splitter and Diffuser Systems

The input beam of a beam splitting or diffusing system is modeled as coherent, monochromatic field with Gaussian amplitude distribution and a beam quality of $\mathrm{M}^{2}=1$. Nevertheless beam splitting and diffuser elements will work also for laser beams with $\mathrm{M}^{2}>1$ or spatially partial coherence. The input beam parameters specified in the session editors are just used for calculation of the spot diameter in the target plane and to check if the distance between the diffraction orders will be larger than the spot diameter. If a laser beam with $M^{2}>1$ should be used the spot diameter in the target plane may be larger than the diameter calculated by the session editor. Please check in this case that the distance between the diffraction orders is larger than the spot diameter of your beam in the target plane.

### 47.1.2 Supported Optical Setups for Beam Splitters and Diffusers

In order to simplify the parameter specification only four different optical setups are supported. Nevertheless the most of the real existing optical systems can be described by one of the idealized setups mentioned below.

- The $\mathbf{1 f}$ - and $\mathbf{2 f}$-setups are containing a lens creating the far field of the diffractive optical element in the focal plane of the lens. The lens is simulated using a lens transmission. The focal length of the lens transmission must be equal to the effective focal length of a real lens or lens system. To simulate the
effect of real lenses after the end of the optimization replace the lens transmission by a real lens or lens system in the resulting Optical Setup.
- The paraxial far field setup assumes a large distance between diffractive optical element and target plane. The light propagation to the target plane is modeled by Fraunhofer diffraction integral. Near field diffraction effects are not considered during the optimization but can be modeled in the resulting Optical Setup.
- Angular spectrum setup allows you to optimize a diffractive optical element creating the desired angular diffraction patterns.

All optical elements in the setups are surrounded by a medium that can be specified together with all other system parameters on the next page. For angular spectrum setup vacuum is always assumed as surrounding medium.

### 47.1.3 Supported Optical Setups for Beam Shapers

In order to simplify the parameter specification only three different optical setups are supported. Nevertheless the most of the real existing optical systems can be described by one of the idealized setups mentioned below.

- The $\mathbf{1 f}$ - and $\mathbf{2 f}$-setups are containing a lens creating the far field of the beam shaping element in the focal plane of the lens. The lens is simulated using a lens transmission. The focal length of the lens transmission must be equal to the effective focal length of a real lens or lens system. To simulate the effect of real lenses after the end of the optimization replace in the resulting Optical Setup the lens transmission by a real lens or lens system.
- The Fresnel setup assumes a large distance between beam shaping element and target plane.

All optical elements in the setups are surrounded by a medium that can be specified together with all other system parameters on the next page.

### 47.1.4 Output Field Parameters for Beam Splitters

The separation of diffraction orders is controlled during the design by the period of the beam splitting element. Depending on the fabrication constraints (pixel size and pixel size increment; see next pages) it is probably not possible to achieve exactly the calculated period of the element. This will lead to small deviations between the desired separation of orders and the practically achieved separation. Both values are displayed on the summary page at the end of the session editor.
An Offset of the desired diffraction orders can be specified on this page. The offset can be for example helpful to separate the zeroth order from the other diffraction orders. A zeroth order may appear because of fabrication tolerances of the surface profile of a diffractive optical element. Please take into account that in case of a height profile with two height levels, a transmission with two phase levels and amplitude-only transmissions always a diffraction pattern symmetric to the optical axis will appear. That means that the offset should be large enough so that all desired orders are shifted above or below the optical axis. Use the Suggest Offset button to get a suggestion for the offset that fulfills this condition.

Since the most diffractive optical elements do not diffract all light into the desired diffraction orders also higher orders will appear (stray light). In order to avoid disturbing effects in the application a Maximum Relative Stray Light Intensity can be specified. Please take into account that very small values could be unrealistic.

### 47.1.5 Output Field Parameters for Diffusers

An Offset of the desired diffraction orders can be specified on this page. The offset can be for example helpful to separate the zeroth order from the other diffraction orders. A zeroth order may appear because of fabrication
tolerances of the surface profile of a diffractive optical element. Please take into account that in case of height profiles with two height levels, transmissions with two phase levels or amplitude-only transmissions always a diffraction pattern symmetric to the optical axis will appear. This means that the offset should be large enough so that all desired orders are shifted above or below the optical axis. Use the Suggest Optional Offset button to get a suggestion for the offset that fulfills this condition.

Since the most diffractive optical elements do not diffract all light in the desired diffraction orders also higher orders will appear (stray light). In order to avoid disturbing effects in the application a Maximum Relative Stray Light Intensity can be specified. Please take into account that very small values could be unrealistic.

### 47.1.6 Output Field Diameter

A rectangular area symmetric to the optical axis is reserved in the target plane for the creation of the desired light pattern. Around this light pattern another rectangular region is used for the distribution of the stray light. The ratio between output field diameter and light pattern diameter is expressed by a Diameter Factor. The output field diameter should be approximately two times larger than the light pattern diameter for continuous DOEs and four times larger than the light pattern diameter for pixelated DOEs in order to reduce the energy loss because of diffraction at rectangular pixels.

Increasing the diameter factor helps to reduce the uniformity error. If a maximum stray light intensity limit was introduced increasing the diameter factor allows to distribute the energy of the stray light over a larger area and helps to reduce the maximum stray light intensity.

The output field diameter is controlled by the feature size of the diffractive optical element. Increasing the output field diameter requires smaller features of the diffractive optical element. Take into account that the feature size can be limited to a minimum value. This will limit the output field size to a maximum value. The manual or automatic selection of the output field size has only an effect if the automatic calculation of pixel size is activated (see later pages). In case of manual adjustment of the pixel size the user is responsible to ensure that sufficiently large output field diameters can be reached by the selected pixel size.

### 47.1.7 Merit Functions for the Iterative Fourier Transform Algorithm

The optimization principle of the Iterative Fourier Transform Algorithm (IFTA) used for optimization of diffractive optical elements differs from other parametric optimization algorithms. Other algorithms often analyze an spread sheet and evaluate the merit functions. In a second step parameters are varied and analysis of spread sheet and evaluation of merit functions is repeated. From the change of merit functions conclusions for further modifications of parameters can be done. The evaluation of the merit functions results is essential for the optimization.
In contrast, the IFTA performs an analysis of the system. It corrects intensity deviations of the output field from the desired output field. This means special constraints will be applied on the output field intensity. In a second step the corrected output field is back propagated in the plane of the diffractive optical element and the element parameters are calculated. Additional constraints must be applied on the element in order to fulfill all fabrication conditions (for example discrete height levels). These two steps are called iteration. All selected merit functions, specifications of the desired output field and specifications of the diffractive optical element are translated as constraints of the output field and the element. Thus an evaluation of the merit functions values is not required.
This means for example achieving a low uniformity error can be done by replacing the real output field intensity by the intensity of the desired output field. Doing this requires not the knowledge of the uniformity error value itself. The maximum relative intensity of stray light can be limited by cutting all intensity values of the stray light that are above a specified limit. Again, the exact value of the merit function is not required for optimization.

Therefore it is not required to evaluate the merit functions values during the optimization. Instead calculation of the values requires additional computational time and will thus reduce the performance of the optimization. The logging of the merit function results can be deactivated using Disable Logging of Merit Functions during Optimization. The optimized Optical Setup will contain detectors and analyzers for evaluation of the merit functions values after optimization.
Seven different merit functions can be used during the optimization of a diffractive optical element and final evaluation. It follows a short overview of available merit functions. The implemented formulas are given in Sec. 137.2.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Window Efficiency | Measures the amount of energy of the input field diffracted in a typically rect- <br> angular or circular signal region in the target plane. The signal region has the <br> shape and the extension of the desired output intensity pattern. The achieved <br> quality of the output field is not considered. This means that for example a <br> lens concentrating all light in the signal region may reach an efficiency of <br> $100 \%$. It is recommended to use the conversion efficiency instead. |
| Conversion Efficiency | Measures the amount of energy of the input field diffracted in a typically rect- <br> angular or circular signal region in the target plane. Any noise in the signal <br> region is ignored. The signal region has the shape and the extension of the <br> desired output intensity pattern. A lens focusing for example all light in the <br> signal region would lead in contrast to the window efficiency to a very low ef- <br> ficiency since the generated spot is typically different from the desired output <br> field and will be considered as noise. |
| Signal to Noise Ratio | The SNR is the ratio between the integral intensity of the output field to the <br> integral intensity of the noise. It is expressed in dB. |
| Uniformity Error | The maximum error of the output field intensity compared to the desired out- <br> put field intensity. The definition is similar to the definition of a contrast. |
| Maximum Relative Inten- | Diffractive optical elements achieve often a conversion efficiency below <br> sity of Stray Light |
| 100\%. This means that not all light is diffracted in the desired output field |  |
| intensity pattern. The remaining light typically appears as stray light around |  |
| tensity | a rectangular or circular signal region in the target plane. This merit function <br> measures the ratio of the maximum intensity of the stray light relative to the |

### 47.1.8 Merit Functions for Refractive Beam Shapers

Five different merit functions can be used for analysis and optimization of a refractive beam shaping element. It follows a short overview of available merit functions. The implemented formulas are given in Sec. 137.2.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Window Efficiency | Measures the amount of energy of the input field diffracted in a typically rect- <br> angular or circular signal region in the target plane. The signal region has the <br> shape and the extension of the desired output intensity pattern. The achieved <br> quality of the output field is not considered. This means that for example a <br> lens concentrating all light in the signal region may reach an efficiency of <br> $100 \%$. It is recommended to use the conversion efficiency instead. |
| Conversion Efficiency | Measures the amount of energy of the input field diffracted in a typically rect- <br> angular or circular signal region in the target plane. Any noise in the signal <br> region is ignored. The signal region has the shape and the extension of the <br> desired output intensity pattern. A lens focusing for example all light in the <br> signal region would lead in contrast to the window efficiency to a very low ef- <br> ficiency since the generated spot is typically different from the desired output <br> field and will be considered as noise. |
| Signal to Noise Ratio | The SNR is the ratio between the integral intensity of the output field to the <br> integral intensity of the noise. It is expressed in dB. |
| Uniformity Error | The maximum error of the output field intensity compared to the desired out- <br> put field intensity. The definition is similar to the definition of a contrast. |
| Maximum Relative Inten- | A beam shaping elements probably does not reach a conversion efficiency <br> of 100 \%. This means that not all light is deflected in the desired output field <br> intensity pattern. The remaining light is typically reflected or appears as stray <br> light around a rectangular or circular signal region in the target plane. This <br> merit function measures the ratio of the maximum intensity of the stray light <br> relative to the mean intensity of the output field within the signal region. |
| sity of Stray Light |  |

### 47.1.9 Transmission Types

Three different types of transmissions are supported. That are:

- An Amplitude-Only Transmission just introduce an amplitude modulation between zero and one to incoming fields. Zero means absorption and one means that light may pass the transmission without change. No phase modulation is allowed. Diffractive optical elements can use for example chromium layers to create an amplitude-only transmission.
- A Phase-Only Transmission creates a phase modulation from $-\pi$ to $+\pi$ without changing the amplitude of an incoming field. Diffractive optical elements with micro structured height profiles can create an phaseonly transmissions.
- A Complex Transmission allows modulation of amplitude and phase of an incoming field. Diffractive optical elements containing a micro structured height profile and additionally a chromium mask can create for example a complex transmission.


### 47.1.10 Period, Pixel Size and Number of Pixels

- The Period of the diffractive optical element is calculated from the angular resolution required for the desired output intensity.
- The Pixel Size of the diffractive optical element is calculated from the maximum deflection angle. This angle follows from the maximum angle of the desired output intensity and an additional frame that is used
for stray light that can not diffracted into the desired intensity pattern. Expert user can set the pixel size to an user defined value but must ensure that the pixel size is small enough to create the desired output intensity with sufficient high quality.
- The Number of Pixels per Period follows just from period and pixel size. Since only an integer number of pixels are allowed the pixel number must be rounded and the period may differ slightly from the optimal value. This rounding leads to small deviation of the output field angular resolution from the desired value. The deviation is displayed on the next page.


### 47.1.11 Import of Arbitrary Input Field

The power weights of the desired diffraction orders of the beam array can be imported from a harmonic field, from an ASCII file or from a bitmap file. Every sampling point in the data file represents one diffraction order. It is typically not necessary to introduce diffraction orders with zero weights in order to generate "free spaces" between the desired orders. These free spaces will result in the later application from illuminating several periods of the diffractive optical element. The weights of the beam array should be specified without a dark frame around the desired diffraction orders. Such a dark frame will be added by the session editor if required.

## Sources: Generating Fields

VirtualLab Fusion provides a growing set of source models. Each model describes an electromagnetic field in a plane. The theoretical background can be found in Sec. 132.
The following chapters explain how to use the generator dialogs, starting with the description of those controls that most source generator dialogs (except that for Stored Fields) have in common. The type specific parameters are described in Sections Sec. 51 and Sec. 52.

## 48 Common Controls of the Source Generator Dialogs

### 48.1 Dialog for Sources in the Optical Setup



Figure 452. Sample edit dialog for light sources in the Optical Setup.

The edit dialogs for light sources in the Optical Setup ( $\hookrightarrow$ Fig. 508) are divided into 3 pages:

- Coordinate Systems $\hookrightarrow$ Sec. 43.8.1
- Position / Orientation $\hookrightarrow$ Sec. 43.8.2
- Source Parameters

The Source Parameters tab is again divided into the following tab pages:

- Basic Parameters $\hookrightarrow$ Sec. 48.1.1
- Specific Parameters; specific for the distinct light sources and thus explained in Sec. 51 to Sec. 52
- Polarization $\hookrightarrow$ Sec. 48.3
- Mode Selection $\hookrightarrow$ Sec. 48.1.2

In the lower left corner of the dialog there are the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| H | Saves the component into the user-defined light sources catalog ( $\rightarrow$ Part V). |
| Validity | This control ( $\leftrightarrows$ Sec. 5.10) indicates whether there are issues with the current configuration. If this is the case you can click on the 国-button for further information. |

### 48.1.1 Basic Parameters



Figure 453. Controls for defining the aperture of the single modes.

On the Basic Parameters tab of the light source dialog ( $\hookrightarrow$ Fig. 453) you can set the aperture of the single modes.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Shape | You can choose whether the single modes have a Rectangular or an Elliptical <br> shape. |
| Size | The size or diameter of the aperture. If the light source determines the aper- <br> ture size automatically, this control is not visible. |
| Relative Edge Width ${ }^{\boxed{P V}}$ | The width of the smoothing edges defined relatively to the lateral extension <br> of the mode. If the extension in $x-$ and y-direction differ, the minimum of both <br> values is taken. |
| Absolute Edge Width ${ }^{\text {PVI }}$ | The width of the smoothing edges in meters ( $\hookrightarrow$ Fig. 454). If the light source <br> determines the aperture size automatically, this control is not visible. |



Figure 454. Definition of the edge width of smoothing edge functions.

For the Panel Type Source ( $\hookrightarrow$ Sec. 52.7.1) the aperture does not change the overall size of the modes. Thus you cannot set a relative edge width of more than $50 \%$ which makes that the whole area of the mode is attenuated by the aperture.

### 48.1.2 Mode Selection



Figure 455. Controls for the selection which wavelengths are to be generated.
On the Mode Selection tab of the light source dialog ( $\hookrightarrow$ Fig. 455) you can set whether All Wavelengths are generated or only a Single Wavelength. In the latter case you can select which wavelength index ${ }^{[\mathrm{Pv}}$ is taken. Furthermore light sources can have their special way of selecting the generated lateral modes. This is explained in the light source specific chapters.

### 48.2 Dialog for Sources in the Main Window

The edit dialogs for sources in the main window (partly also used from within the Optical Setup) have some common controls for all types of source generators.
They define the

- definition of the field via the panel Basic Parameters ( $\hookrightarrow$ Sec. 48.2.1)
- definition of spectral parameters via the panel Spectral Parameters ( $\hookrightarrow$ Sec. 48.2.2)
- definition of the polarization via the panel Polarization ( $\hookrightarrow$ Sec. 48.3)
- selection of (fundamental) modes via the panel Mode Selection ( $\hookrightarrow$ Sec. 48.2.4)
- sampling of the fields via the panel Sampling ( $\hookrightarrow$ Sec. 48.2.5)

The panel Spatial Parameters is type specific, so its contents are described in the corresponding subsections of Sec. 51 and Sec. 52.
The Default Parameters button resets the parameters on all tabs to their default values.

### 48.2.1 Basic Parameters

The panel is shown in Fig. 456 for the selection Automatic Setting. It comprises three parts:

$$
\text { ITEM } \quad \text { DESCRIPTION }
$$

Medium at Source Plane The medium in which the source field is generated. This control is explained in Sec. 34.1.

Source Field: Longitudi- These settings are explained in subsection Sec. 48.2.1.1. nal and Lateral Offset

Input Field: Position, Size These settings are explained in subsection Sec. 48.2.1.2. and Shape


Figure 456. Tab page for setting the basic parameters of a light source.

### 48.2.1.1 Relation between Source Field and Input Field



Figure 457. Effect of a Lateral Offset of $100 \mu \mathrm{~m}$ in x -direction on a Gaussian Wave. The origin of coordinates of the input plane is marked.

We distinguish between the field in the source plane and and the field in the input plane.
By the parameters on the Spatial Parameters tab the field is defined in a certain source plane. For example, this is the waist (plane) for a Gaussian wave.
However, the field put into VirtualLab Fusion by the source dialog might be defined in another plane parallel to the source plane: the input plane.
The group box Source Field: Longitudinal and Lateral Offset allows you to configure the relation between source plane and input plane:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Distance to Input Plane ${ }^{[\mathrm{PV}]}$ | This value describes the distance between input plane and source plane <br> along the z-axis: distance $=z_{\text {Input Plane }}-z_{\text {Source Plane }}$. |
|  | For some of the sources this value is fixed to zero. <br> In the case of spherical and quadratic waves this value must not be zero and <br> the spherical phase radius is set to this value. |
| Lateral Offset ${ }^{[\mathrm{PV}}$ | This value describes the offset between the origins of the coordinates for the <br> source and the input plane. |

Within the Optical Setup the lateral offset specified within this region of the dialog is handled by the usage of coordinate systems.

### 48.2.1.2 Position, Size and Shape of the Input Field

VirtualLab Fusion follows the concept of smooth fields. For physically meaningful fields, jumps in the data should be avoided. Numerically this is achieved by using smoothing edge functions as shown in Fig. 460.


Figure 458. Shifted Gaussian Wave with unchecked Apply Lateral Offset of Source Field.


Figure 459. Shifted Gaussian Wave with checked Apply Lateral Offset of Source Field. Note the larger overall field size.


Figure 460. Definition of the edge width of smoothing edge functions.

The group box Input Field: Position, Size and Shape allows you to define position, size, and shape of this smooth edge in the input plane:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Setting | If checked, a reasonable size (suggested field size) of the field is determined automatically. This option is only available for some light sources, e. g. those defining exponentially decreasing fields. |
| Field Size Factor ${ }^{\text {PV }}$ | The suggested field size is multiplied by this factor for Automatic Setting. |
| Manual Setting | If checked, the field size can be entered by the user. |
| Apply Lateral Offset of Source Field ${ }^{\text {PE }}$ | By default, the resulting input field is centered at the position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ) in the input plane. By checking this box, the field is shifted by the Lateral Offset of the source plane ( $\hookrightarrow$ Sec. 48.2.1.1). Note, the resulting numerical array (sampled field) will still be centered at ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ), so additional zero-values will be generated. An example is given in Fig. 458 and Fig. 459. |
| Shape ${ }^{\text {PE }}$ | The field may be Rectangularly or Elliptically shaped. |
| Diameter ${ }^{[P V}$ | Physical size of the field physical dimension in the input plane. |
| Relative Edge Width ${ }^{\text {[V] }}$ | The width of the smoothing edges defined relatively to the (smaller of the both values of) Diameter. |
| Absolute Edge Width ${ }^{\text {PV }}$ | The width of the smoothing edges, defined in physical units. $\hookrightarrow$ Fig. 460. |

### 48.2.2 Spectral Parameters

At this panel the spectral information for the field has to be defined. In the simplest case, using Power Spectrum Type > Single Wavelength, a single Wavelength ${ }^{\mathbb{P V} \text { can }}$ be defined yielding a monochromatic field. The remaining options, Triplet of Wavelengths and List of Wavelengths, result in polychromatic fields represented by a harmonic field set.
The Weight values are given as intensities, i.e. those values are scaling values for $A^{2}$ of the corresponding fields.
The panel adapts its design to the chosen Type of Power Spectrum. The types Single Wavelength, Triplet of Wavelengths and List of Wavelengths are explained in Sec. 48.2.2.1, Sec. 48.2.2.2, Sec. 48.2.2.3, respectively. The selection Triplet of Wavelengths is a special case of the more general selection List of Wavelengths.

### 48.2.2.1 Single Wavelength



Figure 461. Panel for setting the spectral parameters (Single Wavelength) of a source generator.

Description of parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength ${ }^{[\operatorname{Pv}}$ | The vacuum wavelength. |
| Weight ${ }^{[\mathrm{PV}}$ | The intensity value (scaling of $A^{2}$ ). |
| Preview | Some approximate preview of the resulting color. A wavelength out of the <br> visible range of the spectrum is marked black. |

### 48.2.2.2 Triplet of Wavelengths



Figure 462. Panel for setting the spectral parameters (Triplet of Wavelengths) of a source generator.
Description of the Parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength ${ }^{\text {PE }}$ | The vacuum wavelengths. |
| Weight $^{\text {PV }}$ | The intensity values (scaling of $A^{2}$ ). |
| Preview | Some approximate preview of the resulting color according to the given val- <br> ues. |
| Default RGB Values | Resets the values of the wavelengths and their weights to the default values <br> depending on the current color system (see Sec. 6.7.1), which will result in <br> white light. |

### 48.2.2.3 List of Wavelengths



Figure 463. Panel for setting the spectral parameters (List of Wavelengths) of a source generator.

In this mode you have a table on the upper part of the dialog. There you can change already present data points or delete whole rows. Del deletes the content of the current cell (or the whole row if a complete row is selected). Shift + Del deletes the whole row in any case. This table has four columns:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Index | The mode index. |
| Wavelength | The vacuum wavelengths. |
| Amplitude | The amplitude values for the wavelengths. |
| Phase | The phase values for the wavelengths. |

In the lower part there are some additional buttons:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Add Datapoint | Add a data point to the list of wavelengths. |
| Load from File | Loads the wavelength and weight values from a .txt-file. The format is de- <br> scribed below. |
| Save to File | The wavelength and weight values are saved to a .txt-file. |
| Load from Diagram | The wavelength and weight values are loaded from a diagram. Suitable dia- <br> grams can be generated via the spectrum generators described in Sec. 53. |
| Show Diagram | Shows the wavelength and weight values in a diagram. |

For convenience, the spectral values can be defined also using diagrams or simple text files. An example of the format used for the text files is described below. Comment lines start with '\#', columns must be separated by either spaces, tabs, semicolons, |, or $\&$. The decimal separator must be a period.

```
# Spectrum Data
\begin{tabular}{lll} 
\# Wavelength & Amplitude & Phase \\
\(4.1 \mathrm{E}-07\) & 1 & 0
\end{tabular}
```

4. 5E-07 2
0
4.8E-07
1
0

### 48.2.3 Spatial Parameters

Although this panel is specific to the particular source model, it contains the shared entry Generate Cross Section ( $\hookrightarrow$ Fig. 464).

Generate Cross Section Along X-Axis
Figure 464. Define a 1D simulation by using a cross section.

By checking the box Generate Cross Section, for Classic Field Tracing a 1D cross section (either along x- or $y$-axis) will be generated instead of a 2D field. For the other simulation engines this setting has no effect.

> ITEM DESCRIPTION

Generate Cross Section ${ }^{\text {国 }}$ If checked, a 1D cross section Along X-Axis or Along Y-Axis is generated.

### 48.2.4 Mode Selection

In the case that a spectrum has been defined (more than one wavelength) or that laterally-shifted modes are used (non-coherent simulations), harmonic field sets with several members will be generated. This panel allows to define the number of modes being used for the simulation.
In general, the accuracy of the results increases with the number of modes. However the numerical effort increases as well. So a good compromise has to be found. Additionally, using less modes can already give a good insight into the behavior of optical systems.
The panel allows to define subsets of modes in order to control both accuracy and numerical effort. The spectral values and the laterally-shifted modes are selected independent of each other. However, once a selection of spectral values has been defined, each spectral value will be applied to every lateral mode.


Figure 465. The Mode Selection tab in two different configurations. Left: The mode selection tab for a basic source model having only wavelength modes. Right: The mode selection tab for a partially coherent source with Uniform 2D Grid as Selection Strategy for the lateral modes.

The tab page shown in Fig. 465 is divided into two parts as described below. The first part is the definition of modes. For the definition of the lateral modes several selection strategies are available. The user can also specify the weight function that shall be applied to the lateral modes. The setting for the Definition of Lateral Modes are explained in the following table.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition Strategy | Five strategies are available to define the positions of the lateral modes. They <br> are described below in a separate table. <br> This section is only visible for partially coherent light sources. <br> $(\hookrightarrow$ Sec. 52$)$ |
| Weight Function | You can either use a Constant Weight for all modes or User-Defined Weights <br> per mode. For the latter there is an Edit button which opens a dialog. In this <br> dialog you can define the intensity weights dependent on the lateral position <br> either by programming a snippet ${ }^{\text {DE }}$ or via a data table. See Sec. 5.13 for more <br> details. <br> This section is only visible for partially coherent light sources. <br> $(\leftrightarrows$ Sec. 52$)$ |

The following strategies can be used for the Selection of Lateral Modes.

| SELECTION STRATEGY | DESCRIPTION |
| :---: | :---: |
| Uniform 2D Grid | A uniform rectangular grid of laterally-shifted modes is adjusted to the physical <br>  initial grid is refined by bisection. The Initial Grid Size ${ }^{\text {『v }}$ is $3 \times 3$ modes in Automatic Mode or a user-defined size in Manual mode. |
| Random | The lateral positions of the modes are distributed randomly across the emitting surface. For each consecutive simulation other mode positions are used. You can specify the Number of Lateral Modes ${ }^{\mathbb{D V}}$. |
| Random (seed=0) | The lateral positions of the modes are distributed randomly across the emitting surface whereas for each consecutive simulation the same mode positions are used. You can specify the Number of Lateral Modes ${ }^{\text {DV }}$. |
| User Defined | The user can define the Number of Lateral Modes ${ }^{[\mathbb{V V}}$ and then specify their <br>  and setting up the dialog described in Sec. 5.13. |
| None | Only one lateral mode at the position ( $0 \mathrm{~m} ; 0 \mathrm{~m}$ ) is used. |

The second part of the Mode Selection tab page can be used to select the lateral and spectral modes which shall be used for the simulation. The basis for the mode selection is given by the number of modes specified within the Spectral Parameters tab and the Definition of Lateral Modes group box.
The user can select between different selection strategies to specify which modes shall be used for the simulation. Within this part of the dialog the user can also see several information which allow to get an impression on accuracy and the numerical effort of the current simulation setup.
The following parameters can be accessed within this part of the dialog:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Selection Strategy | This defines the Selection Strategy for selecting certain wavelengths and lateral modes from the full set of modes specified in the Spectral Parameters tab and the Definition of Lateral Modes area on the Mode Selection tab. Four options are available: <br> - Full Set of Spectral and Lateral Modes: All wavelengths given in the Spectral Parameters tab are used. All specified modes will be processed. <br> - Spectral Selection Ordered by Index: The first $n$ wavelengths given in the Spectral Parameters tab are used. $n$ is the Number of Spectral Modes ${ }^{[\mathrm{PV}}$. For each wavelength all lateral modes defined within the above section will be processed. <br> - Spectral Selection Uniform in Index: An algorithm selects $n$ wavelengths which are well distributed across the index range. $n$ is the Number of Spectral Modes ${ }^{\text {DVV }}$. For each wavelength all lateral modes defined within the above section will be processed. <br> - Single Mode Selection: Only one mode is generated by the light source. The user can enter an Index of Spectral Mode and an Index of Lateral Mode to specify which mode shall be generated by the light source. These parameters can be varied within the Parameter Run to perform a complex simulation and reduce the numerical effort (large data may be swapped to hard disc). <br> $n$ is the Number of Spectral Modes. |
| Number of Active Modes | For your information, this section shows the Total Number of Modes which is the product of the Number of Lateral Modes and the Number of Wavelengths. The number of lateral modes again can be the product of the lateral modes for x - and y -direction. Note that the dialog ensures that the Total Number of Modes does not exceed just over 2 billion. |

### 48.2.5 Sampling

The generated field is represented by one or more arrays of sampled data. When using sampled fields, care has to be taken for ensuring that the original fields can always be reconstructed from the sampled fields with sufficient accuracy, that is the Whittaker Shannon theorem[Goo68] has to be taken into account. VirtualLab Fusion provides an automatic sampling mode which takes care of the sampling theorem and suggests corresponding sampling parameters. The user can scale these values or even modify them in the manual mode. The panel is shown in Fig. 466.

| Basic Parameters |  | Spectral Parameters |  |
| :---: | :---: | :---: | :---: |
| Spatial Parameters | Polarization | Mode Selection | Sampling |
| Field Sampling |  |  |  |
| O Automatic Sampling |  |  |  |
| - Manual Sampling |  | Copy Active Parameters from... |  |
| Sampling Points |  | $65 \times$ | 65 |
| O Sampling Distance |  | 23.631 mm x | 23.631 mm |
| Array Size |  | 1.536 mm x | 1.536 mm |
| Embedding |  |  |  |
| Size of Embedding Frame (Sampling Points) |  |  | 10 |
| Total Sampling Points |  | 85 x | 85 |
| Total Array Size |  | 2.0086 mm x | 2.0086 mm |

Figure 466. Panel for Sampling of a source generator.

Description of the parameters:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Sampling | If checked, the sampling parameters will be determined automatically. |
|  |  |
| Oversampling Factor ${ }^{[V]}$ | This parameter can be entered for the Automatic Sampling mode only. The Sampling Distance will be divided by this value. |
| Copy Active Parameters from... | This option is available for the Manual Sampling mode only. If pressed, a window will appear where a document can be selected to copy the Sampling Distance or the number of Sampling Points from, depending on which of both is currently selected. |
| Sampling Points ${ }^{\text {[V] }}$ | In case of Manual Sampling, the number of sampling points can be entered here. This number refers to the array size. |
| Sam | In |
| Array Size | Read Only. The size of the complex array, automatically calculated from Diameter and $(2 \times)$ Absolute Edge Width that are defined on the panel Basic Parameters. |
| Size of Embedding Frame (Sampling Points) | This value defines the size (in sampling points) of the embedding frame which is added to the array of sampled field data. |
| Total Sampling Points | Read Only. Number of sampling points of the resulting field including the embedding frame. |
| Total Array Size | Read Only. Size of the resulting array including the embedding frame. |

### 48.3 Polarization

This panel allows you to enter the Jones vector that determines the relation of $E_{x}$ and $E_{y}$ to the scalar field $U(\hookrightarrow$ Sec. 22.10). You can either enter the Jones vector directly or set the polarization parameters of either linearly, circularly or elliptically polarized light; depending on the selected Type of Polarization.
The following parameters are the same for all polarization types:


Figure 467. Panel for setting the polarization parameters of Linearly Polarized light.

## ITEM FOR

DESCRIPTION
LINEAR POLARIZATION


Figure 468. Panel for setting the polarization parameters of Circularly Polarized light.
ITEM FOR DESCRIPTION

CIRCULAR POLARIZA-
TION

Direction of Rotation $\quad$| The direction of rotation can be either Right Circularly Polarized or Left Cir- |
| :--- |
|  |
| cularly Polarized. |



Figure 469. Panel for setting the polarization parameters of Elliptically Polarized light.

## ITEMS FOR DESCRIPTION <br> ELLIPTICAL POLARIZATION

| Orientation Angle $\sqrt{[\mathrm{Pv}}$ | The angle between the semi-major axis of the polarization ellipse and the <br>  <br> x-axis. Can be in the range between $-180^{\circ}$ and $+180^{\circ}$. |
| :--- | :--- |
| Eccentricity ${ }^{\text {PV }}$ | The (numerical) eccentricity of the polarization ellipse. |
| Direction of Rotation | The direction of rotation can be either Right Elliptically Polarized or Left |
|  | Elliptically Polarized. |


| Basic Parameters |  | Spectral Parameters |  |
| :---: | :---: | :---: | :---: |
| Spatial Parameters | Polarization | Mode Selection | Sampling |
| O Global Polarization Local Polarization |  |  |  |
| Polarization Input |  |  |  |
| Type of Polarization | General Input via Jones Vector $\checkmark$ |  |  |
| $\binom{\mathrm{Jx} \sim}{\mathrm{Jy} \mathrm{\sim}}=\left(\begin{array}{r}0.70711 \\ \hline 0 \\ 0 \\ 0\end{array}\right)$ |  |  |  |
| Representation | Real Part / In | inary Part |  |
| Normalized Jones Vector |  |  |  |
| $\binom{J x}{J y}=($ |  | 0.7107 +0.703 |  |

Figure 470. Panel for General Input via Jones Vector of the polarization parameters.

| ITEMS FOR <br> INPUT OF JONES VEC- | DESCRIPTION |
| :--- | :--- |
| TOR |  |$\quad$| The x-component of the complex Jones vector. Although the Jones vector |
| :--- | :--- |
| is defined as a normalized one (i.e. it has to have a norm of 1), it is not |
| necessary to enter the vector in normalized form, the normalization is done |
| automatically. |

## 49 Multiple Light Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Eigenmode Analyzer

## Accessible:

- Optical Setup: Light Sources > Multiple Light Source
- Light Sources Catalog: Templates > Multiple Light Source

This source model allows you to combine an arbitrary number of other source models (but Image Light Sources, $\rightarrow$ Sec. 52.7).


Figure 471. Edit dialog of a Multiple Light Source.
The edit dialog of this light source ( $\rightarrow$ Fig. 471) has the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| - In Coherent mode, all modes for a certain wavelength are summed up |  |
| conerently. |  |
| - In Incoherent mode, all modes are generated and processed indepen- |  |
| dently. |  |

## Restrictions for Specific Simulation Engines

- For General Profile and Ray Results Profile, Incoherent mode is only possible if for each wavelength there are the same number of modes.
- In the Eigenmode Analyzer ( $\rightarrow$ Sec. 89.2), the result must be a single mode. Thus the Multiple Light Source is restricted to Coherent mode and all light sources must use the same one wavelength.


### 49.1 Duplicate One Light Source



Figure 472. Dialog for the Duplicate One Light Source tool.
This tool for a Multiple Light Source allows you to select one light source by name and how often it is duplicated (Number of Duplicates $n$ ). $n$ duplicates of the original light source are then inserted into the table right after the original one.

### 49.2 Synchronize Selected Parameters

This tool for a Multiple Light Source allows you to select one light source by name from which then selected parameters are copied to all other light sources.


Figure 473. Dialog for the Synchronize Selected Parameters tool.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Select $\quad$ Template $\quad$ Light <br> Source | Allows you to select one light source (by name) from which selected param- <br> eters are copied to all other light sources. |
| Distance to Input Plane | Copies the Distance to Input Plane, which can be found on the Basic Param- <br> eters tab of a light source ( $\hookrightarrow$ Sec. 48.2.1.1). |
| Input Field: Position Size  <br> and Shape Copies all settings from the group box of the same name on the Basic Pa- <br> rameters tab ( $\hookrightarrow$ Sec. 48.2.1.2).  |  |
| Spectral Parameters | Copies all settings from the Spectral Parameters tab ( $\hookrightarrow$ Sec. 48.2.2). |
| Gaussian Parameters | OnLY AVAILABLE IF THE TEMPLATE LIGHT source IS A GAUSSIAN WAVE. <br> Copies all settings from the Spatial Parameters tab of a Gaussian Wave <br> $(\hookrightarrow$ Sec. 51.1) but Generate Cross Section and Reference Wavelength. |

The dialog ensures that a least one of the Parameters to Synchronize is selected.

Some settings cannot be copied to all types of light sources. For example the Distance to Input Plane cannot be copied to a Super-Gaussian Wave and Gaussian Parameters can only be copied to other Gaussian Waves.

## 50 Stored Complete Field

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Optical Setup: Light Sources > Stored Complete Field
- Light Sources Catalog: Templates > Stored Complete Field

With this light source a field that has been generated before can be inserted as source field into an Optical Setup. To use this light source for Classic Field Tracing, you need to set a spatial Harmonic Field or Harmonic Fields Set on the Equidistant Field Data tab. For General Profile and Ray Results Profile you need to set a Ray Distribution on the Non-Equidistant Field Data tab, whereas for General Profile this Ray Distribution must contain field values ( $\hookrightarrow$ Sec. 17.2).


Figure 474. Edit dialog of a stored field source.


No further parameters can be defined, the stored field cannot be modified. Thus no additional panels are visible.

## 51 Basic Source Models



Figure 475. Part of the Sources ribbon showing all Basic Source Models available in the main window. They are explained in the following sections.

The following basic source models are available:

| LIGHT SOURCE | DESCRIPTION |
| :--- | :--- |
| Gaussian Wave | A Hermite- or Laguerre-Gaussian wave. $\hookrightarrow$ Sec. 51.1 |
| Plane Wave | A plane wave traveling in an arbitrary direction. $\hookrightarrow$ Sec. 51.2 |
| Quadratic Wave | A quadratic wave, i.e. a paraxial approximation of a spherical wave. $\lrcorner$ Sec. 51.3 |
| Spherical Wave | A spherical wave generated from a point source at a given distance. $\hookrightarrow$ Sec. 51.4 |
| Super-Gaussian Wave | An isotropic and separable super-Gaussian field. $\hookrightarrow$ Sec. 51.5 |
| Stored Lateral Field | Using this source model any lateral field can be used to define a polychromatic <br> source. $\hookrightarrow$ Sec. 51.6 |
| Ideal Plane Wave | A plane wave with an infinite size traveling in an arbitrary direction. $\hookrightarrow$ Sec. 51.7 |
| Programmable Light | Allows you to define your own field generator. $\hookrightarrow$ Sec. 51.8 |
| Source |  |

### 51.1 Gaussian Wave

## Availability

Toolboxes: All

## Accessible:

- Main window: Sources > Gaussian Wave
- Optical Setup: Light Sources > Basic Source Models > Gaussian Wave
- Light Sources Catalog: Templates > Gaussian Wave

This source model allows you to generate a Hermite- or Laguerre-Gaussian wave ( $\varsigma$ Sec. 132.1). In the following the settings of its edit dialog ( $\hookrightarrow$ Fig. 476) are described.


Figure 476. Parameters for generating a Gaussian wave.
Since the parameters waist, divergence and Rayleigh length depend on each other, one has to define which parameter is the primary choice. Only these values can be modified, the others are computed on the fly and are displayed in the dialog. For computing the values, the selected vacuum wavelength is used, if necessary. During computations, e.g. in an optical system, the primary value is kept fixed. If divergence or Rayleigh length is chosen, then the actual medium wavelength is used to compute the waist of the Gaussian which is generated. In that sense, the primary value is the achromatic constant for the Gaussian wave.
For a Hermite-Gaussian mode, some of the parameters are given for both $x$ - and $y$-direction, which is not explicitly noted in the following table.
Description of the parameters on the Spatial Parameters tab:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Type | Selects whether a Hermite-Gaussian or a Laguerre-Gaussian mode is to be generated. |
| Order ${ }^{\text {PV }}$ | Order of the mode. Order 0 corresponds to a Gaussian fundamental mode, For a Laguerre-Gaussian mode, the left text box refers to the radial order while the right box specifies the angular order. |
| M^2 Parameter | $M^{2}$ parameter of the beam. |
| Reference Wavelength (Vacuum) | The wavelength to which the selected achromatic parameter (waist, divergence, or Rayleigh length) refers. |
| Waist Radius 1/(e^2) ${ }^{\text {[V] }}$ | Beam radius in waist position. The radius is determined by a relative intensity decay by $1 / e^{2}$ for a Gaussian beam. |
| Half-Angle Divergence 1/(e^2) ${ }^{\text {『V }}$ | Half far field divergence angle measured between the optical axis and the $1 / e^{2}$ decay of the intensity. |
| Rayleigh Length ${ }^{\text {[VV }}$ | Rayleigh length of the Gaussian wave. |
| Offset between y - and x plane ${ }^{[\mathrm{PV}}$ | For Hermite-Gaussian modes different longitudinal waist distances can be specified in $x$ - and y -direction, which corresponds to the effect of astigmatism. We define that the waist distance in x-direction is equal to the Distance to Input Plane and the waist distance in y -direction is the sum of Distance to Input Plane and the given Offset between $y$ - and $x$-plane. |
| Copy from Calculator | If one or more Laser Beam Calculators ( $\leftrightarrows$ Sec. 112) are open, you can select one calculator to copy the corresponding values from the calculator to the dialog. <br> A combo box allows you to select whether the $x$-values, $y$-values, and both values, respectively, are filled in the dialog. This setting has only an effect for Hermite-Gaussian waves. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.2 Plane Wave

## Availability

Toolboxes: All
Accessible:

- Main window: Sources > Plane Wave Ill $^{\text {W }}$
- Optical Setup: Light Sources > Basic Source Models > Plane Wave
- Light Sources Catalog: Templates > Plane Wave

This source model allows you to generate a plane wave traveling in an arbitrary direction.


Figure 477. Parameters for generating a plane wave.

The propagation direction of the plane wave can be described in several ways. For this purpose, there are the options Cartesian Angles, Spherical Angles, Wave Number Vector, and Spatial Frequency which are explained in the table below.
Description of the parameters on the Spatial Parameters tab:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Define by | The selection allows different methods for defining the direction of the plane wave as described below. |
| Cartesian Angles | Defines the tilt angles $\alpha$ and $\beta$ (Alpha ${ }^{\text {PV }}$ and Beta $a^{(P V)}$ ) of the plane wave. The angle unit is degrees. |
| Spherical Angles | Defines the tilt angles in spherical coordinates $\phi$ and $\theta$ (Phi ${ }^{[\mathrm{PV}}$ and Theta $a^{\mathrm{PV})}$. The angle unit is degrees. |
| Wave Number Vector | Defines the direction of the plane wave in terms of components $k_{x}{ }^{\mathrm{TV}}$ and $k_{y}{ }^{\mathrm{PV}}$ of the wave number vector $k$. For physical information on how the complex amplitude field is constructed from the components see Eq. (51.1). |
| Spatial Frequency | Defines the direction of the plane wave in spatial frequencies $u^{\mathrm{PV}}$ and $v^{\mathrm{PV}}$ for $x$ and $y$-direction, in units of $1 / m$. |

The resulting harmonic amplitude field $U(x, y)$ is constructed from the given X and Y components $k_{x}$ and $k_{y}$ of the wave number vector by

$$
\begin{equation*}
U(x, y)=\exp \left[i\left(k_{x} x+k_{y} y\right)\right] . \tag{51.1}
\end{equation*}
$$

If the direction is given not as Wave Number Vector but in another representation, the conversion formulas as given in Sec. 139.3 are used.
If the Plane Wave is used within the Optical Setup the direction of the field is handled analytically. A sampling of the linear phase is not necessary at the output of the light source.
The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.3 Quadratic Wave

## Availability

Toolboxes: All

## Accessible:

- Main window: Sources > Quadratic Wave C
- Optical Setup: Light Sources > Basic Source Models > Quadratic Wave
- Light Sources Catalog: Templates > Quadratic Wave

This source model represents a quadratic wave, i. e. a paraxial approximation of a spherical wave.

| Polarization | Mode Selection | Sampling | Ray Selection |
| :---: | :---: | :---: | :---: |
| Basic Parameters | Spectral Parameters |  | Spatial Parameters |
| $\square$ Generate Cross Section |  |  |  |
| Astigmatism |  |  |  |
| Offset between y - and x -Plane |  |  | 0 mm |

Figure 478. Parameters for generating a quadratic wave.

Description of the parameters on the Spatial Parameters tab:

Offset between $y$ - and $x$ - The radius in $x$ - and $y$-direction can be different, which corresponds to the Plane ${ }^{\text {PV }}$ effect of astigmatism. We define that the radius in $x$-direction is equal to the

Distance to Input Plane ${ }^{[V \nabla}$ and the radius in $y$-direction is the sum between Distance to Input Plane and the given value Offset between $y$ - and $x$-plane.

The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.4 Spherical Wave

## Availability

Toolboxes: All

## Accessible:

- Main window: Sources > Spherical Wave (
- Optical Setup: Light Sources > Basic Source Models > Spherical Wave
- Light Sources Catalog: Templates > Spherical Wave

This source model represents a spherical wave generated from a point source at a given distance.

```
Polarization Mode Selection Sampling Ray Selection
Basic Parameters Spectral Parameters Spatial Parameters
Generate Cross Section
The radius is defined by 'Distance to Input Plane' on the 'Basic
Parameters' panel.
```

Figure 479. No further parameters are required for generating a spherical wave. The spherical phase radius is given by Distance to Input Plane.

A spherical wave $U(x, y)$ is defined by

$$
\begin{equation*}
U(x, y)=\frac{z}{r} \exp [i k r] \tag{51.2}
\end{equation*}
$$

with

$$
\begin{equation*}
r=\sqrt{\left(x-x_{0}\right)^{2}+\left(y-y_{0}\right)^{2}+z^{2}} \tag{51.3}
\end{equation*}
$$

where $\left(x_{0}, y_{0}\right)$ and $z$ denote the lateral and longitudinal offset to the origin, respectively. Origin means the center of the spheres described by the equiphase values, and its distance on the z-axis is also denoted as spherical phase radius.
Note on convergence: Whether a spherical wave is convergent or divergent depends on the sign of the spherical phase radius and the sign of the principal propagation direction. If both are equal, the wave is divergent, if not, it is convergent. $\hookrightarrow$ Sec. 131.3.

The distance on the z-axis is represented by Distance to Input Plane ${ }^{\mathbb{D V}}$ at the Basic Parameters panel. Hence, no further parameters are to be described here, see Fig. 479. The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.5 Super-Gaussian Wave

## Availability

Toolboxes: All

## Accessible:

- Main window: Sources > Super-Gaussian Wave प
- Optical Setup: Light Sources > Basic Source Models > Super-Gaussian Wave
- Light Sources Catalog: Templates > Super Gaussian Wave

This source model allows you to generate isotropic and separable super-Gaussian fields ( $\hookrightarrow$ Sec. 132.2).

| Basic Parameters |  | Spectral Parameters |  |
| :---: | :---: | :---: | :---: |
| Spatial Parameters | Polarization | Mode Selection | Sampling |
| $\square$ Generate Cross Section |  |  |  |
| Type $\bigcirc$ Isotropic (Rot.-Symm.) $\bigcirc$ Separable (Rect.-Symm.) |  |  |  |
| Waist Radius |  |  |  |
| Radius |  | $100 \mu \mathrm{~m}$ |  |
| defined at | '2) $\bigcirc 50 \%$ | $\bigcirc$ Fraction | $13.534 \%$ |
| Ede Steepness / Order Ii |  |  |  |
| Edge Steepness / Order |  |  |  |
| Edge Width |  | . $917 \mathrm{\mu m}$ |  |
| Edge Maximum |  | 90\% |  |
| Edge Minimum |  | 10\% |  |
| Order |  | 10 |  |
| Percentage Values | $\bigcirc$ Amplitu | (o) Squ | Amplitude |

Figure 480. Parameters for generating a super-Gaussian wave.

The Spatial Parameters ( $\hookrightarrow$ Fig. 480) are explained in the following table.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Type | Determines the type of the Super Gaussian Wave whether it is /sotropic (rotationally symmetric) or Separable (rectangular symmetric). For the mathematical description see Sec. 132.2. |
| Radius ${ }^{\text {TV }}$ | Determines the Waist Radius of the super Gaussian wave where the intensity of the wave is dropped down to the waist definition level (with respect to the maximum amplitude or intensity) entered below. In case of a separable wave there are also two independent waist radii for every direction. |
| Defined at | The definition level for the waist radius. Given as fraction of the maximum amplitude or intensity, depending on the choice of the percentage value reference. |
| Edge Width | Width of the edge of the super Gaussian function, limited by the minimum and the maximum level. |
| Edge Maximum | Upper definition level for the edge. |
| Edge Minimum | Lower definition level for the edge. |
| Order ${ }^{\text {PV }}$ | Defines the order of the super Gaussian wave. If the type is separable, then two independent orders $m_{x}$ and $m_{y}$ for the x and y -direction are necessary. For numerical reasons, the order(s) must be in the range 0.1 to 100000 . |
| Percentage Values Refer to | Determines if the percentage values of the waist radius definition level, the maximum edge level and the minimum edge level refer to the maximum amplitude or the maximum intensity. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.6 Stored Lateral Field

## Availability

## Toolboxes: All

Accessible:

- Main window: Sources > Stored Lateral Field 숭
- Optical Setup: Light Sources > Basic Source Models > Stored Lateral Field

In this source model, the lateral field distribution $U(x, y)$ of a globally polarized field ( $\hookrightarrow$ Sec. 131.1) is used as a base to define a complete polychromatic source. Spectral Parameters and Polarization of the resulting light source can and must be set independently from the set field.

| Basic Parameters |  | Spectral Parameters |  |
| :--- | :--- | :--- | :---: |
| Spatial Parameters | Polarization | Mode Selection |  |
| Ray Selection |  |  |  |
| Lateral Field |  |  |  |
| Set | Show |  |  |
|  |  |  |  |
| Dispersion Mode |  |  |  |
| Achromatic in Source Plane |  |  |  |
| Achromatic in Far Field |  |  |  |

Figure 481. Parameters for generating a source using a stored lateral field.
Description of the parameters on the Spatial Parameters tab ( $\hookrightarrow$ Fig. 481):

| ITEM | DESCRIPTION |
| :---: | :---: |
| Set | Sets the lateral field, which must be a globally polarized field in spatial domain. Wavelength and polarization of this field are ignored. When you click on this button you can do the following: <br> - Load a lateral field from a .ca2 file. <br> - Select from Documents allows you to select an already open globally polarized harmonic field which is in spatial domain. <br> - Reset the data to the default field. |
| Show | Displays the lateral field being used. |
| Achromatic in Source Plane | Any wavelength is applied to the field without adapting the field in the source plane. |
| Achromatic in Far Field | In this case the sampling distance of the field is modified using the formula $\Delta x_{\text {current }}=\Delta x \cdot \lambda_{\text {current }} / \lambda_{\text {field }}$. Here $\Delta x_{\text {current }}$ is the resulting sampling distance, $\Delta x$ is the sampling distance of the stored lateral field, $\lambda_{\text {field }}$ is the vacuum wavelength of the stored lateral field and $\lambda_{\text {medium }}$ is the vacuum wavelength of the current mode. |

The Sampling Parameters tab is not available as the sampling is taken from the stored field. The remaining tabs of this dialog are explained in Sec. 48.2.

### 51.7 Ideal Plane Wave

## Availability

Optical Setups: Grating Optical Setups

This source model allows you to generate a plane wave with an infinite size traveling in an arbitrary direction.


Figure 482. Dialog for an ideal plane wave.

The effects of unpolarized light can be approximated by using circular polarization.
 polarization control is the same as described in Sec. 48.3, but additionally it allows you to specify the coordinate system the polarization refers to:

| COORDINATE SYSTEM | DESCRIPTION |
| :---: | :---: |
| Coordinate System of Grating | The Jones vector describes the electric field along $x$ - and $y$-axis of the subsequent grating component, respectively. |
| Coordinate System of Light Source | The Jones vector describes the electric field along $x$ - and $y$-axis of the light source, respectively. This is the coordinate system used in all other VirtualLab Fusion light sources. |
| p-s Coordinate System | In grating theory one often uses the nomenclature parallel and senkrecht (= perpendicular) polarization to describe how the electric field vector is orientated to a reference plane (or short p-and s-polarization). This reference plane is defined by the normal vector of the grating surface and the direction vector of the incident light. <br> The conversion from the coordinate system of the light source $\left(E_{x} / E_{y}\right)$ is done with the following equations: $\begin{equation*} E_{\mathbf{s}}=\binom{E_{x}}{E_{y}} \cdot \boldsymbol{n}_{\mathbf{s}} \quad \text { and } \quad E_{\mathrm{p}}=\binom{E_{x}}{E_{y}} \cdot \boldsymbol{n}_{\mathrm{p}} \tag{51.4} \end{equation*}$ <br> $n_{\mathrm{s}}$ and $n_{\mathrm{p}}$ are the normalized directions of s - and p - polarization, respectively (in the coordinate system of the light source). For perpendicular incident $n_{\mathrm{s}}$ is equal to the $y$-axis of the light source. |
| TE-TM Coordinate System | Instead of $p$ - and s-polarization also the nomenclature transversal magnetic and transversal electric, respectively, is used - or short TM / TE. |

### 51.8 Programmable Light Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Eigenmode Analyzer

## Accessible:

- Optical Setup: Light Sources > Basic Source Models > Programmable Light Source
- Light Sources Catalog: Templates > Programmable Light Source

The programmable light source allows you to define your own field generator. This means you write a little snippet defining a complex value which represents the complex amplitude at a certain position $(x ; y)$ in the source plane. In order to allow an analytically stored spherical phase the following concept is applied: if the Distance to Input Plane $r$ is not equal to zero, a spherical phase $\exp (\mathrm{i} k r)$ is multiplied to the values defined in the snippet.


Figure 483. Sample edit dialog for the programmable light source.

Besides Generate Cross Section ( $\hookrightarrow$ Sec. 48.2.3), the spatial parameters tab ( $\hookrightarrow$ Fig. 483) contains the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Snippet | Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ) to edit the snippet defining <br> the source field. A validity indicator $(\hookrightarrow$ Sec. 5.10) shows whether this snippet <br> is consistent. |
| Parameters ${ }^{\text {PEE }}$ | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4 |

The remaining tabs of this dialog are explained in Sec. 48.2.

## 52 Partially Coherent Source Models

VirtualLab Fusion models partially spatially coherent fields by a laterally shifted mode model [VT06; WSK07]. To this end a fundamental mode is generated and laterally shifted. For each lateral position a harmonic field is generated which forms a member of a harmonic fields set. The complete set models the partially coherent field. Theoretically the model requires an infinite number of shifted modes, but in practice, the simulation converges and needs only a limited number of modes.


Figure 484. Part of the Sources ribbon showing all Partially Coherent Source Models available in the main window. They are explained in the following sections.

The following sources can be used to model partially coherent light.

| LIGHT SOURCE | DESCRIPTION |
| :---: | :---: |
| Customized Mode Planar Source | Several copies of the same arbitrary base mode can be placed on different positions of the source plane. The base mode is taken from an already open harmonic field. $\hookrightarrow$ Sec. 52.1 |
| Far Field Source | Several copies of the same arbitrary base mode can be placed on different positions of the source plane. The base mode is calculated from its far field. $\hookrightarrow$ Sec. 52.2 |
| Gaussian Type Planar Source | Several copies of the same Gaussian base mode can be placed on different positions of the source plane. Can be used to simulate LEDs and Excimer lasers. $\hookrightarrow$ Sec. 52.3 |
| Grid Gaussian Planar Source | Several copies of the same Gaussian base mode are placed on a grid. $\hookrightarrow$ Sec. 52.4 |
| Multimode Gaussian Source | Combines several orders of the same Gaussian mode. $\hookrightarrow$ Sec. 52.5 |


| Panel Type Source | Allows you to generate a rectangular grid of pixels (e.g. from an im- <br> ported image) whereas each pixel is represented by a spherical wave mode. <br> $\hookrightarrow$ Sec. 52.7 .1 |
| :--- | :--- |
| Programmable Mode Pla- |  |
| nar Source | Several copies of the same arbitrary base mode can be placed on different <br> positions of the source plane. The base mode is generated from a snippet. <br>  <br> Sec. 52.6 |
| Scanning Source | Allows you to generate a rectangular grid of modes (e.g. from an imported <br> image) whereas each mode is a plane wave mode propagating into another <br> direction. $\hookrightarrow$ Sec. 52.7 .2 |

### 52.1 Customized Mode Planar Source

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Main window: Sources > Customized Mode Planar Source
- Optical Setup: Light Sources > Partially Coherent Light Sources > Customized Mode Planar Source
- Light Sources Catalog: Templates > Customized Mode Planar Source

The Customized Mode Planar Source allows you to combine laterally shifted customized modes to a single source field in a simple way. The lateral positions of the modes are distributed in the source plane with given size. The modes are handled in an incoherent mode and are handled independently as members of a harmonic field set.
This source model supports globally polarized fields in spatial domain as customized modes. Spectral Parameters and Polarization of these modes can be changed.
Source Field Parameters
Size of Source Plane
Base Mode

| $100 \mathrm{\mu m}$ | $\square 100 \mu \mathrm{~m}$ |
| :---: | :---: |
| Set | Show |

Dispersion Mode
() Achromatic in Source Plane
OAchromatic in Far Field

Figure 485. Parameters for generating a source using a customized mode.

The following parameters can be defined on the Spatial Parameters tab.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Size of Source Plane ${ }^{\text {[v }}$ | Size of the source plane (emitting surface). The model assumes that the laterally shifted modes are distributed uniformly across that source plane. |
| Set | Sets the base mode, which must be a harmonic field in spatial domain. The wavelength of this field is ignored. When you click on this button you can do the following: <br> - Load a spatial field from a .ca2 file. <br> - Select from Documents allows you to select an already open spatial field. <br> - Reset the data to the default field. |
| Show | Displays the base mode being used. |
| Achromatic in Source Plane | Any wavelength is applied to the field without adapting the field in the source plane. |
| Achromatic in Far Field | In this case the sampling distance of the field is modified using the formula $\Delta x_{\text {current }}=\Delta x \cdot \lambda_{\text {current }} / \lambda_{\text {field }}$. Here $\Delta x_{\text {current }}$ is the resulting sampling distance, $\Delta x$ is the sampling distance of the stored base mode, $\lambda_{\text {field }}$ is the vacuum wavelength of the stored base mode and $\lambda_{\text {medium }}$ is the vacuum wavelength of the current mode. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 52.2 Far Field Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Light Shaping Optical Setup

## Accessible:

- Optical Setup: Light Sources > Partially Coherent Light Sources > Far Field Source
- Light Sources Catalog: Templates > Far Field Source

The far field source allows you to define a spatially partially coherent light source by its far field. See Sec. 132.4 for physical details.


Figure 486. The Spatial Parameters tab of a Far Field Source. (Local Polarization is defined on the Polarization tab.)
The following parameters can be defined on the Spatial Parameters tab.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Size of Source Plane ${ }^{\text {PV }}$ | Defines the area in which the distinct lateral modes are placed. |
| Definition of Modulation | Defines the complex direction weight functions $D_{l}$, either by Programmable Input or by Databased Input. If you use both input types, the two so defined values are multiplied. If the far field source has been set to Local Polarization on the Polarization tab, you can define two weight functions: the Ex Modulation and the Ey Modulation. The programmable input is described in subsection Sec. 52.2.1 and the databased input in subsection Sec. 52.2.2. |

The lateral shifts of the modes can be defined on the Mode Selection tab. The remaining tabs of this dialog are explained in Sec. 48.2.

### 52.2.1 Programming the Complex Direction Weight Functions

For programming you can use either the spherical angles theta and phi or the Cartesian coordinates $x, y$ and Distance, which is the Distance to Input Plane ${ }^{[\mathrm{PV}}$ defined on the Basic Parameters tab. It is assumed that theta and phi are given in radians and that phi is in the range $-\pi \ldots+\pi$.


Figure 487. The Spatial Parameters tab of a Far Field Source in Programmable Input mode. (Global Polarization is defined on the Polarization tab.)

The following conversion formulas are used to calculate theta and phi. ${ }^{1}$

$$
\begin{align*}
r & =\sqrt{x^{2}+y^{2}+\text { Distance }^{2}}  \tag{52.1}\\
\text { theta } & =\arccos \frac{\text { Distance }}{r}  \tag{52.2}\\
p h i & =\operatorname{atan} 2 \frac{y}{x} \tag{52.3}
\end{align*}
$$

The following controls are used for programming the complex weight functions.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Definition | This group box allows you to program a code snippet defining the complex <br> weight functions. Edit opens the Source Code Editor $(\hookrightarrow$ Sec. 7.3$)$ to edit this <br> snippet, and a validity indicator $(\hookrightarrow$ Sec. 5.10$)$ shows whether this snippet is <br> consistent. |
| Parameters ${ }^{\text {狍 }}$ | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4 |

General information about programming in VirtualLab Fusion can be found in Sec. 7.

[^10]
### 52.2.2 Databased Complex Direction Weight Functions



Figure 488. The Spatial Parameters tab of a Far Field Source in Databased Input mode.

For Databased Input of the complex direction weight functions the following controls can be used.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set $>$ Load | Loads a data array from a .da file. |
| Set $>$ Import | Imports a data array from a bitmap or text file by means of the import wizard <br> described in Sec. 121.2. |
| Set $>$ Select from <br> ments | Allows you to select an already open data array. |
| Set $>$ Reset | Resets the modulation data to its default. |
| Show <br> Preview Table | Shows the current data in a separate data array view ( $\hookrightarrow$ Sec. 13.5). |

The data array to be set must contain only one complex-valued two-dimensional data subset. If both coordinates are given in degrees or radians the coordinates will be interpreted as spherical angles. In this case the xcoordinate is always interpreted as the spherical angle $\phi$ which is defined in the range $-\pi \ldots+\pi$. The ycoordinate is interpreted as the spherical angle $\theta$ within the value range $0 \ldots+\frac{\pi}{2}$.
In any other case the coordinates are used as $x$ - $y$-coordinates.
The labels of the data array and the physical property of the coordinates are adapted automatically.

### 52.3 Gaussian Type Planar Source

## Availability

Optical Setups: General Optical Setup
Accessible:

- Main window: Sources > Gaussian Type Planar Source .
- Optical Setup: Light Sources > Partially Coherent Light Sources > Gaussian Type Planar Source
- Light Sources Catalog: Templates > Gaussian Type Planar Source

This generator can be used to simulate LEDs and Excimer lasers. See Sec. 132.3 for physical details.

| Basic Parameters |  | Spectral Parameters |  |
| :---: | :---: | :---: | :---: |
| Spatial Parameters | Polari | Mode Sele | Sampling |
| $\square$ Generate Cross Section |  |  |  |
| Source Field Parameters |  |  |  |
| Size of Source Plane |  | $100 \mu \mathrm{~m}$ | $100 \mu \mathrm{~m}$ |
| Reference Wavelength (Vacuum) |  |  | 532 nm マ |
| Select Achromatic Parameter: |  |  |  |
| HWHM Divergence Angle (max. 45 degree) |  | $1{ }^{\circ}$ | $1{ }^{\circ}$ |
| Spatial Coherence Length |  | $4.0383 \mu \mathrm{~m}$ | $4.0383 \mu \mathrm{~m}$ |
| W Waist Radius ( $1 / \mathrm{e}^{\wedge} 2$ ) |  | $5.711 \mu \mathrm{~m}$ | $5.711 \mu \mathrm{~m}$ |

Figure 489. Parameters for generating a Gaussian type source field.

Description of the parameters on the Spatial Parameters ( $\hookrightarrow$ Fig. 489) tab:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Size of Source Plane ${ }^{\text {PV }}$ | Size of the source plane (emitting surface). The model assumes that the laterally shifted modes are distributed uniformly across that source plane. In the limit of dense modes the size corresponds to the half maximum. |
| Achromatic Parameter | The chosen value is kept constant over set of wavelengths. The values depend on each other and are recomputed using the reference wavelength. During generation the achromatic parameter is used together with the refractive index and the vacuum wavelength to compute the waist of the fundamental Gaussian modes. |
| HWHM Divergence Angle ${ }^{[\mathrm{PV}}$ | Half width at half maximum divergence angle of the source field (not that of a single fundamental mode). |
| Spatial Coherence <br> Length ${ }^{\text {PV }}$  | Spatial coherence length of the source field. |
| Waist Radius ( $\left.1 / e^{2}\right)^{\text {PV }}$ | Waist radius of the fundamental modes. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 52.4 Grid Gaussian Planar Source

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Main window: Sources > Grid Gaussian Planar Source 㽗
- Optical Setup: Light Sources > Partially Coherent Light Sources > Grid Gaussian Planar Source
- Light Sources Catalog: Templates > Grid Gaussian Planar Source

The Grid Gaussian Planar Source source model allows you to combine laterally shifted Gaussian waves to a single source field in a simple way. The lateral positions are described by a regular grid centered at ( 0,0 ) with given size and a given period (distance between the single waves). Two modes are available: coherent and non-coherent. In the coherent case the laterally shifted waves are added (complex number operation), whereas in the non-coherent case each wave is handled independently as member of a field set.


Figure 490. Parameters for generating a gridded Gaussian wave.

The corresponding edit dialog is shown in Fig. 490. Its Spatial Parameters tab has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Coherent Mode | Flag indicating whether the laterally shifted waves are considered to be in <br>  <br> coherent mode or not. |
| Waist Radius $\left(1 / e^{2}\right)^{[V /}$ | Waist radius of the single Gaussian waves. |
| Grid Period ${ }^{[\operatorname{PV}}$ | Period of the waves, i.e. distance between them. |
| Grid Points ${ }^{[\mathrm{PV}}$ | Size of the grid, i. e. number of Gaussian waves. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 52.5 Multimode Gaussian Source

## Availability

Optical Setups: General Optical Setup

## Accessible:

- Main window: Sources > Multimode Gaussian Source ©
- Optical Setup: Light Sources > Partially Coherent Light Sources > Multimode Gaussian Source
- Light Sources Catalog: Templates > Multimode Gaussian Source

The Multimode Gaussian Source allows you to combine several orders of the same Gaussian mode. First the maximum order has to be defined, then for each order the Weight ${ }^{\mathrm{PVV}}$ (that refers to the intensity) and the absolute Phase Offset ${ }^{[\mathrm{Pv}}$ has to be given in the table at the bottom of the Spatial Parameters tab. This table
also allows you to set certain modes Active or inactive which means that they are not considered in the resulting field.
The fundamental Gaussian mode can be specified by an achromatic parameter: either the waist, the angle of divergence, or the Rayleigh length. This parameter is the same for all base modes. Note that base modes with different wavelengths (according to the settings on the Spectral tab, $\hookrightarrow$ Sec. 48.2.2) can have different waists if the achromatic parameter is the angle of divergence or the Rayleigh length.
In contrast, the higher-order modes have always the same Rayleigh length as the corresponding fundamental mode. This ensures that fundamental mode and corresponding higher-order modes do not diverge during propagation.
For the theory of Gaussian beams see Sec. 132.1.


Figure 491. Parameters for generating a Multimode Gaussian Source.

The following parameters can be defined on the Spatial Parameters tab ( $\hookrightarrow$ Fig. 491).

| ITEM | DESCRIPTION |
| :---: | :---: |
| Type | Selects whether Hermite-Gaussian or Laguerre-Gaussian modes are to be generated. |
| Waist Radius 1/(e^2) ${ }^{\text {PV }}$ | Radius of the fundamental mode in waist position. The radius is determined by a relative intensity decay by $1 / e^{2}$ for a Gaussian beam. |
| Reference Wavelength (Vacuum) | The wavelength to which the selected achromatic parameter refers. |
| Half-Angle Divergence $1 /\left(e^{\wedge} 2\right)^{\text {PV }}$ | Half far field divergence angle of the fundamental mode measured between the optical axis and the $1 / e^{2}$ decay of the intensity. |
| Rayleigh Length ${ }^{\text {PV }}$ | Rayleigh length. |
| Offset between $y$ - and $x$ plane ${ }^{\text {PV }}$ | For Hermite-Gaussian modes different longitudinal waist distances can be specified in $x$ - and $y$-direction, which corresponds to the effect of astigmatism. We define that the waist distance in $x$-direction is equal to the Distance to Input Plane and waist distance in y-direction is the sum between Distance to Input Plane and the given value Offset between $y$ - and $x$-plane. |
| Coherent Accumulation of Modes | If you select Coherent Accumulation of Modes the modes of different orders are added (complex number operation). Otherwise each order is handled independently as member of a harmonic fields set. |
| Maximum Order | Defines the upper limit for the orders being used. Order 0 corresponds to a Gaussian fundamental mode. For a Laguerre-Gaussian mode, the left text box refers to the radial order while the right box specifies the angular order. |

The remaining tabs of this dialog are explained in Sec. 48.2.

### 52.6 Programmable Mode Planar Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Light Shaping Optical Setup

## Accessible:

- Optical Setup: Light Sources > Partially Coherent Light Sources > Programmable Mode Planar Source
- Light Sources Catalog: Templates > Programmable Mode Planar Source

The Programmable Mode Planar Source allows you to program the base mode combine whose laterally shifted copies are distributed in the source plane with given size. The copies are handled in an incoherent mode and are handled independently as members of a harmonic field set. The programmed mode is assumed to be globally polarized. Spectral information can be added using the panel Spectral Parameters.
In order to allow an analytically stored spherical phase the following concept is applied: if the value entered at Distance to Input Plane is not equal to zero, a spherical phase $\exp (\mathrm{i} k r)$ is multiplied to the values defined in the snippet.


Figure 492. The Spatial Parameters tab for a Programmable Mode Planar Source.
Besides Generate Cross Section ( $\varsigma$ Sec. 48.2.3), the spatial parameters tab ( $\hookrightarrow$ Fig. 492) contains

| ITEM | DESCRIPTION |
| :--- | :--- |
| Size of Source Plane ${ }^{\text {『V }}$ | Size of the source plane (emitting surface). The model assumes that the <br> laterally shifted modes are distributed uniformly across that source plane. In <br> the limit (dense modes) the size corresponds to half the maximum. |
| Definition | This group box allows you to program the code snippet defining the base <br> mode. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3) to edit this snippet, <br> and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Parameters ${ }^{\text {国 }}$ | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4 |

General information about programming in VirtualLab Fusion can be found in Sec. 7. The remaining tabs of this dialog are explained in Sec. 48.2.
This source does not provide automatic sampling. However, the definition of the sampling distance is supported in the dialog. In particular we require a sampling of the phase residuals caused by mode shifts with respect to the spherical phase that is defined on axis (originating from the Distance to Input Plane). In the dialog of the source at the Sampling tab, the required sampling distance is displayed ( $\rightarrow$ Fig. 493). If the button Copy Sampling Distance is pressed, the sampling distance is entered into the corresponding fields.

## Sampling Support

According to the maximum shift of the mode and the distance
to input plane, the sampling distance should not be larger than
$(10 \mu \mathrm{~m} \times 10 \mu \mathrm{~m})$.
Copy Sampling Distance
Figure 493. Additional support for the sampling of programmable mode planar source.

### 52.7 Image Light Sources

There are two light sources which allow you to generate a rectangular grid of distinct modes whereas each mode can have its own intensity weight. These weights can either be taken from an arbitrary image which the user specifies. Or they can be constant 1 .
The Panel Type Source ( $\varsigma$ Sec. 52.7.1) places the modes at different positions and thus you can see the pixels of the original image in the near field. The Scanning Source ( $\leftrightarrows$ Sec. 52.7.2) propagates the modes into different directions and thus you can see the original image in the far field.


Figure 494. The Specific Parameters tab of an image light source (here Panel Type Source).
Both light sources have the following controls on the Specific Parameters tab ( $\rightarrow$ Fig. 494) in common.

| ITEM | DESCRIPTION |
| :---: | :---: |
| From Chromatic Fields Set | The intensity of each mode is determined from a Chromatic Fields Set. Note that in this way you can define an intensity distribution for multiple wavelengths. |
| Set Image | Only visible if From Chromatic Fields Set is checked. <br> Allows you to load a Chromatic Fields Set into the dialog. When you click on this button you can do the following: <br> - Load a Chromatic Fields Set from a .cfs file. <br> - Import a Chromatic Fields Set from a bitmap file. $\hookrightarrow$ Sec. 122.2 <br> - Select from Documents allows you to select an already open Chromatic Fields Set. |
| Show Image | Only visible if From Chromatic Fields Set is checked. <br> Shows the currently set Chromatic Fields Set as a separate document. |
| Constant 1 | A constant intensity of 1 is assumed for each pixel. |
| Number of Pixels / Directions | Only visible if Constant 1 is checked. The number of modes to be generated. |
| Wavelength | Only visible if Constant 1 is checked. <br> The wavelength the generated modes have. |

If per wavelength there are more modes to be generated than specified in the Global Options Dialog ( $\hookrightarrow$ Sec. 6.14; Maximum Number of Modes), a warning is shown in the Validity control.


Figure 495. The Mode Selection tab of an image light source (here Panel Type Source).

These light sources also add functionality to the mode selection tab ( $\hookrightarrow$ Fig. 495):

| ITEM | DESCRIPTION |
| :--- | :--- |
| All Pixels / Directions | All modes are generated as specified on the Specific Parameters tab. |
| Select Column | Only modes having the specified Column Index are generated. |
| Select Row | Only modes having the specified Row Index are generated. |
| Select Pixel/Direction | Only the mode with the specified Column Index and Row Index is generated. |

The remaining controls of the edit dialogs are explained in Sec. 48.1.

### 52.7.1 Panel Type Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Light Shaping Optical Setup

## Accessible:

- Optical Setup: Light Sources > Partially Coherent Light Sources > Panel Type Source
- Light Sources Catalog: Templates > Panel Type Source

The Panel Type Source allows you to generate a rectangular grid of pixels (e.g. from an imported image) whereas each pixel is represented by a spherical wave mode.


Figure 496. The edit dialog of the Panel Type Source (Specific Parameters tab).

The Specific Parameters tab of its dialog ( $\hookrightarrow$ Fig. 496) has the following controls specific to the Panel Type Source.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Pixel Pitch | The x-and y-distance of neighbored pixels. |
| Aperture Angle | The full aperture angle. Together with the pixel pitch this determines the Dis- <br> tance to Source Plane, i. e. how far behind the source plane the spherical <br> wave starts from a single point. If the pixel pitch differs in $x$ - and y-direction <br> the larger of the two values is taken for this calculation. |
| Distance to Source Plane | For your information the distance to the source plane is also given. |

The remaining controls of this dialog are explained in Sec. 52.7.

### 52.7.2 Scanning Source

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Light Shaping Optical Setup

## Accessible:

- Optical Setup: Light Sources > Partially Coherent Light Sources > Scanning Source
- Light Sources Catalog: Templates > Scanning Source

The Scanning Source allows you to generate a rectangular grid of modes (e.g. from an imported image) whereas each mode is a plane wave mode propagating into another direction. Modes more in the center of the original image have a smaller deviation from the central direction.


Figure 497. The edit dialog of the Scanning Source (Specific Parameters tab).

The Specific Parameters tab of its dialog ( $\hookrightarrow$ Fig. 497) has the following controls specific to the Scanning Source.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Central Direction | The direction into which the center of the overall field propagates. |
| Field of View | The full field of view, i. e. the difference in the $x$ - and $y$-direction of the outer- <br> most pixels. |
| Angular Pitch | The difference in the $x$ - and $y$-direction of neighbored pixels. |

The remaining controls of this dialog are explained in Sec. 52.7.

## 53 Spectrum Generators



Figure 498. Part of the Sources ribbon showing all available spectrum generators. They are explained in the following sections.

| SPECTRUM GENERATOR | DESCRIPTION |
| :---: | :---: |
| Black Body Spectrum | A discrete sample at equidistant wavelengths from the black body spectral intensity distribution governing the thermal radiation of an idealized black body. $\hookrightarrow$ Sec. 53.1 |
| Gaussian Spectrum | A discrete sample at equidistant wavelengths of the Gaussian spectral intensity distribution which arises in Doppler broadening of a spectral line. $\hookrightarrow$ Sec. 53.2 |
| Homogeneous Spectrum | A constant intensity sampled at equidistant wavelengths. $\hookrightarrow$ Sec. 53.3 |
| Lorentzian Spectrum | A discrete sample at equidistant wavelengths of the Lorentzian spectral intensity distribution which arises in natural lifetime and collision broadening of a spectral line. $\hookrightarrow$ Sec. 53.4 |
| Databased Spectrum | Allows the specification of data points for the generation of a spectrum. $\rightarrow$ Sec. 53.5 |
| Programmable Spectrum | Allows you to program an arbitrary spectrum over wavelength or frequency. $\rightarrow$ Sec. 53.6 |
| Gaussian Pulse Spectrum | An ultra-short pulse with a Gaussian envelope. $\hookrightarrow$ Sec. 53.7 |
| Databased Pulse Spectrum | Allows the specification of data points for the generation of a pulse spectrum. $\rightarrow$ Sec. 53.8 |
| Programmable Pulse Spectrum | Allows you to program an arbitrary pulse spectrum over wavelength or frequency. $\hookrightarrow$ Sec. 53.9 |

### 53.1 Black Body Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Black Body Spectrum $\frac{\Delta}{A}$

The Black Body Spectrum generates a discrete sample at equidistant wavelengths from the black body spectral intensity distribution governing the thermal radiation of an idealized black body ( $\leftrightarrows$ Sec. 132.5.1). Any such distribution is simply depending on the temperature of the body. The edit dialog ( $\hookrightarrow$ Fig. 499) has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Temperature | Allows the selection of the absolute temperature in Kelvin. For your informa- <br> tion also the wavelength is given at which the distribution peaks for the current <br> temperature according to Wien's displacement law. |
| Min. Wavelength | The lower bound of the sampling interval is entered here. |
| Max. Wavelength | The upper bound of the sampling interval is entered here. |
| Sampling Count | The total number of sampled wavelengths is defined here. |



Figure 499. Dialog for adjusting a black body spectrum.

After finishing the dialog, the wavelengths between the given minimum and maximum are computed according to the sampling count with constant sampling increment.
Their intensity values are obtained by integrating the intensity function over an interval of half a sampling increment both at the left and at the right of the wavelength. Thus the sampled wavelengths get an intensity which is representative for a symmetric interval around them.
By re-scaling the computed values, the peak intensity for the sample is arbitrarily set to 1 .
Output is a 2D diagram showing the distribution of the black body radiation at the chosen temperature. The diagram can be used as the spectrum of a polychromatic light source in the generating dialog of the light source.

### 53.2 Gaussian Spectrum

## Availability

Toolboxes: All
Accessible: Sources $>$ Gaussian Spectrum $\frac{\Delta}{\Delta}$

The Gaussian Spectrum generates a discrete equidistant sample of wavelengths with their intensities forming a Gaussian spectral intensity distribution (which arises from Doppler broadening of a spectral line). Any such distribution is characterized by a peak wavelength and by the half width wavelength increment at half-maximum. $\hookrightarrow$ Sec. 132.5.2.
The edit dialog ( $\hookrightarrow$ Fig. 500 ) has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Peak Wavelength | Allows the selection of the wavelength carrying the intensity maximum. |
| Half Width at Half-Max | The wavelength difference that defines the line broadening is entered here. |
| Sampling Count | The number of sampled wavelengths is entered here. |
| Clipping Intensity | Here the intensity ratio relative to peak intensity is determined which delimits <br> the sampling interval. |



Figure 500. Dialog for adjusting a Gaussian spectrum.

After finishing the dialog, the minimal and maximal wavelengths to be included are calculated, and the remaining wavelengths according to the sampling count are computed with constant sampling increment.
Their intensity values are obtained by integrating the intensity function over an interval of half a sampling increment both at the left and at the right of the wavelength. Thus the sampled wavelengths get an intensity which is representative for a symmetric interval around them.
By re-scaling the computed values, the peak intensity for the sample is arbitrarily set to 1 .
Output is a 2D diagram showing the Gaussian distribution. The diagram can be used as the spectrum of a polychromatic light source in the generating dialog of the light source.

### 53.3 Homogeneous Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Homogeneous Spectrum $\underset{A}{\square}$

The Homogeneous Spectrum allows to generate a constant intensity sampled at equidistant wavelengths. Its edit dialog ( $\hookrightarrow$ Fig. 501) has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Central Wavelength | Allows the selection of the wavelength defining the middle of the wavelength <br> band. |
| Spectral Bandwidth | The difference between maximal and minimal wavelength in the selected <br> band is entered here. |
| Sampling Increment | The difference between two adjacent sampled wavelength values is entered <br> here. |



Figure 501. Dialog for adjusting a homogeneous spectrum.

Output is a 2D diagram showing the homogeneous distribution. The intensity values are arbitrarily set to 1 . The diagram can be used as the spectrum of a polychromatic light source in the generating dialog of the light source.
If the bandwidth is not an integral multiple of the wavelength increment, then the wavelength samples are generated symmetrically around the central wavelength. The smallest wavelength in the sample is not larger than the lower band limit, and the largest wavelength in the sample is not smaller than the upper band limit.

### 53.4 Lorentzian Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Lorentzian Spectrum $\underset{\lambda}{L_{\Delta}^{\boxed{~}}}$

The Lorentzian Spectrum generates a discrete sample at equidistant wavelengths of the Lorentzian spectral intensity distribution which arises in natural lifetime and collision broadening of a spectral line. Any such distribution is characterized by a peak wavelength and by the half width wavelength increment at half-maximum. $\hookrightarrow$ Sec. 132.5.3.
The edit dialog ( $\hookrightarrow$ Fig. 502) has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Peak Wavelength | Allows the selection of the wavelength carrying the intensity maximum. |
| Half Width at Half-Max | The wavelength difference that defines the line broadening is entered here. <br> Sampling Count <br> Clipping Intensity |
|  | The number of sampled wavelengths is entered here. <br> Here the intensity ratio relative to peak intensity is determined which delimits <br> the sampling interval. |



Figure 502. Dialog for adjusting a Lorentzian spectrum.

After finishing the dialog, the minimal and maximal wavelengths to be included are calculated, and the remaining wavelengths according to the sampling count are computed with constant sampling increment.
Their intensity values are obtained by integrating the intensity function over an interval of half a sampling increment both at the left and at the right of the wavelength. Thus the sampled wavelengths get an intensity which is representative for a symmetric interval around them.
By re-scaling the computed values, the peak intensity for the sample is arbitrarily set to 1 .
Output is a 2D diagram showing the Lorentzian intensity distribution. The diagram can be used as the spectrum of a polychromatic light source in the generating dialog of the light source.

### 53.4.1 Used Formula

The Lorentzian power spectrum in dependence on the angular frequency $\omega$ is given by the formula

$$
S(\omega)=\frac{S_{0}}{\left(\omega-\omega_{0}\right)^{2}+\Delta \omega^{2}}
$$

where $\omega_{0}$ is the central angular frequency, $\Delta \omega$ the half width at half-maximum of the distribution.
In transforming the density to a function of the wavelength, the relations

$$
\begin{gathered}
\omega_{0}=2 \pi c / \lambda_{0} \\
\Delta \omega=-\omega_{0} / \lambda_{0} \cdot \Delta \lambda
\end{gathered}
$$

were used.
If wavelengths with a minimal intensity $S_{\min }$ (relative to the peak intensity) shall limit the sampled wavelength interval, then corresponding lowest and highest angular frequencies are computed from

$$
\begin{gathered}
\omega_{\min }=\omega_{0}+\Delta \omega \cdot \sqrt{1 / S_{\min }-1} \\
\omega_{\max }=2 \omega_{0}-\omega_{\min }
\end{gathered}
$$

and the equivalent wavelengths follow from $\lambda=2 \pi c / \omega$.

### 53.5 Databased Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Databased Spectrum

The Databased Spectrum generator allows the specification of data points for the generation of a spectrum. The generator can be used for direct specification of the data points, or for reading data point values from a user defined file.
The following settings can be done within the edit dialog of the databased spectrum generator:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Specification in Wave- <br> length / Frequency <br> main | The user can select whether the values defined in the data table shall be used <br> within the wavelength domain, or the frequency domain. |
| Central Wavelength/ Fre- <br> quency | To specify the position of the data points the user has to enter the central <br> wavelength/ frequency. <br> Note that it is ensured that the spectrum covers the same spectral range, i. e. <br> minimum and maximum are kept. Thus the central frequency $v_{c}$ cannot be <br> calculated from the central wavelength $\lambda_{c}$ via $v_{c}=c / \lambda_{c}$. |
| Data Table | The data table allows you to edit the amplitude and phase values of each data <br> point. A data point can be added by clicking on the Add Data Point tool. |
| Size of the Wavelength/ | The user can select whether he likes to define the array size of the wave- <br> length/ frequency window or the sampling distance within wavelength/ fre- <br> quency. <br> Frequency Window |

Note: The databased spectrum generator is only configured correctly if at least two data points are within the data table.
The following data table tools are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Add Data Point | Data table tool to add a new data point. Clicking on this tools triggers the <br> display of a dialog where the user has to enter the amplitude and the phase <br> of the new data point. |
| Load from File | The user can specify a file which shall be used for filling the table of data <br> values. |
| Clear Table | The user can reset the data table by clicking on the Clear Table tool. |

Note: The data values in the table are always interpreted as equidistant data points.
Fig. 503 shows the edit dialog of the databased spectrum generator.


Figure 503. Dialog of the databased spectrum generator.

The result of the databased spectrum generator is a 1D Light Field Object which shows amplitude and phase values over wavelengths. This diagram can be used in polychromatic sources for the specification of the spectral parameters.

### 53.6 Programmable Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Programmable Spectrum

The Programmable Spectrum generator allows the specification of a amplitude / phase function over wavelength or frequency. Within the generator the user has the possibility to program a simple snippet which describes the function which shall be realized by the spectrum generator.
Fig. 504 shows the edit dialog of the programmable spectrum generator.


Figure 504. Dialog of the programmable spectrum generator.
The following settings can be done within the edit dialog of the programmable spectrum generator:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Specification in Wavelength/ Frequency Domain | The user can select whether the return values of the function defined in the snippet shall be used within the wavelength domain, or the frequency domain. |
| Central Wavelength/ Frequency | To specify the position of the data values the user has to enter the central wavelength/ frequency. <br> Note that it is ensured that the spectrum covers the same spectral range, i. e. minimum and maximum are kept. Thus the central frequency $\nu_{c}$ cannot be calculated from the central wavelength $\lambda_{\mathrm{C}}$ via $v_{\mathrm{C}}=c / \lambda_{\mathrm{c}}$. |
| Definition | This group box allows you to program a snippet which generates a distribution of complex values. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3) to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Parameters | The controls in this group box allow you to set the values of the global parameters of the snippet. $\hookrightarrow$ Sec. 7.4 |
| Size of the Wavelength/ Frequency Window | The user can select whether to define the array size of the wavelength / frequency window or the sampling distance within wavelength/frequency. |
| Number Data Points | The number of data points can be entered. The minimum number of data points to define a valid programmable spectrum generator is two. |

The result of the programmable spectrum generator is a 1D Light Field Object which shows amplitude and
phase values over wavelengths. This diagram can be used in polychromatic sources for the specification of the spectral parameters.

### 53.7 Gaussian Pulse Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Programmable Spectrum


Figure 505. Edit dialog for a Gaussian Pulse Spectrum

The Gaussian Pulse Spectrum generator is intended to generate an ultra-short pulse with a Gaussian envelope. Thus its edit dialog ( $\hookrightarrow$ Fig. 505) asks for the parameters of the resulting pulse. As result you obtain a spectrum with a Gaussian shape if the amplitudes are plotted over frequency.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Definition by FWHM | Pulse Duration refers to half the maximum squared amplitude. |
| Definition by $1 / \mathrm{e}$ Diameter | Pulse Duration refers to $1 /$ e times the maximum squared amplitude. |
| Pulse Duration | Specify the duration of the pulse in time. |
| Carrier Wavelength | The wavelength where the pulse spectrum reaches its maximum. |
| Carrier Frequency | For your information also the frequency where the pulse spectrum reaches its maximum is given. |
| Estimated Increase Of Time Window | With this factor you can enlarge the time window in which the pulse is displayed. This factor can be used to ensure that even the broadened pulse after propagation can be displayed correctly. As a side effect, the number of sampling points for the resulting spectrum is enlarged by the same factor. |
| Squared Amplitude Truncation (Frequency Domain) | In theory, a Gaussian spectrum has an infinite width. Thus you can specify a threshold relative to the maximum squared amplitude. Squared amplitudes smaller than this threshold are not taken into account. |
| Resulting Size of Angular Frequency Window | For your information, the resulting band width of the truncated spectrum is given. |
| Squared Amplitude Truncation (Time Domain) | In theory, also the Fourier-transformed pulse would have an infinite width. Thus, a further threshold relative to the maximum squared amplitude is needed for the time domain. |
| Resulting Size of Time Window | For your information, the resulting time window is given to illustrate the effect of the Time Domain threshold. The overall time window displayed after temporal Fourier transform ( $\hookrightarrow$ Sec. 31.2.1) is Resulting Time Window times Estimated Increase Of Time Window. |
| Resulting Samples | For your information; the resulting number of frequency samples which will be generated by the Gaussian Pulse Spectrum Generator. |

### 53.8 Databased Pulse Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Databased Pulse Spectrum

The Databased Pulse Spectrum generator allows the specification of data points for the generation of a pulse spectrum. The generator can be used for direct specification of the data points, or for importing data points from a user defined file.
Fig. 506 shows the edit dialog of the databased pulse spectrum generator.


Figure 506. Dialog of the databased pulse spectrum generator.

The following settings can be done within the edit dialog of the databased pulse spectrum generator:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Specification in Time / Frequency Domain | The user can select whether the values defined in the data table shall be used within the time domain, or the frequency domain. |
| Carrier Wavelength | The carrier wavelength which shall be used for pulse shape generation. |
| Carrier Frequency | The carrier frequency is calculated from the Carrier Wavelength. |
| \{Data Table\} | The data table allows you to edit the amplitude and phase values of each data point. A data point can be added by clicking on the Add Data Point tool. |
| Data Table Tools | Clicking on this button opens a collection of various tools which help you in editing the data table. See below. |
| Size of the Time/Frequency Window | The user can select whether he likes to define the array size of the time / frequency window or the sampling distance within time / frequency. |
| Number Data Points | This control to show the number of data points is read only because the number of data points is specified by the number of entries in the data table. |

Note: The databased pulse spectrum generator is only configured correctly if at least two data points are within the data table.
The following data table tools are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Add Data Point | Data table tool to add a new data point. Clicking on this tools triggers the <br> display of a dialog where the user has to enter the amplitude and the phase <br> of the new data point. |
| Load from File | The user can specify a file which shall be used for filling the table of data <br> values. It must contain two columns (one for the amplitude values, one for <br> the phase values, separated by a space). ' $\because$ must be the number separator <br> and lines can be commented out by prepending ' $\#$ '. |
| Clear Table | The user can reset the data table by clicking on the Clear Table tool. |

Note: The data values in the table are always interpreted as equidistant data points.
The result of the databased pulse spectrum generator is a 1D Light Field Object which shows amplitude and phase values over wavelengths. This diagram can be used in polychromatic sources for the specification of the spectral parameters. The resulting pulse shape which is displayed over wavelength can be transformed to the pulse shape in time domain by performing an inverse Fourier transform. More information on that can be found in Sec. 31.2.1.

### 53.9 Programmable Pulse Spectrum

## Availability

Toolboxes: All
Accessible: Sources > Programmable Pulse Spectrum

The Programmable Pulse Spectrum generator allows the specification of a amplitude / phase function over time or frequency. Within the generator the user has the possibility to program a simple snippet which describes the function which shall be realized by the pulse spectrum generator.
The following settings can be done within the edit dialog of the programmable pulse spectrum generator:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Specification in Time / Fre- <br> quency Domain | The user can select whether the return values of the function defined in the <br> snippet shall be used within the time domain, or the frequency domain. |
| Carrier Wavelength | The carrier wavelength which shall be used for pulse shape generation. |
| Carrier Frequency | The carrier frequency is calculated from the Carrier Wavelength. |
| Definition | This group box allows you to program a snippet which generates a distribution <br> of complex values. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ) to edit this <br> snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10$)$ shows whether this snippet is <br> consistent. |
| Parameters | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\hookrightarrow$ Sec. 7.4 |
| Size of the Time / Fre- <br> quency Window The user can select whether he likes to define the array size of the time / <br> frequency window or the sampling distance within time / frequency. <br> Number Data Points The number of data points can be entered. The minimum number of data <br> points to define a valid programmable pulse spectrum generator is two. |  |

Fig. 507 shows the edit dialog of the generator.


Figure 507. Dialog of the programmable pulse spectrum generator.
The result of the programmable pulse spectrum generator is a 1D Light Field Object which shows amplitude and phase values over wavelengths. This diagram can be used in polychromatic sources for the specification of the spectral parameters. The resulting pulse shape which is displayed over wavelength can be transformed to the pulse shape in time domain by performing an inverse Fourier transform. More information on that can be found in Sec. 31.2.1.

## IX <br> Real Components

This part documents all Real Components like lenses, fibers, holograms, or gratings which are available within the Optical Setup ( $\rightarrow$ Sec. 43) of Virtuallab Fusion.

## 54 Edit Dialog for Real Components (Common Controls)



Figure 508. Example for the edit dialog for real components.

The edit dialogs for all real components ( $\hookrightarrow$ Fig. 508) are divided into several pages:

| PAGE | DESCRIPTION |
| :--- | :--- |
| Coordinate Systems | $\hookrightarrow$ Sec. 43.8 .1 |
| Position / Orientation | $\hookrightarrow$ Sec. 43.8 .2 |
| Structure | The structure tab is specific for the distinct real components and is thus ex- <br> plained in the following chapters. |
| Solver / Function | Not FOR CLASSIC FIELD TRACING AND ONLY FOR CERTAIN COMPONENTS. <br> Explains the algorithm used to simulate the component. |
| Channel Configuration | Not FOR CLASSIC FIELD TRACING. <br>  <br> Sec. 43.9 |
| Fourier Transforms | NOT FOR CLASSIC FIELD TRACING. <br>  <br> Propagation |
| ONLY FOR CLASSIC FIELD TRACING AND CERTAIN ANALYZERS. |  |

In the lower left corner of the dialog there are the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sald | Saves the component into the user-defined component catalog ( $\lrcorner$ Part V). |
| Opens a dialog that shows a three-dimensional view of the component. More |  |
| information about the 3D view is available in Sec. 5.15. |  |

### 54.1 Propagation Tab for Components

This tab is only visible if Classic Field Tracing or certain analyzers are used as simulation engine.


Figure 509. Sample propagation tab for real components showing the propagation matrix (here: General Grating).

```
Sawtooth Grating
Fourier Modal *
```

Figure 510. One cell of the propagation table showing the name of the current building block (top), the currently selected type of propagation (bottom left), and the edit button (bottom right)

The lower part of the propagation tab contains a table representing individual propagation methods for each building block in the component. Each row represents a so-called Boundary Segment, i. e. an Optical Surface with associated stack and the subsequent medium. Each cell ( $\rightarrow$ Fig. 510) has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Name | The name of the corresponding building block. |
| Propagation Selection | Allows you to select the type of propagation for the corresponding building <br> block. |
| Edit | Opens the edit dialog associated with the current propagation. |

If a homogeneous medium is changed to an inhomogeneous one or vice versa, the propagation method for this medium will usually change.
The Component Propagation in the upper part of the tab is a short cut to setting all propagation methods at once. Depending on the type of the component and of the currently active component propagation, there might by some synchronization rules like "A medium has always the same propagation settings as the antecedent surface" or "All stacks have the same propagation settings". The following table gives information about all possible component propagations.

| COMPONENT PROPAGATION | ANNOTATIONS |
| :---: | :---: |
| Collins Integral by ABCD Matrix (For Spherical Lens \& Lens System) | This operator uses the ABCD matrix of the component and thus can handle only certain surface types and homogeneous media All propagation settings are synchronized. $\leftrightarrows$ Sec. 96.5 |
| Customized Propagation <br> (For Double Surface Component, Fiber Element, GRIN Component \& Inhomogeneous Medium Component.) | Uses Thin Element Approximation ( $\checkmark$ Sec. 96.2) propagations for surfaces; several paraxial free space propagations for homogeneous media ( $\varsigma$ Sec. 93) and either the Thin Element Approximation or the Split Step (BPM) propagation ( $\checkmark$ Sec. 96.6) for inhomogeneous media. The settings are synchronized separately for each building block type. |
| Fourier Modal Method (For General Grating) | All propagation settings are synchronized. $\hookrightarrow$ Sec. 96.3 |
| Geometrical Optics <br> (For Light Shaper) | - |
| Geometrical Optics Operator <br> (For Curved Surface, Spherical Lens \& Lens System) | This operator can handle smooth surfaces and homogeneous media. All propagation settings are synchronized. $\lrcorner$ Sec. 96.1 |

The Geometrical Optics Operator shows an additional Advanced Settings sub-tab which is explained in Sec. 96.1.1.
For Customized Propagation there are tools available to Synchronize Surface / Medium Propagation Parameters which means that the settings of the first surface / medium are written to all other surfaces / media.

### 54.2 Editing a Component in the 3D View

If you are in the 3D view of a component ( $\rightarrow$ Sec. 5.15) and you click on a surface with the right mouse button the same surface will appear in red color (signaling the selection) and a context menu with the following entries gets opened ( $\rightarrow$ Fig. 511).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Edit... | Opens the edit dialog ( $\hookrightarrow$ Sec. 35) of the selected surface. |
| Distance... | Opens a dialog for adjusting distance from precedent surface. This menu <br> item is disabled for the first surface. |
| Show Separately | If checked all surfaces except selected one will be hidden. Other surfaces <br> will get visible again by unchecking this item or by clicking Reset View in the <br> general context menu. |

If one performs a double click on a surface the corresponding edit dialog ( $\hookrightarrow$ Sec. 35) will open. By clicking OK in the 3D view dialog all changes made will be inherited by the component.


Figure 511. Context menu of a selected surface in the 3D view.

## 55 Conversion Between Components



Figure 512. Possible conversions between real and ideal components.

Fig. 512 lists all possible conversions between real components (and the ideal component Stored Function). Note that for the Diffractive Lens ( $\hookrightarrow$ Sec. 60.2) and the Diffractive Optical Element (DOE) / Microstructure component ( $\hookrightarrow$ Sec. 60.1) the available conversions depend on their configuration (indicated by gray boxes). The optical setup tool to convert a complete Grating Optical Setup into a General Optical Setup with one or two grating components is explained in Sec. 43.6.2.7. All other conversions can be done via right click on the
icon of the original component in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1). A new component is then added to the Optical Setup which gets all linkages of the original component.

The conversions are done as best as possible, but still the results obtained with the converted component can then differ very much from the results obtained with the original component.

## 56 Index Modulated \& Crystal Components

### 56.1 Crystal Plate

Availability
Optical Setups: General Optical Setup
Accessible: Optical Setup: Components > Index Modulated \& Crystals > Crystal Plate


Figure 513. The structure tab of the Crystal Plate component.

The Crystal Plate component is intended for the rigorous analysis of an anisotropic medium, confined by two plane parallel infinite surfaces. The Structure tab of its edit dialog ( $\hookrightarrow$ Fig. 522 ) provides the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Lateral Extent | In principle, the Crystal Plate component has an infinite lateral extension. However, as this is not feasible for the 3D view ( $\hookrightarrow$ Sec. 5.15) and the light path finder for manual channel configuration ( $\leftrightarrows$ Sec. 43.3.1), a size can be entered here. |
| Aperture | Read-only control which indicates that the component has an infinite lateral extension when simulated. |
| Thickness ${ }^{\text {®V }}$ | The thickness of the crystal can be set here. |
| Waveplate Calculator | FOR UNIAXIAL CRYSTALS AS MEDIUM ONLY. <br> This button opens a Waveplate Calculator ( $\hookrightarrow$ Sec. 119). This will help to configure the uniaxial crystal plate as a waveplate with a certain retarding effect. After closing the calculator dialog with $O k$, the calculated thickness will be set to Thickness and the Orientation will be adapted as well. That means that the optical axis of the crystal is set to the $x$ - $y$-plane of the component automatically. |
| Medium | The optical medium ( $\checkmark$ Sec. 37, $\leftrightarrows$ Sec. 34.1) the crystal consists of. |
| Orientation | For anisotropic Medium only. <br> The orientation of an anisotropic crystal medium in reference to the component's internal coordinate system. In case of uniaxial crystals, only the direction of the optical axis is to be specified ( $\leftrightarrows$ Sec. 5.5). For other types of anisotropic media, a full orientation has to be defined ( $\leftrightarrows$ Sec. 5.6). |
| Coating | A coating ( $\varsigma$ Sec. 36) for front and back face of the crystal can be defined here. It is applied to the outer side of both surfaces. $\leftrightarrows$ Sec. 34.2. |

### 56.2 Index Modulated Components

## Availability

Optical Setups: General Optical Setup \& Laser Resonator Optical Setup
Accessible: Optical Setup: Components > Index Modulated \& Crystal

These components consist of an index modulated medium between two arbitrary surfaces. There are three such components which differ only in their default settings and which media can be used.

- Fiber Element: The default settings resemble an optical fiber and by default a Fiber Medium ( $\rightarrow$ Sec. 37.3.4) is used.
- GRIN Lens: The default settings resemble a gradient index lens. Only GRIN Media ( $\rightarrow$ Sec. 37.3.6) can be used.
- Inhomogeneous Medium Component: By default a Programmable Medium (x-y-z-Modulated) ( $\varsigma$ Sec. 37.3.10) is used.


Figure 514. The Structure tab of an Inhomogeneous Medium Component.
The edit dialog of these components ( $\hookrightarrow$ Fig. 514) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Center Thickness ${ }^{[\mathrm{PV} /}$ <br>  | The distance of the two surfaces measured on the optical axis. |
| Individual Apertures for Each Surface | If you select this option the apertures of the surfaces are set via the Edit button of the First Surface and Second Surface, respectively. |
| Uniform Aperture for Whole Component | If you check this radio button, the same aperture is taken for both surfaces. The common aperture is then set via the Shape and Diameter controls below the radio button. If you double-click on one of the Diameter text boxes, the value from the other text box is being overtaken. |
| First Surface ${ }^{\text {郎 }}$ | Configures the first surface and displays its name. You can Load a new surface from the catalog ( $\leftrightarrows$ Sec. 33), Edit the current surface or View it with the three-dimensional view described in Sec. 35.3. |
| Second Surface ${ }^{\text {PP }}$ | Configures the second surface and displays its name. You can Load a new surface from the catalog ( $\leftrightarrows$ Sec. 33), Edit the current surface or View it with the three-dimensional view described in Sec. 35.3. |
| Medium Between Surfaces ${ }^{\text {Pa }}$ | Configures the medium between the two surfaces and displays its name. You can Load a predefined medium from the catalog ( $\checkmark$ Sec. 33), Edit the current medium ( $\leftrightarrows$ Sec. 37.3.1) or View it with the view described in Sec. 37.2. |

The other tab pages are explained in Sec. 54.

## 57 Multiple Surfaces Components

### 57.1 Lens System

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Components > Multiple Surfaces > Lens System

The Structure tab is divided into four sections (from top to bottom):

1. a preview of the current surface media sequence ( $\hookrightarrow$ Sec. 5.14 )
2. a table with the current surface media sequence
3. a panel with new surfaces which you can drag into the table
4. a button row


Figure 515. The structure tab of the Lens System component showing a sample sequence.

The buttons on this tab have the following functionality:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Tools | The tools for a Lens System are described below. |
| Add | Adds a new surface ${ }^{\text {PE }}$ from the catalog at the end of the table. The same can <br> be achieved by dragging the new surface into the table. |
| Insert | Places a new surface from the catalog before the current surface (which is <br> marked by a triangle in the first table column). |
| Delete | Deletes the selected surface(s). |

The table has the following columns:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Index | The index of the current surface. Note: This item is read-only. |
| Distance ${ }^{\text {PV }}$ | The distance to the precedent surface. The first distance is always zero. |
| Position | The position of the current surface. Note: This item is read-only. |
| Type | The type (or name in case of catalog surface) of the current surface. If the mouse hovers above that column, you can edit or view the current surface ${ }^{\text {PE }}$ or load a new one from the Surfaces Catalog. See also Sec. 34.1. |
| Homogeneous Medium ${ }^{\text {PE] }}$ | The homogeneous medium after the current surface. If the mouse hovers above that column, you can edit or view the medium behind the current surface or load a new one from the Media Catalog. See also Sec. 34.1. Important: The last medium is always identical to that of the transmission type reference coordinate system (see Sec. 43.8.1 for details). Changing that medium will change the embedding medium between this component and the next component (which is connected via the transmission type reference CS) too. |
| Comment | You can enter a comment for a specific surface by clicking into the corresponding comment cell. |

You can select a single table row by clicking into it. By pressing Shift at the same time or with dragging the mouse you can mark consecutive rows. With clicking on the first table column and then drag \& drop the selected rows can be moved (or copied if Shift is pressed at the same time). With Del you can delete the selected surfaces.
The following Tools are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Add Surface from Catalog | Allows loading a surface with preset parameters from the surface catalog <br> ( <br> Sec. 33). |
| Duplicate Selected Sur- <br> face(s) | The currectly selected surfaces are duplicated (including their Distance and <br> Homogeneous Medium). A simple dialog allows you to specify in which row <br> (specified by its Index) the duplicated surfaces are inserted. When you enter <br> $n+1$ with $n$ being the currently highest row index, the surfaces are added at <br> the end of the table. |
| Remove All Surfaces | Removes all surfaces currently set in the table. |
| Synchronize Definition Ar- <br> eas | The definition areas (size and shape) of all surfaces are set to the definition <br> area of the first surface. |
| Apply Coating to All Sur- <br> faces | Loads a coating from the coating catalog and applies it to all (suitable) sur- <br> faces. |
| Remove All Coatings | Removes the coatings from all surfaces (if present). |
| Append Component from | This tool can be used to append the structural information (sequence of sur- <br> faces and media) of a component selected from the catalog. The user has to <br> specify the component that shall be appended. |
| Catalog | You can open a Spread Sheet (file format of VirtualLab Fusion 2 - 4) which <br> is appended at the end of the current surface sequence. |
| Append Spread Sheet | You can open a Zemax OpticStudio® lens file which is appended at the end <br> of the current surface sequence. More details about import from Zemax Op- <br> ticStudio® can be found in Sec. 125.2. |
| Import <br> dio®' Lems File |  |

The other tab pages are explained in Sec. 54 .

### 57.2 Light Guide

## Availability

Optical Setups: Light Guide Optical Setup \& General Optical Setup (only three surface regions per surface layout)

Accessible: Optical Setup: Components > Multiple Surfaces > Light Guide

The Structure > Solid tab is explained in Sec. 57.2.1 and the Structure / Function > Surface Layouts tab in Sec. 57.2.2.
The other tab pages are explained in Sec. 54.

### 57.2.1 Structure > Solid Tab

The Solid tab is divided into four sections (from top to bottom):

1. a 3D preview of the solid ( $\hookrightarrow$ Sec. 5.15 )
2. a table with the current surface media sequence
3. a panel with new surfaces which you can drag into the table
4. a button row


Figure 516. The Solid tab of the Light Guide component showing a sample sequence.
The buttons on this tab have the following functionality:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Tools | The tools are described below. |
| Add | Adds a new surface <br> be achieved by dragging the new surface into the table. |
| Insert | Places a new surface from the catalog before the current surface (which is <br> marked by a triangle in the first table column). |
| Delete | Deletes the selected surface(s). |

The table has the following columns:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\#$ | The index of the current surface. <br> Note: This item is read-only. |
| Position | Shows the absolute position of the surface and allows you to set the position <br> by clicking on the button, either in absolute coordinates or relative to the pre- <br> vious surface. The first surface always has its position fixed to the origin of <br> the internal coordinate system of the component. |
| Orientation | Shows the absolute orientation of the surface and allows you to edit it by <br> clicking on the button, then a dialog with the control described in Sec. 5.6 <br> opens. |
| Surface | The type (or name in case of catalog surfaces) of the current surface. If the <br> mouse hovers above the selected row at that column, you can edit or view the <br> current surface ${ }^{\text {『® }}$ or load a new one from the Surfaces Catalog ( $\neg$ Sec. 34.1). |
| The homogeneous medium after the current surface. If the mouse hovers <br> above the selected row at that column, you can edit or view the medium of <br> the current surface or load a new one from the Media Catalog ( $\leftrightarrows$ Sec. 34.1). <br> Important: The last medium is always identical to that of the transmission <br> type reference coordinate system ( $\rightarrow$ Sec. 43.8.1). Changing that medium <br> will change the embedding medium between this component and the next <br> component (which is connected via the transmission type reference CS) too. |  |
| Comment | You can enter a comment for a specific surface by clicking into the corre- <br> sponding comment cell. |

You can select a single table row by clicking into it. By pressing Shift at the same time you can mark consecutive rows. With Del you can delete the selected surfaces. The following Tools are available:

## ITEM DESCRIPTION

Add Surface from Catalog Allows loading a surface with preset parameters from the surface catalog ( $\rightarrow$ Sec. 33).
Duplicate Selected Sur- The currectly selected surfaces are duplicated (including their Position, Orienface(s) tation, and Back Medium) and inserted after the originally selected surfaces.
Remove All Surfaces Removes all surfaces currently set in the table.
Synchronize Definition Ar- The definition areas (size and shape) of all surfaces are set to the definition
eas area of the first surface.

### 57.2.2 Structure > Surface Layouts Tab

Every surface that has been specified on the Structure > Solid tab ( $\rightarrow$ Sec. 57.2.1) contains a surface layout which in turn may contain several grating regions. The Structure > Surface Layouts tab provides an overview of all that surface layouts as well as editing access to the layouts and their regions.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Surface Name | The name of the surface which has been specified on the Structure > Solid <br> tab. |
| Edit | This button allows editing the layout of the currently selected surface. This <br> has to be done using the dialog described in Sec. 40.2. |
| Info | Information about the number of regions contained by the layout of the cur- <br> rently selected surface. |

### 57.3 Spherical Lens

Availability
Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Components > Multiple Surfaces > Spherical Lens


Figure 517. The edit dialog of the Spherical Lens.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Diameter ${ }^{[\mathrm{PV}}$ | The (aperture) diameter of the lens. |
| Center Thickness ${ }^{\text {PV] }}$ | The center thickness of the lens. If you enter a thickness less than the min- <br> imum thickness (defined by the Diameter and the radii), the thickness is set <br> to the minimum thickness. |
| First Surface | You can set the type of the first surface (Plano, Convex, and Concave, re- <br> spectively). For a Convex or Concave surface you can set the absolute value <br> of the Radius |
| Second Surface curvature. |  |

$$
\begin{align*}
\frac{1}{f_{\text {eff }}} & =(n-1)\left[\frac{1}{R_{1}}-\frac{1}{R_{2}}+\frac{(n-1) d}{n R_{1} R_{2}}\right]  \tag{57.1}\\
f_{\mathrm{b}} & =f_{\text {eff }}\left(1-\frac{(n-1) d}{n R_{1}}\right)  \tag{57.2}\\
f_{\mathrm{f}} & =f_{\text {eff }}\left(1-\frac{(1-n) d}{n R_{2}}\right) \tag{57.3}
\end{align*}
$$

$R_{1}$ and $R_{2}$ are the radii of curvature of the first and second surface, respectively. $n$ is the real refractive index at the Design Wavelength. Eq. (57.1) is the lensmaker's equation.
This component uses a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) to indicate if for example the lens is too thin for the current radii of curvature. The edit dialog cannot be closed with OK in this case.
The other tab pages are explained in Sec. 54.

## 58 Single Surface \& Coating Components

### 58.1 Curved Surface

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Components > Single Surface \& Coating > Curved Surface


Figure 518. The structure tab of a Curved Surface component.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Surface Specification | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to set the optical surface ${ }^{[\boxed{ } \text { 国 }}$ this compo- <br> nent consists of. |
| Homogeneous Medium <br> Behind Surface | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to configure the homogeneous <br> medium |

The other tab pages are explained in Sec. 54.

### 58.2 Off-Axis Parabolic Mirror (Wedge Type)

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Components > Single Surface \& Coating > Off-Axis Parabolic Mirror (Wedge Type)

This component describes an off-axis parabolic mirror used for focusing. Its first surface is a cutout of a paraboloid and its second surface is a plane.


Figure 519. The Structure tab of the Off-Axis Parabolic Mirror (Wedge Type) component.


Figure 520. The fundamental parameters of an Off-Axis Parabolic Mirror (Wedge Type) component.

Its edit dialog ( $\hookrightarrow$ Fig. 519) has the following options on the Structure tab:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reflected Focal Length | The focal length $f$ of the component. Note that this is not the focal length $f_{0}$ <br> of the parent parabola, which is $f_{0}=f \cos ^{2} \beta / 2$. |
| Off-Axis Angle | The angle $\beta$ between incoming and reflected light. $\hookrightarrow$ Fig. 520 |
| Overall Thickness | The maximum extension $T$ of the component in z-direction. $\hookrightarrow$ Fig. 520 |
| Diameter | The diameter $D$ of the circular aperture perpendicular to the z-axis of the <br> component. $\hookrightarrow$ Fig. 520 |
| Medium | The homogeneous medium between the two surfaces. This control is de- <br> scribed in Sec. 34.1. |
| Coating | If needed you can define a coating for the two surfaces. This control is de- <br> scribed in Sec. 34.2. |

The other controls are explained in Sec. 54.

### 58.3 Plane Surface

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Components > Single Surface \& Coating > Plane Surface


Figure 521. The Structure tab of the edit dialog of the Plane Surface component.
The Plane Surface component is intended for the rigorous and fast analysis of the medium transition at a single plane surface. The Structure tab of its edit dialog ( $\rightarrow$ Fig. 522) provides the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component Size ${ }^{[\mathrm{PV}]}$ | In principle the Plane Surface component has an infinite lateral extension. <br> However, as this is not feasible for the 3D view $(\hookrightarrow$ Sec. 5.15$)$ and the light <br> path finder for manual channel configuration ( $\hookrightarrow$ Sec. 43.3 .1$)$, you can enter a <br> Component Size here. |
| Reference Surface | Read-only control to show that the reference surface is a Plane Surface. |
| Aperture | Read-only control to show that the reference surface has an infinite lateral <br> extension when simulated. |
| Coating ${ }^{[\operatorname{PE]}}$ | This control allows you to set the coating which stores the plane layers. <br>  <br> Homogeneous <br> Behind Surface |

The other tab pages are explained in Sec. 54.

### 58.4 Stratified Media

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Components > Single Surface \& Coating > Stratified Media


Figure 522. The Structure tab of the edit dialog of the Stratified Media component.

The Stratified Media component is intended for the rigorous and fast analysis of a sequence of plane layers each
followed by a homogeneous (isotropic or anisotropic) medium. The Structure tab of its edit dialog ( $\hookrightarrow$ Fig. 522) provides the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Component Size ${ }^{\text {[PV }}$ | In principle the Stratified Media component has an infinite lateral extension. However, as this is not feasible for the 3D view ( $\hookrightarrow$ Sec. 5.15) and the light path finder for manual channel configuration ( $\hookrightarrow$ Sec. 43.3.1), you can enter a Component Size here. |
| Reference Surface | Read-only control to show that the reference surface is a Plane Surface. |
| Aperture | Read-only control to show that the reference surface has an infinite lateral extension when simulated. |
| Coating ${ }^{\text {[PE] }}$ | This control allows you to set the coating which stores the plane layers. $\rightarrow$ Sec. 34.2 |
| Homogeneous Medium Behind Surface | This control ( $\hookrightarrow$ Sec. 34.1) allows you to configure the homogeneous medium ${ }^{\text {P® }}$ behind the plane surface this component consists of. |

The other tab pages are explained in Sec. 54.

## 59 Single Surface \& Function Components

### 59.1 Functional Grating

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Components > Functional Single Surface > Functional Grating

The Functional Grating component analyzes an infinite periodic grating by directly defining the diffraction orders.


Figure 523. The Structure tab of the Functional Grating component.
On the Structure tab of the edit dialog of this component ( $\rightarrow$ Fig. 523) you can set the following.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component Size ${ }^{\boxed{V V}}$ | In principle the Grating Component has an infinite lateral extension. However, <br> as this is not feasible for the 3D view ( $\leftrightarrows$ Sec. 5.15) and the light path finder <br> for manual channel configuration ( $\checkmark$ Sec. 43.3.1), you can enter a Component |
|  | Size here. |

On the Function tab you can Edit which diffraction orders have which efficiency. This is done separately For Illumination From Front Side and For Illumination From Back Side using the control described in in Sec. 5.12. On the Channel Configuration > Grating Order Channels sub-tab you then can define which these orders are considered for further simulation, separately For Illumination From Front Side and For Illumination From Back Side.
The remaining controls and tab pages are explained in Sec. 54.
In the Optical Setup View ( $\leftrightarrows$ Sec. 43.1), a Functional Grating has a specific context menu entry to convert it into a Grating ( $\leftrightarrows$ Sec. 60.3).

### 59.2 Functional Meta Lens

## Availability

Optical Setups: General Optical Setup
(Only for General Profile or Ray Results Profile if Flat Lens Package is present.)
Accessible: Optical Setup: Components > Functional Single Surface > Functional Meta Lens


Figure 524. The Channel Operator sub-tab of a Functional Meta Lens.
A Functional Meta Lens consists of a single plane surface ( $\leftrightarrows$ Sec. 35.2.7) on which a channel operator describing a focusing meta material is applied. The structure tab of its edit dialog ( $\rightarrow$ Fig. 524) has three sub-tabs: the Solid sub-tab ( $\leftrightarrows$ Sec. 59.2.1), the Channel Operator sub-tab ( $\leftrightarrows$ Sec. 59.2.2), and the Meta Material Model sub-tab ( $\leftrightarrows$ Sec. 59.2.3).
Furthermore, this tab has a button Import from 'Zemax OpticStudio®' System to import a Binary 2 surface into this component, $\hookrightarrow$ Sec. 125.3.
The remaining controls and tab pages are explained in Sec. 54.
In the Optical Setup View ( $\checkmark$ Sec. 43.1), a Functional Meta Lens has a specific context menu entry to convert it into a Diffractive Lens ( $\leftrightarrows$ Sec. 60.2).

### 59.2.1 Solid Sub-Tab

The Solid sub-tab of the Functional Meta Lens component has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Surface Specification | This control $\left(\hookrightarrow\right.$ Sec. 34.1) allows you to edit the plane surface ${ }^{[P E}$ this compo- <br> nent consists of. |
| Homogeneous Medium This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to configure the homogeneous <br> Behind Surface medium ${ }^{[P E}$ behind the surface. |  |

### 59.2.2 Channel Operator Sub-Tab

The channel operator adds the following phase $\phi$ (in radians) to the phase of the incident light:

$$
\begin{equation*}
\phi=M \sum_{i} A_{i} \cdot \rho^{2 i} \tag{59.1}
\end{equation*}
$$

$M$ is the index of the diffraction order, $A_{i}$ the Coefficient ${ }^{[\mathbb{P V}}$ of the $i^{\text {th }}$ monomial, $2 i$ is the Exponent, and $\rho$ the normalized radius (the distance from the optical axis divided by the Normalization Radius ${ }^{\mathrm{PV}}$ ).
The Degree of Polynomial sets the maximum exponent $2 i$.

### 59.2.3 Meta Material Model Sub-Tab

This sub-tab defines whether the Convergent Mode and/ or Divergent Mode are simulated assuming an idealized meta material.

### 59.3 Functional Modulated Metasurface

## Availability

Optical Setups: General Optical Setup
(Only for General Profile or Ray Results Profile if Flat Lens Package is present.)
Accessible: Optical Setup: Components > Functional Single Surface > Functional Modulated Metasurface


Figure 525. The Channel Operator sub-tab of a Functional Modulated Metasurface.
A Functional Modulated Metasurface consists of a single plane surface ( $\leftrightarrows$ Sec. 35.2.7) on which a programmable channel operator describing a metasurface hologram is applied. The structure tab of its edit dialog ( $\hookrightarrow$ Fig. 525) has three sub-tabs:

- the Solid sub-tab which is the same as for the Functional Meta Lens ( $\leftrightarrows$ Sec. 59.2.1)
- the Channel Operator sub-tab ( $\varsigma$ Sec. 59.3.1) , and
- the Meta Material Model sub-tab ( $\rightarrow$ Sec. 59.3.2)

The remaining controls and tab pages are explained in Sec. 54.
In the Optical Setup View ( $\neg$ Sec. 43.1), a Functional Modulated Metasurface has a specific context menu entry to convert it into a Holographic Optical Element ( $\rightarrow \mathrm{Sec} .60 .4$ ).

### 59.3.1 Channel Operator Sub-Tab

You can program both the effect on the wavefront and the gradient of the wavefront using the corresponding Edit button which opens the Source Code Editor ( $\rightarrow$ Sec. 7.3). A validity indicator ( $\leftrightarrows$ Sec. 5.10 ) shows whether this snippet is consistent.

### 59.3.2 Meta Material Model Sub-Tab

This sub-tab defines whether the Design Mode and / or its Conjugate Mode are simulated assuming an idealized meta material.

## 60 Single Surface \& Stack Components

### 60.1 Diffractive Optical Element (DOE) / Microstructure

## Availability

Optical Setups: General Optical Setup (Only for General Profile and Ray Results Profile.)
Accessible: Optical Setup: Components > Single Surface \& Stack > Diffractive Optical Element (DOE) / Microstructure

This component is listed under two names (Diffractive Optical Element (DOE) and Microstructure) for convenience.


Figure 526. The Channel Operator sub-tab of a Microstructure.

Such a component consists of a single plane surface ( $\hookrightarrow$ Sec. 35.2.7) on which a channel operator describing a microstructure is applied. The structure tab of its edit dialog ( $\hookrightarrow$ Fig. 526) has two sub-tabs:

- the Solid sub-tab ( $\hookrightarrow$ Sec. 60.1.1)
- the Channel Operator sub-tab ( $\hookrightarrow$ Sec. 60.1.2) .

The remaining controls and tab pages are explained in Sec. 54.
In the Optical Setup View ( $\hookrightarrow$ Sec. 43.1), a Microstructure has specific context menu entries to convert it into other component types ( $\hookrightarrow$ Sec. 55).

### 60.1.1 Solid Sub-Tab

The Solid sub-tab of the Microstructure Component has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Surface Specification | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to edit the plane surface ${ }^{[P E]}$ this compo- <br> nent consists of. |
| Homogeneous Medium <br> Behind Surface | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to configure the homogeneous <br> medium |

### 60.1.2 Channel Operator Sub-Tab

The microstructure can be defined as ideal structure (Complex Surface Response) or as real structure (Stack). If defined as transmission, you can use the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Set | Sets the desired Jones Matrix Transmission. When you click on this button you can do the following: <br> - Load a Jones Matrix Transmission from a .ca2 file. <br> - Select from Documents allows you to select an already open Jones Matrix Transmission. <br> - Reset the data to the default transmission. |
| Show | Shows the Complex Amplitude document containing the currently set transmission. |
| Interpolation Method | You can decide whether a Continuous or a Pixelated interpolation is used to interpolate the given data. |

If defined as stack, you can use the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Stack ${ }^{\text {PE }}$ | Configures a stack with one or more micro-structured surfaces and displays its name. You can Load another stack from the catalog ( $\hookrightarrow$ Sec. 33). Furthermore, you can Edit the current stack ( $\hookrightarrow$ Sec. 39.2) or View it. |
| On Front Side of Base Surface | If checked it is assumed that the stack is placed on the front side of the base surface. This means that in comparison to its normal orientation it is rotated by $180^{\circ}$ about the y-axis and thus points against the optical axis. Sec. 39.1.2 shows an example. |
| On Back Side of Base Surface | If checked it is assumed that the stack is placed on the back side of the base surface. This means that it is used in its normal orientation. |
| Method for Stack Analysis | The propagation method used for the stack analysis. In contrast to Thin Element Approximation, the Advanced Thin Element Approximation additionally can handle parabasal effects and absorption. |
| Accuracy Factor ${ }^{\text {PV }}$ | The accuracy factor used for the propagation through the stack, separately for $x$ - and $y$-direction. |
| Sampling Distance ${ }^{\text {[V] }}$ | Instead of the Accuracy Factor you can also specify directly the used sampling distance for x - and y -direction. |

### 60.2 Diffractive Lens

## Availability

Optical Setups: General Optical Setup
(Only for General Profile or Ray Results Profile if Flat Lens Package is present.)
Accessible: Optical Setup: Components > Single Surface \& Stack > Diffractive Lens


Figure 527. The Solid sub-tab of a Diffractive Lens.

A Diffractive Lens consists of a single plane surface ( $\hookrightarrow$ Sec. 35.2.7) on which a channel operator describing a diffractive focusing structure is applied. The structure tab of its edit dialog ( $\hookrightarrow$ Fig. 527) has three sub-tabs: the Solid sub-tab ( $\hookrightarrow$ Sec. 60.2.1), the Channel Operator sub-tab ( $\hookrightarrow$ Sec. 60.2.2), and the Diffractive Structure Model sub-tab ( $\hookrightarrow$ Sec. 60.2.3).
Furthermore, this tab has a button Import from 'Zemax OpticStudio®' System to import a Binary 2 surface into this component, $\hookrightarrow$ Sec. 125.3.
The other tab pages are explained in Sec. 54.
In the Optical Setup View ( $\hookrightarrow$ Sec. 43.1), a Diffractive Lens has a specific context menu entry to convert it into a Functional Meta Lens ( $\hookrightarrow$ Sec. 59.2). A Diffractive Lens in Real Structure mode ( $\hookrightarrow$ Sec. 60.2.4.1) can additionally be converted into a Microstructure ( $\hookrightarrow$ Sec. 60.1).

### 60.2.1 Solid Sub-Tab

The Solid sub-tab of the Diffractive Lens component ( $\hookrightarrow$ Fig. 527) has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Surface Specification | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to change the surface ${ }^{[P E]}$ this component <br> consists of. |
| Homogeneous Medium <br> Behind Surface | This control $(\hookrightarrow$ Sec. 34.1$)$ allows you to configure the homogeneous <br> medium |

### 60.2.2 Channel Operator Sub-Tab

The channel operator adds the following phase $\phi$ (in radians) to the phase of the incident light:

$$
\begin{equation*}
\phi=M \sum_{i} A_{i} \cdot \rho^{2 i} \tag{60.1}
\end{equation*}
$$

$M$ is the index of the diffraction order, $A_{i}$ the Coefficient ${ }^{[\mathbb{P V}}$ of the $i^{\text {th }}$ monomial, $2 i$ is the Exponent, and $\rho$ the normalized radius (the distance from the optical axis divided by the Normalization Radius ${ }^{\mathrm{PV}}$ ). The Degree of Polynomial sets the maximum exponent $2 i$.

### 60.2.3 Diffractive Structure Model Sub-Tab



Figure 528. The Diffractive Structure Model sub-tab of a Diffractive Lens if a Real Structure is assumed.

Whereas the Channel Operator sub-tab defines the phase and thus the direction of the single diffraction orders, the Diffractive Structure Model ( $\hookrightarrow$ Fig. 528) defines the efficiencies of the diffraction orders. This can be done assuming either an Idealized Grating Structure ( $\leftrightarrows$ Sec. 60.2.4) or a Real Structure ( $\hookrightarrow$ Sec. 60.2.4.1).

### 60.2.4 Efficiencies from Idealized Grating Structure

In case of an Idealized Grating Structure you simply define the Efficiency ${ }^{\mathbb{P V}}$ per Order in a table. The table rows are sorted automatically by the Order number. With buttons you can add a new order to the end of the table or remove the currently selected order from the table.

### 60.2.4.1 Efficiencies from Real Structure

A Real Structure can be defined with the following controls ( $\hookrightarrow$ Fig. 528):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Design Wavelength ${ }^{[\operatorname{PV}}$ | The (vacuum) wavelength used for the translation from the wavefront defined <br> on the Channel Operator tab to a height profile. |
| Height Scaling Factor $^{[\operatorname{PV}]}$ | Allows you to alter the modulation depth of the overall structure to change the <br> efficiencies of the distinct orders. |
| Use Profile Quantization | If you check this option the diffractive structure is quantized according to the <br> Number of Height Levels. |
| Export Structure | OnLY AVAILABLE IF USE PROFILE QUANTIZATION IS CHECKED. <br> Allows you to export the diffractive structure into various file formats using the <br> dialog described in Sec. 127.2. |
| Orders for Simulation | Allows you to define which of the diffractive orders is used for simulation. All <br> other orders are suppressed to improve simulation performance and to get <br> clearer results. |

The structure is then analyzed by means of the Thin Element Approximation ( $\hookrightarrow$ Sec. 96.2) if the local grating period is larger than 5 times the wavelength. Otherwise the Fourier Modal Method ( $\hookrightarrow$ Sec. 96.3) is used.

### 60.3 Grating

```
Availability
Optical Setups: General Optical Setup
(Only for General Profile or Ray Results Profile if VirtualLab Fusion Advanced is present.)
Accessible: Optical Setup: Components > Single Surface & Stack > Grating
```

The Grating component analyzes an infinite periodic grating rigorously by means of the FMM / RCWA solver ( $\hookrightarrow$ Sec. 96.3)


Figure 529. The Structure tab of the Grating component.
On the Structure tab of its edit dialog ( $\hookrightarrow$ Fig. 529) you can set the following.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component Size $^{\text {PV }}$ | In principle the Grating Component has an infinite lateral extension. However, <br> as this is not feasible for the 3D view ( $\neg$ Sec. 5.15) and the light path finder <br> for manual channel configuration ( $\neg$ Sec. 43.3.1), you can enter a Component <br> Size here. |
| Grating Stack | Here you first define the periodicity of the grating (1D-Periodic (Lamellar) or <br> 2D-Periodic), then the optical stack ( $\neg$ Sec. 39) describing the grating. To this <br> end the control described in Sec. 34.1 is used. |
| Additionally you can define the orientation of the grating stack, i. e. whether it <br> is placed On Front Side of Reference Surface or On Back Side of Reference |  |
| Surface. |  |

On the Channel Configuration > Grating Order Channels sub-tab you can define which orders are considered for further simulation, separately For Illumination From Front Side and For Illumination From Back Side.
The efficiencies of the simulated orders are calculated by the FMM / RCWA solver ${ }^{\text {『® }}$ ( $\leftrightarrows$ Sec. 96.3). You can Edit it on the Solver tab. On the Solver > Sampling sub-tab you can set the Number of Sampling Points for Look-Up Table, which means for how many incident directions efficiencies are calculated rigorously.

The other tab pages are explained in Sec. 54. In the Optical Setup View ( $\hookrightarrow$ Sec. 43.1), a Grating has specific context menu entries to convert it into other component types ( $\hookrightarrow$ Sec. 55).

Note that for simulations the thickness of the stack is ignored, a phase term $e^{i k z}$ with $z$ being the thickness of the stack is not applied.

### 60.4 Holographic Optical Element

## Availability

Optical Setups: General Optical Setup
(Only for General Profile or Ray Results Profile if Flat Lens Package is present.)
Accessible: Optical Setup: Components > Single Surface \& Stack > Holographic Optical Element


Figure 530. The Channel Operator sub-tab of a Holographic Optical Element.

A Holographic Optical Element consists of a single plane surface ( $\hookrightarrow$ Sec. 35.2.7) on which a programmable channel operator describing a hologram is applied. The structure tab of its edit dialog ( $\hookrightarrow$ Fig. 530) has three sub-tabs:

- the Solid sub-tab which is the same as for the Diffractive Lens ( $\hookrightarrow$ Sec. 60.2.1),
- the Channel Operator sub-tab ( $\hookrightarrow$ Sec. 60.4.1), and
- the Diffractive Structure Model sub-tab which is the same as for the Diffractive Lens ( $\hookrightarrow$ Sec. 60.2.3) The other tab pages are explained in Sec. 54.
In the Optical Setup View ( $\hookrightarrow$ Sec. 43.1), a Holographic Optical Element has a specific context menu entry to convert it into a Functional Modulated Metasurface ( $\hookrightarrow$ Sec. 59.3).


### 60.4.1 Channel Operator Sub-Tab

You can program both the effect on the wavefront and the gradient of the wavefront using the corresponding Edit button which opens the Source Code Editor ( $\leftrightarrows$ Sec. 7.3). A validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent.

### 60.5 Microlens Array

The Microlens Array component supports the specification of a microlens array using a reference surface and a stack. The stack is used to define the structure per period. In addition to the configuration for the structure, the component comes with an advanced channel handling. It supports a lateral channel decomposition, which means per illuminated microlens, a channel mode is generated, which is propagated through the subsequent system. The user can specify some additional options, which are also described within this chapter.


Figure 531. The Solid page of the edit dialog of the Microlens Array component.
Fig. 531 shows the solid page (on the structure slider) of the Microlens Array component. The following parameters can be specified by the user:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component Surface | The microlens array structure is defined on a reference surface. Currently <br> only plane reference surfaces are supported. This control is currently read- <br> only. |
| Domain: Size and Shape | The user can specify the size of the domain/reference surface. The user can <br> select between rectangular and elliptical shape. |
| Medium behind Surface | The medium specification after the surface/microlens array can be config- <br> ured in this section of the dialog. |
| Effect on Field Outside of | If light hits the component and is larger than the size of the domain of the <br> component, it needs to be decided how the field outside is handled. In general <br> blocking or passing is supported. In the current version of VirtualLab Fusion <br> only blocking aperture is supported. |

Next to the specification of the reference surface (and its domain) the user can define the surface add-ons on the corresponding tab page.


Figure 532. The Surface Add-On page of the edit dialog of the Microlens Array component.

Fig. 532 shows the location, where the user can specify the surface add-on. In this case we support the specification of a stack. The period of the stack is used to define the period of the microlens array. The stack should only contain one surface (at least in current implementation). It is recommended that the stack period and the period of the surface in the stack are defined synchronously.

In addition to the structure definition, the component supports an advanced channel configuration.
On the Channel Configuration page the following sub-pages are available:

| PAGE | DESCRIPTION |
| :--- | :--- |
| Master Channels | On this page the user can specify the master channels that shall be used for <br> field tracing (surface channels for $+/+,+/-,-/+$, and $-/-)$. |
| Sub-Channels: x-Domain | Here the user can define the handling for the sub-channels in x-domain. |
| Sub-Channels: k-Domain | Here the user can define the handling for the sub-channels in k-domain. |
| Region Boundary Man- | For the channels (master and sub-channels) the user can specify aperture |
| agement | settings in this section of the dialog. <br> Channel Mode Manage- <br> ment |



Figure 533. The Master Channel page of the edit dialog of the Microlens Array component.

Fig. 533 shows the table to configure the master/surface channels of the Microlens Array component. The configuration is the same as for all other components in VirtualLab Fusion. For the surface (here only one) the plus-plus, plus-minus, minus-minus and minus-plus channel can be opened or closed. This information will be evaluated by the light path finder. In case of pre-configured channel configuration the table is read-only and filled automatically from the system configuration.


Figure 534. The Sub-Channel: X-Domain page of the edit dialog of the Microlens Array component.
Fig. 534 shows the tab page for the configuration of the sub-channels in $x$-domain.
The following options can be selected from the user:

| PAGE | DESCRIPTION |
| :--- | :--- |
| None | If None mode is selected no channel decomposition will be performed. <br> VirtualLab Fusion has a build-in channel decomposition, which is applied if <br> a pointwise sequence is terminated and the mesh of the input field is non- <br> bijective. |
| Structure-Related | In case of Structure-Related channel decomposition, the information of the <br> sub-channels is extracted from the structure (in case of the microlens array <br> the periodic rectangular cells of the stack on the size of the surface domain). <br> If this option is selected a well-defined index logic (in form of a slug) is used <br> to enumerate the channels. On the bottom of the page a schematic scheme <br> is displayed to visualize the index logic of the channels. |
| Channel Mask Data | The user can also specify the channel mask for decomposition as a set of <br> masks (regions). In this case the region information is used for the channel <br> decomposition. This option is not available in current implementation. |
| Programmable | Alternatively the user can implement the channel mask using the VirtualLab <br> Fusion snippet technology. This option is not available in current implemen- <br> tation. |

On the Sub-Channels: k-Domain page there are several options for the channel decomposition in k-domain.

This is not available for the Microlens Array and all options are disabled. This is a preparation for further components that perform a channel decomposition in k-domain (and x-domain).
On the Region Boundary Management page there are several numerical parameters available to define the aperture handling of the master and the subchannel.


Figure 535. The Region Boundary Management page of the edit dialog of the Microlens Array component.

Fig. 535 shows the tab page for the configuration region boundary/aperture settings of the Microlens Array component. The tab page is divided into two parts:

## REGION

## DESCRIPTION

Master Region \& Compo- In this section the user can specify the parameters for the soft edge for the nent master region. The size of the master region is defined on the Solid page of the component. The user can define the location of the edge. The edge can be configure as Inner Soft, Outer Soft or Shared Soft edge. In addition the user needs to specify the size of the edge. This configuration can be done by specification of Relative or Absolute edge width.

## Sub-Channel Regions

In this section the user can specify the parameters for the soft edge for the sub-regions (x-domain). The size of the sub-regions is implicitly defined by the period of the stack (for Structure-Related channel definition). The user can define the location of the edge. The edge can be configure as Inner Soft, Outer Soft or Shared Soft edge. In addition the user needs to specify the size of the edge. This configuration can be done by specification of Relative or Absolute edge width.

On the last page of the Channel Configuration main section of the edit dialog of the Microlens Array component the user has the option to specify the way how the evaluated channels are handled.


Figure 536. The Channel Mode Management page of the edit dialog of the Microlens Array component.
For the channel mode management the following options are currently available:

| REGION | DESCRIPTION |
| :--- | :--- |
| All Channel Modes | If this option is selected, all channels, that are illuminated by the incident light <br> will be processed as output modes. This might be the most consistent speci- <br> fication, but can be lead also to high numerical effort, because depending on <br> the size of the incident light and the size of the channels a high number of <br> channels might be generated. |
| Selected Channel Mode | In addition we also support the processing of one selected channel mode <br> only. The channel mode that should be processed is selected by index of the <br> channel. The index logic for Structure-Related channel definition is visualized <br> (schematic) on the Sub-Channels: $x$-Domain tab page. |

For the channel mode management more options will be added in future.

## 61 Programmable Component

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Components > Programmable Component

This component allows the user to define an own propagation through a user defined component, more precisely
to manipulate the incoming field in an arbitrary way. This can be done by programming so called snippets, which is some source code to be written by the user in C\#.
Furthermore, there is complete freedom for positioning a Programmable Component, i. e. the reference coordinate systems ( $\hookrightarrow$ Sec. 43.8) as well as the input transface ( $\hookrightarrow$ Sec. 93.1 ) can be defined by the user.

### 61.1 Geometry of a Programmable Component

The geometry of a Programmable Component has to be defined by the user, so its definition is completely different from that of other real components. Every building block like optical surfaces, media and so on has to be defined as so called Global Parameter inside the source code editor. Even though there are three different kinds of snippets (described below in Sec. 61.2), each global parameter will be accessible from within each of the snippets, no matter where it has been defined first. For more information regarding the general use of snippets and the source code editor, please see Sec. 7.3.


Figure 537. Example for the bounding box of a prism.

Since the geometry is defined by the user, there is no preview available for this kind of component. But it may be useful, mainly for the positioning ( $\hookrightarrow$ Sec. 61.3), to define a bounding box which is a cuboid meant to circumscribe the whole component ( $\hookrightarrow$ Fig. 537). It can be defined in the panel Bounding Box on page Structure of the edit dialog of the Programmable Component ( $\hookrightarrow$ Fig. 538).


Figure 538. The input controls for the bounding box of a Programmable Component.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Width in $\mathbf{X}$ | Width of the bounding box. |
| Height in $\mathbf{Y}$ | Height of the bounding box. |
| Thickness in $\mathbf{Z}$ | Thickness of the bounding box, may be zero. |

## Note

The Bounding Box will have no effect for the propagation through the component or for any of its functionality. It serves two helpful purposes only. If the box is defined adequately, it allows to get an impression of the components dimensions inside the 3D view of the complete Optical Setup ( $\hookrightarrow \mathrm{Fig}$. 539). And it provides the positions of the two default reference points ( $\leftrightarrows$ Sec. 61.3): one is situated in the center of the front side of the bounding box and one in the center of the box's back side.


Figure 539. Example for viewing the bounding box of a Programmable Component in the system's $3 D$ view.

### 61.2 Propagating through a Programmable Component



Figure 540. The controls for defining the propagation through a Programmable Component.

Defining the propagation through a Programmable Component requires the following controls which can be found on the tab page Structure > Component Specification ( $\hookrightarrow$ Fig. 540).

| ITEM | DESCRIPTION |
| :---: | :---: |
| Relative Position of Field to Position of Input Transface | The field reaching the Programmable Component is always rotated into the Input Transface plane. But if the option Resolve via Zero Padding is checked, equidistant field data will be also padded into zeros in a way that the new origin of the field's coordinate system will be identical to that of the input transface. If the option Keep Stored in the Field's Coordinate System is chosen, no additional preparation will be done. |
| Snippet for Equidistant Field Data | The snippet defining the effect of the Programmable Component on the input field if equidistant field data enters the component. This always happens if the system is analyzed with Classic Field Tracing. Edit opens the Source Code Editor ( $\leftrightarrows$ Sec. 7.3), and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. <br> $\hookrightarrow$ Sec. 61.2.1 |
| Snippet for Non- <br> Equidistant Field and <br> Ray Data   | The snippet defining the effect of the Programmable Component on the input field if non-equidistant data enters the detector. This always happens if the system is analyzed with General Profile or Ray Results Profile. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3), and a validity indicator ( $\hookrightarrow$ Sec. 5.10) shows whether this snippet is consistent. $\rightarrow \text { Sec. 61.2.2 }$ |
| Parameters ${ }^{\text {阿 }}$ | The controls in this group box allow you to set the values of the global parameters of the snippets. $\rightarrow \text { Sec. } 7.4$ |

Programmable Components might be set to a mode where the source code cannot be changed and thus the Input Field Preparation and the Algorithms groupboxes are hidden.

More general information about programming in VirtualLab Fusion can be found in Sec. 7.

### 61.2.1 Snippet for Equidistant Field Data

Here, the effect of the Programmable Component on the InputField has to be programmed. This field is represented by a HarmonicFieldsSet inside the snippet. This kind of object may contain several single harmonic fields which can e.g. represent field data for different wavelengths. They are accessible via InputField[0], InputField[1], and so on.
The code in this snippet may contain any manipulation of the field. Especially, it has to describe the propagation of the field from the Input Transface of the Programmable Component to its Output Transface, including free space propagations and rotations as well as every effect caused by the building blocks of the element's geometry like surfaces and media. Input and Output Transface are the "transfer interfaces" where the field is taken from the free space propagation operator before and given to the free space propagation operator behind the element, respectively. For more information about this concept have a look at Sec. 93.1.

### 61.2.2 Snippet for Non-Equidistant Field and Ray Data

Within the Optical Setup the Programmable Component has no well defined geometry because it is fixed within the source code. So the user has the possibility to implement how an InputRay is manipulated by the programmable component.
The user can specify the following parameters for each ray:

- Position
- Direction
- Optical Path Length / Absolute Phase
- Absorption
- Wavefront Surface Response
- Field Scaling Values
- Complex Surface Response
- Coherent Index

This snippet is used if the system is evaluated with either the General Profile or the Ray Results Profile engine. It is also used for the evaluation of optical path lengths of a system within pulse simulations.
The default implementation of this snippet defines that there is no effect on the incident ray. The user can define any method to modify the parameters of the ray but he is responsible that the implementation of the Snippet for Equidistant Field Data and the Snippet for Non-Equidistant Field and Ray Data provide the correct functionality.

### 61.3 Positioning a Programmable Component

As every other component, a programmable one is positioned via reference coordinate systems, defining relative positions and orientations. For more information about these concepts see Sec. 43.8. Here, the definition of user defined reference points and reference coordinate systems, available only for the Programmable Component, is described.

### 61.3.1 User-Defined Reference Points

There are always two predefined Reference Points for every Programmable Components which can neither be changed nor removed. These Reference Points lie in the center of the front and the back side of the Bounding Box. So every reference coordinate system can be located in one of these two points. By default, the front center is used for the referring "Input" coordinate system and the back center is used for the transmission type reference coordinate system (see Sec. 61.3.2 below).
If more reference points are needed, they can be added on the page Coordinate Systems of the Programmable Component's edit dialog. In the panel Reference Points a list of all defined Reference Points as well as an Edit button can be found ( $\hookrightarrow$ Fig. 541).


Figure 541. The overview for the Reference Points of a Programmable Component.
The Edit button will open the dialog for defining new Reference Points shown in Fig. 542.

| Define Reference Points |  |  |  | $\times$ |
| :---: | :---: | :---: | :---: | :---: |
| List of Reference Points (with Positions in the Internal Coordinate System): |  |  |  |  |
| Description | X | Y | Z | - Remove |
| Front Center of Bounding Box | 0 mm | 0 mm | 0 mm | + Add |
| Back Center of Bounding Box | 0 mm | 0 mm | 0 mm |  |
| Center of Front Side | 10 mm | 7.5 mm | 0 mm |  |
|  |  |  | Cancel | Help |

Figure 542. The edit dialog for user defined Reference Points of a Programmable Component.
The following options are available in this dialog:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\square$ Remove | Removes the selected user defined Reference Point. |
| $\oplus$ Add | Adds a new user defined Reference Point. |
| Description | The unique name of the Reference Point. |
| $\mathbf{X} / \mathbf{Y} / \mathbf{Z}$ | The $x / y / z-c o o r d i n a t e ~ o f ~ t h e ~ R e f e r e n c e ~ P o i n t ~(r e f e r r i n g ~ t o ~ t h e ~ c o m p o n e n t ' s ~ I n-~$ <br> ternal Coordinate System). |

### 61.3.2 User-Defined Reference Coordinate Systems

In order to have maximum freedom in positioning an Optical Setup Element, reference coordinate systems are used. For a Programmable Component, they can be added, changed and removed on the page Coordinate Systems of the Programmable Component's edit dialog, inside the panel Reference Coordinate Systems ( $\hookrightarrow$ Fig. 543) .


Figure 543. The edit dialog for the Reference Coordinate Systems of a Programmable Component.
The following options are available in this panel:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\oplus$ Add | Adds a new user defined reference coordinate systems. |
| $\boxminus$ Remove | Removes the selected reference coordinate systems. Can be used only if <br> the reference CS is not already in use for positioning of subsequent Optical <br> Setup Elements. Furthermore, removing is not possible for the referring "In- <br> put" coordinate systems and the last reference coordinate system besides <br> "Input". |
| Name | The unique name of the reference coordinate systems. Can be changed only <br> if it is not already in use for positioning of subsequent Optical Setup Elements. <br> The name of the referring "Input" coordinate system cannot be changed as <br> well. |
| Reference Point | The Reference Point for defining the origin of the reference coordinate system <br> can be selected here. Please see also Sec. 61.3.1 and Sec. 43.8. |
| Axes | Pushing the button opens a new dialog (see Fig. 544 and description below) <br> for setting the base vectors of the reference coordinate system. The axes <br> have to form a right handed Cartesian coordinate system. |

The axes of an reference coordinate system are to be defined using the dialog shown in Fig. 544.

| Edit Coordinate Axes $\times$ |  |  |  |
| :---: | :---: | :---: | :---: |
| Coordinate Axes (with Directions in the Internal Coordinate System): |  |  |  |
| XAxis | 1 | 0 | 2 |
| Y Axis | 0 | 1 | 0 |
| Z Axis | -2 | 0 | 1 |
| Validity: 0 |  | Canc | Help |

Figure 544. Dialog for the definition of the axes of reference coordinate systems.

The options in this dialog are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| X/Y/Z Axis | The $x / y / z-a x i s ~ o f ~ t h e ~ r e f e r e n c e ~ c o o r d i n a t e ~ s y s t e m ~ t o ~ b e ~ e d i t e d . ~ A l l ~ a x e s ~ h a v e ~$ <br> to form a right-handed Cartesian coordinate system and are to be defined <br> relative to the Internal Coordinate System of the Programmable Component. |
| Validity | This control $(\hookrightarrow$ Sec. 5.10$)$ indicates whether or not the entered axes are valid. |

## 62 Subsystem

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Components > Subsystem

The Subsystem component can be configured to use a complete Optical Setup within an Optical Setup Element. The subsystem has to fulfill some restrictions to be used within the Subsystem Component.
Fig. 545 shows the edit dialog of the Subsystem Component.


Figure 545. The edit dialog of the Subsystem component. Within this example no subsystem is configured yet.

The following settings are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set | The Set button can be used to set a subsystem into the Subsystem com- <br> ponent. The system has to fulfill several requirements which are explained <br> below. After clicking the Set button and selecting the subsystem to set the <br> requirements are checked and the Optical Setup is set into the Subsystem <br> component. |
| Remove | By clicking on the Remove button the underlying system is removed. |
| Show | By clicking on the Show button the underlying system is displayed as <br> VirtualLab Fusion document. |

The following rules have to be fulfilled in order to set up a consistent subsystem into the Subsystem component:

1. There must be an active light source.
2. The system has to be configured consistently.
3. Only one detector which defines the output of the subsystem.
4. There has to be a unique path to the output detector.

All parameters of the Optical Setup Elements within the subsystem are available for Parameter Extraction ( $\hookrightarrow$ Sec. 43.5).

With Pre-Selected Channel Configuration ( $\leftrightarrows$ Sec. 43.3.1) all surfaces of a component but the first one have only one transmission channel open. As this affects also the subsystem component, subsystems with reflection work properly only with Manual Channel Configuration for General Profile and Ray Results Profile.

## 63 Light Shaper

## Availability

Optical Setups: Light Shaping Optical Setup
Accessible: Optical Setup: Components > Multiple Surfaces > Diffractive Light Shaper / Refractive Light Shaper


Figure 546. The structure tab of the edit dialog for a diffractive light shaper.
A light shaper consists of two plane surfaces on which one boundary operator can be placed. This operator can be either a Grating Cells Array ( $\leftrightarrows$ Sec. 40.1.1) for a Diffractive Light Shaper or a Prism Cells Array ( $\leftrightarrows$ Sec. 40.1.2) for a Refractive Light Shaper.
The homogeneous region between this two surfaces is referred to as base block. Therefor the user has to specify the homogeneous Base Block Medium and the Thickness of Base Block. Geometrical Optics is used to propagate through the component.
The Structure tab of the component has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Base Block Medium ${ }^{\text {PE }}$ | The homogeneous medium between the two surfaces. This control is described in Sec. 34.1. |
| Thickness ${ }^{\text {[V] }}$ | The thickness of the base block, i.e. the distance between the two plane surfaces along the z-direction. |
| Use Operator on First Surface I <br> Use Operator on Second Surface | A Light Shaping Optical Setup allows the usage of diffractive, refractive and reflective cells array ( $\hookrightarrow$ Sec. 40.1) either on the first surface (pointing towards the light source) or on the second surface. The type of cell array which shall be used is selected by clicking on the corresponding menu item in the main menu. The currently active cells array can be edited with the corresponding Edit button. |

The other tab pages are explained in Sec. 54 .

## 64 General Grating Component in a Grating Optical Setup



Figure 547. The edit dialog for a General Grating component.

This grating component consists of a base block on whose boundaries optical stacks ${ }^{\mathbb{P V}}$ ( $\hookrightarrow$ Sec. 39) can be placed. The base block is a homogeneous region. Therefor the user has to specify the homogeneous Base Block Medium and the Thickness of Base Block. The stacks can be an arbitrary combination of surfaces and media.
On the bottom of the edit dialog ( $\hookrightarrow$ Fig. 547) you can set up the Preview Wavelength. If you open the edit dialog it is set to the wavelength of the active light source, but you can alter it to any wavelength for which the materials used in the component provide refractive index data. The preview wavelength is used for the calculation of the refractive indices

- in the stack preview which can be accessed via the corresponding View buttons in the Structure > Solid tab.
- in the stack edit dialog which can be accessed via the corresponding Edit buttons in the Structure > Solid tab.
- in the diffraction order calculation and the transition point preview of the FMM edit dialog ( $\hookrightarrow$ Sec. 96.3.1).


### 64.1 Structure Tab

There are the following controls on the Structure tab ( $\hookrightarrow$ Fig. 547):

| ITEM | DESCRIPTION |
| :---: | :---: |
| 1D-Periodic (Lamellar) / 2D-Periodic | Defines the periodicity of the grating. Depending on this setting, several controls in the edit dialog of stacks ( $\hookrightarrow$ Sec. 39.2) and of the FMM ( $\hookrightarrow$ Sec. 96.3.1) change. |
| Base Block Medium ${ }^{\text {PE] }}$ | Allows to view and change the homogeneous medium of the base block. These controls are described in Sec. 34.1. |
| Thickness of Base Block ${ }^{\text {PV }}$ | Allows to set the thickness of the base block. Can be also set to zero if the effects of the base block shall be ignored. |
| Use Stack on First Surface/ <br> Use Stack on Second Surface | Allows you to switch on/off the stack on the front and the rear side of the base block, respectively. If switched off, the stack is not used for the grating analysis but still stored in the component. If you switch it back on, the same stack is available again and can be viewed and changed with the controls described in Sec. 34.1. Both stacks can be used at the same time. |
| No rotation about z-axis/ Rotation about z-axis by $180^{\circ}$ | If a stack is placed on the front side of the base block, it is rotated by $180^{\circ}$ about the y-axis - compared to placement on the rear side and the view displayed in the stack edit dialog ( $\leftrightarrows$ Sec. 39.2). With Rotation about z-axis by $180^{\circ}$ you can apply an additional rotation about the z-axis. Sec. 39.1.2 discusses that in more detail with explanatory figures. |
| Tools | This button reveals two tools which ease the set-up of a grating component. |
| Tools > Swap Stacks | This tool swaps the stacks so that the first stack becomes the second stack and vice versa. |
| Tools > Reduce Component to First Stack | This tool is a short cut for the following steps: <br> 1. Disable the second stack. <br> 2. Set the thickness of the base block to zero. <br> 3. Change the medium of the transmission type reference coordinate system to equal the Base Block Medium. <br> This tool is only enabled if the thickness of the first stack is larger than zero, as otherwise this tool would make the component inconsistent. |

The overall thickness of the grating component (= thickness of first stack + thickness of base block + thickness of second stack) must not be zero. Otherwise the validity indicator in the bottom left corner ( $\hookrightarrow$ Sec. 5.10) shows a white-red cross.
On the bottom of this page the Common Period of both stacks is shown for your information. This period influences the computational effort of the FMM.

## Calculation of the Common Period

If both stacks are used:

1. Both stack periods are rounded to a multiple of 1 pm to deal with possible numerical errors.
2. The least common multiple of this rounded periods is taken as common period.

### 64.2 Propagation Tab

Grating components can be analyzed by means of the Fourier Modal Method (FMM; $\hookrightarrow$ Sec. 96.3). With its edit dialog the number of diffraction orders and the structure decomposition can be set.
You can also use a special version of the Thin Element Approximation operator ( $\hookrightarrow \mathrm{Sec} .96 .2$ ) which ensures that exactly one period is analyzed with sufficient resolution.

## 65 Double Surface Component

## Availability

Optical Setups: Laser Resonator Optical Setup
Accessible: Optical Setup: High Reflective (Start) Mirrors > Outer Surface of Double Surface Component; Laser Crystal


Figure 548. The Structure tab of the Double Surface Component.

This component consists of two surfaces with a medium in between. The structure tab of its edit dialog ( $\hookrightarrow$ Fig. 548 ) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Center Thickness ${ }^{\text {PV }}$ | The distance of the two surfaces measured on the optical axis. |
| Individual Apertures for Each Surface | If you select this option the apertures of the surfaces are set via the Edit button of the First Surface and Second Surface, respectively. |
| Uniform Aperture for Whole Component | If you check this radio button, the same aperture is taken for both surfaces. The common aperture is then set via the Shape and Diameter controls below the radio button. If you double-click on one of the Diameter text boxes, the value from the other text box is being overtaken. |
| First Surface ${ }^{\text {PE] }}$ | Configures the first surface and displays its name. You can Load a new surface from the catalog ( $\hookrightarrow$ Sec. 33), Edit the current surface or View it with the three-dimensional view described in Sec. 35.3. |
| Second Surface ${ }^{\text {PE }}$ | Configures the second surface and displays its name. You can Load a new surface from the catalog ( $\hookrightarrow$ Sec. 33), Edit the current surface or View it with the three-dimensional view described in Sec. 35.3. |
| Medium Between Surfaces | Configures the medium between the two surfaces and displays its name. You can Load a predefined medium from the catalog ( $\hookrightarrow$ Sec. 33), Edit the current medium ( $\hookrightarrow$ Sec. 37.3.1) or View it with the view described in Sec. 37.2. |

The other tab pages are explained in Sec. 54.

## X <br> Ideal Components and Functions

In contrast to Real Components consisting of surfaces and media there are also Ideal Components. This name doesn't mean that these elements work without any numerical error or physical approximation but rather that they are idealized by some means.
Sec. 66 describes the controls that all Ideal Components have in common.
The functionality of Transmission Functions ( $\leftrightarrows$ Sec. 67) is completely defined by a single mathematical operator $\mathcal{T}(x, y)$ which is multiplied with the incoming field. These functions can also be used in the main window via the Functions ribbon tab to generate Jones Matrix Transmission documents which can then be manipulated or multiplied with harmonic fields.
The remaining Ideal Components are explained in Sec. 68 to Sec. 73.

## 66 Edit Dialog of Ideal Components



Figure 549. Example for the edit dialog for Ideal Components.

The edit dialogs for all Ideal Components ( $\hookrightarrow$ Fig. 508) are divided into several pages:

- Coordinate Systems $\hookrightarrow$ Sec. 43.8.1
- Position / Orientation $\hookrightarrow$ Sec. 43.8.2
- Function: This page is specific for the distinct ideal components and is thus explained in the following chapters. But it may contain a Basic Parameters tab as described in Sec. 66.1.
- Channel Configuration $\hookrightarrow$ Sec. 43.9
- Fourier Transforms $\hookrightarrow$ Sec. 43.4.2


### 66.1 Basic Parameters

In the upper part of this tab page you can select one out of three Construction Methods, which are explained in the table below. Depending on the construction method, the tab page looks like shown in Fig. 550 or like in Fig. 551.


Figure 550. Tab page for setting the Basic Parameters of a transmission function with the construction method Single Function with Aperture.


Figure 551. Tab page for setting the Basic Parameters of a transmission function with the construction method Periodic Function.

| CONSTRUCTION METHOD | DESCRIPTION |
| :---: | :---: |
| Single Function without Aperture | Only available in the Optical Setup. Not available for Aperture and Zernike Fringe / Seidel Aberrations transmission. <br> There are no specific controls for this construction method. |
| Single Function with Aperture | The aperture is applied by multiplying the actual transmission value $t$ by 1 inside and by 0 outside the specified aperture. The edge of the aperture can be defined smooth, then the values don't "jump" from 1 to 0 but follow a Gaussian function (decreasing to a value of 0.01 ) as shown in Fig. 552. <br> The controls to setup the aperture are explained in a separate table below. In case of an Aperture transmission function, this option is named just Single Function. |
| Periodic Function | Not available for Zernike Fringe / Seidel Aberrations transmission. In this case you can set the Period ${ }^{\mathbb{P V}}$ of the function. |



Figure 552. Definition of the edge width of an aperture.

The following controls ( $\hookrightarrow$ Fig. 550) are specific for the Single Function with Aperture construction method:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Setting | If checked, a reasonable size of the aperture for the transmission function is <br> determined automatically. This option is available for some functions only, <br> e.g. exponentially decreasing ones. |
| Manual Setting | If checked, the aperture size has to be entered by the user. <br> Shape |
| The aperture may be Rectangularly or Elliptically shaped. |  |
| Relative Edge Width ${ }^{[\mathbb{P V}}$ | The width of the aperture edge, defined relatively to the (smaller of the both <br> values of) diameter. |
| Absolute Edge Width ${ }^{[\mathrm{PV}}$ | The width of the aperture edge, defined in physical units. $\hookrightarrow$ Fig. 310. |

For an Aperture transmission, a separate aperture cannot be set on the Basic Parameters tab. For a Zernike Fringe / Seidel Aberrations transmission, only circular apertures are allowed.
The following controls ( $\hookrightarrow$ Fig. 551) are specific for the Single Function with Aperture construction method:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Period $^{\text {PV }}$ | If Periodic Function was chosen as Construction Method, here the length of <br> the period for the replication is set. The first value is used for replication in <br>  <br>  <br>  <br>  <br>  <br> Specific for grating transmissions: For gratings, the Pecond one for the $y$-direction. will be deter- <br>  <br> mined automatically from the Grating Period and the Rotation Angle, both to <br> be specified at the Physical Parameters panel. |

## 67 Transmission Functions

Generally, the change of amplitude, phase, and polarization of an electromagnetic field can be described by an operator $\mathcal{T}$ named Transmission Operator. Its function is mathematically described as

$$
\begin{equation*}
E_{\mathrm{xy}}^{\mathrm{out}}(x, y)=\mathcal{T} E_{\mathrm{xy}}^{\mathrm{in}}(x, y) \tag{67.1}
\end{equation*}
$$

### 67.1 Transmission Functions in the Main Window

If you want to apply a transmission function to a harmonic field in the main window, you have to prepare this operation by first generating a document called Jones Matrix Transmission via the items in the ribbon group Functions > Transmission Functions. This document consists of a complex scalar component $t(x, y)$ that can change amplitude and phase of the input field, and the Jones matrix $\mathcal{J}(\hookrightarrow$ Sec. 69), that has an effect on the polarization (but in the most cases at least on amplitude or phase too). The transmission process, that means the application of the transmission operator onto the field, can then be simulated by multiplying the harmonic field with the Jones matrix transmission. This can be done via Manipulations > Array - Array Operation > Multiplication ( $\hookrightarrow$ Sec. 22.1.1).
The resulting output field is calculated by

$$
\begin{equation*}
\boldsymbol{E}_{\mathrm{xy}}^{\text {out }}=t\left(\mathcal{J} \cdot \boldsymbol{E}_{\mathrm{xy}}^{\text {in }}\right) \tag{67.2}
\end{equation*}
$$



Figure 553. The edit dialog for generating a Jones Matrix Transmission (here: Random Phase Transmission) in the main window.

The edit dialog of transmission functions ( $\hookrightarrow$ Fig. 553 ) has the following controls specific to the main window.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Generate Cross Section | If checked, a one-dimensional cross section either Along x-Axis or Along $y$ - <br>  <br>  <br> Axis through the defined two-dimensional value distribution will be generated. <br> Default Parameters |

The remaining controls that all types of transmissions have in common are explained in Sec. 66.1 (Basic Parameters tab) and Sec. 67.3.1.1 (Sampling tab), respectively. The type specific parameters are described in Sec. 67.5.1 to Sec. 67.6.4.

### 67.2 Transmission Functions in the Optical Setup

If you want to apply a transmission function to a harmonic field inside an Optical Setup, you can do this by adding the corresponding Ideal Component. The controls specific to transmissions are embedded in the general Ideal

Components dialog ( $\hookrightarrow$ Sec. 66). The controls that all types of transmissions have in common are explained in Sec. 66.1 (Basic Parameters tab) and Sec. 67.3.1.2 (Sampling tab), respectively. The type specific parameters are described in Sec. 67.5.1 to Sec. 67.6.4.

### 67.3 Common Controls of the Transmission Generator Dialogs

Some parameters are common for all types of transmission generator. They regard the lateral sampling of the function, the size and shape of the aperture and the periodicity and are entered via the two tab pages Basic Parameters (Sec. 66.1) and Sampling (Sec. 67.3.1). The third panel Physical Parameters is type specific, so its contents are described in the appropriate sections below.

### 67.3.1 Sampling

As in the Optical Setup transmission functions are applied directly on an incoming harmonic field, the Sampling tab of a transmission function looks and behaves differently in the main window ( $\hookrightarrow$ Sec. 67.3.1.1) and in the Optical Setup ( $\hookrightarrow$ Sec. 67.3.1.2).

### 67.3.1.1 Sampling in the Main Window



Figure 554. Tab page for setting the Sampling parameters of a transmission function in the main window.

Description of the parameters:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Sampling | If checked, the sampling parameters will be determined automatically. |
| Manual Sampling | If checked, the sampling parameters have to be entered by the user. |
| Accuracy Factor | This parameter can be entered for the Automatic Sampling mode only. The Sampling Distance will be divided by this value. |
| Copy Active Parameters from... | This option is available for the Manual Sampling mode only. If pressed, a window will appear where a document can be selected to copy the Sampling Distance or the number of Sampling Points from, depending on which of both is currently selected. |
| Sampling Points | In case of Manual Sampling, the number of sampling points can be entered here. |
| Sampling Distance | In case of Manual Sampling, the sampling distance can be entered here. |
| Array Size | The size of the transmission function, automatically calculated from the settings on the Basic Parameters tab: <br> - In case of a Single Function with Aperture: Diameter plus two times the Absolute Edge Width . <br> - In case of a Periodic Function: Equal to the Period. |

### 67.3.1.2 Sampling in the Optical Setup



Figure 555. Tab page for setting the Sampling parameters of a transmission function in the Optical Setup.
Description of the parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Sampling | If checked, the sampling parameters will be determined automatically. |
| Keep Sampling | The sampling parameters of the incoming harmonic field are used. |
| Manual Sampling | If checked, the sampling parameters have to be entered by the user. |
| Accuracy Factor | This parameter can be entered for the Automatic Sampling mode only. The <br> suggested sampling distance will be divided by this value. However, if the <br> sampling distance of the incoming harmonic field is smaller, it will be taken <br> instead. |
| Sampling Points | In case of Manual Sampling, the number of sampling points can be entered <br> here. |
| Sampling Distance | In case of Manual Sampling, the sampling distance can be entered here. |

### 67.4 Programmable Function

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup

Accessible: Optical Setup: Ideal Components > Programmable Function

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.5). The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.5 Apertures and Lenses

### 67.5.1 Aperture

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Aperture
- Optical Setup: Ideal Components > Apertures and Lenses > Aperture

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.1). The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.5.2 Ideal Lens

## Availability

## Toolboxes: All

Accessible:

- Main window: Functions > Ideal Lens
- Optical Setup: Ideal Components > Apertures and Lenses > Ideal Lens

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.3). If this transmission is created in the main window, the Wavelength Dependency is fixed to Chromatic.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.5.3 Spherical Phase

## Availability

## Toolboxes: All

## Accessible:

- Main window: Functions > Spherical Phase
- Optical Setup: Ideal Components > Apertures and Lenses > Spherical Phase

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.7). If this transmission is created in the main window, the Wavelength Dependency is fixed to Chromatic.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.5.4 Stop

## Availability

## Toolboxes: All

## Accessible:

- Main window: Functions > Stop
- Optical Setup: Ideal Components > Apertures and Lenses > Stop

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.8). The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.5.5 Zernike \& Seidel Aberrations

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Zernike \& Seidel Aberrations
- Optical Setup: Ideal Components > Apertures and Lenses > Zernike \& Seidel Aberrations

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.9).
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.6 Grating Transmissions

### 67.6.1 Rectangular Grating Transmission

## Availability

## Toolboxes: All

Accessible:

- Main window: Functions > Rectangular Grating
- Optical Setup: Ideal Components > Grating Transmissions > Rectangular Grating Transmission

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.2.1). If this transmission is created in the main window, the Wavelength Dependency is not available - always the set up Modulation Depth is used.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.6.2 Sawtooth Grating Transmission

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Sawtooth Grating $\mathbf{N T}$
- Optical Setup: Ideal Components > Grating Transmissions > Sawtooth Grating Transmission

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.2.2). If this transmission is created in the main window, the Wavelength Dependency is not available - always the set up Modulation Depth is used.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.6.3 Sinusoidal Grating Transmission

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Sinusoidal Grating NT
- Optical Setup: Ideal Components > Grating Transmissions > Sinusoidal Grating Transmission

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.2.3). If this transmission is created in the main window, the Wavelength Dependency is not available - always the set up Modulation Depth is used.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.6.4 Triangular Grating Transmission

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Triangular Grating $M$
- Optical Setup: Ideal Components > Grating Transmissions > Triangular Grating Transmission

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.2.4). If this transmission is created in the main window, the Wavelength Dependency is not available - always the set up Modulation Depth is used.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.7 Random Diffusers

### 67.7.1 Random Cells Diffuser and Speckle Type Diffuser

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > Diffusers > Random Cells Diffuser and Ideal Components > Diffusers > Speckle Type Diffuser

The Random Cells Diffuser generates a pattern of cells with a fixed Cell Size but random amplitude and/or phase. The Speckle Type Diffuser applies an interpolation between the cells - thus you see speckles as in reality.


Figure 556. Physical Parameters for a Random Cells Diffuser and a Speckle Type Diffuser.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Use Seed | You can use this option to obtain reproducible results despite the random distribution of the amplitude and/or phase values: With the same Seed ${ }^{\text {PV }}$ and the same physical settings you always obtain the same pattern. |
| Modulation Mode | The Amplitude Mode generates a random amplitude distribution, the Phase Mode generates a random phase distribution. In Complex Mode both amplitude and phase are altered independently. |
| Maximum Amplitude ${ }^{\text {[VV }}$ | In Amplitude Mode or Complex Mode, a random amplitude between zero and Maximum Amplitude is chosen per cell/speckle. |
| Maximum Phase ${ }^{\text {[V }}$ | In Phase Mode or Complex Mode, a random phase between -Maximum Phase and +Maximum Phase is chosen per cell/speckle. |
| Cell Size ${ }^{\text {『V }}$ | If you select this Grid Definition, you enter the cell size directly. |
| Divergence Angle ${ }^{\text {[VV }}$ | In this mode, the cell size is calculated from the full divergence angle using the grating equation Eq. (67.3). |
| Pattern Diameter ${ }^{\text {[VV }}$ | In this mode, you define the overall size of the diffraction pattern at a certain Distance. These values yield the divergence angle and thus the cell size. |
| Achromatic | For the grating equation Eq. (67.3), the wavelength of the incoming harmonic field is taken. |
| Chromatic | The given Wavelength is used for the grating equation Eq. (67.3). |

The following relation is used for the conversion from divergence angle $\alpha$ to cell size $d_{\text {grid }}$, where $n$ is the
refractive index and $\lambda$ is the wavelength.

$$
\begin{equation*}
d_{\text {grid }}=\frac{\lambda}{2 n \sin (0.5 \alpha)} \tag{67.3}
\end{equation*}
$$

### 67.7.2 Random Phase

## Availability

Toolboxes: All
Accessible: Functions > Random Phase 㴔


Figure 557. Physical Parameters for a Random Phase transmission.
The following options and parameters ( $\varsigma$ Fig. 557) are available:

| ITEM |  | DESCRIPTION |
| :---: | :---: | :---: |
| Generate <br> Phase | Quantized | If checked, the generated transmission is quantized, which means that it contains only phase values that are elements of the set $\{-\pi+2 \pi j / Q: j=0,1, \ldots, Q-1\}$, where $Q$ denotes the Number of Quantization Levels. |
| Number of Levels | Quantization | Number of quantization levels used for generating quantized transmissions. |
| Generate <br> Transmission | Hermitean | If checked, the generated transmission is Hermitean, i.e. $t(x, y)=$ $t^{\star}(-x,-y)$, where ${ }^{\star}$ denotes the Hermitean conjugate. |

### 67.8 Miscellaneous Functions

### 67.8.1 Linear Phase

## Availability

Toolboxes: All
Accessible:

- Main window: Functions > Linear Phase $\mathbb{N}$
- Optical Setup: Ideal Components > Miscellaneous Functions > Linear Phase

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\leftrightarrows$ Sec. 41.3.4). If this transmission is created in the main window, the Wavelength Dependency is fixed to Chromatic.
Within the Optical Setup the linear phase which is applied by the functional operator is handled as analytical parameter.
The controls that all transmission functions have in common are described in Sec. 67.3.

### 67.8.2 Single Phase Dislocation

## Availability

Toolboxes: All

## Accessible:

- Main window: Functions > Single Phase Dislocation
- Optical Setup: Ideal Components > Miscellaneous Functions > Single Phase Dislocation

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\varsigma$ Sec. 41.3.6).
The controls that all transmission functions have in common are described in Sec. 67.3.

## 68 Stored Function

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup

Accessible: Optical Setup: Ideal Components > Stored Function

The controls specific for this transmission function are identical to those of the corresponding boundary response ( $\hookrightarrow$ Sec. 41.3.10).
The controls that all transmission functions have in common are described in Sec. 67.3.
In the Optical Setup View ( $\hookrightarrow$ Sec. 43.1), a Stored Function has a specific context menu entry to convert it into a Microstructure ( $\hookrightarrow$ Sec. 60.1).

## 69 Jones Matrix Multiplication

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Ideal Components > Jones Matrices

Some optical elements and devices influence the polarization state of light. Mathematically this process can be described by a change of the electric field vector by a matrix, called Jones matrix $\mathcal{J}$

$$
\begin{equation*}
\boldsymbol{E}_{\mathrm{xy}}^{\text {out }}=\mathcal{J} \cdot \boldsymbol{E}_{\mathrm{xy}}^{\mathrm{in}} . \tag{69.1}
\end{equation*}
$$

For globally polarized fields, this means a change of the Jones vector:

$$
\begin{equation*}
J_{\text {out }}=\mathcal{J} \cdot J_{\text {in }} . \tag{69.2}
\end{equation*}
$$

For your convenience, the four important cases of Phase Shift, Polarizer, Retarder, and Rotator are implemented as separate components in VirtualLab Fusion (described in the following sections Sec. 69.2 to Sec. 69.5). That means, the user does not have to enter the Jones matrix but only one single parameter describing the appropriate physical effect. For other cases an arbitrary Jones Matrix component can be used. The controls described in Sec. 69.1 to Sec. 69.5 are embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 69.1 Jones Matrix

For the multiplication of an arbitrary Jones matrix this function is used.


Figure 558. Controls for defining the parameters of an arbitrary Jones matrix multiplication.
The following parameters are available for a General Jones Matrix Multiplication ( $\hookrightarrow$ Fig. 558):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Jones Matrix ${ }^{\text {PV }}$ | Matrix with four complex entries. |
| Representation | Representation of the complex values in the Jones matrix. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

The control shown in Fig. 558 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 69.2 Phase Shift

A Phase Shift adds a phase difference $\phi$ to both $E_{x}$ and $E_{y}$. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
\exp (i \phi) & 0  \tag{69.3}\\
0 & \exp (i \phi)
\end{array}\right)
$$



Figure 559. Controls for defining the parameters of a Phase Shift.

The following parameters are available for a Phase Shift component ( $\hookrightarrow$ Fig. 559):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Phase Shift ${ }^{[\mathrm{PV}}$ | The phase shift $\phi$ for both $E_{x}$ and $E_{y}$. |
| Jones Matrix | The resulting Jones matrix that describes the phase shift. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

The control shown in Fig. 559 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 69.3 Polarizer

A linear polarizer is a kind of optical filter that will pass only that part of $E_{\mathrm{xy}}$ which oscillates in a certain direction. If this direction is given by an angle $\alpha$, the corresponding Jones matrix is given by

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos ^{2} \alpha & \sin \alpha \cos \alpha  \tag{69.4}\\
\sin \alpha \cos \alpha & \sin ^{2} \alpha
\end{array}\right)
$$

| Parameters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Polarization Angle |  | $45^{\circ}$ | Type | General | $\checkmark$ |
| Jones Matrix |  |  |  |  |  |
| $\left(\begin{array}{ll}J x x & J x y \\ & \\ J y x & J y y\end{array}\right)=($ | 0.5 0.5 | + |  | $0.5+$ $0.5+$ | $\binom{0 i}{0 i}$ |
|  |  |  |  | $\checkmark$ Hermitian Matrix | $\square$ Unitary Matrix |

Figure 560. Controls for defining the parameters of a linearly polarizing Jones matrix multiplication.
The following parameters are available for a Polarizer component ( $\hookrightarrow$ Fig. 560):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Polarization Angle ${ }^{\text {可 }}$ | The angle of the plane of polarization of the filtered, linearly polarized light. |
| Type | Here you can select one of the two special cases Along x Direction, which <br> corresponds to a polarization angle of $\alpha=0^{\circ}$, which means that the compo- <br> nent $E_{y}$ is set to 0, or Along y Direction, which corresponds to a polarization <br> angle of $\alpha=90^{\circ}$, which means that the component $E_{x}$ is set to 0. The case of <br> an arbitrary polarization angle is called General. |
| Jones Matrix | The resulting Jones matrix that describes the linear polarization. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

The control shown in Fig. 560 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 69.4 Retarder

Retarders as e.g. quarter-wave plates or half-wave plates "retard" $E_{y}$ against $E_{x}$ by a phase difference $\phi$. Thereby linearly polarized light can be transformed into circularly polarized and vice versa, for example. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
1 & 0  \tag{69.5}\\
0 & \exp (-i \phi)
\end{array}\right)
$$

| Parameters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase Delay | 0 rad | Type | General | $\checkmark$ |
| Jones Matrix |  |  |  |  |
| $\left(\begin{array}{ll}J x x & J x y \\ \\ J y x & J y y\end{array}\right)=($ | $1+$ $0+$ | $0 i$ $0 i$ | $0+$ $1+$ | $\left.\begin{array}{l}0 i \\ 0 i\end{array}\right)$ |
|  |  |  | ( Hermitian Matrix | $\checkmark$ Unitary Matrix |

Figure 561. Controls for defining the parameters of a Jones matrix retardation.

The following parameters are available for a Retarder component ( $\hookrightarrow$ Fig. 561):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Phase Delay ${ }^{[\mathrm{PV}}$ | The phase shift $E_{y}$ shall get. |
| Type | Here you can select one of the two important special cases Quarter-Wave <br>  <br> Retarder, which corresponds to a phase delay of $\pi / 2$, used for transforming <br> linearly polarized light to circularly polarized and vice versa, or Quarter-Wave <br> Retarder, which corresponds to a phase delay of $\pi$, used for transforming <br> right-circularly polarized light into left-circularly and vice versa. The case of <br> an arbitrary phase delay is called General. |
| Jones Matrix | The resulting Jones matrix that describes the retardation. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

The control shown in Fig. 561 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

### 69.5 Rotator

The angle of rotation $\theta$ of the plane of polarization determines the Jones matrix as follows

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos \theta & -\sin \theta  \tag{69.6}\\
\sin \theta & \cos \theta
\end{array}\right)
$$



Figure 562. Controls for defining the parameters of a Jones matrix rotation.

The following parameters are available for a Rotator component ( $\hookrightarrow$ Fig. 562):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rotation Angle ${ }^{\text {PV }}$ | The angle by which the plane of polarization shall be rotated. |
| Jones Matrix | The resulting Jones matrix that describes the rotation of the plane of polar- <br> ization. |
| Hermitian Matrix | Indicates whether the matrix is Hermitian. |
| Unitary Matrix | Indicates whether the matrix is unitary. |

The control shown in Fig. 562 is embedded in the general dialog for Ideal Components which is described in Sec. 66.

## 70 Beam Splitters

Both kinds of idealized beam splitters (Ideal Beam Splitter $\hookrightarrow$ Sec. 70.1 as well as Polarization Beam Splitter $\hookrightarrow$ Sec. 70.2 ) can be regarded as being infinitely thin semi-transparent mirrors, splitting the incident light into
two different directions. One fraction of light is transmitted straight forward without any direction change. The remaining fraction is reflected following the law of reflection.
The transmitted part can be obtained by connecting the next setup element to the transmission type reference coordinate system. The reflected part is provided to a setup element connected to the reflection type reference coordinate system correspondingly.
The only difference between both types of beam splitters is the calculation of the fractions provided by each of the output reference coordinate system connections.
The following sketches illustrate the functions of the two output reference coordinate systems in three different positioning setups: The first figure Fig. 563 shows the output directions if the beam splitter is not rotated at all. The second figure Fig. 564 illustrates the output directions in case of a basal rotation of the splitter. In the third figure Fig. 565 the effect of an isolated rotation of the splitter on the output directions can be seen.


Figure 563. If the beam splitter is not rotated at all, the mirror normal is the direction vector $(+\sqrt{0.5}, 0,+\sqrt{0.5})^{T}$. A field which travels into local positive z-direction will be split into one transmitted part, running unmodified into local positive zdirection further on and a reflected part, traveling into local negative $x$-direction.


Figure 564. If the beam splitter is rotated basal using a rotation matrix $M$, the mirror normal is the direction vector $\boldsymbol{M} \cdot(+\sqrt{0.5}, 0,+\sqrt{0.5})^{T}$. Due to the rotation being basal, the elements connected to the reference coordinate systems are rotated (referring to global coordinates) as well. A field which travels into local positive z-direction will be split into one transmitted part, running unmodified into local positive z-direction further on and a reflected part. The latter one follows the law of reflection, depending on the mirror's orientation.


Figure 565. If the beam splitter is rotated isolated using a rotation matrix $M$, the mirror normal is the direction vector $\boldsymbol{M} \cdot(+\sqrt{0.5}, 0,+\sqrt{0.5})^{T}$. Due to the rotation being isolated, the elements connected to the reference coordinate systems are not rotated as well. A field which travels into local positive z-direction will be split into one transmitted part, running unmodified into local positive z-direction further on and a reflected part. The latter one follows the law of reflection, depending on the mirror's orientation.

### 70.1 Ideal Beam Splitter

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > beam Splitters > Ideal Beam Splitter

The Ideal Beam Splitter has two types of reference output coordinate systems: Output 0 and Output 1. The output 0 is a transmission type system which provides an unmodified field as described above. The output 1 is a reflection type system that gives a mirrored field which follows the law of reflection as mentioned above.
The energy of the incoming field is split up between both of the outputs. With a slider control you can set the specific Ratio ${ }^{\text {PV }}$ of distributing the energy of the input field to the output fields. Or you can directly set the percentage for one of the two output coordinate systems.


Figure 566. The edit controls for an Ideal Beam Splitter.

The other tab pages are explained in Sec. 66.

### 70.2 Polarization Beam Splitter

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > beam Splitters > Polarization Beam Splitter

The output reference coordinate system "y@100\%" is a reflection type system which gives a mirrored field following the law of reflection. The output reference coordinate system "x@100\%" is a transmission type system, leaving the field's orientation unchanged. See also Fig. 563 to Fig. 565.


Figure 567. The edit controls for a Polarization Beam Splitter.

A polarization beam splitter splits the incoming light according to its degree of polarization. The amplitudes of the different outputs at each of the output reference coordinate systems ("x@100\%" and "y@100\%") are
calculated as follows.

$$
\begin{align*}
& E_{\mathrm{x} @ 100 \%}=\binom{\sqrt{0.5+0.5 p} \cdot E_{x}}{\sqrt{0.5-0.5 p} \cdot E_{y}}  \tag{70.1}\\
& E_{\mathrm{y} @ 100 \%}=\binom{\sqrt{0.5-0.5 p} \cdot E_{x}}{\sqrt{0.5+0.5 p} \cdot E_{y}} \tag{70.2}
\end{align*}
$$

$p$ is the Polarization Degree ${ }^{[\mathrm{PV}}$.
For $p=0$, the polarization beam splitter behaves just like a normal ideal beam splitter with an energy ratio of $50 \%$, while for $p=100 \%$, the field is split into pure $E_{x}$ and pure $E_{y}$ polarization.
The other tab pages are explained in Sec. 66.

## 71 Manipulators

The following manipulation functions are available as Ideal Components in the Optical Setup.

- Field Size and Sampling ( $\hookrightarrow$ Sec. 22.8.2)
- Identity Operator ( $\hookrightarrow$ Sec. 71.1)
- Lateral Shift ( $\hookrightarrow$ Sec. 71.2)
- Sample Spherical Phase ( $\hookrightarrow$ Sec. 71.3)


### 71.1 Identity Operator / Coordinate Break

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Ideal Components > Manipulators > Identity Operator; Coordinate Break

This Ideal Component just returns the incoming field. It can be helpful if you want to change the position of a set of detectors at the same time: Just connect the detectors with the Identity Operator and change the position of the Identity Operator. Fig. 568 shows the edit dialog of the identity operator.


Figure 568. The dialog for an Identity Operator.

ITEM

## DESCRIPTION

Calculate Field in Opera- With this option the user can specify for the Classic Field Tracing whether tor Plane the field shall be calculated in the plane of the identity operator or not. If this checkbox is switched off the ideal component is used for positioning only. The Coordinate Break element which can be found in the Optical Setup Tree is actually an Identity Operator where this option is switched off by default.

### 71.2 Lateral Shift

Availability
Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > Manipulators > Lateral Shift

This operator allows you to shift the incoming field both in $x$ - and $y$-direction by the specified Lateral Shift $\frac{\mathrm{PV}}{}$. The other settings are explained in Sec. 66.


Figure 569. The dialog for setting up a Lateral Shift.

### 71.3 Sample Spherical Phase

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > Manipulators > Sample Spherical Phase

This Ideal Component just resamples the incoming harmonic field so that the spherical phase radius can be removed by a subsequent Optical Setup Element without loss of information. It has no specific settings; the general edit dialog for Ideal Components is explained in Sec. 66.
See also Sec. 12.1.1 for the concept of the spherical phase radius.

## 72 Mirrors

### 72.1 Ideal Plane Mirror

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Ideal Components > Mirrors > Ideal Plane Mirror


Figure 570. The edit dialog for an Ideal Plane Mirror with Function tab selected.
The Ideal Plane Mirror is an idealized plane mirror with the specified Reflectance ${ }^{\text {PV }}$. You can determine the Mirror Inclination via the control for defining an element’s orientation ( $\hookrightarrow$ Sec. 5.6).
The other tab pages are explained in Sec. 66.

### 72.2 Ideal Spherical Mirror

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Ideal Components > Mirrors > Spherical Mirror


Figure 571. Appearance of the Physical Parameters tab in a General Optical Setup.
The Function tab of the edit dialog of a spherical mirror ( $\hookrightarrow$ Fig. 571) has three sub-tabs. The Basic Parameters sub-tab is explained in Sec. 66.1 and the Sampling tab is explained in Sec. 67.3.1.2.
The Physical Parameters sub-tab allows you to enter the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Mirror Radius $^{[\mathrm{PV}}$ | The radius of curvature if the mirror was a real mirror. A negative value means <br> a concave mirror, i.e. a incident plane wave is converging after reflection. |
| Reflectance $^{\boxed{P V}}$ | Allows you to consider the absorption of a real mirror inside the specified <br> aperture. This factor, which must be between 0 and 1, is multiplied to the <br> intensity values of the incident field. The reflectance outside the aperture (if <br> one is specified) is always zero. |

Additional settings for outcoupling are available on this tab in a Laser Resonator Optical Setup (if the mirror is not used as start mirror):

ITEM

## DESCRIPTION

Transmittance
Aperture ${ }^{\text {PV }}$

Inside Via this value the user sets the transmittance inside the aperture at the outcoupling mirror. If Resulting from Reflectance is chosen, the transmittance is adapted via $T=1-R$ automatically. In case of Manual Setting an arbitrary value between 0 and 1 can be adjusted. The value of Reflectance will be leaved unchanged in this case.

Transmittance Outside Herewith the transmittance outside the aperture can be adjusted. This setting
Aperture ${ }^{\text {PV }}$ allows the user to build up unstable resonators.


Figure 572. Appearance of the Physical Parameters tab in a Laser Resonator Optical Setup.

The other tab pages are explained in Sec. 66.

### 72.3 Ideal Stored Mirror Function

Availability
Optical Setups: Laser Resonator Optical Setup
Accessible: Optical Setup: Ideal Components > Mirrors > Ideal Stored Mirror Function


Figure 573. The edit dialog for an Ideal Stored Mirror with Function tab selected.
The Function tab of the edit dialog of the Ideal Stored Mirror Function (Fig. 573) has the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set | Sets a Jones Matrix Transmission which represents the mirror function. |
| Show | Shows the stored mirror function as Jones Matrix Transmission. |
| Interpolation Method | Specifies whether the given sampled data is interpolated or not. |
| Reflectance | The reflectance of the mirror, i.e. a value between 0 and 1. |

The other tab pages are explained in Sec. 66.

## 73 Special Components

The following ideal components are available at Ideal Components > Special Components in the Optical Setup Tree.
-1f-Setup ( $\hookrightarrow$ Sec. 31.1.1)

- 2f-Setup ( $\leftrightarrows$ Sec. 31.1.1)
- ABCD Matrix Setup ( $\hookrightarrow$ Sec. 73.1)
- Evanescent Field Filter ( $\leftrightarrows$ Sec. 73.2)
- Field Decomposition ( $\hookrightarrow$ Sec. 73.3)


### 73.1 ABCD Matrix Setup

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Ideal Components > Special Components > ABCD Matrix Setup

This Ideal Component allows you to define an ABCD matrix from an arbitrary number of optical elements. The effect of this ABCD matrix on the incoming field is then simulated

- for General Profile and Ray Results Profile with the ray transfer equation Eq. (134.1) and
- for Classic Field Tracing with the propagation algorithm given by Collins Eq. (134.3). For this propagation technique the matrix elements $A$ and $B$ of the resulting $A B C D$ matrix must not be zero.


Figure 574. The edit dialog for the $A B C D$ Matrix Setup. The validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows a warning because matrix element A is zero and thus Classic Field Tracing cannot be used to propagate through this Ideal Component.

The edit dialog of this component is the general edit dialog for Ideal Components ( $\leftrightarrows$ Sec. 66). Its Function tab ( $\lrcorner$ Fig. 574) comprises the control to define the ABCD matrix ( $\hookrightarrow \mathrm{Sec} .5 .16$ ) and additionally the following controls:
ITEM DESCRIPTION

| Resulting ABCD Matrix | Shows the resulting ABCD matrix. |
| :--- | :--- |
| Copy from Calculator | Copies the $A B C D$ matrix elements from an $A B C D$ Law Calculator <br> $(\hookrightarrow$ Sec. 104). |

### 73.2 Evanescent Field Filter

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Ideal Components > Special Components > Evanescent Field Filter

This Ideal Component just eliminates the evanescent part of the field and reduces the sampling accordingly. Only propagating plane waves remain in the spectrum of plane waves representation of the field. It can be helpful to study the importance of evanescent fields. It has no specific settings; the general edit dialog for Ideal Components is explained in Sec. 66.

### 73.3 Field Decomposition

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Ideal Components > Special Components > Field Decomposition

This Ideal Component decomposes a field laterally into distinct modes which can improve performance.


Figure 575. The Physical Parameters sub-tab of the Field Decomposition component.

The Function tab of the edit dialog of a Field Decomposition component ( $\hookrightarrow$ Fig. 575) has two sub-tabs. The Basic Parameters sub-tab is explained in Sec. 66.1. The Physical Parameters sub-tab allows you to enter the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Type of Decomposition ${ }^{[P E]}$ | Allows you to choose between Rectangular Segments and Annular Ellipses. <br> Fig. 576 illustrates the two decomposition types. |
| Relative Edge Width for  <br> Decomposition ${ }^{[\operatorname{PV}]}$ Hard edges in a mode can lead to unwanted effects. Thus you have the op- <br> portunity to define a relative edge width during which the field values decrease <br> from their original values to zero. The larger this value, the softer the edge <br> becomes but also the larger the overlap of the modes becomes, which leads <br> to higher numerical effort. <br> Number of Segments ${ }^{[\mathbb{P V}}$ ONLY FOR RECTANGULAR SEGMENTS <br> Defines the number of segments in both x-and y-direction, respectively. <br> Number of Annuli ${ }^{[\mathbb{P V}}$ ONLY FOR ANNULAR ELLIPSES <br> Defines the number of "rings". |  |

The other tab pages are explained in Sec. 66.


Figure 576. A field decomposed into lateral segments (to which different colors were assigned). Left: $3 \times 2$ Rectangular Segments, right: 6 Annular Ellipses.

## XI Detectors: Evaluating Data

Detectors evaluate field data or even a numerical data array in various ways. For example you can extract the value at a certain point, determine the spot size, or calculate the magnetic field.

## 74 Detectors in the Optical Setup

### 74.1 Base Dialog

All detectors in the Optical Setup use the same base dialog which has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Coordinate Systems | $\hookrightarrow$ Sec. 43.8.1 |
| Position / Orientation | $\hookrightarrow$ Sec. 43.8.2 |
| Detector Parameters > Detector Window and Resolution | $\hookrightarrow$ Sec. 74.1.1 |
| Detector Parameters > Detector Function | Contains the specific settings for the respective detector. |
| Free Space Parameters | $\hookrightarrow$ Sec. 43.4.2 |
| H Save | Saves the detector to the catalog ( $\hookrightarrow$ Sec. 33). Not visible if the edit dialog is shown from within the detectors catalog. For technical reasons the Pulse Evaluation detector cannot be saved. |

### 74.1.1 Detector Window and Resolution



Figure 577. The Detector Window and Resolution sub-tab page.

The Detector Window and Resolution sub-tab page of a detector ( $\hookrightarrow$ Fig. 577) allows you to configure both size and position of the detector window as well as the resolution of the detector. The incident field is interpolated accordingly.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Scale Window Size by Factor | If this option is checked, you can define a scaling factor separately for $x$ - and $y$-direction. A scaling factor larger than one means that the incident field is embedded, a factor smaller than one means that it is cropped. |
| Set Window Size | If this option is checked, you can directly set the size of the detector window. |
| Copy from ... <br> \{Detector Window\} | Copies the detector window from an open document window with a rectangle marker. The size and the position of the selection in that document are set into the dialog. This can also be done via right click on the detector icon in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1). |
| Center Position | The center position of the detector window relative to the internal coordinate system of the detector. |
| Scale Sampling Distance by Oversampling Factor | If this option is checked, you can define a scaling factor separately for both $x$ - and $y$-direction. A scaling factor larger than one makes the sampling of the incident field finer, a factor smaller than makes it coarser. |
| Set Sampling Distance | If this option is checked, you can directly set the resolution of the detector. |
| Set Number of Sampling Points | With this option you can choose from various predefined resolutions. Global Options refers to the default number of sampling points defined in the Global options dialog ( $\hookrightarrow$ Sec. 6.12). If you select User-Defined you can choose an arbitrary number of sampling points. <br> Independent from the number of sampling points a one-dimensional input field always stays one-dimensional. In contrast, if you specify only one sampling point for one direction, you can make a two-dimensional field onedimensional. |
| Copy from ... <br> \{Detector Resolution\} | Copies the resolution from an open document window displaying either a harmonic field or a harmonic fields set. The sampling distance of that document is used for it. |
| Interpolation Method | Defines which interpolation method is to be used if resampling of the incident field is necessary. |

The functionality of the Copy from ... button for the detector window can also be accessed from the context menu of a detector in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1).

### 74.2 Copy Settings from Other Detector

This tool can be accessed via the context menu of a detector symbol in the Optical Setup View ( $\hookrightarrow$ Sec. 43.1). It copies certain settings from a template detector to the currently selected detector.


Figure 578. The dialog to copy certain settings from another detector.
Its edit dialog ( $\hookrightarrow$ Fig. 578) has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Template Detector | Here you can select the detector from which the settings are copied. The <br> currently selected detector is excluded from that list because it is the target <br> of the copy operation. |
| Detector Window and <br> Resolution | If this option is checked, all settings on the Detector Window and Resolution <br> tab $(\hookrightarrow$ Sec. 74.1 .1$)$ are copied from the template detector. |
| Position and Orientation | If this option is checked, the basal position and orientation settings <br> $(\hookrightarrow$ Sec. 43.8 .2 .2$)$ are copied from the template detector. |

### 74.3 Programmable Detector

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Programmable Detector

The Programmable Detector allows you to evaluate the incoming field with a snippet.
The Detector Parameters tab contains two sub-tabs: the Detector Window and Resolution sub-tab which is explained in Sec. 74.1.1 and the Detector Function sub-tab which is explained below.
The remaining tab pages are explained in Sec. 74.1. General information about programming in VirtualLab Fusion can be found in Sec. 7.


Figure 579. The Detector Function page of the Programmable Detector.
On this tab page you can define the detector function by two snippets (for equidistant and non-equidistant data,
respectively). In these snippets you have access to the incoming field in spatial domain via the InputField variable in case of equidistant data and the RayTracingResult variable in case of non-equidistant data, respectively. In both cases the field in spectral domain is available via the SpectralField variable, a ModeCollection which can contain a mix of equidistant and non-equidistant member fields. The settings on the Detector Window and Resolution tab are already applied to the fields available within the snippets.
For equidistant data the user can specify whether the incident field shall be calculated centered to the optical system and whether the linear phase of the incident field shall be handled analytically or be sampled before applying the snippet of the Programmable Detector.
The Detector Function tab ( $\hookrightarrow$ Fig. 579) contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Evaluate Field in x-Domain | If you check this option, the field in x-domain is calculated and available as InputField or RayTracingResult variable in the snippets. Otherwise these variables are null. |
| Evaluate Field in k-Domain | If you check this option, the field in k-domain is calculated and available as SpectralField variable in the snippets. Otherwise this variable is null. The dialog ensures that at least the spatial or the spectral field is evaluated. |
| Linear Phase | The user can specify whether the linear phase of the incident equidistant field shall be sampled (option Resolve via Sampling) or whether it is handled analytically by the snippets (option Keep Stored as Vector). |
| Relative Position of Field to Position of Input Transface | The field reaching the Programmable Detector is always rotated into the detector plane. But if the option Resolve via Zero Padding is checked, equidistant field data will be also padded into zeros in a way that the new origin of the field's coordinate system will be identical to that of the detector. If the option Keep Stored in the Field's Coordinate System is chosen, no additional preparation will be done. |
| Snippet for Equidistant Field Data | The snippet evaluated by the Programmable Detector if equidistant field data enters the detector. This happens if the system is analyzed with Classic Field Tracing or if the system is analyzed with General Profileand the last Fourier transform done is not a pointwise one. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3), and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Snippet for Non- <br> Equidistant Field and <br> Ray Data   | The snippet evaluated by the Programmable Detector if non-equidistant data enters the detector. This happens if the system is analyzed with General Profile and the last Fourier transform done is a pointwise one or if the system is analyzed with Ray Results Profile. Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3), and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. |
| Parameters ${ }^{\text {PE] }}$ | The controls in this group box allow you to set the values of the global parameters of the snippets. $\hookrightarrow$ Sec. 7.4 |

Programmable Detectors might be set to a mode where the source code cannot be changed and thus the Input Field Preparation group box, the Use Field in Spatial / Spectral Domain check boxes, and the Algorithms groupbox are hidden.

## Notes for Snippet Developers

A Programmable Detector can also be used in the main window ( $\hookrightarrow$ Sec. 75.1). Then the ParentSystem / ParentLightPath is null and the IndexOfDetector is -1 , which must be handled in the snippets.

### 74.4 Universal Detector

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Field Visualization > Universal Detector

This detector can be used to evaluate any vectorial component ( $E_{x}, E_{y}, E_{z}, H_{x}, H_{y}$, or $H_{z}$ ) of an incoming light distribution. These components are given as different subsets of an Electric, Magnetic or Electromagnetic Field ( $\hookrightarrow$ Sec. 13.1, $\hookrightarrow$ Sec. 13). If the incoming light has multiple modes, one field is generated per mode and all resulting data are collected in one Set Of Objects ( $\leftrightarrows$ Sec. 16). Depending on the subsequent configuration coherent modes can be added up (with different settings) or not.
The implemented formulas for the calculation of the magnetic field are given in Sec. 137.7.1.
Based on the Electromagnetic Field any merit function can be evaluated. This is realized in VirtualLab Fusion by detector Add-ons which are available in the Universal Detector.


Figure 580. The edit dialog of the Universal Detector.

The edit dialog of this detector ( $\hookrightarrow$ Fig. 580) provides the following sub pages for different configuration settings:

| ITEM | DESCRIPTION |  |
| :--- | :--- | :--- |
| Field Quantities | Via the controls on this tab page the user can define which field quantities in <br> which domain shall be evaluated. A detailed description of the parameters <br> can be found under Sec. 74.4 .1 |  |
| Detector <br> Domain) | Window | (x- |
| On this tab page the user specifies the detector window and the resolution |  |  |
| (for gridded data) for the evaluated field in x-domain. For details please check |  |  |
| Sec. 74.4.2. |  |  |

In the following sections the controls on the tab pages are explained more in detail.

### 74.4.1 Field Quantities

The tab page Field Quantities allows the user to specify the electromagnetic field components to evaluate as well as the domains in which the component shall be calculated. A selection of advanced configuration options are also available which are explained below.
Fig. 581 shows the controls to configure the field quantities.


Figure 581. The user interface to configure the field quantities within the universal detector (and the system modeling analyzer).

The following settings can be configured

| ITEM | DESCRIPTION |
| :---: | :---: |
| Components | Allows the user to select which vectorial components of the field are evaluated. The dialog ensures that at least one component is selected. |
| Domain | The user can select whether to evaluate the electromagnetic field in $x$-domain and/or k-domain. The dialog ensures that at least one option is selected. |
| Configure Field Data Visualization by Electromagnetic Field Quantity AddOn | In the controls explained above the user configures which quantities/domains shall be calculated by the detector. This input data is provided to the detector Add-Ons of the Universal Detector. A standard add-on is the output of the data. Here the user can select what of the evaluated quantities should be generated as document windows in VirtualLab Fusion. By clicking on the configuration button a dialog opens in which the mentioned configuration can be done. More information on that see Sec. 74.4.5.1. |
| Apply Paraxial Approximation for Component Calculation | The Universal Detector provides an option to calculate field components by paraxial assumptions. Typically the field components Ex and Ey are provided by the engine. All other components can be calculated from these two field component. To speed up detector evaluation VirtualLab Fusion provides an option to use simplified formulas for the field component calculation. This enable also that there is no need to have special versions of detector addons with paraxial assumptions. |
| Sum Mutual Coherent Modes | Source modes in VirtualLab Fusion are typically incoherent (different or same wavelength). During propagation through an optical setup a source mode could be split into different modes (e.g. at a grating), where the modes are typically coherently to each other. The Universal Detector provides an option whether the coherent modes should be summed up before further processing via Detector Add-ons. If the user decides to Sum Mutual Coherent Modes additional options will be available to define how the modes shall be summed up. |
| How to Sum Mutually Coherent Modes | If the user selected to Sum Mutual Coherent Modes, he needs to specify the summation type how the modes shall be summed up. There are various Summation Types how coherent modes can be summed up: Coherent Summation, Incoherent Summation, and Partial Coherent Summation. For the latter you can specify the degree of coherence by entering a Coherence Time ${ }^{\text {[V] }}$ (or copying it from a Coherence Time \& Length Calculator $\lrcorner$ Sec. 105). |

Note: The settings in these control define which field component in which domain shall be calculated. This is not identical with the result visualization of the Universal Detector. The values to show as data array are configured under Electromagnetic Field Quantities. Detailed information see Sec. 74.4.5.1.

### 74.4.2 Detector Window (x-Domain)

The user can specify the detector window and the resolution (for gridded data) in $x$-domain for the Universal Detector. The configurations are done in the tab page Detector Window ( $x$-Domain).
Fig. 582 shows the user interface to configure the detector window in $x$-domain.


Figure 582. The user interface to configure the detector window (x-domain) within the universal detector (and the system modeling analyzer).

In these controls the user can specify the following parameters:
ITEM DESCRIPTION

| Detector Window <br> tered Around | The user has to specify where the output data of the detector shall be given. <br> VirtualLab Fusion provides two options to the user: Detector Position and <br> Center of Field Mode. |
| :--- | :--- |
| Lateral Window Position | In x-domain the user has an additional freedom to define also a lateral shift of <br> the coordinate system. This option is independent to the general positioning <br> control of each optical system element. |
| Detector Window Size | In the group box Detector Window Size the user can specify the window size <br> for evaluation of the field component. The window size can be specified From |
|  | Field Data or via Manual Setting. In case of From Field Data the field size <br> might be different for each mode that illuminates the detector. In that case the |
|  | user can specify an additional Size Scaling Factor. In case of Manual Setting <br> the same detector window size is applied on each incident field mode. In this <br> case the user needs to specify the Window Size directly. |
| Detector Grid Resolution | Finally the user can specify in the section Detector Grid Resolution the grid <br> which is used to generate gridded data by the Universal Detector. The user <br> has again two options for the general specification of the resolution: From |
|  | Field Data or Manual Setting. In case From Field Data each incident mode is <br> analyzed and the input sampling is used as detector grid. The user can op- |
| tionally enter a Grid Period Scaling Factor. If the user selects Manual Setting |  |
| all incident modes will converted on the same grid. In case Manual Setting is |  |

### 74.4.3 Detector Window (k-Domain)

The user can also specify the detector window and the resolution (for gridded data) in k-domain for the Universal Detector. The configurations are done in the tab page Detector Window (k-Domain). The configuration is quite similar to the Detector Window (x-Domain). Main difference is that size and grid period are specified in wave numbers and not in length unit.
Fig. 583 shows the user interface to configure the detector window in k-domain.


Figure 583. The user interface to configure the detector window (k-domain) within the universal detector (and the system modeling analyzer).

In these controls the user can specify the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Detector Window <br> tered Around | Cen- |
| The user has to specify where the output data of the detector shall be given. <br> VirtualLab Fusion provides two options to the user: Detector Position and <br> Center of Field Mode. |  |
|  | In the group box Detector Window Size the user can specify the window size <br> for evaluation of the field component. The window size can be specified From <br> Field Data or via Manual Setting. In case of From Field Data the field size <br> might be different for each mode that illuminates the detector. In that case the <br> user can specify an additional Size Scaling Factor. In case of Manual Setting <br> the same detector window size is applied on each incident field mode. In this <br> case the user needs to specify the Window Size directly. |
| Detector Grid Resolution | Finally the user can specify in the section Detector Grid Resolution the grid <br> which is used to generate gridded data by the Universal Detector. The user <br> has again two options for the general specification of the resolution: From <br> Field Data or Manual Setting. In case From Field Data each incident mode is <br> analyzed and the input sampling is used as detector grid. The user can op- <br> tionally enter a Grid Period Scaling Factor. If the user selects Manual Setting <br> all incident modes will converted on the same grid. In case Manual Setting is <br> selected the user has the option to select whether to Set Grid Period (which <br> corresponds to the sampling distance) or to Set Grid Points. |

### 74.4.4 Gridless Data

VirtualLab Fusion supports also the evaluation of the electromagnetic field of gridless data by the Universal Detector. The gridless output is only possible if the incident light at the detector comes in gridless format. In addition there is another limitation, which will not allow the generation of gridless data output of the Universal Detector: In case more than one coherent mode illuminates the detector and the user has defined to sum up the coherent modes this summation can also be only done on an equidistant grid. In case the input data is gridded but the user defined to show only gridless data the detector will fall back to gridded data output. Fig. 584 shows the user interface to configure the gridless data output of the Universal Detector.


Figure 584. The user interface to configure the gridless data output of the universal detector (and the system modeling analyzer).

The user can specify the following options in the section Gridless Data:

## DESCRIPTION

Show Result w/o Interpolation for Gridless Data

By selecting Yes for Show Result w/o Interpolation for Gridless Data the user defines that he likes to generate gridless data as detector output. If the incident light of the detector comes in gridded format gridless data will not be generated by the detector. If Yes is selected additional options are shown below the decision controls.
Show Interpolated Result If the user selects to generate gridless data he can activate to generate also on Equidistant Grid gridded data. If this option is checked and the input field comes in gridless format the Universal Detector will generate gridless as well as gridded data. data shall contain Field Values or only Positions, Directions and Wavefront data. The generation of Positions, Directions and Wavefront corresponds to the standard results generated in classical ray tracing software. Note: In the modeling profile Ray Result the universal detector is restricted to generate always Positions, Directions and Wavefront data.
Gridless Sampling Points Finally the user can specify the gridless sampling points that shall be generated. The user has two options: Use Number of Points from Field Data or to use Manual Sampling. In case of Number of Points from Field Data the number and location of points for gridless data is directly used from the input field of the detector. If the user decides to use Manual Sampling the point selection mode has to be specified. VirtualLab Fusion supports the following selection modes: $x$ - $y$-Grid, Hexapolar and Random. For the specification of $x-y$-Grid the user needs to specify the number of points in $x$ - and $y$-direction. In case of Hexapolar the density has to specified. In Random point selection mode the user need to specify the number of points, the seed value for random generation and also whether a mesh shall be generated for the random generated points. Detailed information can be found in Sec. 43.4.4.1.

### 74.4.5 Detector Add-ons

In the tab page Add-ons the user has the option to define a tree of Detector Add-ons. $\hookrightarrow$ Fig. 585 shows the user interface to specify the detector Add-ons.


Figure 585. The user interface to define the detector add-ons which can be used within the universal detector.
A detector add-on is typically defined by a user-defined/customized snippet. This enables the full flexibility to develop any merit function the user has in mind even if the merit function is not yet available as prepared addon. VirtualLab Fusion comes with a variety of predefined detector add-ons which can be easily synchronized via pushing the corresponding button (via internet).
Note that you can chain the add-ons: One add-on can use the output of another add-on as input. Thus in the end you have a tree of add-ons with the Data from Universal Detector as root. There is a pre-defined add-on Electromagnetic Field Quantities ( $\hookrightarrow$ Sec. 74.4.5.1) directly dependent on Data from Universal Detector.
In the tree view on top of the tab page you can use drag \& drop to resort the add-ons and change their dependencies (a child entry always gets its input from the direct parent). For each add-on there are the following controls available in the tree view.

| ITEM | DESCRIPTION |
| :---: | :---: |
| 煖/ | Allows you to toggle whether the output of this add-on is shown (\%) or not ( its output is required as input for another add-on. |
| ね | For the Electromagnetic Field Quantities this button opens the dialog described in Sec. 74.4.5.1. For all other add-ons the dialog described in Sec. 74.4.5.2 allows you to edit and save the add-on. |
| $\times$ | Closes the add-on. Before, you are asked whether you want to save the add-on snippet. |

On the bottom of this tab page there are the following buttons.

| ITEM | DESCRIPTION |
| :--- | :--- |
| New | Adds a new default add-on. |
| Load | Loads and adds an add-on stored on hard disc. By default a folder with add- <br> ons prepared by LightTrans is opened. |
| Duplicate | Duplicates the selected add-on and append it to the detector add-on tree. For <br> this operation a detector add-on has to be selected in the tree above. Note: <br> The default add-on (Electromagnet Field Quantities) cannot be duplicated. |
|  | The folder with the add-ons prepared by LightTrans is updated via Internet. <br> Optionally also the snippets of all favorites ( 4 Sec. 76.9 ) are then updated <br> if they have the same name as a predefined addon. The values of your fa- <br> vorites's snippet parameters are kept. |

## Note for Snippet Developers

Note that an Universal Detector can also be used in the main window ( $\hookrightarrow$ Sec. 75.1). Then the ParentSystem is null and the DetectorIndex is -1 , which must be handled in the snippet.

### 74.4.5.1 Electromagnetic Field Quantities

The Universal Detector comes always with the Electromagnet Field Quantities add-on by default. This add-on can not be removed from the tree. It is also not possible to change its position in the tree of detector add-ons. The task of the Electromagnet Field Quantities add-on is to show the available field components in its domains. The detector add-on could be disabled. In addition it allows to define a subset of the information evaluated by the Universal Detector.
$\hookrightarrow$ Fig. 586 shows the edit dialog of the Electromagnetic Field Quantities add-on.


Figure 586. The edit dialog of the Electromagnet Field Quantities add-on.

Within the edit dialog the following options can be configured

| ITEM | DESCRIPTION |
| :---: | :---: |
| Field Components | Allows you to select which vectorial components of the field shall be displayed. Only calculated field components (from Universal Detector or System Modeling Analyzer can be selected. The dialog ensures that at least one component is selected. |
| Domain | The user can select whether to show the field in x-domain and/or k-domain. Only domains which are calculated can be selected |
| Amplitude | If selected only the amplitude of the field will be generated as output. |
| Amplitude/Phase (w/o Wavefront Phase) | The user can also select whether to show amplitude and phase of the calculated field component. The phase will be given in 2PI modulo format and will not include the smooth wavefront phase. |
| Wavefront Phase | In addition to the amplitude (and 2PI modulo phase) of the field component, it is also supported to show the wavefront phase. The wavefront phase will be displayed as a separate data array and is common for all field components. |
| Wavefront Phase w/o Spherical Part | For many applications it might be meaningful to investigate only the residuals of the wavefront phase. Therefore the user can select whether to show the wavefront phase without the spherical part. The spherical part is evaluated by fitting of the given wavefront phase data. |
| Show Polarization El- lipses | Only available if at least two E-Field Components are selected. If checked, polarization ellipses for the E-field will be calculated and added to the output. |
| Plane | Only available if Show Polarization Ellipses is checked. <br> If all three E-Field Components are selected, the plane to calculate the ellipses for can be chosen here. |
| 䃜 | Only visible if Show Polarization Ellipses is checked. <br> This button will open a dialog for configuring the view settings for the graphics add-on which visualizes the polarization ellipses. It is described in Sec. 11.7.3. |
| Ignore Vanishing Jones Vectors | If checked, no polarization ellipses will be calculated at positions where the amplitudes of both of the Jones vector's components are below a certain fraction (given be Threshold) of the maximum field amplitude (see also Sec. 11.8). |
| Threshold | Only available if Ignore Vanishing Jones Vectors is checked. The threshold for identifying vanishing Jones vectors. |
|  | The color table ( $\hookrightarrow$ Sec. 11.2.4) to be used (initially) in the resulting document window. |
| Color Table |  |
| Color for Undefined Values | The user can select a color for undefined values. This will be used (initially) in the resulting document window. |
| Interpolation Method | The interpolation method of the resulting data array(s). |

### 74.4.5.2 Edit Dialog for Detector Add-ons



Figure 587. The edit dialog for a (sample) detector add-on.

The edit dialog for detector add-ons ( $\hookrightarrow$ Fig. 587) has the following standard controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Name | The name of the detector add-on. It is equal to the Title defined on the Snippet <br> Help tab when you click on Edit. |
| Edit | Opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3 ). |
| Read Me | Shows the Snippet Help ( $\hookrightarrow$ Sec. 7.3 .3$)$ in a separate window. <br> Validity <br> $H$ |
| The validity indicator $(\hookrightarrow$ Sec. 5.10$)$ shows whether the snippet defining the <br> detector add-on is consistent. |  |
| Saves the detector add-on to hard disc so that it can be loaded into another |  |
| detector. If you save the add-on in the default path, it is added to the Favorites |  |
| in the ribbon for Data Arrays and Harmonic Fields Sets ( $\leftrightarrows$ Sec. 76.9$).$ |  |

In addition to the standard controls mentioned in the table above the dialog may contain a list of user controls which are dynamically defined by the type of global parameters of the detector add-on, $\hookrightarrow$ Sec. 7.4.

### 74.5 Field Visualization

### 74.5.1 Angular Spectrum Visualizer

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Detectors > Field Visualization > Angular Spectrum Visualizer

This detector shows the angular spectrum, i. e. the (physical) Fourier transform ( $\hookrightarrow$ Sec. 31.1) of the field. The used dialog is nearly the same as for the Raw Data Detector, described in Sec. 74.5.5.

### 74.5.2 Camera Detector

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Light Shaping Optical Setup

## Accessible:

- Optical Setup: Camera Detector; Detectors > Field Visualization > Camera Detector
- Ribbon: Detectors > Camera Detector


Figure 588. The specific settings for the camera detector in a General or a Light Guide Optical Setup.


Figure 589. The specific settings for the camera detector in a Light Shaping Optical Setup.

The settings of the Camera Detector depend on the type of Optical Setup it is used in. It can also be applied on harmonic fields and harmonic fields set via Detectors > Camera Detector. In this case it behaves as if it would be used in a General Optical Setup.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Handling of Coherence | Only available in a Light Shaping Optical Setup <br> The camera detector supports two operation modes to evaluate the distinct modes of the incident field. In Standard Mode the coherent modes are interpreted coherently. The Incoherent Approximation evaluates the incident coherent modes by incoherent superposition which can speed up calculations. |
| Coherence Parameters | Only available in a General or a Light Guide Optical Setup <br> There are various Summation Types how coherent modes can be summed up: Coherent Summation, Incoherent Summation, and Partial Coherent Summation. For the latter you can specify the degree of coherence by entering a Coherence Time ${ }^{\mathrm{PV} V}$ (or copying it from a Coherence Time \& Length Calculator $\hookrightarrow$ Sec. 105). These settings have no effect for Classic Field Tracing as this engine only supports incoherent modes. |
| Components to Integrate | Only available in a General or a Light Guide Optical Setup <br> You can select one or more vectorial components which are shown in the result. In a Light Shaping Optical Setup always Ex-Component and EyComponent are used and thus this group box is invisible. |
| Real Color / False Color | Allows you to preset the color mode ( $\hookrightarrow$ Sec. 14.2) of the resulting Chromatic Fields Set if it is a two-dimensional one. |
| \{Color Table Button\} | Only for False Color mode. <br> Allows you to select one color table ( $\hookrightarrow$ Sec. 11.2.4). |

If the Camera Detector is used in a Light Shaping Optical Setup, both the size of the Detector Window and the Detector Resolution can only be set manually.

The remaining controls of this dialog are explained in Sec. 74.1.

### 74.5.3 PSF \& MTF

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Field Visualization > PSF \& MTF

This detector calculates both the Point Spread Function (PSF) and the Modulation Transfer Function (MTF). The user is responsible to place the detector at the appropriate evaluation position (= focus), which is expected to be different depending on the system's settings (e. g. illumination).


Figure 590. The edit dialog for the PSF \& MTF detector.

Its edit dialog ( $\hookrightarrow$ Fig. 590) has the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Apply Ideal Lens | If this option is checked you can set a focal length. Then the field is propagated into the focus of an Ideal Lens with that focal length. Otherwise it is assumed that the field entering the detector is already in the focus. |
| Summation Type | If there is more than one coherent mode, the modes can be added coherently, incoherently, or partially coherently. For the latter you can specify the degree of coherence by entering a Coherence Time ${ }^{\text {PV }}$ (or copying it from a Coherence Time \& Length Calculator $\hookrightarrow$ Sec. 105). This setting has no effect for Classic Field Tracing as this engine only supports incoherent modes. |
| Components to Integrate | Allows you to select which vectorial components of the field are integrated and thus taken into account for the PSF and MTF calculation. $E_{x}, E_{y}$ and/or $E_{z}$ can be used whereas the dialog ensures that at least one component is selected. |
| PSF | Allows you to set whether the PSF is returned as Chromatic Fields Set ( $\hookrightarrow$ Sec. 14) by the detector. |
| Real Color / False Color | Only visible if PSF is checked. <br> Allows you to preset the color mode ( $\hookrightarrow$ Sec. 14.2) of the resulting Chromatic Fields Set with the PSF data. Only has an effect if the incident field is twodimensional. |
| MTF | Allows you to set whether the MTF is returned as Data Array(s) by the detector. |
| Along $x$-Axis / <br> Along y-Axis / <br> Two-Dimensional | Only visible if MTF is checked. <br> By default the two-dimensional MTF is shown. But you can also select that an cross section Along x-Axis or Along y-Axis is shown additionally. This cross section always starts with a spatial frequency or line density of zero. |
| Versus Line Density / Versus Wave Number | Only visible if MTF is checked. <br> The MTF can be plotted either Versus Line Density with the unit cycles or line pairs per millimeter. Or it can be plotted Versus Wave Number with the unit 1/m. |
| Calculate Line Density I Wave Number Limit | Only if Along X-Axis or Along Y-Axis is checked <br> If checked, the line density or wave number is calculated where the contrast first falls below the specified limit. |
| Color Table | Allows you to preset the color table for the two-dimensional Chromatic Fields Set with the PSF data in False Color mode and the two-dimensional Data Array with the MTF Data. |

The dialog ensures that you cannot unselect all output possibilities.
Fig. 603 shows how the edit dialog looks like if the detector is used in the main window (via Detector from Catalog; $\hookrightarrow$ Sec. 75.1). If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.5.4 Radial / Azimuthal Polarization

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Field Visualization > Radial / Azimuthal Polarization

This detector plots the radial component $E_{\rho}$ and/or the azimuthal component $E_{\phi}$ ( $\hookrightarrow$ Fig. 591) of a field into a data array. If the field consists of multiple modes the data arrays for the distinct modes are collected in a Set of Data Arrays ( $\hookrightarrow$ Sec. 16).


Figure 591. Decomposition of the electric field vector E into Cartesian components (blue) and polar coordinate components (green).

The conversion from $E_{x}$ and $E_{y}$ to $E_{\phi}$ and $E_{\rho}$ is done by the following equations:

$$
\begin{align*}
& E_{\rho}(\rho, \phi)=\cos \phi E_{x}(x, y)+\sin \phi E_{y}(x, y)  \tag{74.1}\\
& E_{\phi}(\rho, \phi)=-\sin \phi E_{x}(x, y)+\cos \phi E_{y}(x, y) \tag{74.2}
\end{align*}
$$

The polar coordinates are given by $\rho=\sqrt{x^{2}+y^{2}}$ and $\phi=\operatorname{atan} 2 y / x^{1}$.


Figure 592. The edit dialog of the Polarization Detector. Note that you cannot uncheck the only selected polarization component as then no component would be selected.

The edit dialog for the detector is shown in Fig. 592 and has the following controls and the Detector Function sub-tab.

[^11]Polarization Components You can select either the $E_{-}$Rho-Component $E_{\rho}$, the $E_{-}$Phi-Component $E_{\phi}$, or to Evaluate both. The dialog ensures that at least one polarization component is selected.

The remaining controls of this dialog are explained in Sec. 74.1.

### 74.5.5 Raw Data Detector

## Availability

Optical Setups: General Optical Setup, Grating Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Detectors > Field Visualization > Raw Data Detector

A Raw Data Detector gives the raw field data at the position where it is placed. These raw data can be either equidistant or non-equidistant. Its edit dialog ( $\hookrightarrow$ Fig. 593) allows you to preset several view settings like the visible region for equidistant data.


Figure 593. Dialog with the Settings for the Raw Data Detector.
The Use for One-Dimensional Fields adapts the dialog to either one-dimensional or two-dimensional harmonic fields.
If you click on the Copy from ... button a dialog appears where you can select any open Harmonic Field or Harmonic Fields Set document. The view settings of this document determine the values within the dialog (the visible region specifies the settings for the View Size).
Furthermore there are two tab pages.
The General tab of the dialog ( $\hookrightarrow$ Fig. 593) has the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sample Linear Phase | Flag that indicates whether the analytically stored linear phase of the input field shall be sampled. If this option is not selected the linear phase is removed from the field and an information about the removed linear phase term is plotted into the Messages tab of the VirtualLab Fusion main window. |
| Sample Quadratic Phase | Flag that indicates whether the analytically stored quadratic phase of the input field shall be sampled. If this option is not selected the quadratic phase is removed from the field and an information about the removed quadratic phase term is plotted into the Messages tab of the VirtualLab Fusion main window. |
| Light View / Data View | Sets whether light view or data view shall be visible in the resulting field and adapts the dialog accordingly. |
| Use Cubic Interpolation | If checked, the cubic interpolation for the view ( $¢$ Sec. 11.2.1) is used. |
| Display Mode | You can choose either Visual Perception or Linear Intensity Detector. $\rightarrow$ Sec. 12.2.1 |
| Field / Polarization Quantity | Either the Field Quantity ( $\hookrightarrow$ Sec. 11.1) or the eccentricities or angles of the polarization ellipses ( $\hookrightarrow$ Fig. 12.2.2.3) can be displayed by the Raw Data Detector. |
| Vectorial Component I Combined Component | Depending on the selected Field / Polarization Quantity, you can either select the Vectorial Component (for Field Quantities except Summed Squared Amplitudes, $\hookrightarrow$ Sec. 12.2.2.2) or the Combined Component for Summed Squared Amplitudes ( $\hookrightarrow$ Sec. 11.1). <br> This control is not visible if Polarization Eccentricities or Polarization Angles are set as Field / Polarization Quantity. |
| Show Polarization Ellipses | If neither Polarization Eccentricities nor Polarization Angles are selected as Field / Polarization Quantity, polarization ellipses can be shown as overlay in the view (see Fig. 91 for an example). |
| Polarization Plane | Actually, the field vector at a certain point describes a polarization ellipse in the plane perpendicular to the propagation direction. For clarity, VirtualLab Fusion only shows polarization ellipses which result from projecting this ellipse onto one of the coordinate planes. This Polarization Plane can be defined by the user if polarization ellipses are shown - either as Show Polarization Ellipses overlay or as Field / Polarization Quantity. |
| Color Palette | For the Data View or the Linear Intensity Detector mode of the Light View, you can choose one out of several color tables ( $\hookrightarrow$ Sec. 11.2.4). This color table is used for the shown mode and the shown field quantity only. All other color tables are taken from the Global Options dialog ( $\hookrightarrow$ Sec. 6.9). |
| Physical Aspect Ratio / <br> Free Aspect Ratio | The Aspect Ratio ( $\hookrightarrow$ Sec. 11.5) used for displaying the field. |
| Show Whole Field | If checked, it is not zoomed into the field, i.e. you will see the whole field. Thus, Center Position and View Size are disabled. |
| Center Position | These two text boxes allow you to specify the center ( $x$ - and $y$-position) of the region you want to see. If you have checked Use for One-Dimensional Fields only one text box is shown. |


| View Size | These two text boxes allow you to specify the size in x-and y-direction of the <br> region you want to see. If you have checked Use for One-Dimensional Fields <br> only one text box is shown. |
| :--- | :--- |

The Graphic Tools page ( $\hookrightarrow$ Fig. 594) allows you to preset the visibility, position and extension (if applicable) of the three marker types ( $\hookrightarrow$ Sec. 11.3). If you have checked Use for One-Dimensional Fields only one input box is shown for all entries and a profile line cannot be specified.


Figure 594. Graphic Tools page of the Raw Data Detector dialog.

The remaining controls of this dialog are explained in Sec. 74.1. Note that in a Grating Optical Setup the Raw Data Detector cannot be tilted and shifted.

For data view settings which are not set by this dialog, always the settings from the Global Options dialog ( $\hookrightarrow$ Sec. 6.11) are taken into account. This applies for e.g. the Artifacts Threshold and the Scaling of the polarization ellipses.

### 74.6 Merit Functions

### 74.6.1 Beam Parameters

## Availability

Toolboxes: All

## Accessible:

- Optical Setup: Detectors > Basic Detectors > Beam Parameters
- Ribbon: Detectors > Beam Parameters

The beam parameters of a wave are calculated based on the second momentum theory ( $\hookrightarrow$ Sec. 137.1). If the ribbon item Detectors > Beam Parameters is clicked the dialog shown in Fig. 595 will appear. The following beam parameters can be calculated (for the underlying formulas see Sec. 137.1):

| ITEM | DESCRIPTION |
| :--- | :--- |
| Diameter $\mathbf{X}$ | The diameter measured from the optical axis along the x-axis. |
| Diameter $\mathbf{Y}$ | The diameter measured from the optical axis along the y-axis. |
| Waist Diameter $\mathbf{X}$ | The waist diameter measured from the optical axis along the x-axis. |
| Waist Diameter $\mathbf{Y}$ | The waist diameter measured from the optical axis along the y-axis. |
| Full Divergence Angle $\mathbf{X}$ | The full angle of divergence angle measured from the optical axis along the <br> x-axis. |
| Full Divergence Angle $\mathbf{Y}$ | The full angle of divergence angle measured from the optical axis along the <br> y-axis. |
| Waist Distance $\mathbf{X}$ | The distance of the present z-position of the wave from the waist measured <br> along the x-axis. |
| Waist Distance $\mathbf{Y}$ | The distance of the present z-position of the wave from the waist measured <br> along the y-axis. |
| $\mathbf{M}^{2}$-Parameter in | The M ${ }^{2}$ parameter of the wave measured along the x-axis. |
| $\mathbf{x - D i r e c t i o n ~}$ | The M ${ }^{2}$ parameter of the wave measured along the y-axis. |
| $\mathbf{M}^{2}$-Parameter in | The x-position of the centroid. |
| $\mathbf{y}$-Direction | The y-position of the centroid. |
| Centroid $\mathbf{X}$ | The angle between the principal axis of the wave and the x-axis. |
| Centroid $\mathbf{Y}$ | Rotation Angle of the Prin- <br> cipal Axis |



Figure 595. Edit dialog if the Beam Parameters detector is used in the main window.

The edit dialog of this detector ( $\hookrightarrow$ Fig. 595) offers the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Vectorial Component | Selects the complex amplitude ( $E_{x}$ or $E_{y}$ ) for which the beam parameters shall be calculated. |
| Beam Parameters | This section of the dialog allows you to select the beam parameters to be evaluated. With the Selection Tools you can Select All entries or Unselect All entries. |
| Calculate Beam Parameters Relative to the Centroid | If checked, then in a first step always the centroid of the wave is determined and in a second step all beam parameters are calculated relative to the centroid. |
| Calculate Beam Parameters Relative to the Principal Axis. | If not checked all beam parameters are calculated along the $x$ - and $y$-axis. If checked, then in a first step the rotation angle of the principal axis of the wave measured to the x -axis is determined. In a second step all beam parameters are calculated relative to the principal axis and not to the $x$ - and $y$-axis. |
| Refine Sampling to Fully Sampled Spherical Phase | Harmonic fields may contain analytical spherical phase factors. In the paraxial case, the detector truly accounts for the spherical phase without actually measuring it on the sampling points of the field. In the non-paraxial case, analytical spherical phase factors must be sampled in a correct manner in order to ensure an unbiased evaluation of the beam parameters. If checked, VirtualLab Fusion is forced to interpolate the field for a lossless sampling of the spherical phase factor. In presence of a spherical phase factor with small radius this option can dramatically increase the computing time and memory resources needed. <br> This option has an effect only for Classic Field Tracing or in the main window. To get the analogous behavior for General Profile, you should activate the option Scale Sampling Distance by Oversampling Factor on the Detector Window and Resolution tab ( $\leftrightarrows$ Sec. 74.1.1). Then the sampling is refined to completely sample the analytic quadratic phase of the field. |
| Values having less than ... of the maximum intensity are ignored. | For mathematical reasons the beam parameters detector is very sensitive to noise which can change the results by a factor 10 or more. Thus this setting allows you to ignore all field values having less than the given percentage of the maximum squared amplitude in the field. <br> You can set this value to zero to switch off this noise filtering. |

Fig. 595 shows how the edit dialog looks like if the detector is used in the main window. If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.6.2 Diffractive Optics Merit Functions

## Availability

Toolboxes: All
Accessible:

- Optical Setup: Detectors > Basic Detectors > Diffractive Optics Merit Functions
- Ribbon: Detectors > Diffractive Optics Merit Functions

Diffractive Optics Merit Functions are a collection of merit functions that are typically used to evaluate beam
shaping, beam splitting and light diffusing systems. VirtualLab Fusion supports the following merit functions. The corresponding formulas are given in Sec. 137.2.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Window Efficiency | The part of the paraxial power of the input field diffracted inside the signal <br> region. |
| Conversion Efficiency | The part of the paraxial power of the input field diffracted in the part of the <br> signal that is inside the signal region. Noises inside the signal region are <br> ignored. |
| Signal to Noise <br> (SNR) | The strength of the signal relative to the noises measured in dB. |
| Uniformity Error | The maximum deviation of the output field squared amplitude from the signal <br> field squared amplitude inside the signal region. |
| Relative Zeroth Order In-  <br> tensity The paraxial intensity of a field component (squared amplitude) of the ze- <br> roth order of the output field related to somewhat like the mean value of the <br> intensities of the desired output orders. <br> Zeroth Order Efficiency The part of the paraxial power of the input field diffracted into the zeroth order. <br> Maximum Relative Inten- The relative maximum intensity outside of the signal region. <br> sity of Stray Light A real valued or complex scaling factor between the complex amplitude of <br> the output field in the signal region and the complex amplitude of the desired <br> Optimal Scale Factor output field. The optimal scale factor is typically used for the calculation of <br> the most standard merit functions. |  |

These merit functions can be calculated via Detectors > Diffractive Optics Merit Functions or in an Optical Setup. Most of the Diffractive Optics merit functions can also be logged during the IFTA optimization ( $\hookrightarrow$ Sec. 97).


Figure 596. Edit dialog if the Diffractive Optics Merit Functions detector is used in the main window.

The edit dialog of this detector ( $\hookrightarrow$ Fig. 596) offers the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | Selects the vectorial component $\left(E_{x}\right.$ or $\left.E_{y}\right)$ for which the merit functions shall <br> be calculated. |
| Selected Merit Functions | Allows the selection of the standard merit functions that shall be calculated. <br> With the Selection Tools you can Select All entries or Unselect All entries. |
| Desired Output Field | Allows the selection of the desired output field used for the calculations. |
| Evaluation Region Mode | Allows you to define the way how the Evaluation Region is determined. There <br> are four possibilities: <br> 1. Arbitrary Evaluation Region: Allows you to Set an arbitrary harmonic <br> field as evaluation region. |
| 2. Create from Desired Output Field: The chosen Vectorial Component <br> of the Desired Output Field is used as evaluation region, whereby all |  |
| absolute values larger than zero are taken into account for computing |  |
| the merit functions. |  |
| 3. Equal to Incident Field Selection: If you choose this option (which is |  |
| only available in the main window), you must select an open harmonic |  |


| Evaluation Region | If you have chosen Arbitrary Evaluation Region as Evaluation Region Mode, the Set button allows to either <br> - Load a suitable Complex Amplitude File from hard disc or <br> - select a harmonic field document which is already opened in the main window. |
| :---: | :---: |
| Allow Scale Freedom | The Show button allows you to to view the currently set evaluation region. If checked the scale factor ( $\hookrightarrow$ Sec. 138.1.1) is calculated for all merit functions calculations, otherwise the scale factor is set to one. |
| Signal Type | Sets the specific type of the signal, i.e. for which field quantity the merit functions are being evaluated. Can be either Amplitude, Squared Amplitude, Complex Amplitude or Phase. |
| Efficiency Related to Incident Field of Optical System | If this item is checked all efficiency calculations are related to the power of the incident field. In this way, possible energy losses in the optical system (e.g. caused by absorption or reflection) can be considered. <br> If this detector is used in the Optical Setup, the incident field is the field directly after the light source. If this detector is used in the main window, you can define an arbitrary Incident Field. |
| Incident Field | Only available in the Main Window. <br> There are two buttons to define an arbitrary incident field. The Set button allows you to either <br> - Load a suitable Complex Amplitude File from hard disc or <br> - select a suitable document which is already opened in the main window. In both cases the set incident field must be a spatial harmonic field. The Show button allows you to to view the currently set incident field. |

Fig. 596 shows how the edit dialog looks like if the detector is used in the main window. If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.6.3 Multimode Fiber Coupling Efficiency

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Merit Functions > Multimode Fiber Coupling Efficiency

This detector calculates how much of the incident light can couple into either a step-index fiber or a gradient index fiber. This evaluation is done per wavelength.


Figure 597. The edit dialog for the Multimode Fiber Coupling Efficiency detector.

Its edit dialog ( $\hookrightarrow$ Fig. 597) has the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Mode Type | Allows you to select between Linearly Polarized Bessel modes which occur in step-index fibers and Linearly Polarized Laguerre modes which occur in gradient index fibers. |
| Efficiency Related to Source Field | If this item is checked the calculated efficiency will be related to the power of the field directly after the light source. This means that the efficiency will become smaller due to e.g. absorption and reflections in the optical setup. |
| Core Diameter | The core diameter $d$ of the fiber. |
| Core Material | Allows you to set the material in the fiber core with the control described in Sec. 34.3. Only the real-valued refractive index $n_{\text {core }}(\lambda)$ is used. |
| Cladding Material | Only for Linearly Polarized Bessel modes <br> Allows you to set the material of the fiber cladding with the control described in Sec. 34.3. Only the real-valued refractive index $n_{\text {cladding }}(\lambda)$ is used. |
| Gradient Constant | Only for Linearly Polarized Laguerre modes <br> For gradient index fibers the refractive index distribution is given by $\begin{equation*} n^{2}(r)=n_{\text {core }}(\lambda)^{2}\left(1-2 \Delta\left(\frac{r}{r_{0}}\right)^{2}\right) \tag{74.3} \end{equation*}$ <br> whereas $n_{\text {core }}$ is the refractive index in the center given by the Core Material; $r_{0}=d / 2$ is the core radius; and $\Delta$ is the gradient constant. |
| Maximum Azimuthal Order / Maximum Radial Order | Defines how many modes are considered for the calculation of the coupling efficiency. |
| Validity | This control indicates whether the current configuration is valid, $\hookrightarrow$ Sec. 5.10. Error messages can be shown in a separate dialog. <br> For example it is checked that the modes are not cut off, which would be the case if the cutoff parameter $V=\pi / \lambda \cdot d \sqrt{n_{\text {core }}^{2}-n_{\text {cladding }}^{2}}$ is less than 1. Also $V>300$ is not practical. |

### 74.6.4 Power

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Detectors > Merit Functions > Power


Figure 598. The edit dialog for the power detector.

This detector calculates the power $P$ in watts, either for the complete field in the detector plane or for a region of it. It is calculated via

$$
\begin{equation*}
P=n \frac{\epsilon_{0}}{2} c \sum_{i} \Delta_{i} \cdot A_{i}^{2} \tag{74.4}
\end{equation*}
$$

$n$ is the refractive index derived from the embedding medium of the field, $\epsilon_{0}$ is the dielectric constant and $c$ is the vacuum speed of light. $A_{i}$ is the squared amplitude of the data point $i$ and $\Delta_{i}$ is the area this data point occupies (sampling distance in x-direction times sampling distance in y-direction for equidistant data).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Components to | You can select any combination of Ex-Component, Ey-Component, and Ez- |
| Evaluate | Component. The dialog ensures that at least one vectorial component is se- |
|  | lected. The squared amplitudes of all selected components are summed up |
|  | to the $A_{i}$ in Eq. (74.4). |

The remaining controls of this dialog are explained in Sec. 74.1.

### 74.6.5 Pulse Evaluation

## Availability

Optical Setups: General Optical Setup
Accessible: Optical Setup: Detectors > Merit Functions > Pulse Evaluation

This detector combines several settings for both the evaluation of pulses ( $\hookrightarrow$ Sec. 74.6.5.1) and of the optical path length for distinct wavelengths ( $\hookrightarrow$ Sec. 74.6.5.2).
A validity control in the bottom left corner ( $\hookrightarrow$ Sec. 5.10 ) indicates whether there are issues with the current configuration. If this is the case you can click on the -button for further information.
The remaining controls of this dialog are explained in Sec. 74.1.

### 74.6.5.1 Pulse Evaluation

The actual Pulse Evaluation tab page ( $\hookrightarrow$ Fig. 599) allows you to plot the field data of a polychromatic fields set over wavelength and over time. In this way you can examine the pulse shape if the incoming harmonic fields set represents a laser pulse.
To this end, you can choose to extract the field

1. at a specific position, resulting in 1D Data Arrays with wavelength/time being the x-axis,
2. at a line, resulting in 2D Data Arrays with wavelength/time being the x-axis, and/or
3. at a specific region, resulting in 2D Data Arrays with one subset per wavelength/time value. Out of such a data array, an animation can be generated using Manipulations > Create Animation


Figure 599. The settings for the actual pulse evaluation, here for the Pulse (3D) mode.

More specifically, the Pulse Evaluation tab page has the following options:

## ITEM

DESCRIPTION

| Vectorial Component to <br> Evaluate | You can select at least one of the vectorial components $E_{x}, E_{y}$, and $E_{z}$. For <br> each selected vectorial component separate data arrays are shown. |
| :--- | :--- |
| Oversampling Factor | With this factor you can adjust the sampling and thus the accuracy in the time <br> domain. A higher oversampling factor leads to a smaller sampling distance. |
| Exclude Time Shift | The pulse needs a certain time $t_{\mathrm{s}}$ to propagate through the system. If you <br> check this option, the shown pulse reaches its peak at the time $t_{\mathrm{s}}$. Otherwise <br> the pulse is centered around the time of 0 s. The time $t_{\mathrm{s}}$ is the time shift as <br> calculated by the set Fit Method for Evaluation. |
| Extend Time Window | If you check this option, an oversampling in frequency domain is introduced <br> depending on the settings on the Frequency Sampling on the Optical Path <br> Length Evaluation tab. The residuals of the fitted linear phase function and <br> the correct phase function are used for this oversampling. Thus the set Fit <br> Method for Evaluation also alters the effect this setting. |
|  | An oversampling in frequency domain leads to an embedding in time domain, |
| thus a larger time window is shown. |  |


| Fit Method for Evaluation | Allows you to select any of the three fit methods explained in Sec. 74.6.5.2. The fit method influences the effect of Exclude Time Shift and Extend Time Window. |
| :---: | :---: |
| Pulse at Point (1D) | On this tab page you can select and configure the Evaluation of Pulse at Point (1D). This means you extract the field data at a specific Position $(x, y)^{\text {DV }}$ resulting in 1D Data Arrays with wavelength/time being the $x$-axis. <br> If you click the Copy From... button, you can select a document window showing two-dimensional (field) data from whose point marker ( $\varsigma$ Sec. 11.3) the new Position $(x, y)$ is taken. <br> For the 1D evaluation, you can also choose to calculate the Minimum, Maximum and / or Full Width Half Maximum of the resulting data arrays. |
| Pulse at Line (2D) | On this tab page you can select and configure the Evaluation of Pulse at Line (2D). This means you extract the field data at a certain line (defined by Start Point $(x, y)$ and End Point $(x, y)$ ). The result of this evaluation are 2D Data Arrays with wavelength/time being the $x$-axis. <br> If you click the Copy From ... button, you can select a document window showing two-dimensional (field) data from whose line marker ( $\leftrightarrows$ Sec. 11.3) the new Start Point ( $x, y$ ) and End Point $(x, y)$ are taken. |
| Pulse (3D) | On this tab page you can select and configure the Evaluation of Pulse (3D). This means you extract the field data from a certain region (defined by Center Point ${ }^{\text {DV }}$ and Size). The result of this evaluation are 2D Data Arrays with one subset per wavelength / time value. <br> If you click the Copy From... button, you can select a document window showing two-dimensional (field) data from whose rectangle or ellipse marker ( $\leftrightarrows$ Sec. 11.3) the new Center Position and Size are taken. <br> As the 3D evaluation can be quite costly, you can adjust the sampling defining either the Resolution or the number of Sampling Points. |

### 74.6.5.2 Optical Path Length Evaluation

As explained in Sec. 74.6.5.1, the pulse evaluation depends on a fit method. This refers to several methods of fitting a linear function to optical path lengths (or more precisely: absolute phases) versus frequency $v$. The Optical Path Length Evaluation tab ( $\hookrightarrow$ Fig. 600) allows you to configure the Pulse Evaluation detector so that it shows these fitted functions.


Figure 600. The settings for the optical path length evaluation.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Evaluate Optical Path <br> Length | This checkbox defines whether the optical path length over the frequencies $v$ <br> shall be shown. |
| Evaluate Phase by Optical | This checkbox defines whether the absolute versus the frequencies $v$ shall <br> be shown. |
| Fath Length | The first type of linear fit does not consider dispersion effects in the optical <br> system the detector is placed in. The user can specify whether the fitted <br> linear function shall be drawn additionally in the phase diagram and whether <br> the residuals shall be evaluated. |
| Dispersion |  |

Fit II: Time Shift by Re- The second type of linear fit does consider dispersion effects in the optical gression system the detector is placed in. The dispersion effect is fitted by a linear regression to the absolute phase curve. The user can specify whether the fitted linear function shall be drawn additionally in the phase diagram and whether the residuals shall be evaluated.

Fit III: Time Shift with Dis- The third type of linear fit does consider dispersion effects in the in the optical persion system the detector is placed in. The dispersion effect is evaluated by the group velocity of the pulse. The user can specify whether the fitted linear function shall be drawn additionally in the phase diagram and whether the residuals shall be evaluated.

| Automatic Sampling | VirtualLab Fusion estimates the frequency sampling for the selected light <br> path. The calculated oversampling factor will be logged into the logging win- <br> dow of VirtualLab Fusion. |
| :--- | :--- |
| Manual Sampling | The manual sampling mode allows the user to enter a self-defined Oversam- <br> pling Factor (Frequencies). |

Oversampling Factor (Fre- For Manual Sampling the oversampling factor can be configured to use more quencies) frequencies for the OPL analysis. This oversampling factor will also influence the Extend Time Window option on the Pulse Evaluation tab ( $\hookrightarrow$ Sec. 74.6.5.1).


Figure 601. Resulting diagrams of the Optical Path Length Evaluation of a sample Optical Setup.

Fig. 601 shows some sample results generated by the Optical Path Length Evaluation tab.
The slopes of the fitted linear functions give the time shift, i. e. the time the pulse needed to propagate through the (sub-)system. The Optical Path Length Evaluation logs the obtained time shifts into the detector window (one per selected fit method), see Fig. 602 for an example. The time shifts can be used for further investigations of pulses in VirtualLab Fusion, especially for the temporal Fourier Transformation ( $\hookrightarrow \mathrm{Sec}$. 31.2.1).
The residual functions calculated by the Optical Path Length Evaluation can be used to increase the time window for the Inverse Temporal Fourier Transformation, see Sec. 31.2.1.

| Detector | Sub - Detector | Result |
| :---: | :---: | :---: |
| OPL Analyzer | Linear Fitt: Time Shitt without Dispersion | 19.246 ps |
|  | Linear Fitll: Time Shift by Regression | 18.941 ps |
|  | Linear Fit Ill: Time Shift with Dispersion | 18.945 ps |

Figure 602. The slope of the linear fits is logged into the Detector Results tab of the VirtualLab Fusion main window.

### 74.6.6 Singlemode Fiber Coupling Efficiency

## Availability

Toolboxes: All
Accessible:

- Optical Setup: Detectors > Basic Detectors > Singlemode Fiber Coupling Efficiency
- Ribbon: Detectors > Fiber Coupling Efficiency

This detector allows the calculation of the coupling efficiency of the incident field into a single mode fiber. Actually this function does not calculate the modes of a fiber. The fiber mode must be specified separately. For a description of the physical background see Sec. 137.3.


Figure 603. Dialog for the calculation of the fiber coupling efficiency of a harmonic field in the main window.
The edit dialog of this detector ( $\hookrightarrow$ Fig. 603) offers the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Specify Gaussian Mode Field | If you check this option, a Gaussian mode field is calculated directly from either the numerical aperture of the fiber or the diameter of the fiber mode. |
| Fiber NA ${ }^{\text {V }}$ | Allows you to enter the numerical aperture of the fiber if you want to Specify Gaussian Mode Field. |
| Mode Field Diameter $\left(1 / \mathrm{e}^{\wedge} 2\right)^{[\mathrm{PV}}$ | Allows you to enter the $1 / e^{2}$ diameter of the Gaussian mode field. |
| Specify Customized Mode Field | Instead of specifying a Gaussian mode field you can also use an arbitrary Mode Field. |
| Mode Field | There are two buttons to define an arbitrary mode field. The Set button allows you to either <br> - Load a suitable Complex Amplitude File from hard disc or <br> - select a suitable document which is already opened in the main window. In both cases the set mode field must be a spatial harmonic field. The Show button allows you to to view the currently set mode field. |
| Efficiency Related to Incident Field of Optical System | If this item is checked the calculated efficiency will be related to the power of the incident field. In this way, possible energy losses in the optical system (e. g. caused by absorption or reflection) can be considered. <br> If this detector is used in the Optical Setup, the incident field is the field directly after the light source. If this detector is used in the main window, you can define an arbitrary Incident Field. |
| Incident Field | Only available in the Main Window. <br> There are two buttons to define an arbitrary incident field. The Set button allows to either <br> - Load a suitable Complex Amplitude File from hard disc or <br> - select a suitable document which is already opened in the main window. In both cases the set incident field must be a spatial harmonic field. The Show button allows you to to view the currently set incident field. |

Fig. 603 shows how the edit dialog looks like if the detector is used in the main window. If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.6.7 Spot Size

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Merit Functions > Spot Size


Figure 604. The edit dialog of the Spot Size detector.

This detector can be used to measure the spot size of the incident beam with different measurement algorithms. For Classic Field Tracing and General Profile the beam diameter algorithms of the beam parameters detector are used ( $\hookrightarrow$ Sec. 74.6.1), whereas for locally polarized fields the amplitudes of $E_{x}$ and $E_{y}$ are summed up. For Ray Results Profile the user can select whether he likes to measure the RMS or the peak value of the incident ray bundle.
The edit dialog ( $\hookrightarrow$ Fig. 604) of this detector has the following options.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Evaluation of All Modes Together | If this option is checked, all modes are regarded as one ensemble for which one spot size is determined. |
| Evaluation of All Modes Separately | If this option is checked, the spot size is determined separately for each individual mode. |
| Use Centroid as Reference | Flag whether the spot size is measured relatively to the centroid of the field. If this option is not selected, the position of the central ray (General Profile and Ray Results Profile) or the center of the field (Classic Field Tracing) will be used as reference. |
| Refine Sampling to Fully Sampled Spherical Phase | Harmonic fields may contain analytical spherical phase factors. If this option is checked, VirtualLab Fusion is forced to interpolate the field for a lossless sampling of the spherical phase factor. In presence of a spherical phase factor with small radius this option can dramatically increase the computing time and memory resources needed. |
| Values having less than ... of the maximum intensity are ignored. | For mathematical reasons the beam parameters detector is very sensitive to noise which can change the results by a factor 10 or more. Thus this setting allows you to ignore all field values having less than the given percentage of the maximum squared amplitude in the field. <br> You can set this value to zero to switch off this noise filtering. |
| Detect RMS | The user can select whether the RMS definition shall be used for size measurement. |
| Detect Peak Value | The user can select whether the peak value definition shall be used for size measurement. |
| Measure Radial Spot Size | Option for the detection of the RMS or peak value. If this option is selected the radial size is determined by the detector and thus the detector generates only one output value for the size. If this option is not selected the detector will calculate the RMS or peak value separately for x - and y -direction. |

The remaining controls of this dialog are explained in Sec. 74.1.

### 74.6.8 Uniformity Detector

## Availability

Optical Setups: Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Merit Functions > Uniformity Detector

This detector calculates the average summed squared amplitude $I_{i}$ within small pupils around various positions $\rho_{i}$. The pupils all have the same size and shape (rectangular or elliptical). From these $I_{i}$ the following values are calculated:

- The minimum value $I_{\min }$ and the maximum value $I_{\max }$
- Uniformity error $U=\frac{I_{\text {max }}-I_{\text {min }}}{I_{\text {max }}+I_{\text {min }}}$
- Arithmetic mean and standard deviation


Figure 605. The edit dialog of the Uniformity Detector.

The edit dialog ( $\hookrightarrow$ Fig. 605) has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Summation Type | If there is more than one coherent mode, the overlaying modes can be added <br> coherently, incoherently, or partially coherently. For the latter you can specify <br> the degree of coherence by entering a Coherence Time <br>  <br> a Coherence Time \& Length Calculator copying it from <br> for Classic Field Tracing as this engine only supports incoherent modes. This setting has no effect |
| Pupil Parameters | Here you can define Shape and Size |

### 74.7 Point Evaluation

### 74.7.1 Two Point Contrast

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Detectors > Point Evaluation > Two Point Contrast


Figure 606. The dialog for the Two Point Contrast detector.

This detector allows you to calculate the contrast between the values (a certain field quantity of a certain vectorial component) at two specified positions in the detector plane. If $V_{1}$ is the larger value and $V_{2}$ the smaller one, the contrast $C$ is defined by

$$
\begin{equation*}
C=\frac{V_{1}-V_{2}}{V_{1}+V_{2}} \tag{74.5}
\end{equation*}
$$

On the Detector Parameters tab page of its dialog ( $\hookrightarrow$ Fig. 606), the following settings can be made.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Position $1^{\text {[VV }}$ | The first position in physical coordinates. With the Copy From button you can copy the physical position from the Point Manipulation Cross of the selected harmonic field or harmonic field set. |
| Position 2 ${ }^{\text {PV }}$ | The second position in physical coordinates. With the Copy From button you can copy the physical position from the Point Manipulation Cross of the selected harmonic field or harmonic field set. |
| Field Quantity | The Field Quantity ( $\checkmark$ Sec. 11.1) for which the contrast is calculated. |
| Vectorial Component I Combined Component | Depending on the selected Field Quantity, you can either select the Vectorial Component ( $\hookrightarrow$ Sec. 12.2.2.2) or the Combined Component (for Summed Squared Amplitudes, $\hookrightarrow$ Sec. 11.1). |

The remaining tab pages are explained in Sec. 74.1.

### 74.7.2 Value Monitoring

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup
Accessible: Optical Setup: Detectors > Point Evaluation > Value Monitoring


Figure 607. The dialog for the Value Monitoring detector.

This detector calculates a value (a certain field quantity of a certain vectorial component) at a specific position in the detector plane. To this end a pointwise sinc interpolation is used in case of Classic Field Tracing. It can be especially helpful for the Parameter Run ( $\hookrightarrow$ Sec. 44). On the Detector Parameters tab page of its dialog ( $\hookrightarrow$ Fig. 607), the following settings can be made.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Detect Value at ${ }^{\text {PV }}$ | The position in physical coordinates for which the specified Field Quantity and <br> component shall be given. |
| Copy From | You can copy the physical position from the Point Manipulation Cross of the <br> selected harmonic field or harmonic field set. |
| Field Quantity | The Field Quantity ( $\hookrightarrow$ Sec. 11.1) which shall be shown. |
| Vectorial Component $\quad$ I | Depending on the selected Field Quantity, you can either select the Vecto- <br> rial Component $(\hookrightarrow$ Sec. 12.2.2.2) or the Combined Component (for Summed <br> Combined Component |
| Squared Amplitudes, $\hookrightarrow$ Sec. 11.1). |  |

The remaining tab pages are explained in Sec. 74.1.

### 74.8 Wavefront Detectors

These detectors all evaluate the smooth wavefront and thus allow to remove an off-axis spherical phase from the phase of a field. To this end the control described in Sec. 74.8.1.
They are evaluated per mode, in case of locally polarized fields the wavefront of the vectorial component ( $E_{x}$ or $E_{y}$ ) with the larger power is used.
Assume Geometric Field Zone for Detector Evaluation is always checked for these detectors as a wavefront is only well defined if there are no diffraction effects.

### 74.8.1 Control for Setting the Reference Wavefront



Figure 608. The control for setting the reference wavefront.
This control ( $\hookrightarrow$ Fig. 608) allows you to define a reference wavefront which is subtracted from the incident field prior to further analysis. It has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Constant Phase | The phase front is evaluated unchanged. (The Piston coefficient of the <br> Zernike \& Seidel Aberrations Detector $(\hookrightarrow$ Sec. 74.8 .5$)$ contains the average <br> phase.) <br> This mode has no additional parameters. |
| Linear Phase | The average phase and a possible linear phase is subtracted from the phase <br> front before the actual evaluation. In this case you have two Determination <br> options for the linear phase: Fitted Direction and User-Defined Direction; see <br> table below. |
| Spherical Phase | An off-axis spherical phase is subtracted from the phase front before the ac- <br> tual evaluation. In this case you have three Determination options for the <br> radius and the origin of the spherical phase: Fitted Radius and Origin, User- <br> Defined Radius at Optimized Origin, and User-Defined Radius and Origin; <br> see table below. |


| DETERMINATION MODE | DESCRIPTION |
| :---: | :---: |
| Fitted Direction / <br> Fitted Radius and Origin | All parameters are determined automatically by VirtualLab Fusion. |
| User-Defined Direction | For Linear Phase <br> The average phase is determined by VirtualLab Fusion. The Linear Phase is entered by the user as Cartesian angles $\alpha$ and $\beta$. The direction in other direction conventions can be copied from a Direction Converter ( $\leftrightarrows$ Sec. 108) using the From Calculator button. |
| User-Defined Radius at Optimized Origin | For Spherical Phase <br> The average phase and the origin of the spherical phase are determined by VirtualLab Fusion. The Phase Radius is entered by the user. |
| User-Defined Radius and Origin | For Spherical Phase <br> The average phase is determined by VirtualLab Fusion. The Phase Radius and the Origin of the spherical phase are entered by the user. As mathematically a spherical phase with an offset corresponds to a spherical phase plus a linear phase, you can also enter Linear Phase ( $\alpha, \beta$ ) instead of Origin ( $x, y$ ). If you want to enter the direction in another convention than Cartesian angles $\alpha$ and $\beta$ you can use the From Calculator button to copy it from a Direction Converter ( $\leftrightarrows$ Sec. 108). |

74.8.2 Polynomial Aberrations Fit

## Availability

Optical Setups: General Optical Setup \& Light Guide Optical Setup
Accessible: Optical Setup: Detectors > Wavefront Detectors > Polynomial Aberrations Fit


Figure 609. Dialog for the calculation of a polynomial phase or aberrations approximation in the main window (via Detector from Catalog; $\hookrightarrow$ Sec. 75.1).

This detector performs a least squares polynomial fit to the phase of the evaluated harmonic field with selectable degree of the polynomial (between 1 and 12, inclusively).
Its edit dialog ( $\hookrightarrow$ Fig. 609) has the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Polynomial Degree | The maximal exponent sum $m+n$ of the basis monomials $x^{m} \cdot y^{n}$ to be used. |
| \{Reference Wavefront\} ${ }^{\text {PE }}$ | This control is explained in Sec. 74.8.1. |
| Maximum Number of Data Points Used For Fitting ${ }^{\text {PV }}$ | For fields with many sampling points or rays fitting can be very time consuming. Thus by default only 1000 random data points with non-zero amplitude are extracted from the mode. But you can change this for speed up or convergence tests. |
| Phase Fitted by Polynomial / <br> Aberrations Fitted by Polynomial | If checked, the fitted polynomial is displayed in a data array. |
| Difference of Phase to Polynomial Fit / Difference of Aberrations to Polynomial Fit | If checked, the difference of the original phase (relative to reference wavefront) to the fitted phase of the selected field, i. e. the fitting error, is displayed in a data array. |
| Phase Radius \& Origin | Only for Optimized Radius and Origin <br> The phase radius and the origin of the spherical phase are given as detector results. |
| Origin | Only for User-Defined Radius at Optimized Origin The origin of the spherical phase is given as detector result. |

Fig. 612 shows how the edit dialog looks like if the detector is used in the main window. If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.8.3 RMS of Phase

This detector has been superseded by the Wavefront Error detector ( $\hookrightarrow$ Sec. 74.8.4) AND might be REMOVED IN A FUTURE VERSION.


Figure 610. Dialog for the calculation of the root mean square of the phase in the main window.

This detector enables the user to calculate the Root Mean Square (RMS) of the phase.
If used in the main window the dialog shown in Fig. 610 will appear. The following table gives an overview over the possible settings of the dialog:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Unwrap Phase | Phase is unwrapped before RMS calculation. |
| Apply Weighting | If checked, the phase values are weighted according to the corresponding <br> amplitude or squared amplitude. |
| ${\text { Reference Wavefront } \boldsymbol{\}}^{[\operatorname{PE}}}^{\text {Subtract Average Phase }}$ | This control is explained in Sec. 74.8.1. |
| Average phase is subtracted before RMS calculation. |  |

If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\hookrightarrow$ Sec. 74.1).

### 74.8.4 Wavefront Error

## Availability

Optical Setups: General Optical Setup, Light Guide Optical Setup, and Laser Resonator Optical Setup Accessible: Optical Setup: Detectors > Wavefront Detectors > Wavefront Error

This detector calculates the deviation of the wavefront in the incoming field distribution from a reference wavefront (in wavelengths).
For the simulation engines General Profile and Ray Results Profile, the evaluation is done per coherent mode.


Figure 611. The dialog for the Wavefront Error detector.
On the Detector Parameters tab page of its dialog ( $\rightarrow$ Fig. 607), the following settings can be made.

| ITEM | DESCRIPTION |
| :--- | :--- |
| \{Reference Wavefront ${ }^{\text {[PE }}$ | This control is explained in Sec. 74.8 .1. |
| Data Arrays | The deviation of the phase from the reference wavefront is given as data <br> array. It is given in multiples of the wavelength and as one subset per coherent <br> mode. |
| Peak-to-Valley | The peak-to-valley value (i. e. the maximum deviation minus the minimum <br> deviation) of the wavefront error is output. It is given in multiples of the wave- <br> length and as one value per coherent mode. |
| RMS | The root mean square of the wavefront error is output. It is given in multiples of <br> the wavelength and as one value per coherent mode. You can either apply a <br> Weighting by Amplitude or by Squared Amplitude to ensure that phase values <br> from almost dark regions of the field do not influence the resulting RMS value. |
| Phase Radius \& Origin | OnLY FOR OPTIMIZED RADIUS AND ORIGIN <br> The phase radius and the origin of the spherical phase are given as detector <br> results. |
| Origin | OnLY FOR USER-DEFINED RADIUS AT OPTIMIZED ORIGIN <br> The origin of the spherical phase is given as detector result. |

The phase radius is the distance between the detector plane and the source plane of the spherical phase. The remaining controls are explained in Sec. 74.1.

### 74.8.5 Zernike \& Seidel Aberrations Detector

## Availability

Toolboxes: All

## Accessible:

- Optical Setup: Detectors > Basic Detectors > Zernike Fringe / Seidel Aberrations
- Ribbon: Detectors > Zernike Fringe / Seidel Aberrations

This detector allows the calculation of the Zernike fringe, Zernike standard, and Seidel aberrations within a circular pupil. They refer to wavelengths. For example a Zernike fringe tilt of 1 corresponds to phase values in the range $-1 \lambda(=-2 \pi) \ldots+1 \lambda(=+2 \pi)$. The corresponding formulas are given in Sec. 134.2.
The evaluation is done per mode. A spherical phase factor can be separated from the phase front to be fitted.


Figure 612. Dialog of the Zernike \& Seidel Aberrations Detector in the main window.

If the ribbon item Detectors > Zernike Fringe / Seidel Aberrations is clicked, the dialog shown in Fig. 612 will appear. It allows the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Evaluate as | You can choose between Zernike Fringe Aberrations, Zernike Standard Aberrations, and Seidel Aberrations. |
| Polynomial Degree | Only for Zernike Standard Aberrations <br> Allows you to set the maximum polynomial degree of the used Zernike terms, and thus indirectly the number of coefficients to be detected. |
| \{Reference Wavefront\} ${ }^{\text {PEE }}$ | This control is explained in Sec. 74.8.1. |
| Maximum Number of Data Points Used For Fitting ${ }^{\text {PV }}$ | For mode fields with many sampling points or rays fitting can be very time consuming. Thus by default only 1000 random data points with non-zero amplitude are extracted from the mode. But you change this for speed up or convergence tests. |


| Calculate Maximum Radial Extent | If you select this option the maximum radial extent of the fitted polynomial is determined automatically from the smallest centered circle containing all data points with non-zero amplitude. |
| :---: | :---: |
| Set Maximum Radial Extent | The maximum radial extent can influence the actual coefficients of the polynomial quite strongly. Thus if e. g. the aperture of a Zernike \& Seidel Aberrations Ideal Component ( $\leftrightarrows$ Sec. 67.5.5) is not fully illuminated by the mode field you can obtain unexpected results. To avoid this you can set a certain maximum radial extent manually. |
| Aberrations / Phase Fitted by Zernike Fringe / Zernike Standard/ Seidel Polynomial | If checked, the unwrapped aberrations fit respective the phase fit is displayed in a data array per mode. |
| Difference of Aberrations / Phase to Zernike Fringe/ Zernike Standard/ Seidel Fit | If checked, the difference of the original phase to the fitted phase of the selected field (i. e. the fitting error) is displayed in a data array per mode. |
| Phase Radius \& Origin | Only for Optimized Radius and Origin The phase radius and the origin of the spherical phase are given as detector results. |
| Origin | Only for User-Defined Radius at Optimized Origin The origin of the spherical phase is given as detector result. |

The phase radius is the distance between the detector plane and the source plane of the spherical phase. Fig. 612 shows how the edit dialog looks like if the detector is used in the main window. If this detector is used in an Optical Setup, a dialog with additional controls is used ( $\rightarrow$ Sec. 74.1).

Note that coefficients being less than $10^{-8}$ the maximum coefficient are set to zero.

## 75 Detectors for Harmonic Fields and Harmonic Fields Sets

Several detectors can be applied to harmonic fields or harmonic fields sets via the Detectors ribbon. If you are in the Data View ( $\rightarrow$ Sec. 12.2.2) of a Harmonic Fields Set you can decide whether you want to apply the detector to all member fields or only to the currently visible one, either via a separate dialog or a checkbox at the very bottom of the edit dialog. If you are in the Light View ( $\leftrightarrows$ Sec. 12.2.1), always all member fields are evaluated. The Camera Detector and the Complex Histogram detector are an exception: they are always applied to all member fields.

### 75.1 Detector from Catalog

Via Detectors > Detector from Catalog you can apply any detector from the detector catalog (but pulse evaluation detectors) on the current harmonic field or harmonic fields set.
If you click on this ribbon item, first the catalog dialog ( $\rightarrow$ Sec. 33) opens where you can select a detector. Then a dialog ( $\rightarrow$ Fig. 613) with further options opens.


Figure 613. The edit dialog for the Detector from Catalog ribbon item.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Load | Loads another detector from the catalog ( $\hookrightarrow$ Sec. 33). |
| Edit | Edits the current detector. |
| View | Always disabled as detectors have no distinct view. |
| Apply to All Fields in Har- | ONLY FOR THE DATA VIEW ( $\hookrightarrow$ SEC. 12.2.2) OF HARMONIC FIELDS SETS |
| monic Fields Set | If checked, the detector is evaluated for all member fields of the Harmonic <br>  <br>  <br>  <br> Fields Set. Otherwise only the currently visible member field is evaluated. <br> In the Light View always all member fields are evaluated and thus this option <br> is not shown. |
| Validity | Indicates whether a valid detector is currently selected. $\leftrightarrows$ Sec. 5.10 |

## Hint

Programmable Detectors using the ParentLightPath variable cannot be used in the main window.

### 75.2 Physical Detectors

The following physical detectors are available for harmonic fields and harmonic fields sets in the main window.

- Beam Parameters; $\hookrightarrow$ Sec. 74.6.1
- Diffractive Optics Merit Functions; $\hookrightarrow$ Sec. 74.6.2
- Fiber Coupling Efficiency; $\hookrightarrow$ Sec. 74.6.6
- Wavefront Error; $\hookrightarrow$ Sec. 74.8.4
- Spherical Phase Radius; $\hookrightarrow$ Sec. 137.6
- Zernike Fringe / Seidel Aberrations; $\hookrightarrow$ Sec. 74.8.5


### 75.3 Field Components

### 75.3.1 Electric Field

This option enables you to extract the electric field components ( $E_{x}, E_{y}$, and $E_{z}$ ) of a harmonic field and to store them into different subsets of a data array.


Figure 614. X-component of the electric field of a Gaussian wave, linearly polarized in x-direction.

### 75.3.2 Magnetic Field (H-Field)

This detector allows you to calculate the magnetic field components $H_{x}, H_{y}$, and $H_{z}$ from a harmonic field. The components of the magnetic field ( $H_{x}, H_{y}$, and $H_{z}$ ) are stored in different subsets of a data array.


Figure 615. $X$-component of the magnetic field of a Gaussian wave, linearly polarized in x-direction.

The data array supports the configuration of view settings as described in Sec. 13.5.
The implemented formulas are given in Sec. 137.7.1.

### 75.3.3 Poynting Vector

This detector displays the components of the time averaged Poynting vector of a harmonic field. In the data array contains the $x$-component, the $y$-component, and the $z$-component of the Poynting vector. The $z$-component of the time averaged Poynting vector is in general the intensity of the electrical field. Only for paraxial fields the
intensity is proportional to the sum of the squared amplitudes of the $x$ - and $y$-field component. The components of the averaged Poynting vector are stored in different subsets of the data array.


Figure 616. Z-component of the Poynting vector of a Gaussian wave.
The data array supports the configuration of view settings as described in Sec. 13.5.
The implemented formulas are given in Sec. 137.7.2.

### 75.4 Numerical Detectors

All detectors described in this section show their output in the Detector Results window. Unless otherwise noted, they are applicable for harmonic fields, harmonic fields sets, transmissions, and signal regions.

### 75.4.1 Average

Via Detectors > Average the average of every field quantity (squared amplitude, amplitude, phase, real and imaginary part) will be calculated. The average $\bar{c}$ is defined by

$$
\begin{equation*}
\bar{c}=\frac{1}{N_{x} N_{y}} \sum_{i=0, j=0}^{N_{x}, N_{y}} c_{i, j} \tag{75.1}
\end{equation*}
$$

$N_{x}$ and $N_{y}$ are the number of sampling points in $x$ - and $y$-direction. $c_{i, j}$ stands for any field quantity of the sampling point $[i, j]$.


Figure 617. The edit dialog shown if the average detector is applied on harmonic fields sets.

For harmonic fields or harmonic fields sets this detector has an edit dialog ( $\hookrightarrow$ Fig. 617) with the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | The vectorial component to be evaluated (either $E_{x}$ or $\left.E_{y}\right)$ can be selected. |
| Apply to All Fields in Har- | ONLY FOR THE DATA VIEW ( $\hookrightarrow$ SEC. 12.2.2) OF HARMONIC FIELDS SETS |
| monic Fields Set | If checked, the detector is evaluated for all member fields of the Harmonic <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> In the Light View always all member fields are evaluated and thus this option <br> is not shown. |

### 75.4.2 Complex Histogram

Creates a histogram showing how often complex numbers in certain equidistant intervals occur within a harmonic field. The histogram shows a selectable part of the complex number plane. The creation of a onedimensional histogram showing just how often certain real or imaginary parts occur is also possible.
In addition it is output how many distinct values occur, i. e. how many of the intervals in the complex histogram are non-zero. In this way you can for example count to how many levels the data was quantized.
For locally polarized fields a histogram for both the $E_{x}$ - and the $E_{y}$-component of the field is generated.


Figure 618. Dialog for the Complex Histogram detector.

After the selection of this menu item the dialog shown in Fig. 618 will appear. It allows the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Real Axis Enable | Enables or disables the real axis in the complex histogram. If the real axis and <br> the imaginary axis are enabled a two-dimensional histogram will be created. <br> If one axis is disabled a one-dimensional histogram will be created. |
| Real Axis Min | The minimum real value of all complex numbers of the harmonic field that is <br> taken into account for the calculation of the histogram. |
| Real Axis Max | The maximum real value of all complex numbers of the harmonic field that is <br> taken into account for the calculation of the histogram. |
| Real Axis Steps | The number of intervals used between Real Axis Min and Real Axis Max for <br> the creation of the histogram. |
| Imaginary Axis Enable | Enables or disables the imaginary axis in the complex histogram. If the real <br> axis and the imaginary axis are enabled a two-dimensional histogram will be <br> created. If one axis is disabled a one-dimensional histogram will be created. |
| Imaginary Axis Min | The minimum imaginary value of all complex numbers of the harmonic field <br> that is taken into account for the calculation of the histogram. |


| Imaginary Axis Max | The maximum imaginary value of all complex numbers of the harmonic field <br> that is taken into account for the calculation of the histogram. |
| :--- | :--- |
| Imaginary Axis Steps | The number of intervals used between Imaginary Axis Min and Imaginary Axis <br> Max for the creation of the histogram. |
| Get Field Extrema | Detects automatically the minimum and maximum real and imaginary value <br> and sets the results in the dialog. |
| Apply to All Fields in Har- | OnLY FOR HARMONIC FIELDs SETS <br> monic Fields Set |
|  | If checked, the detector is evaluated for all member fields of the Harmonic <br>  <br> Fields Set. Otherwise only the currently visible member field is evaluated. <br> In the Light View always all member fields are evaluated and thus this option <br> is not shown. If the Harmonic Fields Set contains both locally and globally <br> polarized fields, this option is also not shown as in this case it is not possible |
| to evaluate all fields at once. As both rules contradict each other, an error is |  |
| shown if both conditions are met. |  |

### 75.4.3 Field Deviation

This detector provides a convenient way to calculate the absolute differences between the amplitudes and phases of two harmonic fields or two harmonic fields sets, respectively. The results are written into different subsets of a Data Array. For harmonic fields sets one data array per member field is returned, bundled into a Set of Data Arrays.
This detector can be used via Detectors > Field Deviation. Then a dialog opens where you can select the second harmonic field / harmonic fields set. In case of harmonic fields sets, the number of member fields must be the same for the two documents. If the two fields to compare do not have the same sampling, they are resampled to a common sampling (largest field size and smallest sampling distance).

### 75.4.4 Minimum / Maximum Value

Via Detectors > Minimum / Maximum Value maximum and minimum value of every field quantity and their respective position in the field will be calculated.


Figure 619. The edit dialog shown if the minimum / maximum detector is applied on harmonic fields or harmonic fields sets.

For harmonic fields or harmonic fields sets this detector has an edit dialog ( $\hookrightarrow$ Fig. 619) with the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | The vectorial component to be evaluated (either $E_{x}$ or $\left.E_{y}\right)$ can be selected. |
| Apply to All Fields in Har- | OnLY FOR THE DATA VIEW ( $\hookrightarrow$ SEC. 12.2.2) OF HARMONIC FIELDS SETS |
| monic Fields Set | If checked, the detector is evaluated for all member fields of the Harmonic <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> In the Light View always all member fields are evaluated and thus this option <br> is not shown. |

### 75.4.5 Momentum



Figure 620. Dialog for momentum calculation

The dialog in Fig. 620 can be accessed via Detectors > Momentum. It has the following entries.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | ONLY FOR LOCALLY POLARIZED FIELDS <br> Selects the vectorial component $\left(E_{x}\right.$ or $\left.E_{y}\right)$ for which the momenta shall be <br> calculated. |
| Order $\mathbf{X}$ | The order in x of the momentum which shall be calculated (see below). |
| Order $\mathbf{Y}$ | The order in y of the momentum which shall be calculated (see below). |
| Order ThetaX | The order in $\Theta_{x}$ of the momentum which shall be calculated (see below). |
| Order ThetaY | The order in $\Theta_{y}$ of the momentum which shall be calculated (see below). |
| Apply to All Fields in Har- | OnLY FOR THE DATA VIEw $(\hookrightarrow$ SEc. 12.2.2) of HARMONIC FIELDS SETS <br> monic Fields Set <br> If checked, the detector is evaluated for all member fields of the Harmonic |
|  | Fields Set. Otherwise only the currently visible member field is evaluated. |
| In the Light View always all member fields are evaluated and thus this option |  |
| is not shown. |  |

All values have to be positive integers inclusive zero. The calculated momenta will be shown in the Detector Results tab page.
The momentum theory is very useful to determine the beam parameters ( $\hookrightarrow$ Sec. 74.6.1) of an arbitrary wave with global polarization. The formulas are given in Sec. 137.8

### 75.4.6 Standard Deviation

Via Detectors > Standard Deviation the standard deviation $\sigma$ from the average $\bar{c}(\hookrightarrow$ Sec. 75.4.1) can be calculated for every field quantity (squared amplitude, amplitude, phase, real and imaginary part). It is defined by

$$
\begin{equation*}
\sigma=\sqrt{\frac{1}{N_{x} N_{y}} \sum_{i=0, j=0}^{N_{x}, N_{y}}\left(c_{i, j}-\bar{c}\right)^{2}} \tag{75.2}
\end{equation*}
$$

$N_{x}$ and $N_{y}$ are the number of sampling points in $x$ - and $y$-direction. $c_{i, j}$ stands for any field quantity of the sampling point $[i, j]$.

| Vectorial Component |  | $\times$ |
| :---: | :---: | :---: |
| Vectorial Component | Ex Component | $\checkmark$ |
| $\checkmark$ Apply to All Fields in Harmonic Fields Set |  |  |
|  | Ok |  |

Figure 621. The edit dialog shown if the standard deviation detector is applied on harmonic fields or harmonic fields sets.

This detector has an edit dialog ( $\hookrightarrow$ Fig. 621) with the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | The vectorial component to be evaluated (either $E_{x}$ or $E_{y}$ ) can be selected. |
| Apply to All Fields in Har- | ONLY FOR THE DATA VIEW ( $\hookrightarrow$ SEC. 12.2.2) OF HARMONIC FIELDS SETS |
| monic Fields Set | If checked, the detector is evaluated for all member fields of the Harmonic <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> Fields Set. Otherwise only the currently visible member field is evaluated. <br> In not shown. |

### 75.4.7 Summed Norm

Via Detectors > Summed Norm the summed norm of the whole field component can be calculated. Additionally, if a range or rectangle marker is visible, the summed norm within the current selection and the ratio between these two values is calculated.
The summed norm $S$ of a certain region is defined as the sum of the squared amplitude $A^{2}$ of each pixel in this region:

$$
\begin{equation*}
S=\sum_{i=0, j=0}^{N_{x}, N_{y}} A^{2} \tag{75.3}
\end{equation*}
$$

$N_{x}$ and $N_{y}$ are the number of sampling points in x-and y-direction, respectively. $A^{2}$ is the squared amplitude of either $E_{x}$ or $E_{y}$ if the data view ( $\hookrightarrow$ Sec. 12.2.2) is visible or the summed intensity if the light view ( $\hookrightarrow$ Sec. 12.2.1) is visible.

| Vectorial Component |  | $\times$ |
| :---: | :---: | :---: |
| Vectorial Component Ex Component$\square$ Apply to All Fields in Harmonic Fields Set |  |  |
|  |  |  |
|  | Ok |  |

Figure 622. The edit dialog of the summed norm detector.

In case this detector is applied on the data view a dialog ( $\hookrightarrow$ Sec. 622) with the following options is shown:
ITEM DESCRIPTION

| Vectorial Component | The vectorial component to be evaluated (either $E_{x}$ or $E_{y}$ ) can be selected. |
| :--- | :--- |
| Apply to All Fields in Har- | OnLY FOR THE DATA VIEW ( $\hookrightarrow$ SEC. 12.2.2) OF HARMONIC FIELDS SETS |
| monic Fields Set | If checked, the detector is evaluated for all member fields of the Harmonic |
|  | Fields Set. Otherwise only the currently visible member field is evaluated. |
|  | In the Light View always all member fields are evaluated and thus this option |
|  | is not shown. |

## 76 Detectors for Data Arrays

All the detectors in this section work for (gridded) Numerical Data Arrays ( $\hookrightarrow$ Sec. 13.5) as well as for document types based on gridded data arrays (chromatic fields sets [ $\hookrightarrow$ Sec. 14] and pulse and field components [ $\leftrightarrows$ Sec. 15]).

### 76.1 Data Point Average

Via Detectors > Data Point Average the average of one or more selected field quantities will be calculated. The average $\bar{c}$ refers to the set of all data points (instead of a unit area like $m^{2}$ or $\mathrm{mm}^{2}$ or the like) and is defined by

$$
\begin{equation*}
\bar{c}=\frac{1}{N_{x} \cdot N_{y}} \sum_{i=0, j=0}^{N_{x}, N_{y}} c_{i, j} \tag{76.1}
\end{equation*}
$$

$N_{x}$ and $N_{y}$ are the number of data points in x - and y -direction. $c_{i, j}$ stands for any field quantity of the data point $[i, j]$.
For objects with complex-valued data or with more than one subset, a dialog opens where you can select one or more field quantities ( $\hookrightarrow$ Sec. 11.1) for which the data point average is calculated. If you select/unselect All, all/no field quantities are selected. Furthermore, you can select whether the calculation shall be done on all of the subsets or only on the currently visible one.

### 76.2 Complex Histogram

Creates a histogram showing how often complex numbers in certain equidistant intervals occur within the data. The histogram shows a selectable part of the complex number plane. The creation of a one-dimensional histogram showing just how often certain real or imaginary parts occur is also possible.
In addition it is output how many distinct values occur, i. e. how many of the intervals in the complex histogram are non-zero. In this way you can for example count to how many levels the data was quantized.


Figure 623. Dialog for the Complex Histogram Detector for Data Arrays.
After the selection of this menu item the dialog shown in Fig. 623 will open. It allows the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Evaluate Current Subset / | Allows to select whether the calculation shall be done for all subsets or only <br> for the currently visible one. |
|  | Note: If Evaluate All Subsets is selected, no Min or Max values can be en- <br> tered because they could strongly vary in range and meaning for the different <br> subsets. |
| Real Axis Enable | Enables or disables the real axis in the complex histogram. If the real axis and <br> the imaginary axis are enabled, a two-dimensional histogram will be created. <br> If one axis is disabled a one-dimensional histogram will be created. |
| Real Axis Min | For EVALUATE CURRENT SUBSET MODE ONLY. <br>  |


| Real Axis Max | For Evaluate Current Subset mode only. <br> The maximum real value that is used for the calculation of the histogram. |
| :---: | :---: |
| Real Axis Steps | The number of intervals used between Real Axis Min and Real Axis Max for the creation of the histogram. |
| Imaginary Axis Enable | FOR COMPLEX DATA ONLY. <br> Enables or disables the imaginary axis in the complex histogram. If the real axis and the imaginary axis are enabled, a two-dimensional histogram will be created. If one axis is disabled a one-dimensional histogram will be created. |
| Imaginary Axis Min | For complex data and the Evaluate Current Subset mode only. <br> The minimum imaginary value that is used for the calculation of the histogram. |
| Imaginary Axis Max | For complex data and the Evaluate Current Subset mode only. The maximum imaginary value that is used for the calculation of the histogram. |
| Imaginary Axis Steps | FOR COMPLEX DATA ONLY. <br> The number of intervals used between Imaginary Axis Min and Imaginary Axis Max for the creation of the histogram. |
| Get Field Extrema | For Evaluate Current Subset mode only. <br> Detects automatically the minimum and maximum real and imaginary value and sets the results into the dialog. |

### 76.3 Full Width at Half Maximum

For real-valued data, this detector calculates the width which corresponds to half of the maximum value of a lateral data distribution. Therefor the position of the first maximum in the field is calculated. Starting from this position, the innermost positions are searched in both (i.e. $x$ - and $y$-) directions for these positions where the function falls below the half of the maximum value.
For objects with complex-valued data or with more than one subset, a dialog opens where you can select one or more field quantities ( $\hookrightarrow$ Sec. 11.1) for which the full width at half of the maximum is calculated. If you select/unselect All, all/no field quantities are selected. Furthermore, you can select whether the calculation shall be done on all of the subsets or only on the currently visible one.

### 76.4 Minimum / Maximum (Position and Value)

For real-valued data, this detector searches for the minimum / maximum value and the (smallest) $x$-( $y$-)position where the minimum / maximum is reached.
For objects with complex-valued data or with more than one subset, a dialog opens where you can select one or more field quantities ( $\hookrightarrow$ Sec. 11.1) for which the minimum / maximum is calculated. If you select/unselect All, all/no field quantities are selected. Furthermore, you can select whether the calculation shall be done on all of the subsets or only on the currently visible one.

### 76.5 Standard Deviation

Via Detectors > Standard Deviation the standard deviation $\sigma$ from the average $\bar{c}(\hookrightarrow$ Sec. 76.1) can be calculated for one or more given field quantities. It is defined by

$$
\begin{equation*}
\sigma=\sqrt{\frac{1}{N_{x} \cdot N_{y}} \sum_{i=0, j=0}^{N_{x}, N_{y}}\left(c_{i, j}-\bar{c}\right)^{2}} \tag{76.2}
\end{equation*}
$$

$N_{x}$ and $N_{y}$ are the number of data points in $x$ - and $y$-direction. $c_{i, j}$ stands for any field quantity of the data point $[i, j]$.
For objects with complex-valued data or with more than one subset, a dialog opens where you can select one or more field quantities ( $\hookrightarrow$ Sec. 11.1) for which the standard deviation is calculated. If you select/unselect All, all/no field quantities are selected. Furthermore, you can select whether the calculation shall be done on all of the subsets or only on the currently visible one.

### 76.6 Uniformity Error

ONLY FOR TWO-DIMENSIONAL DATA ARRAYS.

The uniformity error detector can be applied by clicking on the ribbon item Detectors > Uniformity Error. The user needs to specify a desired output field that is used to evaluate the uniformity error. The uniformity error $E_{\text {unif }}$ is defined as follows:

$$
\begin{equation*}
E_{\mathrm{unif}}=\frac{Q_{\max }-Q_{\min }}{Q_{\max }+Q_{\min }} \tag{76.3}
\end{equation*}
$$

$Q_{\text {min/max }}$ is the smallest/largest occurring quotient of the values in the data array divided by the values in the desired output field.
The output of the detector are the minimum quotient $Q_{\min }$, the maximum quotient $Q_{\max }$ and the calculated uniformity error.


Figure 624. The edit dialog of the Uniformity Error Detector.

Fig. 624 shows the edit dialog of the uniformity detector. The following setting can be done by the user:
DESCRIPTION
Desired Output Field > Set The user has to specify a desired output field as data array. If you click on this button you can do the following:

- Load a data array from a .da file.
- Import a data array from a bitmap or text file by means of the import wizard described in Sec. 121.2.
- Select from Documents allows you to select an already open data array. In any case the data array has to contain only one subset. It has to be equidistant and the data has to be real-valued.
Desired Output Field $>$ Shows the desired output field as separate Data Array document.
Show

Evaluate Current Subset/
Evaluate All Subsets

If you click on the first control, only the currently visible subset is evaluated. If you click on the latter, all subsets of the Data Array are evaluated separately. These controls are only visible if the Data Array contains more than one subset.

### 76.7 Sum within Selection

Using Detectors > Sum Within Selection, the sum of all values inside a previously marked selection can be obtained.
This detection works for one-dimensional as well as for two-dimensional Numerical Data Arrays. As described in Sec. 11.3, a coordinate range has to be selected in the 1D case, a rectangle or elliptic selection is prerequisite in the 2D case.
In each of the cases, data points which are covered only partially by the selection are considered according to the intersection between the data point's coordinate range and the selection.

### 76.8 Add Polarization Ellipses

The ribbon button Detectors > Add Polarization Ellipses allows you to calculate polarization ellipses for Electric or Electromagnetic Fields ( $\hookrightarrow$ Sec. 13.1) either if none were calculated by the Universal Detector $(\hookrightarrow$ Sec. 74.4 ) or if the ellipses shall be calculated anew for whatever reason. This functionality is described in Sec. 32.3 in more detail.

### 76.9 Apply Detector Add-on

The ribbon button Detectors > 疑Apply Detector Add-on allows you to apply any detector add-on onto Data Arrays ( $\hookrightarrow$ Sec. 13) and Chromatic Fields Sets ( $\hookrightarrow$ Sec. 14) just like the Universal Detector does ( $\hookrightarrow$ Sec. 74.4.5). Via clicking on the upper part of the split button or on Apply Detector Add-on in its lower part, you can load a detector add-on from hard disc. Then the dialog explained in Sec. 625 opens where you can change the loaded snippet or create a new one.
In addition the lower part of the button contains those add-ons that you have stored as favorite in the edit dialog for detector add-ons ( $\leftrightarrows$ Sec. 76.9.1, Sec. 74.4.5.2). And it has the additional entry Update Predefined Add-ons which loads the most up-to-date addons from the Wyrowski Photonics Website. Optionally also the snippets of all favorites are then updated if they have the same name as a predefined addon. The values of your favorites's snippet parameters are kept.

### 76.9.1 Dialog for Applying a Detector Add-on on a Data Array



Figure 625. Edit dialog for a detector add-on.

| ITEM | DESCRIPTION |
| :---: | :---: |
| New Add-on | Allows you to load the add-on to be applied, either From Template or From File. |
| Edit | Opens the source code editor for the add-on's snippet. |
| \{Parameter Box\} | This box contains the parameters defined in the snippet if there are any. $\rightarrow$ Sec. 7.4 |
| Wave Front Data (Optional) | Data which describe the wave front of a electric/magnetic/ electromagnetic field can be set, removed or shown here if needed. Wave Front Data means the Wavefront Phase mentioned in Sec. 74.4 which is the smooth part of the phase of the field in the detector plane. Only this data, extracted by the Universal Detector shall be used if needed (because the data have to correspond to the calling field by all means). Whether or not this data are to be set at all depends on the actual add-on's snippet. |
| Medium to Use Detector In | The optical medium the add-on shall be applied in can be defined here ( $\leftrightarrows$ Sec. 37.3.1, $\lrcorner$ Sec. 34). |
| ¢ | Saves the add-on as separate file into the Favorites folder. Shortcuts to these files are shown when you click on the lower part of the Apply Detector Add-on button ( $\hookrightarrow$ Sec. 76.9). |

## XII <br> Analyzers: Evaluating Optical Systems

Analyzers evaluate an Optical Setup or a single Optical Setup Element in a special way, independent from the simulation engines described in Sec. 43.4.
For example the Distortion Analyzer ( $\checkmark$ Sec. 78) calculates the distortion introduced by one Optical Setup Element, whereas the Eigenmode Analyzer ( $\leftrightarrows$ Sec. 89) calculates the eigenmode of a complete laser resonator optical setup.

## 77 Coating Analyzer

Only available in a General Optical Setup.
Knowing the reflection properties of a certain surface is very important for many applications. If these properties don't meet the needs of the optical setup, it may be necessary to equip the surface with a coating.
The function of the Coating Analyzer is the evaluation of the reflection and transmission values of an optical surface in order to provide a base for the decision on applying a coating. The improvement achieved by a certain coating can be evaluated too. Supported outputs are tables with Fresnel coefficients as well as data arrays ( $\hookrightarrow$ Sec. 13.5) showing the dependencies of a certain coefficient on wavelength and angle of incidence. The analyzer element has to be configured before each use via its edit dialog which is called by double click on the element's symbol in the Optical Setup View or on the corresponding table entry in the Optical Setup Table. It has a wizard structure and has to be filled by the sequential steps described in the following subsections.

### 77.1 Selection of the Surface to Analyze

At first, the component that contains the surface to analyze has to be selected. The component can be a Curved Surface ( $\lrcorner$ Sec. 58.1), Lens System ( $\hookrightarrow$ Sec. 57.1) , or Spherical Lens ( $\hookrightarrow$ Sec. 57.3 ) which must be linked to the active light source. Then, the surface itself can be selected.

| Select Surface to Analyze |  |  |
| :--- | :--- | :---: |
| Component | Spherical Lens \#2 |  |
|  |  |  |
| Surface | $1 \star$ |  |
|  |  |  |

Figure 626. Controls for selecting the surface to analyze.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component | The component the surface to be analyzed belongs to. This may be either a |
|  | Curved Surface, a Lens System, or a Spherical Lens. |
| Surface | The surface to be analyzed. It is selected by its index inside its component. |

### 77.2 Selection of Analyzer Output

## Select Ouput

Reflectance Only
O All Coefficients [Table]
O Incidence Angle Dependent Coefficients [Data Array]
(O) Wavelength Dependent Coefficients [Data Array]

Wavelength and Angle Dependency [Data Array]

Figure 627. Controls for selecting the analyzer's output.

The following types of output are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reflectance Only | Only the reflectance for TE and TM is calculated and shown in the Detector <br> Results tab of the main window. |
| All Coefficients [Table] | The reflectance, transmittance, and the complex Fresnel coefficients will be <br> calculated for TE as well as for TM for a given wavelength, angle of incidence <br> and lateral position on the surface. |
| Incidence Angle Depen- <br> dent Coefficients [Data Ar- | The user will have to select up to four parameters to calculate a 1D data array <br> for. It will show the dependency of this parameter on the angle of incidence <br> for a given wavelength. |
| Way] | The user will have to select up to four parameters to calculate a 1D data <br> array for. It will show the dependency of this parameter on the wavelength for <br> a given angle of incidence. |
| Wavelength and Angle De- | The user will have to select up to four parameters to calculate a 2D data array <br> pendency [Data Array] <br> for. It will show the dependencies of this parameter on the wavelength and <br> the angle of incidence. |

## Note on Optimization

This analyzer can be used for Parametric Optimization ( $\lrcorner$ Sec. 102) under the following conditions:

1. Reflectance Only is used as output mode. In this case you can optimize the reflectance for one specific wavelength and incidence angle.
2. For any of the data array outputs you can use the Parametric Optimization if you select that the reflectance (= reflection intensity coefficient) is calculated. Because then the minimum and maximum reflectance as well as the arithmetic mean of all reflectance values in the resulting data arrays are being calculated and those values can be used as optimization constraints.

### 77.3 Configuring the Analyzer Output

Each type of output requires certain parameters that are described in the following.

### 77.3.1 Reflectance Only and All Coefficients [Table]



Figure 628. Configuration of the Reflectance Only or the All Coefficients output.


Figure 629. Example for an output of all Fresnel coefficients in one table.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Lateral Position on Sur- <br> face | Coordinates of the position on the surface where the Fresnel coefficients shall <br> be calculated for. |
| Wavelength | Wavelength the coefficients shall be calculated for. |
| Incidence Angle | Incidence angle the calculation shall be done for. It is defined in relation to <br> the normal vector of the surface to analyze. |
| Use Collimation Angle | If this box is checked, the incidence angle is determined from the angle be- <br> tween the normal vector of the surface to be analyzed and the output axis <br> of the Optical Setup Element which prepends it in the execution sequence of <br> the Optical Setup. $\hookrightarrow$ Fig. 630. |



Figure 630. Meaning of the collimation angle: Angle between the normal vector of the surface to analyze and the output axis of its prepended element in the Optical Setup (Reference Element).

### 77.3.2 Incidence Angle Dependent Coefficients [Data Array]



Figure 631. Configuration of the Incidence Angle Dependent Coefficients output.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Intensity Coefficients | Select this option if you want to calculate reflectance or transmittance. |
| Complex Fresnel Coeffi- <br> cients | Select this option if you want to calculate the complex reflection and trans- <br> mission coefficients. |
| Reflection / Transmission | Select here if reflection and / or transmission coefficients shall be calculated <br> and returned as separate subsets in the resulting data array. |
| perpendicular (TE) / paral- <br> lel (TM) | Select here which polarization state(s) shall be calculated and returned as <br> separate subsets in the resulting data array. |
| Wavelength | Wavelength the coefficients shall be calculated for. |
| Angle Range | Range of incidence angles the calculation shall be done for. |

### 77.3.3 Wavelength Dependent Coefficients [Data Array]



Figure 632. Configuration of the Wavelength Dependent Coefficients output.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Intensity Coefficients | Select this option if you want to calculate reflectance or transmittance. |
| Complex Fresnel Coeffi- <br> cients | Select this option if you want to calculate the complex reflection and trans- <br> mission coefficients. |
| Reflection / Transmission | Select here if reflection and/or transmission coefficients shall be calculated <br> and returned as separate subsets in the resulting data array. |
| perpendicular (TE) / paral-  <br> lel (TM) Select here which polarization state(s) shall be calculated and returned as <br> separate subsets in the resulting data array. <br> Wavelength Range Range of wavelengths the coefficients shall be calculated for. <br> Incidence Angle Angle of light incidence the calculation shall be done for. <br> Use Collimation Angle <br> If this box is checked, the incidence angle is determined from the angle be- <br> tween the normal vector of the surface to be analyzed and the output axis <br> of the Optical Setup Element which prepends it in the execution sequence of <br> the Optical Setup. $\hookrightarrow$ Fig. 630.  |  |

### 77.3.4 Wavelength and Angle Dependency [Data Array]



Figure 633. Configuration of the Wavelength and Angle Dependency output.


Figure 634. Example for a 2D data array output of the reflectance for TM polarization.

ITEM
Intensity Coefficients
Complex Fresnel Coefficients

Reflection / Transmission
perpendicular (TE) / paral-

| $\begin{array}{l}\text { perpendicular (TE) / paral- } \\ \text { lel (TM) }\end{array}$ | $\begin{array}{l}\text { Select here which polarization state(s) shall be calculated and returned as } \\ \text { separate subsets in the resulting data array. }\end{array}$ |
| :--- | :--- |
| Wavelength Range | Range of wavelengths the coefficients shall be calculated for. |
| Angle Range | Range of incidence angles the calculation shall be done for. |

## DESCRIPTION

Select this option if you want to calculate reflectance or transmittance.
Select this option if you want to calculate the complex reflection and transmission coefficients.

Select here if reflection and / or transmission coefficients shall be calculated and returned as separate subsets in the resulting data array.

Angle Range Range of incidence angles the calculation shall be done for.

## 78 Distortion Analyzer

## Only available in a General Optical Setup.

The Distortion Analyzer calculates the distortion of a laser beam introduced by one component for various angles in one direction. It works for the index modulated components ( $\hookrightarrow$ Sec. 56.2), a Lens System ( $\hookrightarrow$ Sec. 57.1), a Spherical Lens ( $\hookrightarrow$ Sec. 57.3), or a Curved Surface ( $\hookrightarrow$ Sec. 58.1).
For each angle a small ray bundle is propagated through the selected component and the so calculated deflection $y_{\text {real }}$ compared to the reference deflection $y_{\text {ref }}$ yields the distortion $D$ for this angle.

$$
\begin{equation*}
D=\frac{y_{\mathrm{real}}-y_{\mathrm{ref}}}{y_{\mathrm{ref}}} \tag{78.1}
\end{equation*}
$$

whereas $y_{\text {ref }}=f \cdot \tan \alpha$ for $\operatorname{Tan}\left(\right.$ Theta) distortion and $y_{\text {ref }}=f \cdot \alpha$ for Theta distortion. $f$ is the effective focal length of the analyzed component.


Figure 635. The edit dialog for the distortion analyzer in Single Distortion Values mode.

The edit dialog of this analyzer ( $\hookrightarrow$ Fig. 635) has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component to Analyze | Allows you to select any allowed component. If there is only one suitable <br> component in the Optical Setup, it is used automatically without the necessity <br> to edit the dialog first. |
| Calculate Distortion for | If this option is checked, the effective focal length $f$ is determined automati- <br> cally by evaluating the selected component. Otherwise the user can set the <br> Effective Focal Length. |
| Effective Focal Length | OnLY IF CALCULATE DISTORTION FOR EFFECTIVE FocAL LENGTH is NOT <br> CHECKED. |
| The effective focal length of the component. |  |

[^12] and the angle of maximum distortion are additionally calculated.

## 79 Field Curvature Analyzer

Only available in a General Optical Setup.
The Field Curvature Analyzer calculates the field curvature for both tangential and sagittal plane by evaluating the focus position for various incident angles or positions. It works for the index modulated components ( $\leftrightarrows$ Sec. 56.2), a Lens System ( $\hookrightarrow$ Sec. 57.1), a Spherical Lens ( $\hookrightarrow$ Sec. 57.3), or a Curved Surface ( $\hookrightarrow$ Sec. 58.1). For each angle or position a small ray bundle is propagated through the selected component and its focus position is determined.


Figure 636. The edit dialog for the field curvature analyzer for a Finite Object Distance in Single Field Curvature Values mode.

The edit dialog of this analyzer ( $\hookrightarrow$ Fig. 636) has the following options.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Component to Analyze | Allows you to select any allowed component. Note that this component needs not to be connected to a light source. If there is only one suitable component in the Optical Setup, it is used automatically without the necessity to edit the dialog first. |
| Evaluate Field Curvature Relative to Focal Plane | If this option is checked, the evaluation is done in the focal plane $z=f_{0}$ of the component where $f_{0}$ is the effective focal length for on-axis incidence. In case the active light source has more than one wavelength you can choose the Reference Wavelength which is used for the calculation of $f_{0}$. Otherwise the user can set the Evaluation Distance, measured from the reference point of the transmission coordinate system of the Component to Analyze ( $\leftrightarrows$ Sec. 43.8.1.3). |
| Finite Object Distance | If this option is not checked, the evaluation is done with collimated ray bundles entering the component with certain angles. Otherwise ray bundles are created which originate in the given Distance to Object Plane at a certain object height (= distance from optical axis). |
| Results for Sagittal Plane / Results for Tangential Plane | Allows you to define whether the results for the tangential plane (contains the optical axis) and / or the sagittal plane (perpendicular to the tangential plane) are calculated. The dialog ensures that at least one plane is selected. |
| Angle Range / <br> Object Height Range | Defines along which direction the field curvature is calculated ( $x$ - or $y$-axis of the component, whereas in both cases the positive or the negative range can be used). |
| Field Curvature Data Array | You can scan a complete angle range and the results are returned as data array - or as set of data arrays if the light source of the system emits more than one wavelength. |
| Single Field Curvature Values | In this case you directly enter the angles or object heights you want to analyze. This mode allows you to optimize the field curvature of certain angles or object heights with the Parametric Optimization ( $\hookrightarrow$ Sec. 102). |
| Maximum Angle / <br> Maximum Object Height | Only for Field Curvature Data Array <br> The maximum angle or object height of the scanned range. The minimum angle always equals the Scanning Step Size. |
| Scanning Step Size | Only for Field Curvature Data Array <br> The distance between two consecutive angles or object heights in the scanned range. |
| Number of Field Curvature Values | Only for Single Field Curvature Values <br> The number of angles or object heights for which you want to calculate the field curvature. Then you can enter the concrete values of the angles or object heights in a simple table. |

Independent of whether Field Curvature Data Array or Single Field Curvature Values is selected, the maximum field curvature and the angle or object height of maximum field curvature are additionally calculated.

## 80 Field Inside Component Analyzer: Split Step

## Only available in a General Optical Setup.

The Field Inside Component Analyzer: Split Step can be used to visualize the field components inside an
inhomogeneous region of the optical system. To enable this analysis the split step propagation needs to be selected within an index-modulated component ( $\hookrightarrow$ Sec. 56.2) or a Double Surface Component ( $\hookrightarrow$ Sec. 65). For each step of the split step propagation along the z-direction an intermediate result is calculated which is then processed further by this analyzer.


Figure 637. The edit dialog of the Field Inside Component Analyzer for the split step propagation.

Fig. 637 shows the edit dialog of the analyzer which allows the following settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Optical Setup Element To Analyze | The user needs to select the Optical Setup Element that shall be evaluated. Within the combobox all available components in the underlying Optical Setup will be listed. |
| Harmonic Field Component | In this group box you can set up which harmonic field components ( $E_{x}, E_{y}, E_{z}$, $H_{x}, H_{y}, H_{z}, S_{x}, S_{y}$ and/or $S_{z}$ ) are extracted from the intermediate fields. Each field component is shown in a data array in a Set of Data Arrays ( $\rightarrow \mathrm{Sec} .16$ ). In case of two-dimensional fields a subset is generated for each z-position. In case of one-dimensional fields the components are plotted along the $z$ direction in a single two-dimensional subset. |
| Evaluate Power Along z | The user can specify whether the power shall be calculated per z-slab. The resulting function will be visualized within a one-dimensional data array. |
| Evaluate Custom Merit Function | For several applications it can be helpful to define customized merit functions for the propagation through inhomogeneous media. The user can define a snippet which calculates a list of physical values out of each intermediate result. The result is a one-dimensional data array where the physical values are plotted versus the $z$-position in individual subsets. |
| Custom Merit Function Evaluation | Only if Evaluate Custom Merit Function is checked. <br> This group box allows you to program the evaluation snippet. Edit opens the Source Code Editor ( $\varsigma$ Sec. 7.3) to edit this snippet, and a validity indicator ( $\leftrightarrows$ Sec. 5.10) shows whether this snippet is consistent. Below there is a region where you can set the values of the global parameters of the snippet (if present); $\leftrightarrows$ Sec. 7.4. |

The dialog ensures that at least one output is selected.

## 81 Focal Length Analyzer

## Only available in a General Optical Setup.

This analyzer calculates both the effective and the back focal length of the index modulated components ( $\varsigma$ Sec. 56.2), a Lens System ( $\leftrightarrows$ Sec. 57.1 ), a Spherical Lens ( $\leftrightarrows$ Sec. 57.3 ), or Curved Surface ( $\hookrightarrow$ Sec. 58.1). This is done by ray tracing and evaluating a paraxial ray bundle.


Figure 638. The edit dialog of the Focal Length Analyzer.
Its edit dialog, shown in Fig. 638, has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Component to Analyze | Allows you to select any allowed component. Note that this component needs <br> not to be connected to a light source. If there is only one suitable component <br> in the Optical Setup, it is used automatically without the necessity to edit the <br> dialog first. |
| Evaluate All Wavelengths <br> of Active Light Source | In this mode the focal lengths are calculated for all wavelengths specified in <br> the active light source (those with index 0). |
| Evaluate $\quad$ Single $\quad$ Wave- <br> length | In this mode you can set the wavelength for which the focal lengths are cal- <br> culated. |

## 82 Optical Path Length Analyzer

## Only available in a General Optical Setup.

The Optical Path Length Analyzer can be used to evaluate the optical path lengths of a sub-path in the underlying Optical Setup. The active source in the Optical Setup must be configured as a polychromatic source, because otherwise this analyzer would generate no valuable output. The sampling in the frequency domain has to be adapted for the specified sub-path. Therefor the user can select the Automatic Sampling mode. In this case, VirtualLab Fusion will estimate the oversampling factor for the frequency domain. Alternatively the user can specify an oversampling factor for the frequencies manually. This oversampling factor will increase the accuracy of further investigations, e.g. the Inverse Temporal Fourier Transformation ( $\leftrightarrows$ Sec. 31.2.1).
The user can specify the end element (= detector) of the sub-path to be evaluated and as well as the output of the analyzer. The Optical Path Length Analyzer can display the optical path length over frequencies $v$ or the absolute phase over the frequencies $v$. Additionally a linear function can be fitted to the absolute phase. For the linear fit the Optical Path Length Analyzer provides three different methods.
Fig. 639 shows the edit dialog of the Optical Path Length Analyzer.


Figure 639. The edit dialog of the Optical Path Length Analyzer. The user can set up the sub-path which shall be evaluated as well as the output of the analyzer.

| ITEM | DESCRIPTION |
| :---: | :---: |
| From Light Source | The active light source in the Optical Setup the analyzer is placed in. This light source must be polychromatic, otherwise an error will be shown if the analyzer processed. |
| To Detector | The user can specify the end element (= detector) of the sub-path for which the optical path length shall be evaluated. The end element must be connected with the active light source by a unique path. |
| Evaluate Optical Path Length | This checkbox defines whether the optical path length versus the frequencies $v$ shall be shown. |
| Evaluate Phase by Optical Path Length | The Optical Path Length Analyzer can also calculate the absolute phase. By checking this option a diagram is shown where the phase over $v$ can be investigated. |
| Fit I: Time Shift without Dispersion | The first type of linear fit does not consider dispersion effects in the system which shall be analyzed. The user can specify whether the fitted linear function shall be drawn additionally in the phase diagram and whether the residuals shall be evaluated. |
| Fit II: Time Shift by Regression | The second type of linear fit does consider dispersion effects in the system which shall be analyzed. The dispersion effect is fitted by a linear regression to the absolute phase curve. The user can specify whether the fitted linear function shall be drawn additionally in the phase diagram and whether the residuals shall be evaluated. |
| Fit III: Time Shift with Dispersion | The third type of linear fit does consider dispersion effects in the system which shall be analyzed. The dispersion effect is evaluated by the group velocity of the pulse. The user can specify whether the fitted linear function shall be drawn additionally in the phase diagram and whether the residuals shall be evaluated. |
| Automatic Sampling | VirtualLab Fusion estimates the frequency sampling for the selected light path. The calculated oversampling factor will be logged into the logging window of VirtualLab Fusion and additionally be shown when the dialog is opened the next time. |
| Manual Sampling | The manual sampling mode allows the user to enter a self-defined oversampling factor (of frequencies). |
| Oversampling Factor (Frequencies) | The oversampling factor can be configured to use more frequencies for the OPL analysis. This oversampling factor will also increase the accuracy of further investigations, e.g. the Inverse Temporal Fourier Transformation ( $\leftrightarrows$ Sec. 31.2.1). |



Figure 640. Diagrams generated by the Optical Path Length Analyzer for a sample Optical Setup.

Fig. 640 shows some sample results of the Optical Path Length Analyzer for a sample system.
The slopes of the fitted linear functions give the time shift, i. e. the time the pulse needed to propagate through the (sub-)system. The Optical Path Length Analyzer logs the obtained time shifts into the detector window (one per selected fit method, $\hookrightarrow$ Fig. 641). The time shifts can be used for further investigations of pulses in VirtualLab Fusion, especially for the temporal Fourier Transformation ( $\hookrightarrow$ Sec. 31.2.1).
The residual functions calculated by the Optical Path Length Analyzer can be used to increase the time window for the Inverse Temporal Fourier Transformation ( $\hookrightarrow$ Sec. 31.2.1).

| Detector | Sub - Detector | Result |
| :---: | :---: | :---: |
| OPL Analyzer | Linear Fitl: Time Shift without Dispersion | 19.246 ps |
|  | Linear Fitll: Time Shift by Regression | 18.941 ps |
|  | Linear Fit Ill: Time Shift with Dispersion | 18.945 ps |

Figure 641. The slope of the linear fits is logged into the Detector Results tab on the bottom of the VirtualLab Fusion main window.

## 83 Parameter Variation Analyzer

## Not for a Laser Resonator Setup.

This analyzer allows you to define a parameter variation for the underlying Optical Setup and then evaluate the results of that variation with a snippet.


Figure 642. The dialog of the Parameter Variation Analyzer.

Fig. 642 shows its dialog. In the upper part there is a button to Configure Parameter Variation. It opens a dialog with the same pages as for the Parameter Run (but welcome page and results table). $\hookrightarrow$ Sec. 44.2 - Sec. 44.4. After configuring the parameter variation, some basic information about it are shown next to the button.
Below there is a group box Evaluate Results to program the evaluation snippet. In this snippet you can change and start the parameter variation (if necessary multiple times), then retrieve the results from this variation and evaluate them.
Edit opens the Source Code Editor ( $\hookrightarrow$ Sec. 7.3) to edit this snippet, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) shows whether this snippet is consistent. Below there is a region where you can set the values of the global parameters of the snippet (if present); $\hookrightarrow$ Sec. 7.4.

## 84 Grating Order Analyzer

Only available in a Grating Setup.

The Grating Order Analyzer ( $\hookrightarrow$ Fig. 643) calculates the coordinates, Rayleigh coefficients, and efficiencies of all diffraction orders of a grating.
The edit dialog of the analyzer contains two tabs, the General tab ( $\hookrightarrow$ Fig. 643), and the Single Orders tab described in Sec. 84.1. The General tab allows you to select which kind of output you want to obtain. The dialog ensures that always at least one output is specified - you cannot uncheck the last checked check box.


Figure 643. The General tab of the Grating Order Analyzer.

| OUTPUT | DESCRIPTION |
| :--- | :--- |
| Order Collections | If checked, an Order Collection is generated, one each for Transmission, Re- <br> flection, and/or the Incident Wave (as reference). An Order Collection docu- <br> ment ( $\lrcorner$ Sec. 18) contains the coordinates, efficiencies, and Rayleigh coeffi- <br> cients of all the respective orders. |
| Single Order Output | If checked, the coordinates, efficiencies, and Rayleigh coefficients of sin- <br> gle orders are output as physical values into the Detector Results Panel <br> ( $\measuredangle$ Sec. 4.3). In this case a new tab page Single Order Output ( $\hookrightarrow$ Sec. 84.1) <br> is shown where you can define what data is shown for which orders. You can |
| select whether you are interested in the orders for Transmission, Reflection, |  |
| and/or the Incident Wave (as reference). |  |

The directions are calculated by means of the grating equation ( $\varsigma \mathrm{Sec} .139 .5$ ) and if necessary converted by the formulas given in Sec. 139.3. The Rayleigh coefficients are calculated by the propagation method set up in the edit dialog of the component ( $\checkmark$ Sec. 64.2). The calculation of the efficiencies is explained in Sec. 139.6.

### 84.1 Single Order Output

Only available if Single Order Output is checked on the General tab.


Figure 644. The Single Orders tab of the Grating Order Analyzer.

The Single Orders tab ( $\hookrightarrow$ Fig. 644) of the Grating Order Analyzer allows you to configure which data about single orders is shown in the Detector Results Panel ( $\hookrightarrow$ Sec. 4.3). It has the following options.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Selection Strategy | With this option you can restrict the shown orders. The following three strategies are available: <br> - AII: No restrictions apply <br> - Above Efficiency Threshold: Only (propagating) orders above the given Efficiency Threshold are shown. <br> - Order Range: All orders in the range between Minimum Order (inclusive) and Maximum Order (inclusive) are shown. This is the recommended mode for the Parametric Optimization ( $\hookrightarrow$ Sec. 102) and the optiSLang Bridge ( $\leftrightarrows$ Sec. 103). |
| Coordinates | This group box allows you to select which coordinates of the individual orders are shown in the Detector Results Panel. If you select Positions you can set a Distance for which the positions are calculated. <br> Note that angles and positions are only shown for propagating orders, not for evanescent ones. |
| Efficiencies / <br> Rayleigh Coefficients | Allows you to select which data of the individual orders is shown. |

The dialog ensures that you select at least one of the Coordinates or one of the Rayleigh Coefficients or the Efficiencies.

## 85 Ellipsometry Analyzer

Only available in a Grating Optical Setup.

This analyzer calculates the Rayleigh coefficient $R=A e^{i \phi}$ of one selected order for both TM and TE polarization (or $p$ and $s$ polarization). From this derived properties such as the resulting polarization ellipse are calculated - in dependency from wavelength and angle.


Figure 645. The dialog for the Ellipsometry Analyzer.

Its edit dialog ( $\hookrightarrow$ Fig. 645) has the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Analyzed Output | This analyzer can be either applied to the Rayleigh coefficients for Reflection or Transmission. |
| Selected Order | Index of the selected order. For 1D-periodic gratings the second index should be zero. |
| Output | Amplitude Component $\Psi$ and Phase Difference $\Delta$ can be used to calculate the resulting polarization ellipse for linearly polarized incident light. They are defined by the equation $\frac{R_{\mathrm{TM}}}{R_{\mathrm{TE}}}=\tan \Psi \cdot \mathrm{e}^{\mathrm{i} \Delta}$ <br> The Müller Matrix $\boldsymbol{\mathcal { M }}$ describes the transformation of the Stokes parameters by the analyzed element. $\mathcal{M}=\left(\begin{array}{cccc} 1 / 2\left(A_{\mathrm{p}}+A_{\mathrm{s}}\right) & 1 / 2\left(A_{\mathrm{p}}-A_{\mathrm{s}}\right) & 0 & 0 \\ 1 / 2\left(A_{\mathrm{p}}-A_{\mathrm{s}}\right) & 1 / 2\left(A_{\mathrm{p}}+A_{\mathrm{s}}\right) & 0 & 0 \\ 0 & 0 & A_{\mathrm{p}} \cdot A_{\mathrm{s}} \cdot \cos \Delta & A_{\mathrm{p}} \cdot A_{\mathrm{s}} \cdot \sin \Delta \\ 0 & 0 & -A_{\mathrm{p}} \cdot A_{\mathrm{s}} \cdot \sin \Delta & A_{\mathrm{p}} \cdot A_{\mathrm{s}} \cdot \cos \Delta \end{array}\right)$ |
| Used Physical Property for Angles | Both $\Psi$ and $\Delta$ are in principle angles. You can determine whether their unit should be degrees or radians. |
| Phase Shift of TM Relative to TE | The given value is added to $\Delta$. This can make the calculated diagrams more comparable with those found in the literature or obtained by measurements. |
| \{Parameter Variation\} | This table allows you to start kind of a parameter run ( $\hookrightarrow$ Sec. 44) over wavelength and spherical angle $\vartheta$. This means that for each combination of the specified wavelengths and angles the desired Output is being calculated and then plotted versus wavelength into a 1D data array. The different angles form distinct subsets. This means that at least 2 wavelengths Steps must be specified, but its possible to specify only one angle. |

## 86 Field Inside Component Analyzer: FMM

Only available in a Grating Optical Setup.

This analyzer calculates the field inside a grating rigorously by means of the Fourier Modal Method ( $\leftrightarrows$ Sec. 96.3). If the grating component ( $\hookrightarrow$ Sec. 64.1) is 1D-periodic, the result is a single Data Array showing the field in the $x$-z-plane at $y=0$. If the grating component is 2D-periodic, the result is a Set of Data Arrays with one Data Array for each z-layer.


Figure 646. Field inside a dielectric sawtooth grating for an incidence angle $\theta=20^{\circ}$. Left: 1 period shown, right: 2 periods shown. Then the sawtooth structure is more clearly recognizable.


Figure 647. The dialog for the Field Inside Component Analyzer: FMM.
Its edit dialog ( $\hookrightarrow$ Fig. 647) has the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | In this group box you can set up which vectorial components ( $E_{x}, E_{y}, E_{z}, H_{x}$, <br> $H_{y}$ and/or $H_{z}$ ) are shown in the resulting data array ( $\varsigma$ Sec. 13.5). The dialog <br> ensures that at least one vectorial component is selected. |
| Forward Propagating / | For detailed analyses you can switch off the influence of either the forward or <br> the backward propagating modes. |
| Number of Periods | Sometimes the structure of the field inside a grating can be recognized more <br> easily if more than one period is shown (See Fig. 646 for an example). Thus <br> you can set the Number of Periods which can be any real number greater <br> than or equal to 1. |
| Usually the base block of a grating component is much larger than the grating <br> stacks. Thus the special effects of the stacks might not be resolved in the <br> result field. To circumvent this problem, you can can restrict the $z$-Range to |  |
| First Stack Only or Second Stack Only. Showing the Whole Component or |  |
| Base Block Only is also possible. For example, Fig. 646 was made with the |  |
| option First Stack Only. |  |

## 87 Polarization Analyzer

Only available in a Grating Optical Setup.

This analyzer can be used for optimizing polarizers and anti-reflection structures. It computes either the summed reflection or transmission efficiency for two orthogonal polarization directions and calculates advanced merit functions like the polarization contrast out of it. To this end, the propagation currently configured in the grating component is used. The summed efficiency is either calculated from all (propagating) orders or from a user-defined order range.
The polarization directions can be given in the following coordinate systems:

COORDINATE SYSTEM
DESCRIPTION
Coordinate System of The Jones vector describes the electric field along $x$ - and $y$-axis of the grating Grating component, respectively.

Coordinate System of The Jones vector describes the electric field along $x$ - and $y$-axis of the light Light Source source, respectively.
p-s Coordinate System In grating theory one often uses the nomenclature parallel and senkrecht (= perpendicular) polarization to describe how the electric field vector is orientated to a reference plane (or short p - and s-polarization). This reference plane is defined by the normal vector of the grating surface and the direction vector of the incident light.
The conversion from the coordinate system of the light source $\left(E_{x} / E_{y}\right)$ is done with the following equations:

$$
\begin{equation*}
E_{\mathbf{s}}=\binom{E_{x}}{E_{y}} \cdot \boldsymbol{n}_{\mathbf{s}} \quad \text { and } \quad E_{\mathrm{p}}=\binom{E_{x}}{E_{y}} \cdot \boldsymbol{n}_{\mathrm{p}} \tag{87.1}
\end{equation*}
$$

$n_{\mathrm{s}}$ and $n_{\mathrm{p}}$ are the normalized directions of s - and p - polarization, respectively (in the coordinate system of the light source). For perpendicular incident $n_{\mathrm{s}}$ is equal to the $y$-axis of the light source.
TE-TM Coordinate System
Instead of p - and s -polarization also the nomenclature transversal magnetic and transversal electric, respectively, is used - or short TM / TE.


Figure 648. The edit dialog for the polarization analyzer.
The edit dialog for this analyzer ( $\hookrightarrow$ Fig. 648) has the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Analyzed Output | This analyzer can be either applied to the efficiencies for Reflection or Transmission. |
| Analyzed Orders | With this option you can restrict the analyzed orders. The following two strategies are available: <br> - All: The summed efficiency of all propagating orders is evaluated. <br> - Order Range: All orders in the range between Minimum Order (inclusive) and Maximum Order (inclusive) are taken into account for the summed efficiency. |
| Polarization Refers to | Allows you to specify the coordinate system the polarization refers to, see table above. |
| Output | The following outputs can be calculated: <br> - Efficiency Ex-Direction $I_{x}$, that is the overall reflection/transmission efficiency for $E_{x}$-polarization. <br> - Efficiency Ey-Direction $I_{y}$, that is the overall reflection/transmission efficiency for $E_{y}$-polarization. <br> - Polarization Contrast $P=I_{x} / I_{y}$ <br> - Average Efficiency $A=\frac{\left(I_{x}+I_{y}\right)}{2}$ |
| Vary Wavelength and/or Orientation | Shows some additional controls allowing you to start kind of a parameter run ( $\leftrightarrows$ Sec. 44) over wavelength and/or the available orientation angles. This means that for each combination of the specified wavelengths or orientation angles the desired Output is being calculated and stored in a data array. Fig. 648 shows a sample configuration of the dialog where the spherical angles $\theta$ and $\phi$ are varied. See also the note below. |
| Advanced Output | If you check Diagram the resulting data array is shown as separate data array view ( $\hookrightarrow$ Sec. 13.5): 1D data array if one parameter is varied, 2D data array if two parameters are varied, 1D data array with data plotted versus iteration number if more than two parameters are varied. <br> For each selected output $\omega$ (i. e. either $I_{x}, I_{y}, A$ and / or $P$ ) you can calculate additional merit functions: the Minimum $\omega_{\min }$, the Maximum $\omega_{\max }$ and the Uniformity Error $U=\frac{\omega_{\max }-\omega_{\text {min }}}{\omega_{\max }+\omega_{\text {min }}}$. With the results shown in Fig. 648 the maximum polarization contrast would be 107.35 (for a wavelength of 500 nm and an incident angle of $4^{\circ}$ ), the minimum polarization contrast would be 10.125 (for a wavelength of 400 nm and an incident angle of $0^{\circ}$ ) and thus the uniformity error of the polarization contrast would be $82.763 \%$. |

The dialog ensures that always at least one output is checked.

## Note on the available angles

If you create a new Polarization Analyzer in your Optical Setup, the available angles in the Polarization Analyzer are set according to the Orientation Definition Type of the grating component in that Optical Setup. But you change it with the Orientation Definition control. See Sec. 139.2 for details about the various orientation definition types.

## Note on using the analyzer with Parameter Extraction

If the wavelength and/or the orientation are varied, it is not possible to vary the same parameter(s) via normal parameter extraction (Parameter Run, Parametric Optimization, Parameter Overview, ...) at the same time.

## 88 Programmable Grating Analyzer

Only available in a Grating Optical Setup.


Figure 649. The dialog for the Programmable Grating Analyzer.
This analyzer can be used to define a user-defined merit function on the rigorous calculated result of the Fourier Modal Method. The analyzer allows the access to the rigorous calculated Rayleigh coefficients as well on the calculated efficiencies. The following settings can be configured

| ITEM | DESCRIPTION |
| :--- | :--- |
| Algorithm | This group box allows you to program a code snippet defining the merit func- <br> tion. Edit opens the Source Code Editor $(\rightarrow$ Sec. 7.3$)$ to edit this snippet, and <br> a validity indicator $(~$ <br> Sec. 5.10$)$ shows whether this snippet is consistent. |
| Parameters ${ }^{\text {国 }}$ | The controls in this group box allow you to set the values of the global param- <br> eters of the snippet. $\leftrightarrows$ Sec. 7.4 |

## 89 Eigenmode Analyzer

## Only available in a Laser Resonator Optical Setup.

The eigenmode analyzer calculates eigenmodes and eigenvalues of resonator systems.

### 89.1 Eigenmode Algorithms

For computing eigenmodes two iterative algorithms from numerical linear algebra are available:

- Fox-Li algorithm, also known as power iteration
- Arnoldi algorithm

Both methods are being discussed in general books on linear algebra. The algorithm of Fox-Li is discussed in [Sie86] also from the physical point of view. General information about these algorithms can be found e.g. on Wikipedia (here for the power iteration and here for the Arnoldi algorithm). Usually one can expect that the Arnoldi algorithm requires much less iterations compared to the Fox-Li algorithm. Further the Arnoldi algorithm provides the option to compute estimates for higher order modes.
The eigenmode computation is based on applying these operators to a system that represents a round trip of the resonator. Such a system is generated internally from the resonator system that is being defined in the Optical Setup by the user. After each round trip the resulting mode is resampled according to the sampling defined by the initial mode and the additional resampling operator ( $\hookrightarrow$ Sec. 89.2).


Figure 650. The dialog for the Eigenmode Analyzer.

In the Algorithm panel ( $\hookrightarrow$ Fig. 650) you can select the algorithm to be used. In both cases, the Number of Iterations ${ }^{\text {国 }}$ must be given as stopping criterion of the iteration. Additionally, the stopping criterion based on the Relative Deviation Threshold ${ }^{[\mathrm{PE}}$ can be activated. Then the iteration stops as soon as one of the criteria is fulfilled. The deviation value (default 1e-6) refers to a relative deviation (rescaled) $d_{R}$ between two successive iterates $f_{i+1}, f_{i}$ :

$$
\begin{equation*}
d_{R}=\frac{\left\|\tilde{f}_{i+1}-f_{i}\right\|}{\left\|f_{i}\right\|} \tag{89.1}
\end{equation*}
$$

where $\tilde{f}_{i+1}:=c \cdot f_{i+1}$ with a complex constant $c$ that is chosen such that the absolute deviation (rescaled) $d_{A}$ is minimal:

$$
\begin{equation*}
d_{A}=\left\|\tilde{f}_{i+1}-f_{i}\right\| \tag{89.2}
\end{equation*}
$$

If the Arnoldi algorithm is selected, also the option Compute Higher Modes is available. The number of higher modes being computed is restricted by the number of iterations. Only those modes with an eigenvalue above 10 per cent of the largest eigenvalue are computed. Note, the numerical accuracy decreases for higher modes.

### 89.2 Initial Mode Parameters and Sampling

The iterative algorithm requires some initial mode. This mode can be defined at the corresponding tab page of the analyzer, see Fig. 651.


Figure 651. The Initial Mode tab of the dialog for the Eigenmode Analyzer.
The initial mode is used as start mode of the iteration. Further this mode defines the wavelength of the resonator and the initial state of polarization. The medium that is associated with the initial mode is used as embedding medium behind the left mirror element of the resonator.
Several types of an initial mode are available: Multiple Light Source ( $\leftrightarrows \mathrm{Sec} .49$ ), Gaussian Wave ( $\leftrightarrows \mathrm{Sec} .51 .1$ ), Plane Wave ( $\varsigma$ Sec. 51.2), Programmable Light Source ( $\leftrightarrows$ Sec. 51.8), Quadratic Wave ( $\leftrightarrows$ Sec. 51.3), Spherical Wave ( $\leftrightarrows$ Sec. 51.4), Stored Lateral Field ( $\leftrightarrows$ Sec. 51.6 ) and Super-Gaussian Wave ( $\hookrightarrow$ Sec. 51.5 ). It can be defined via the Edit button. The wavelength of the mode is available for Parameter Extraction ( $\leftrightarrows$ Sec. 43.5). The initial mode is placed right of the most left element (mirror) of the resonator. This position is called reference plane. We define a reference sampling in this reference plane that is applied after each round trip iteration. The reference sampling is defined from the initial mode together with the resampling operator. This operator ${ }^{\text {国 }}$ can be configured via the Edit button and behaves like the Field Size and Sampling manipulation in the Optical Setup ( $\leftrightarrows$ Sec. 22.8.2).
After starting the iteration the sampling is written into the Messages tab. The sampling should be chosen to match the resulting mode. If it is to small or undersampled no convergence will be achieved. Otherwise the computation effort might be too large.

### 89.3 Outcoupling Mode

At the end of the eigenmode computation the outcoupling mode is being computed. In case of an ideal spherical mirror as right boundary of the resonator, the outcoupling is defined by transmittance settings of the mirror ( $\hookrightarrow$ Fig. 572 ). The medium specified here ( $\hookrightarrow$ Fig. 652) will just be used as embedding medium of the outcoupling mode.
Otherwise the right mirror of the resonator is ignored and replaced by a simple change of media considering preservation of energy in paraxial approximation without Fresnel effects (i. e. $T=1$ ):

$$
\begin{equation*}
\left|\mathbf{E}^{\prime}\right|^{2}=|\mathbf{E}|^{2}\left|\frac{n_{1}}{n_{2}}\right|, \tag{89.3}
\end{equation*}
$$

where $n_{1}$ and $n_{2}$ are the real parts of the refractive indices before and after the media change. For this purpose the external medium is specified on the outcoupling tab ( $\hookrightarrow$ Fig. 652).


Figure 652. The Outcoupling tab of the dialog for the Eigenmode Analyzer.

How to enter the homogeneous medium is described in Sec. 34.1.

### 89.4 Logging

During iteration logging is available. This logging can be configured at the logging tab ( $\hookrightarrow$ Fig. 653).


Figure 653. The Logging tab of the dialog for the Eigenmode Analyzer.

The logging refers to the reference plane. After each round trip the current iterate of the eigenmode, the corresponding beam radius and the deviation of successive iterates ( $\hookrightarrow$ Sec. 89.1) can be computed. Switching off the logging will slightly reduce the computation time.
The Edit View Settings button allows you to set the way how the eigenmodes are shown. To this end the same settings as for the Raw Data Detector ( $\hookrightarrow$ Sec. 74.5.5) can be used.

### 89.5 Iteration Document

Starting the eigenmode analyzer results in an Iteration Document ( $\hookrightarrow$ Fig. 654). This document simply consists of the Results page of the parameter run document ( $\hookrightarrow$ Sec. 44.5).


Figure 654. The Iteration Document of the Eigenmode Analyzer.
The document contains the logging of the iteration. Eigenmode at reference plane, eigenvalues (first and second), deviation, losses $\left((1-\text { eigenvalue })^{2}\right)$ and beam radius at reference plane are included. These values
support convergence control. Additional data can be computed at the end of each iteration step using detectors, see Sec. 43.11.2.
With the $>$ Go! button or the Iteration $\gg$ Go! ribbon item you can start the calculation of the iterations. Then these buttons turn into a Stop button allowing you to stop the calculation.

## 90 Local Linear Grating Approximation Analyzer

## Availability

Optical Setups: Light Shaping Optical Setup ( $\hookrightarrow$ Sec. 43.11.4)
Accessible: In the Optical Setup: Analyzers > Local Linear Grating Analyzer

The diffraction efficiencies of the gratings in a Grating Cells Array ( $\hookrightarrow$ Sec. 40.1.1) can be given by the user. Or they can be calculated rigorously by means of the Fourier Modal Method. However, these rigorous simulations can be quite time consuming and they require VirtualLab Fusion Advanced. Thus they have been separated from the actual simulation by implementing the following workflow.

1. To a Light Shaping Optical Setup with one Diffractive Light Shaper ( $\lrcorner$ Sec. 63) you add a Local Linear Grating Approximation (LLGA) Analyzer.
2. You execute this analyzer which extracts all grating parameters present in the Grating Cells Array of the Light Shaper.
3. You configure the resulting LLGA Results Generator ( $\hookrightarrow$ Sec. 45) and start the rigorous simulations, if necessary on a more powerful PC or workstation or on a computer which is eligible to run VirtualLab Fusion Advanced.
4. You load the results from the LLGA Results Generator into the Order Configuration tab of the Grating Cells Array.

## 91 Grating Channel Analyzer

Only available in a Light Guide Optical Setup.

This analyzer examines the grating regions to determine which orders are propagating in the light guide. For real gratings it also generates a LUT Results Generator ( $\hookrightarrow$ Sec. 46) which then analyzes the efficiencies of these orders rigorously.
It has an edit dialog to predefine whether a custom Fourier Modal Method shall be used for the rigorous analyses, $\hookrightarrow$ Sec. 96.4.

## XIII Propagations: Operators for Propagating Fields

VirtualLab Fusion offers a large variety of free space propagation operators which can only be used for homogeneous, isotropic media ( $\rightarrow$ Sec. 93). Real components ( $\rightarrow$ Part IX) can contain surfaces and both homogeneous and inhomogeneous media. Thus they need special propagations ( - Sec. 96).

## 92 Common Controls

These controls are active for those operators that provide controls for modifying the output field size and sampling in order to simplify their handling. The button Full Automating indicates whether each of the panels described in the following subsections is set to Automatic Sampling. Furthermore, with this button you can reset all panels to Automatic Sampling, i. e. to the default values.

### 92.1 Accuracy Settings

This panel ( $\hookrightarrow$ Fig. 655) is used to adapt the sampling of the input field to minimize numerical errors. There are different ways to determine the sampling parameters:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Sampling | The correct sampling of the input field is ensured by VirtualLab Fusion. You can adjust the automatic sampling with the Accuracy Factor ${ }^{\text {PV }}$. The greater this factor the more sampling points will be in the input field. A factor of 1 (default) means the number of sampling points VirtualLab Fusion uses normally for automatic sampling. If you want to further minimize numerical errors you can set this factor to values greater than 1. In this case the propagation will be more time consuming. Vice versa, if you set the factor to values between 0 and 1 you can speed up propagation, but more numerical errors will be present. |
| Keep Sampling Unchanged | The sampling of the input field is not changed. |
| Calculate from Input Field Sampling | The original sampling of the input is taken as reference, but you can decrease the sampling distance with the Sampling Factor and embed the field with the Embedding Factor. Both factors can be set separately for $x$ - and $y$-direction. A factor of 1 refers to the original parameters of the input field and a factor larger than 1 increases both accuracy and numerical effort. Only available for the thin element approximation (Sec. 96.2) and the split-step propagation ( $\hookrightarrow$ Sec. 96.6), where it replaces the Keep Sampling Unchanged setting. |
| Manual Sampling | In this mode you can adapt either the Sampling Points or the Sampling Distance if you want to find the best compromise between numerical errors and calculation time. The Array Size is just given for your information. If you check this item, Manual Sampling is also selected for the Output Field Sampling and the Size and Shape of Output Field panel (Sec. 92.2 and Sec. 92.3). <br> For some propagation operators you can decrease numerical errors if you embed the field into a zeroized frame. Therefore these operators have additional Embedding Factors for $x$ - and $y$-direction which can be changed only together with the Sampling Distance. An embedding factor of 1 refers to the original size of the input field. <br> The Copy Active Parameters from button allows you to select another harmonic field, from which either the Sampling Points or the Sampling Distance are copied, depending on what item is activated. |

Depending on the propagation operator and whether it is used in the main window or in the Optical Setup, certain items may not be available. Two examples are given in Fig. 655 and Fig. 656. Furthermore, if you select Manual

Sampling in the Optical Setup only the activated entries (Sampling Points or the Sampling Distance) are shown as the other parameters are not calculated until you propagate through the Optical Setup ( $\hookrightarrow$ Fig. 656). If a propagation operator dialog has no accuracy panel, the sampling is kept unchanged.


Figure 655. Accuracy tab for Fresnel propagation in the main window in Manual Sampling Mode.


Figure 656. Accuracy tab for thin element approximation in Manual Sampling Mode.

### 92.2 Output Field Sampling

| Propagation Parameters |  | Accuracy |  |
| :---: | :---: | :---: | :---: |
| Size and Shape of Output Field |  | Output Field Sampling |  |
| $\bigcirc$ Automatic Sampling |  |  |  |
| () Manual Sampling | Copy Active Parameters from... |  |  |
| O Sampling Points | 760 | x | 760 |
| O Sampling Distance | 2.664 mm | x | 2.664 um |
| Array Size | 2.0246 mm | x | 2.0246 mm |
| Embedding |  |  |  |
| Size of Embedding Frame (Sampling Points) |  |  | 10 |
| Total Sampling Points | 780 | x | 780 |
| Total Array Size | 2.0779 mm | x | 2.0779 mm |

Figure 657. Panel for adjusting the output field sampling.

For the two Rayleigh Sommerfeld Operators the sampling of the resulting field can be adjusted via the panel shown in Fig. 657.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Sampling | The correct sampling of the output field is ensured by VirtualLab Fusion. |
| Oversampling Factor ${ }^{[V]}$ | The greater this factor the more sampling points will be in the output field. A factor of 1 (default) means the number of sampling points VirtualLab Fusion uses normally for automatic sampling. Increasing this factor increases the number of sampling points and decreases the sampling distance accordingly. Vice versa, setting this factor to values between 0 and 1 decreases the number of sampling points. <br> This item is only visible if Automatic Sampling is selected. |
| Manual Sampling | In this mode you can adapt either the Sampling Points or the Sampling Distance if you want to find the best compromise between numerical errors and calculation time. The Array Size is just given for information. |
| Copy Active Parameters from | This button allows you to select another harmonic field, from which either the Sampling Points or the Sampling Distance are copied, depending on what items are activated. |
| Sampling Points | Allows you to specify the number of sampling points for both directions. |
| Sampling Distance | Allows you to specify the sampling distance for both directions. |
| Array Size | For your information, the array size (i. e. Sampling Points $\times$ Sampling Distance) is given. |
| Size of Embedding Frame (Sampling Points) | You can add a zeroized frame around the output with the given width in sampling points. |
| Total Sampling Points | This value corresponds to Sampling Points $+2 \times$ Size of Embedding Frame. |
| Total Array Size | This value gives the total array size, i.e. the Array Size plus the size of the embedding frame. |

### 92.3 Size and Shape of Output Field



Figure 658. Panel for setting size and shape of output field.
For the two Rayleigh Sommerfeld Operators as well as the Geometrical Optics Operator, the size and shape of the resulting field is adjustable. The concerning dialog tab is shown in Fig. 658.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Setting | The correct size of the output field is ensured by VirtualLab Fusion. |
| Field Size Factor ${ }^{\text {DV }}$ | The greater this factor the larger the output field will be. A factor of 1 (default) <br> means the field size VirtualLab Fusion uses normally as automatic setting. <br> Increasing this factor increases the field size. Vice versa, setting this factor <br> to values between 0 and 1 decreases field size. <br> This item is only visible if Automatic Setting is selected. |
| Manual Setting | In this mode you can adapt the Shape, the Diameter, and the Edge Width. |
| Shape | You can choose whether a Rectangular or Elliptical virtual aperture is applied <br> to the output field. Standard for automatic sampling is a rectangular virtual <br> aperture. |
| Diameter | Determines the field size for both x- and y-direction. |
| Relative Edge Width | The width of the virtual aperture relative to the field size. |
| Absolute Edge Width | The width of the virtual aperture in physical coordinates. |
| Size of Embedding Frame | You can add a zeroized frame around the output with the given width in sam- <br> (Sampling points) <br> This parameter is only available for the Geometrical Optics Operator. |

## 93 Free Space Operators

VirtualLab Fusion offers a large variety of free space propagation operators which can be used for homogeneous, isotropic media. These operators can be used for the linkages of the Optical Setup ( $\rightarrow$ Sec. 93.1). All operators having an icon in the following table can be used via the Propagations ribbon tab of Harmonic Fields and Harmonic Fields Set as well.

| OPERATOR | DESCRIPTION |
| :---: | :---: |
|  Operator | Automatic selection of light propagation method that is physical sufficiently accurate but also as fast as possible. The propagation method tests the physical accuracy of Spectrum of Plane Waves Operator, Fresnel Operator, Far Field Operator, and Geometrical Optics Operator. $\leftrightarrows$ Sec. 93.2 |
| ${ }_{\mathrm{F}}^{\mathrm{F}}$ ) Far Field Operator | Paraxial and non-paraxial light propagation from beam waist to far field, far field to beam waist and from far field to any other far field plane. $\leftrightarrows$ Sec. 93.3 |
| 8) Geometrical Optics Operator | Light propagation in geometrical optics approximation. Diffraction and interference effects are neglected. $\leftrightarrows$ Sec. 96.1 |
| ${ }_{\text {WP }}$ W) Spectrum of Plane Waves Operator | Rigorous light propagation. $\checkmark$ Sec. 93.4 |
| Rayleigh Sommerfeld Operator <br>  mation) | Rigorous light propagation. $\hookrightarrow$ Sec. 93.5 |
| F) Fresnel Operator | Light propagation in paraxial approximation. $\hookrightarrow$ Sec. 93.6 |
| (\$) Combined SPW/Fresnel Operator | Light propagation in paraxial approximation that combines Spectrum of Plane Waves Operator and Fresnel Operator to improve the calculation speed and reduce the required RAM memory. $\rightarrow$ Sec. 93.7 |
| Rayleigh Expansion Propagation | Only available in a Grating Optical Setup. <br> Rigorous light propagation of propagating and evanescent diffraction orders behind a grating. $\leftrightarrows$ Sec. 93.8 |
| Cells Array Propagation | Only available in a Light Shaping Optical Setup. Light propagation after grating cells arrays. $\rightarrow$ Sec. 93.9 |
| Geometric Rotation Operator | Only available for 2D fields, not for propagating 1D field sections. An operator for rotating fields in geometrical optics approximation. $\rightarrow$ Sec. 93.1.1 |
| Diffractive Rotation Operator | Only available for 2D fields, not for propagating 1D field sections. A rigorous operator for rotating fields. $\hookrightarrow$ Sec. 93.1.2 |

### 93.1 Propagation between Optical Setup Elements <br> Only valid for Classic Field Tracing in a General or Laser Resonator Optical Setup.

Generally, the propagation of a field between Optical Setup Elements is equivalent to propagating the field between two arbitrarily positioned planes. These planes are related to the Optical Setup Elements involved and are called transfaces. This is a special shortcut for "transfer interface" and means the location of the field transfer between two kinds of operators. The output transface $\tau_{1}$ of the start element is the plane where the output of the propagation through this element is given to the homogeneous medium free space operator. The input transface $\tau_{2}$ of the target element is the plane where the output of the free space operator is given to the propagation operator of the second element.
The position and orientation of the output transface - the starting point for the homogeneous medium free space operator - is determined by the propagation through the start element and the type of the reference output coordinate system chosen for this element (but the output coordinate system does not have to be identical to this transface's position and orientation). It is stored after the element's propagation in the coordinate system of
the field itself: the origin of this coordinate system is identical to the position of the transface and the orientation is given by the coordinate system's $x-y$-plane.
The position and orientation of the input transface - the end point for the homogeneous medium free space operator - is determined by the geometry of the target element and, of course, the relative position of the target element to the start element.
There are two general cases to be distinguished for the propagation between Optical Setup Elements, related to two different algorithms used for propagating the field from output transface $\tau_{1}$ to input transface $\tau_{2}$ :

1. The planes $\tau_{1}$ and $\tau_{2}$ are parallel. The algorithm used for this configuration is shown in Fig. 659.
2. The planes $\tau_{1}$ and $\tau_{2}$ are not parallel. The algorithm used for this configuration is shown in Fig. 660. Please note: this case cannot be simulated with 1D fields.


Figure 659. Algorithm for the propagation between Optical Setup Elements where output transface and input transface are parallel. There are two operations at most: the actual free space propagation followed by a lateral shift.


Figure 660. Algorithm for the propagation between Optical Setup Elements where output transface and input transface are not parallel. The operators 1: actual free space propagation and 3: rotation operation can be configured by the user.

In the following, only those two steps of the complete algorithm will be described which can be configured by the user himself:

1. The free space operator used to propagate the free space distance between two parallel planes.
2. The rotation operator which is used if the input transface of the target element is rotated relative to the output transface of the start element. Please note: This operator cannot be used with 1D fields.
More information on coordinate systems can be found in Sec. 43.8.
The configuration dialogs of both of these operators can be accessed via the dialog shown in Fig. 661, having two tab pages.


Figure 661. The dialog to select the propagation method which shall be used for simulating the free space between the start element and the target element of a linkage.

| TAB PAGE | DESCRIPTION |
| :--- | :--- |
| Free Space Operator | On this tab page you can select one of the available free space operators. <br> Depending on the type of the Optical Setup ( $\hookrightarrow$ Sec. 43.11) different operators <br> are available. The Edit button opens the edit dialog of the currently selected <br> operator, explained in the corresponding help chapter (see below). |
| Rotation Operator | On this tab page you can choose between the Geometric Rotation Operator <br> $(\hookrightarrow$ Sec. 93.1 .1$)$ and the Diffractive Rotation Operator ( $\leftrightarrows$ Sec. 93.1.2). The |
|  | Edit button opens the edit dialog of the currently selected operator which is <br> explained in the corresponding help chapter. |

### 93.1.1 Geometrical Rotation Operator

Fig. 662 shows the edit dialog of the Geometric Rotation Operator.


Figure 662. Dialog for setting the approximation parameters for the Geometric Rotation Operator.

The following parameters can be specified on the Approximation Parameters tab page:

| Phase Derivative Approxi- <br> mation Level | The Geometric Rotation Operator works with direction information that is de- <br> rived from the phase of the incident light. The directions are typically evalu- <br> ated by fitting a smooth function into the phase of the incident field. The user <br> can define which type of smooth phase function shall be fitted. Alternatively <br> the local derivative can be used to evaluate the direction data numerically. |
| :--- | :--- |
| Polynomial Degree | In case of polynomial fit this number defines the maximal exponent sum $m+n$ <br> of the basis monomials $x^{m} \cdot y^{n}$ used for the phase fit. The default value is 6. |
| Tube Resolution | The user can specify whether the tubes shall be defined automatically or man- <br> ually. In Automatic mode the user can specify an Accuracy Factor ${ }^{\text {PV }}$ which <br> increases the number of tubes that are used within the geometrical optics op- <br> erator. Alternatively the user can specify the Number of Tubes ${ }^{\text {PV }}$ directly in <br> Manual mode. |

The size and sampling of the target field can be specified on the Target Field Sampling tab page which is shown in Fig. 663.


Figure 663. Dialog for setting the target field size and sampling for the Geometric Rotation Operator.

The user can enter the following parameters:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Sampling in Target Plane | The user can specify whether the sampling distance/number of sampling points of the target field shall be set automatically. In Automatic mode the user can specify an Oversampling Factor ${ }^{[\mathrm{PV}}$ which can be used to increase the resolution of the output field. Alternatively the user can specify the number of Sampling Points ${ }^{[\mathrm{PV}}$ or the Sampling Distance ${ }^{[\mathrm{PV}]}$ directly in Manual mode. |
| Field Size Factor ${ }^{\text {PV }}$ | The Geometric Rotation Operator uses the same algorithm to estimate the field size of the output field as the Diffractive Rotation Operator. By adapting the Field Size Factor this field size can be increased or decreased. |

### 93.1.2 Diffractive Rotation Operator



Figure 664. Dialog for setting the parameters for the Diffractive Rotation Operator.

There are only two parameters which can be set for the Diffractive Rotation Operator in its edit dialog ( $\hookrightarrow$ Fig. 664):
ITEM DESCRIPTION

| Field Size Factor ${ }^{[\mathbb{P V}}$ | Factor by which the field size of the resulting field of the rotation operation will <br> be enlarged in each direction. |
| :--- | :--- |
| Oversampling Factor $^{[\sqrt{V V}}$ | Factor by which the sampling distance of the resulting field of the rotation <br> operation will be reduced in each direction. |

### 93.2 Automatic Propagation Operator

The Automatic Propagation Operator selects the appropriate propagation operator from either SPW Operator ( $\hookrightarrow$ Sec. 93.4), Fresnel Propagation Operator ( $\hookrightarrow$ Sec. 93.6), Far Field Operator ${ }^{1}$ ( $\hookrightarrow$ Sec. 93.3), and Geometrical Optics Operator ( $\hookrightarrow$ Sec. 96.1). The selection is based on finding a compromise between numerical accuracy and numerical effort required for computing the propagated field. The selection algorithm is shown in Fig. 665.


Figure 665. Flowchart for the selection algorithm applied by the automatic propagation operator.

Both the deviation of the propagation operator and its numerical effort are estimated by one-dimensional calculations and a comparison with a SPW reference result in 1D. The primary criterion for selecting the operator

[^13]is that the deviation must not exceed a certain fraction of the total energy of the field. This is the Deviation Threshold specified in the Accuracy tab. From the admissible set of operators (deviation below limit), the operator with the lowest numerical effort is selected. Further, the numerical effort is assumed to be some limit (number of sampling points). The effort limit is taken from the value Maximum Number of Sampling Points per Field defined in the Global Options, $\hookrightarrow$ Sec. 6.14. Furthermore, the parameter Power Portion for Field Size Estimation ( $\hookrightarrow$ Sec. 6.12) is used to estimate the field size of the propagated field. A more detailed description is given in [WK11].
The different implementations of this operator for the main window and the Optical Setup ( $\hookrightarrow$ Sec. 43) are discussed in the following subsections.

### 93.2.1 Implementation in the Main Window

If the automatic propagation is used in the main window you can do an analysis prior to the actual propagation by clicking on the Analyze button. The resulting window as shown in Fig. 666 displays the estimated values for deviation and numerical effort and the estimated sampling of the propagated field. In the case of a Harmonic Fields Set, the analysis can be done per member field by selecting the index of the member and Analyze it. The operator used for the actual propagation can depend on the selected member.


Figure 666. Results of the analysis if the automatic propagation is used in the main window.

The tab for editing the general Propagation Parameters is shown in Fig. 667.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Propagation Distance | The propagation distance. |
| SPW Operator | If checked, the SPW Operator can be selected. |
| Fresnel <br> erator | Propagation Op- If checked, the Fresnel Propagation Operator can be selected. <br> Far Field Operator If checked, the Far Field Operator can be selected. <br> Geometrical Optics Oper- <br> ator If checked, the Geometrical Optics Operator can be selected. <br> Analyze Press this button to perform the analysis, compute estimates for deviation <br> and numerical effort. Displays the results and the selected operator. <br> Ok Starts the actual propagation. |



Figure 667. Dialog for editing the settings of the Automatic Propagation Operator.

Via the Accuracy tab you can set the following:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Accuracy Factor | The accuracy factor for the individual operators. It also influences the esti- <br> mate of the size of the propagated field. |
| Deviation Threshold | The fraction of the total energy of the field which "suitable" propagation tech- <br> niques must not exceed. |
| Power Portion for Field | The Power Portion for Field Size Estimation specifies how much of the energy <br> of the incoming field is present in the output field. This value must be below <br> Size Estimation |
| $100 \% . A$ higher value means both increased accuracy and computational <br> effort. |  |
| Analysis for one member | If checked, you can select which member field determines the used propaga- <br> tion operator. If unchecked, the propagation operator is determined indepen- <br> dently for each member field. |



Figure 668. Panel for accuracy settings.

### 93.2.2 Implementation in the Optical Setup

If the automatic propagation is used within the Optical Setup ( $\hookrightarrow$ Sec. 43), no separate analysis can be done. However, corresponding information can be found in the logging window ( $\hookrightarrow$ Sec. 43.6.8) after the simulation is finished.
The tab for editing the general Propagation Parameters has the following parameters.

| ITEM | DESCRIPTION |
| :--- | :--- |
| SPW Operator | If checked, the SPW Operator can be selected. |
| Fresnel Propagation Op- <br> erator | If checked, the Fresnel Propagation Operator can be selected. |
| Far Field Operator | If checked, the Far Field Operator can be selected. |
| Geometrical Optics Oper- <br> ator | If checked, the Geometrical Optics Operator can be selected. |

Via the Accuracy tab you can set the following:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Accuracy Factor ${ }^{\text {PV }}$ | The accuracy factor for the individual operators. It also influences the estimate of the size of the propagated field. This setting might also be set for the whole Optical Setup via the Property Browser ( $\leftrightarrows$ Sec. 43.4.7.1). |
| Deviation Threshold ${ }^{\text {PV] }}$ | The fraction of the total energy of the field which "suitable" propagation techniques must not exceed. This setting might also be set for the whole Optical Setup via the Property Browser ( $\hookrightarrow$ Sec. 43.4.7.1). |
| Power Portion for Field Size Estimation ${ }^{[\mathrm{PV}]}$ | The Power Portion for Field Size Estimation specifies how much of the energy of the incoming field is present in the output field. This value must be below 100 \%. A higher value means both increased accuracy and computational effort. |
| Analysis for one member only | If checked, you can select which member field determines the used propagation operator. If unchecked, the propagation operator is determined independently for each member field. |

The setting Analysis for one member only available in the main window can be set only for the whole Optical Setup via the Property Browser ( $\hookrightarrow$ Sec. 43.4.7.1).

### 93.3 Far Field Operator



Figure 669. Dialog of the Far Field Operator.
The Far Field Operator has the dialog shown in Fig. 669. Its Propagation Parameters tab allows the user to enter the propagation distance and the propagation mode. Three different propagation modes are supported: propagation from Waist to Far Field, Far Field to Waist, and Far Field to Far Field. Additionally it is possible to select between the general Far Field Operator (Non-Paraxial) and a Paraxial (Fraunhofer) approximation. The Accuracy tab is explained in Sec. 92.1.

If used in the Optical Setup, the Propagation Distance cannot be set as it is determined from the positions of the Optical Setup Elements. Thus, the corresponding controls are not visible.

The implemented formulas are given in Sec. 136.1.2.

### 93.4 Spectrum of Plane Waves Operator



Figure 670. Dialog of the propagation with spectrum of plane waves (SPW), Fresnel transform or a combination of both.

If this operator is used for a linkage ( $\hookrightarrow$ Sec. 93.1) its edit dialog has only the Accuracy tab explained in Sec. 92.1. If used in the main window, there is an additional Propagation Parameters tab with the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Propagation Distance | The propagation distance. Can be positive and negative. |

The implemented formulas are given in Sec. 136.1.3.

### 93.5 Rayleigh Sommerfeld Operator



Figure 671. Dialog of the propagation with Rayleigh Sommerfeld Convolution operator showing the Propagation Parameters tab. The dialog for the Rayleigh Sommerfeld Summation operator is equivalent.

For this propagation operator two distinct numerical implementations are available ( $\hookrightarrow$ Sec. 136.1.4), namely Rayleigh Sommerfeld Convolution and Rayleigh Sommerfeld Summation. The corresponding dialog ( $\hookrightarrow$ Fig. 670) has three tab pages which are explained in $\hookrightarrow$ Sec. 92 .
If used in the main window, there is an additional Propagation Parameters tab with the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Propagation Distance | The propagation distance. Can be positive and negative. |

### 93.6 Fresnel Propagation Operator

If the Fresnel Propagation Operator is used for a linkage ( $\hookrightarrow$ Sec. 93.1) its edit dialog ( $\hookrightarrow$ Fig. 670) has only the Accuracy tab explained in Sec. 92.1. If used in the main window, there is an additional Propagation Parameters tab with the following controls:

> ITEM

DESCRIPTION
Propagation Distance $\quad$ The propagation distance. Can be positive and negative.

The implemented formulas are given in Sec. 136.1.5.

### 93.7 Combined SPW / Fresnel Operator

This propagation operator automatically combines the spectrum of plane waves propagation ( $\hookrightarrow$ Sec. 93.4) and the Fresnel propagation ( $\hookrightarrow$ Sec. 93.6) to achieve an efficient propagation of paraxial waves free of numerical
errors. For propagation of harmonic fields close to the waist of a wave, spectrum of plane waves is used. For larger distances the Fresnel propagation is used. Sec. 136.1.6 explains in more detail when which propagation is used.
If this operator is used for a linkage ( $\leftrightarrows$ Sec. 93.1) its edit dialog ( $\leftrightarrows$ Fig. 670) has only an Accuracy tab where you can set the accuracy factor ( $\varsigma \mathrm{Sec} .92 .1$ ). If used in the main window, there is an additional Propagation Parameters tab with the following controls:
ITEM DESCRIPTION

Propagation Distance $\quad$ The propagation distance. Can be positive and negative.

### 93.8 Rayleigh Expansion Propagation

Only available in a Grating Optical Setup.


Figure 672. The Dialog for the Rayleigh Expansion Propagation.
This free space operator can take advantage of the Rayleigh coefficients calculated by rigorous methods. It has the following options:
ITEM DESCRIPTION

| Always Return Two- <br> Dimensional Fields  | If the grating component is set to 1D-periodic mode ( $\leftrightarrows$ Sec. 64.1) or if for one direction only one order is calculated by the FMM ( $\leftrightarrows \mathrm{Sec} .96 .3 .1$.1), the resulting fields will be one-dimensional. However, the two-dimensional field view can be more intuitive. Thus you can enforce two-dimensional fields by checking this option. |
| :---: | :---: |
| Number of Periods ${ }^{\text {『VV }}$ | Sometimes it can be more intuitive if more than one period is shown, which can be set with this option. For 2D-periodic gratings this setting affects both $x$ - and $y$-direction of the resulting field. |
| Output Field Oversampling Factor ${ }^{\text {PV }}$ | The number of sampling points per period is the number of calculated diffraction orders times the Output Field Oversampling Factor. |
| Apply Evanescent Field Filter | Evanescent waves vanish after a very short propagation distance. By checking this option you can enforce that they vanish even for a propagation distance of zero. |

The implemented algorithm is documented in Sec. 136.1.7.

### 93.9 Cells Array Propagation

Only available in a Light Shaping Optical Setup.

This free space operator is available after the Light Shaper component. The Grating Cells Array performs a mode decomposition, where all modes have the same intensity distribution but are located in different positions and have different propagation directions. The free space operator uses these analytic information of the light field object in the input plane and calculate the positions of the modes in the output plane. Additionally the intensity distribution of all modes is propagated by wave optical propagation techniques into the target plane. This propagation operator can be selected by the user. The user can use the Far Field Operator ( $\hookrightarrow$ Sec. 93.3) or the Automatic Propagation Operator ( $\hookrightarrow$ Sec. 93.2). By default the Far Field Operator is used. The output of the free space operator is a new light field object which contains the propagated mode and the analytic stored positions and directions for all modes. This light distribution can be used for further investigations within the Camera Detector ( $\leftrightarrows$ Sec. 74.5.2).


Figure 673. The Dialog for the Cells Array Propagation

Fig. 673 shows the edit dialog of the Cells Array Propagation. Its has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Propagation Operator | Here you can choose between Far Field Operator or Automatic Propagation <br> Operator as wave optical propagation. |
| Edit | Edits the currently selected propagation operator. |
| Accuracy Factor | Influences the spot size in the target plane of the propagated wave. An ac- <br> curacy factor of 1 means that $95 \%$ of the power of the propagated spots will <br> be used for further investigation. Increasing the Accuracy Factor by 1 means <br> that $0.5 \%$ will be added to this power portion. So an Accuracy Factor of 11 <br> means that $100 \%$ of the propagated field will be used. |

## 94 2D / 3D Propagation

For Harmonic Fields, Harmonic Fields Sets, and Ray Distributions in the main window there is the ribbon button Propagations > 2D Propagation / Propagations > 3D Propagation (depending on the dimensionality of the field). This button opens a dialog to create a Parameter Run in which the field is propagated by different distances. From this Parameter Run you then can generate instructive diagrams or animations showing how the field evolves, see Fig. 674 for an example.


Figure 674. Interference of two Gaussian beams. This is the result of a one-dimensional Harmonic Field propagated to different distances with the 2D Propagation feature. The results where then combined into a two-dimensional data array.

Said dialog ( $\hookrightarrow$ Fig. 675) has the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Propagation Method | OnLY FOR HARMONIC FIELDS AND HARMONIC FIELDS SETS <br> You can select and Edit any of the operators listed in Sec. 93 <br> able for both one- and two-dimensional harmonic fields. |
| Start Point | The minimum propagation distance. |
| End Point | The maximum propagation distance. |
| Number of Propagation | The number of propagation steps between the start point and the end point <br> (including). |
| Steps | OnLY FOR HARMONIC FIELDS AND HARMONIC FIELDS SETS |
| Remove Constant Phase |  |
| Factor exp(ikz) | During the propagation typically a constant phase factor exp $(i k \Delta z)$ depending <br> on the propagation distance will occur. Its fast oscillation along the optical axis <br> makes it difficult to notice the change of the phase, the real and imaginary part <br> of the harmonic field during the propagation. Enable this option to remove the <br> constant phase factor (recommended for real and imaginary part and phase <br> display). |



Figure 675. The dialog for defining a 3D Propagation for a Harmonic Field or Harmonic Fields Set.

When this dialog is closed with OK, a Parameter Run ( $\hookrightarrow$ Sec. 44) with the appropriate settings is created
and started automatically. After the Parameter Run completes you can create a nice-looking combined output ( $\hookrightarrow$ Sec. 44.5.1).

## 95 Propagation through Idealized Systems

The Propagations tab for Harmonic Fields and Harmonic Fields Sets also offers the possibility to propagate through simple, idealized setups. 1 f -Setup and 2 f -Setup are described in Sec.31.1.1. ABCD Matrix Simulation is described in the following section.

### 95.1 ABCD Matrix Simulation

## Availability

Toolboxes: All
Accessible: Harmonic Field and Harmonic Fields Set: Propagations $\left.>_{c \mathrm{D}}^{\mathrm{AB}}\right) \mathrm{ABCD}$ Matrix Simulation

This function is a generalization of the 1 f -Setup/2f-Setup ( $\leftrightarrows$ Sec. 31.1.1): You can define an arbitrary system as ABCD matrix through which the current Harmonic Field or Harmonic Fields Set is propagated in an idealized way. VirtualLab Fusion also offers the ABCD Law Calculator ( $\hookrightarrow$ Sec. 104) which has similar functionality for Gaussian waves. Furthermore, in an Optical Setup you can use the ABCD Matrix Setup component ( $\hookrightarrow$ Sec. 73.1).


Figure 676. Dialog for defining the parameters of an $A B C D$ matrix propagation.
Fig. 676 shows the edit dialog for an $A B C D$ matrix simulation. It has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Simulation Type | You can choose between three methods (Collins Integral, Spectrum of Plane <br> Waves, and Rayleigh-Sommerfeld Convolution). See Sec. 134.1 for an ex- <br> planation of these methods. |
| Allow Scaling of Field Pa- <br> rameters during Propaga- <br> tion | If checked, the field will be resampled to avoid numerical problems. This <br> option is only available if the matrix element B is not zero. |
| Propagate Inverse by Us- <br> ing Inverted Matrix | Using the inverse ABCD matrix corresponds to an inverse propagation. Thus <br> this checkbox allows you to invert the ABCD matrix being used for the simu- <br> lation. |
| Resulting ABCD Matrix | Shows the automatically calculated ABCD Matrix of the combination of the <br> optical elements. |
| ABCD Matrix Control | Allows you to define the system ABCD matrix by composing it of an arbitrary <br> number of optical elements. $\hookrightarrow$ Sec. 5.16 |

## 96 Propagation Operators for Real Components

For real components in the Optical Setup ( $\hookrightarrow$ Sec. 43), the following propagation operators are available:

| COMPONENT PROPAGATION | ANNOTATIONS |
| :---: | :---: |
| Collins Integral by ABCD Matrix <br> (For Spherical Lens \& Lens System) | This operator uses the ABCD matrix of the component and thus can handle only certain surface types and homogeneous media. All propagation settings are synchronized. $\hookrightarrow$ Sec. 96.5 |
| Customized Propagation <br> (For Double Surface Component, Fiber Element, GRIN Component \& Inhomogeneous Medium Component.) | Uses Thin Element Approximation ( $\hookrightarrow$ Sec. 96.2) propagations for surfaces; several paraxial free space propagations for homogeneous media ( $\hookrightarrow$ Sec. 93) and either the Thin Element Approximation or the Split Step (BPM) propagation ( $\hookrightarrow$ Sec. 96.6) for inhomogeneous media. The settings are synchronized separately for each building block type. |
| Fourier Modal Method (For General Grating) | All propagation settings are synchronized. $\hookrightarrow$ Sec. 96.3 |
| Geometrical Optics (For Light Shaper) | - |
| Geometrical Optics Operator <br> (For Curved Surface, Spherical Lens \& Lens System) | This operator can handle smooth surfaces and homogeneous media. All propagation settings are synchronized. $\hookrightarrow$ Sec. 96.1 |

### 96.1 Geometrical Optics Operator

The Geometrical Optics Propagation Operator is available both for free space propagation through homogeneous media and for propagation through real components. It is based on the principles of geometrical optics. The propagation is performed along rays. In our case, the direction of rays is defined by so called Channels. Rays within one channel have different position but the same direction. The operator first builds up the channels. In a second step, rays are propagated. In the first step, the directions of the channels have to be computed in the initial plane from the field data. In particular the phase of the field is used. The actual phase of the field
is replaced by a fitted phase using different levels of approximation: Constant phase, Linear phase, linear and Spherical phase, linear, spherical and Cylindrical phase. From this phase approximation the directions of the channels are computed. Alternatively the Local Gradient of the phase can be used to define the channel directions. Further, the channels are defined throughout the system by stepping from surface to surface. Depending on the settings of the operator, this procedures takes Refraction into account or not. Once the channels are defined, the rays carrying the field information are propagated through the system. The path of the rays is defined by the channels. Depending on the settings of the operator Fresnel Effects and Cross Talk is taken into account or not.
A detailed description of the operator is given in an external paper. An explanation of the Size and Shape of Output Field tab is given in Sec. 92.3.
The Propagation Parameters tab ( $\hookrightarrow$ Fig. 677) has the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| A: Constant | Take $(0,0,1)$ as direction of rays in the input plane. |
| B: Linear | Perform a fit of a linear phase for defining the directions of rays in the input <br> plane. |
| C: B + Spherical | Perform a fit of a linear and spherical phase for defining the directions of rays <br> in the input plane. |
| D: C + Cylindrical | Perform a fit of a linear, spherical and cylindrical phase for defining the direc- <br> tions of rays in the input plane. |
| E: Polynomial | Perform a general polynomial fit of the phase for defining the directions of rays <br> in the input plane. The maximal exponent sum $m+n$ of the basis monomials <br> $x^{m} \cdot y^{n}$ can be set on the Accuracy tab |
| F: Local Gradient | Take the local gradient for defining the directions of rays in the input plane. |
| I: Optical Path Length | Consider the optical path length only during tracing rays through the system. <br> Consider the optical path length and Fresnel effects during tracing rays <br> through the system. |
| III: I + Refraction | Consider the optical path length and refraction during tracing rays through the <br> system. <br> IV: III + Fresnel |
| V: IV + Cross Talk: | Cons through the system. |
| rays ther the optical path length, refraction, Fresnel effects and cross-talk |  |
| between $E_{x}$ and $E_{y}$ during tracing rays through the system. |  |


| Geometrical Optics Operator |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Propagation Parameters | Accuracy | Size and Shap | of Output field |  |  |
| Propagation Model |  |  |  |  |  |
| Phase 1 Effects | $\begin{aligned} & \text { 1: Optical } \\ & \text { Path Length } \end{aligned}$ | II:It <br> fressel |  | $\begin{gathered} \mathrm{N}: I I I+ \\ \text { Fressel } \end{gathered}$ | $\begin{aligned} & V_{\text {Vive }} \\ & \text { Crostalk } \end{aligned}$ |
| A. Constant | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| B: Linear | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| C: B+ Spherical | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 |
| D: C + Cylindical | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| E: Polynomial | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| F: Local Gradient | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |

Figure 677. Dialog for editing the Geometrical Optics Operator showing the tab with propagation parameters.

The Accuracy tab ( $\hookrightarrow$ Fig. 678) has the following parameters:

ITEM

| Number of Channels | Number of channels being used. |
| :---: | :---: |
| Accuracy Factor ${ }^{\text {PV }}$ | In the automatic mode, the accuracy factor (I) scales the number of channels being used. |
| Number of Rays to Be Traced | Sets the number of rays that are to be traced. These numbers correspond to the number of sampling points of the output field. |
| Accuracy Factor ${ }^{\text {PV }}$ | In the automatic mode, the accuracy factor (II) scales the number of rays being traced. |
| Polynomial Degree | In case that option E: Polynomial is being selected, this number defines the maximal exponent sum $m+n$ of the basis monomials $x^{m} \cdot y^{n}$ used for the phase fit. |



Figure 678. Tab for editing the accuracy settings.

### 96.1.1 Advanced Settings

If for a Curved Surface, Lens System, or Spherical Lens you have selected Geometrical Optics Operator as Component Propagation, the Advanced Settings sub-tab of the Propagation tab allows you to choose whether you want to Minimize Use of Geometric Optics or not ( $\hookrightarrow$ Fig. 679). This is important for concave surfaces only, as there is no difference between these options in the case of non-concave ones.


Figure 679. Advanced Settings tab for the geometrical optics operator.

| ITEM | DESCRIPTION |
| :--- | :--- |
| No (faster) | Wave-optical propagation techniques are used till the aperture plane is <br> reached, then geometrical optics is applied. This is the faster option, but <br> at the expense of less accuracy. |
| Yes (slower) | The use of wave-optical propagation techniques is maximized, but at the ex- <br> pense of a slower calculation. |

### 96.2 Thin Element Approximation

| Edit Thin Element Approximation |  |  | $\times$ |
| :---: | :---: | :---: | :---: |
| Propagation Parameters Accuracy |  |  |  |
| Incident Field \} Effects | I: Optical Path Length | II: I+ Fresnel |  |
| A: Paraxial | $\bigcirc$ | ( |  |
| B: Parabasal | $\bigcirc$ | $\bigcirc$ |  |

Figure 680. Propagation Parameters tab for the thin element approximation operator.
The thin element approximation can be used for propagating through surfaces, homogeneous and inhomogeneous (index modulated) media. It is assumed that paraxial/parabasal conditions hold. The paraxial mode is documented by [Goo68]. Using the paraxial mode, the method is identical to the mode Al/All of the geometrical optics operator, see Sec. 96.1. The implemented algorithm is documented in Sec. 136.2.1.
The edit dialog ( $\hookrightarrow$ Fig. 680) has two tabs: The Propagation Parameters tab explained below and the Accuracy tab explained in Sec. 92.1.
The Propagation Parameters tab consists of a table with the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| A: Paraxial | Take $(0,0,1)$ as direction of rays in the input plane. |
| B: Parabasal | Perform a fit of a linear phase for defining the directions of rays in the input <br> plane. This option will be available in a future version of VirtualLab Fusion. |
| I: Optical Path Length | Consider the optical path length only during tracing rays through the system. |
| II: I + Fresnel | Consider the optical path length and Fresnel effects during tracing rays <br> through the system. This option is not available if the parabasal operator <br> is used for inhomogeneous or homogeneous media. |

### 96.3 Fourier Modal Method / Rigorous Coupled-Wave Analysis

Only available in the Grating Package.

The Fourier Modal Method (FMM) or Rigorous Coupled-Wave Analysis (RCWA) is a rigorous propagation technique. This method demands the periodicity of all physical values that are involved in the associated setup, i. e. the analyzed structure and the input field and consequently also the output field have to be periodical ${ }^{1}$ ( $\hookrightarrow$ Fig. 681). For more details about the FMM see [Kno78; Li96; Tur97; Li01].

[^14]

Figure 681. Physical setup which is expected for analyses using the Fourier Modal Method.
The FMM requires a structure built up by a sequence of discrete arbitrary cells which are characterized by their complex refractive index ( $\hookrightarrow$ Fig. 681). The sizes of these cells define so called transition points in lateral direction which create a sequence of layers in longitudinal direction on their part ${ }^{1}$. To analyze non-discrete structures configure the FMM to use a sufficient large number of layers and transition points.

## Order Limit of the FMM

A maximum of 23170 grating orders can be analyzed by the FMM. For 1D-periodic gratings this corresponds in best case to a period of roughly $12000 \times$ wavelength. But for 2D-periodic gratings this limit translates to e.g. $152 \times 152$ orders or at most $(75 \times \text { wavelength })^{2}$. However, RAM consumption and computational effort increase very rapidly with the number of orders, so that the practical limit is much lower.

### 96.3.1 Editing the Fourier Modal Method

There are in principle two things you can edit for the FMM: the number of diffraction orders ( $\hookrightarrow$ Sec. 96.3.1.1) and how the grating to analyze is decomposed into blocks of constant refractive indices ( $\hookrightarrow$ Sec. 96.3.1.2). In the edit dialog of the FMM they can be edited on different tab pages.

### 96.3.1.1 Setting the Number of Diffraction Orders

One numerical parameter for the FMM is the overall number of diffraction orders considered during calculation. A higher number means increased accuracy but higher numerical effort. Fig. 682 show the controls to edit this as well as the additional information label.

[^15]

Figure 682. The Numerical Parameters tab of the FMM where you can adjust the number of calculated orders in case of a 2D-periodic grating.

You can either specify the Number of Diffraction Orders ${ }^{[\mathrm{PV}}$ or the Number of Evanescent Orders ${ }^{[\mathrm{PV}}$. In the first case you can specify the number of diffraction orders directly. In the latter case, the overall number of diffraction orders calculated by the Fourier Modal Method is the number of evanescent orders plus the number of propagating orders. The dialog ensures that always an odd number (greater or equal 3 ) of diffraction orders is calculated.
The information gives the following information:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of calculated <br> diffraction orders | The number of orders calculated by the FMM. |
| Number of propagating <br> orders | This number is calculated for reflection and transmission from the grating <br> equation $(\hookrightarrow$ Sec. 139.5) for perpendicular incident. As this information de- <br> pends on the wavelength, you can set the preview wavelength which is then <br> also used for the decomposition preview ( $\hookrightarrow$ Sec. 96.3.1.3, Sec. 96.3.1.4). |

For a 2D periodic grating you can specify the numbers of orders separately for the x - and the y -direction.

### 96.3.1.2 Decomposition into Layers and Transition Points

The transition points are always generated for the range -Period/2 $\ldots+$ Period $/ 2$, but are stored internally with positive positions. Thus, the x-coordinates in the decomposition preview are shifted by half a period in comparison to all other previews and results.


Figure 683. The Structure Decomposition tab of the FMM in case of a 2D-periodic grating component with two stacks.
With the controls shown in Fig. 683, you can adjust the decomposition of a real structure into Layers and Transition Points on the Advanced Settings sub-tab.
This tab page comprises three parts. In the upper part you can adjust the layer decomposition with the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic | The layer decomposition is done automatically. |
| Accuracy Factor ${ }^{\text {EV }}$ | A greater value means that the decomposition lasts longer and that more lay- <br> ers are generated, which increases the calculation time of the Fourier Modal <br> Method. (Doubling the number of layers means roughly double the calcula- <br> tion time.) |
| Manual | An equidistant layer decomposition is used. |
| Number of Layers $\sqrt{\text { EV }}$ | The specified number of layers is distributed equidistantly over the modulated <br> region. If stacks are placed on both surfaces of the grating component, the <br> number of layers is used per stack. |
| Overall Thickness | The overall thickness of the modulated region, which is is the sum of the <br> extensions of the two stacks. |

In the middle part of the tab page you can adjust the transition point decomposition with the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic | The transition point decomposition is done automatically as described in a <br> technical note. The size of the smallest detectable features is given in the <br> info label. |
| Accuracy Factor ${ }^{\text {PV }}$ | A greater value means that smaller features are detectable but also that the <br> decomposition lasts longer. |
| Manual | The transition points are distributed equidistantly. Each layer has the same <br> number of transition points. |
| Number of Points | The specified number of transition points is distributed equidistantly over one <br> Period of the structure. |
| Point Distance ${ }^{\text {臤 }}$ | Instead of the Number of Points the user can also specify the distance be- <br> tween transition points. Then, the number of points is calculated from this <br> value and the Period. |
| Period | The period of the modulated region. |

The lower part contains an information label and the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Remove Redundant Data | Especially if you have set the decomposition to Manual redundant data may <br> occur (i. e. transitions between identical refractive indices or layers with the <br> same refractive index distribution). If you check this item, such redundant <br> data is removed after the decomposition. |
| Decomposition Preview | Opens a preview of the resulting decomposition. The preview for 1D-periodic <br> gratings is explained in Sec. 96.3.1.3 and the preview for 2D-periodic gratings <br> in Sec. 96.3.1.4. |

The information label gives the following information:
ITEM DESCRIPTION
(Maximum) Total number The total number of layers including one layer for the base block. In case Re of layers move Redundant Data is checked this gives the maximum number of layers - which is only reached if there are no redundant layers.

Minimum transition point The size of the smallest detectable feature. If no such small features are distance present in the structure, Automatic decomposition yields only larger distances between consecutive transition points.

Transition point distances of less than 0.1 nm can only be resolved in Manual mode without Remove Redundant Data.

### 96.3.1.3 Decomposition Preview for 1D-Periodic Gratings



Figure 684. The Transition Point Preview showing a combination of a volume grating with a triangular grating.

The decomposition preview ( $\hookrightarrow$ Fig. 684) has a diagram tab and a table tab showing the layers and transition points used for the Fourier Modal Method. Furthermore, the overall dimensions of the grating component are given.
The positions in the table tab are "up-to-positions". In the example given in Fig. 685, the refractive index 1.4611 is in the range from $1.3989 \mu \mathrm{~m}$ to $1.6011 \mu \mathrm{~m}$. The Reference Wavelength used for the calculation of the refractive indices can be set on the bottom of the dialog.


Figure 685. Example showing a part of the table tab of the decomposition preview for 1D-periodic gratings

In the diagram tab, the data is shown in a data array view ( $\hookrightarrow$ Sec. 13.5). In particular, the view has the same context menu which allows you to change the shown field quantity ( $\hookrightarrow$ Sec. 11.1) to e. g. imaginary part, change the aspect ratio ( $\hookrightarrow$ Sec. 11.5) or the color table ( $\hookrightarrow$ Sec. 11.2.4).
Furthermore you can zoom via mouse wheel or via the context menu, exactly as for data arrays ( $\hookrightarrow$ Sec. 11.4). However, this zooming always scales both dimensions of the data array. Thus a better suited Zoom tool is available for this preview: If you click on the Zoom button, a separate dialog is shown where you can specify exactly the rectangular region to be shown in the diagram. If you click Show Whole Component on said dialog, you can reset the view to show the complete data. If the grating component contains only one stack, then this stack is shown by default. Otherwise the whole component is shown. The table always shows the complete data.
The 乌-button shows the currently set up diagram as separate data array view ( $\hookrightarrow$ Sec. 13.5).

### 96.3.1.4 Decomposition Preview for 2D-Periodic Gratings



Figure 686. The decomposition preview for 2D-periodic gratings.

The decomposition preview for 2D-periodic gratings shows the refractive index distribution of one period in the currently selected layer, either as Diagram or as Table. In the lower section of the dialog you can set up the Reference Wavelength used for the calculation of the refractive indices as well as the Layer Index. As further information the position and thickness of this layer are given.

|  |  | X |  |  |
| :--- | :---: | ---: | ---: | ---: |
|  |  | 0 m | 323.4 nm | 676.6 nm |
| $\searrow$ | 0 m | 1.0003 | 1.4611 | 1.0003 |

Figure 687. Example showing a part of the table tab of the decomposition preview for 2D-periodic gratings.

Non-equidistant data arrays are used for the preview ( $\lrcorner$ Sec. 13). In particular, the view has the same context menu which allows you to change the shown field quantity ( $\hookrightarrow$ Sec. 11.1) to e. g. imaginary part, zoom into the view ( $\hookrightarrow$ Sec. 11.4), change its aspect ratio ( $\hookrightarrow$ Sec. 11.5) or the color table ( $\hookrightarrow$ Sec. 11.2.4).
Via the context menu of the table you can copy the current selection to the Windows ${ }^{\text {TM }}$ clipboard. Via the Q-button you can generate a separate data array document of the current view.
The constant interval interpolation is used ( $\lrcorner$ Sec. 13.2.1) and thus the positions in the table are "from-positions". In the example given in Fig. 687, the block with the refractive index of 1.4611 covers the x-range from 323.4 nm to 676.6 nm .

### 96.4 Custom Fourier Modal Method

Only available in the AR/VR/XR Package.

You can analyze the efficiencies of the grating regions rigorously with the Fourier Modal Method (FMM) implemented in VirtualLab Fusion ( $\hookrightarrow$ Sec. 96.3). However, if you want you can also use your own FMM available in a separate dynamic link library (DLL) programmed with the . Net framework of Microsoft.
This DLL must contain at least a namespace of arbitrary name with a class of arbitrary name in which a static
method with arbitrary name is included. But this method must have parameters of the following types in the given order:

| TYPE | DESCRIPTION |
| :--- | :--- |
| OpticalStack | The stack with correctly set medium in front of the stack (MediumBefore) and <br> medium behind the stack (MediumAfter). |
| double | The vacuum wavelength with which the stack is illuminated. |
| Vector3D | The incident wave vector. |
| VectorC | $E_{x}$ - and $E_{y}$-component of the input plane wave. |

The return value of this method must be of type RigorousSimulationResultsForPlaneWaveInput, a type containing both efficiencies and Rayleigh coefficients for both transmitted and reflected light.
Most of the data types mentioned above are defined in the VirtualLabAPI.dII.


Figure 688. The control to define a custom FMM.

There is a control ( $\hookrightarrow$ Fig. 688) to define the location of the custom FMM. It has the following settings:
ITEM
DESCRIPTION

| Use Customized <br> Modal Method | If this option is not checked, the VirtualLab FMM is used to calculate rigorous <br> results of gratings. |
| :--- | :--- |
| Select DLL | ONLY IF USE CUSTOMIZED FOURIER MODAL METHOD IS CHECKED. <br> The user can select the DLL which provides the customized FMM. |
| Name of Class | ONLY IF USE CUSTOMIZED FOURIER MODAL METHOD IS CHECKED. <br> It is necessary to define the class which contains the FMM function to apply <br> for FMM. The name of the class has to be unique within the selected DLL. |
| Name of Fourier Modal  <br> Method ONLY IF USE CUSTOMIZED FOURIER MODAL METHOD IS CHECKED. <br> In addition the user needs to specify the function name which contains the  <br> FMM calculation. This method must have the input and output parameters as  |  |
|  | described above. |

## Tip

You might want to define for example accuracy factors for your FMM. This can be done on the Additional Parameters tab of the stacks in the Light Guide component ( $\leftrightarrows$ Sec. 57.2). The parameters defined there are then also available for Parameter Extraction, thus e.g. for Parameter Run and Parametric Optimization.

### 96.5 Collins Integral by ABCD Matrix

If the optical surfaces of a component or rather their optical effects can be described by the ABCD matrix formalism, one can decide to use the propagation algorithm given by Collins [Col70]. For a Lens System or a Spherical Lens this method can be selected as Component Propagation on the Propagation Methods sub-tab ( $\hookrightarrow$ Sec. 54.1).

In this case the Propagation Methods sub-tab has one additional control:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Info | This will write some information to the Messages tab of the main window: The |
|  | ABCD matrix for transmission as well as the complex transmission coefficient |
|  | (for the whole component). All these values are determined for the default <br> wavelength $(\hookrightarrow$ Sec. 6.1 .1$)$ and assume air in front of the component. |

The Collins integral cannot be used for reflection as always a propagation distance is required which is not present for reflection on the first surface.
The controls in the edit dialog ( $\hookrightarrow$ Sec. 92.1) allow you to adjust the accuracy of the calculation.

### 96.6 Split Step (BPM) Propagation

This propagation operator is only available as part of the Customized Propagation for inhomogeNEOUS MEDIA.

This propagation operator is applicable for inhomogeneous media with small refractive index modulation $\delta n \ll$ $n$. Furthermore, paraxial conditions are assumed to hold and the influence of reflected waves is assumed to be negligible. The operator is based on the classical ideas of paraxial beam propagation methods, see e. g. [YL92] and [TY82]. The implemented algorithm is documented in Sec. 136.2.2.


Figure 689. Propagation Parameters tab for the split step (BPM) propagation.

The Propagation Parameters tab of its edit dialog ( $\hookrightarrow$ Fig. 689) allows you to either set the Number of Steps ${ }^{[\mathrm{PV}]}$ (n) used for the propagation or the Maximum Step $\operatorname{Size}{ }^{\mathbb{P V}}(\Delta z)$. The automatic selection of the step size will be added in a future version of VirtualLab Fusion. In the bottom part of the dialog the user can select the integration method which shall be used to include the refractive index modulation during the split step propagation. The user can select between Use Trapezoid Integration and Use Numerical Integration. The trapezoid integration is faster because only three points will be used to calculate the refractive index integral. We recommend the usage of the trapezoid integration for very slow index modulations and especially for z-invariant media. The Accuracy tab can be used to define the numerical parameters of the split step propagation. Fig. 690 shows the user control which can be used to control the split step propagation numerically.


Figure 690. Accuracy tab for the split step (BPM) propagation.

The following parameters can be entered by the user:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Automatic Field Size | For automatic field size determination the incident field size and the media specification is taken into account. For several media field size estimation rules are implemented. If the Automatic Field Size mode is selected the user can enter a Field Size Factor ${ }^{[\mathrm{PV}}$ which influences the field size estimation directly. |
| Keep Field Size | The keep field size mode can be used if the incident field size shall be kept. In that case the user can enter the Embedding Factor ${ }^{[\mathbb{P V}}$ which will be multiplied on the field size of the incident field. |
| Manual Field Size | For manually defining the field size used for propagation the Manual Field Size mode can be selected. The user has to specify the Field Size ${ }^{\mathbb{D V}}$ for xand y-direction. |
| Automatic Sampling | The automatic sampling mode can be used to adapt the sampling of the incident field automatically to the size of the features in the inhomogeneous medium. If this mode is selected the user can enter an Oversampling Factor ${ }^{\sqrt{P V}}$ which influences the sampling adaption of the incident field. |
| Keep Sampling | If the user selects the keep sampling mode the sampling of the incident field is kept for the simulation through the index modulated media. The user can enter a Sampling Factor ${ }^{\text {DV }}$ which is applied on on the incident field. |
| Manual Sampling | The manual sampling mode allows the specification of the Sampling Distance ${ }^{\mathrm{PV}}$ or the Number of Sampling Points ${ }^{\mathbb{P V}}$ manually. |

## XIV <br> Design \& Optimization

VirtualLab Fusion offers four algorithms to design the optimal optical elements for your needs:

- IFTA Optimization: You can design transmissions acting for example as paraxial beam splitters and beam shapers. $\leftrightarrows$ Sec. 97
- Cells Array Design: A special design approach where the desired functionality is achieved by many small optical elements (gratings, prisms, or mirrors). $\leftrightarrows$ Sec. 100
- Light Guide Design: Special design algorithm for light guides used in AR \& VR devices. $\leftrightarrows$ Sec. 101.2
- Parametric Optimization: Intended for the optimization of selected parameters of an Optical Setup ( $\leftrightarrows$ Sec. 43). The merit function used therefor can be freely configured. $\leftrightarrows$ Sec. 102


## 97 IFTA Optimization

## Availability

Toolboxes: Diffractive Optics Package
Accessible: Ribbon: File $>$ New $>$ IFTA Optimization or Start $>$ New $>$ 造 IFTA Optimization

The IFTA optimization document supports two transmission design methods (the actual Iterative Fourier Transform Algorithm Approach or IFTA [AWS97] and Geometrical Optics Beam Shaping) as well as basic analysis features. The designed transmissions can be exported to a real structure or to fabrication data using the structure design ( $\hookrightarrow$ Sec. 98).
The corresponding document window is divided into three panels which are described in the following.

### 97.1 Specification Panel

The specification panel contains data for specifying the transmission design problem. The consistency of these values can be checked via IFTA Optimization > Check Consistency.
All the data contained in the specification panel is stored when saving a transmission design document.
The controls of the specification panel ( $\hookrightarrow$ Fig. 691) are ordered in several groups, which are described in the following subsections.


Figure 691. Specification panel of the standard transmission design.

### 97.1.1 Input Field

The input field can be chosen either to be constant or it can be set to any single globally polarized harmonic field.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | Wavelength of input field. |
| Constant Input Field | For selecting a constant input field with the given wavelength. This corre- <br> sponds to the illumination of the transmission by an untilted plane wave. |
| Arbitrary Input Field | Selected when the input field was set to a given harmonic field (see below). <br> Set |
| After pressing this button, the user is asked for selecting a globally polarized <br> harmonic field, a copy of which is included into the design problem document <br> as input field. |  |
| Show | Show a copy of the current input field. |

The input field can be adapted to the sampling of the transmission ( $\hookrightarrow$ Sec. 97.1.2) via IFTA Optimization $>$ Embed / Extract Input Field. This function is especially useful after changing the embed frame width in the specification panel ( $\hookrightarrow$ Sec. 97.1).

### 97.1.2 Transmission

The Transmission group box enables you to choose sampling parameters and the type of the transmission function to be optimized.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Points | Number of sampling points in $x$ - and $y$-direction. |
| Sampling Distance | Sampling distance in $x$-and $y$-direction. |
| Type of Transmission | The available types of transmission functions are documented below. |
| Number of Quantization <br> Levels | Contains the number of quantization values for quantized transmission types. |

The following transmission types are supported:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Continuous Phase-Only | The transmission $\mathcal{T}(x)$ is a continuous phase-only function, i. e. at each position $x$ the condition $\|\mathcal{T}(x)\|=1$ is fulfilled. |
| Quantized Phase-Only | The transmission $\mathcal{T}(x)$ is an equidistantly quantized phase-only function, i. e. at each position $x$ the condition $\mathcal{T}(x) \in \widetilde{\mathcal{M}}_{\text {phase, } Q}$ is fulfilled, where $\widetilde{\mathcal{M}}_{\text {phase, } Q}$ is given in Eq. (97.1). |
| Continuous AmplitudeOnly | The transmission $\mathcal{T}(x)$ is a normalized amplitude-only function, i. e. at each position $x$ the conditions $\|\mathcal{T}(x)\|<1$ and $\arg [\mathcal{T}(x)]=0$ are fulfilled. |
| Quantized Amplitude- Only | The transmission $\mathcal{T}(x)$ is an equidistantly quantized amplitude-only function, i. e. at each position $x$ the condition $\mathcal{T}(x) \in \widetilde{\mathcal{M}}_{\mathrm{ampl}, \mathrm{Q}}$ is fulfilled, where $\widetilde{\mathcal{M}}_{\mathrm{ampl}, \mathrm{Q}}$ is given in Eq. (97.2). |
| Complex | The transmission $t(x)$ is a normalized complex-valued function, i.e. at each position $x$ the condition $\|t(x)\|<1$ is fulfilled. |

Possible quantization values for quantization to $Q$ equidistant phase-only values:

$$
\begin{equation*}
\widetilde{\mathcal{M}}_{\text {phase }, Q}=\{\exp (i 2 \pi j / Q): j \in \mathbb{Z}\} \tag{97.1}
\end{equation*}
$$

Possible quantization values for quantization to $Q$ equidistant amplitude-only values:

$$
\begin{equation*}
\widetilde{\mathcal{M}}_{\mathrm{ampl}, Q}=\{j /(Q-1): j \in[0, Q-1]\} . \tag{97.2}
\end{equation*}
$$

### 97.1.3 Propagation

The settings within this group box determine the propagation operator which is to be used between transmission and signal plane.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Type of Propagation | The supported propagation operators are explained below. |
| Propagation $\quad$ Distance <br> Focal Length | Propagation distance between transmission and output plane or focal dis- <br> tance of considered $2 f$-setup. |
| Embed Frame Width | If this value is greater than 0 , the transmission field is embedded into a frame <br> of zero-samples of the given width before applying the propagation operator. <br> If in x-direction $N_{x}$ sampling values are specified for the transmission func- <br> tion ( $\hookrightarrow$ Sec. 97.1 .2$)$ and an embed frame width $N_{\text {embed }}$ is specified, then the <br> transmission is embedded to a size of $\left(N_{x}+2 N_{\text {embed }}\right)$. |
| Pixelation Factor | For the propagation operators which do not correspond to Fourier transforms, <br> it can be necessary to simulate pixelation effects ( $\hookrightarrow$ Sec. 138.1.2) by replacing <br> each sampling point by $N_{\text {pix }} \times N_{\text {pix }}$ sampling points, where $N_{\text {pix }}$ is the given |
| pixelation factor. Pixelation is applied after embedding. |  |

The following propagation operators are supported:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Far Field (Angular Spec- <br> trum) | Corresponds to performing a spatial Fourier transform ( $\hookrightarrow$ Sec. 31.1). The <br> output plane coordinates are given in angular spectrum domain. |
| $\mathbf{1 f - / 2 f - S e t u p ~}$ | Corresponds to performing a spatial Fourier transform ( $\hookrightarrow$ Sec. 31.1). The <br> output plane coordinate system is related to the back focal plane of a 2f-setup <br> $(\hookrightarrow$ Sec. 31.1.1). This setting applies also for 1f-setups. |
| Fresnel Transform | Corresponds to the Fresnel transform propagation ( $\hookrightarrow$ Sec. 93.6) with output <br> coordinate scaling as given in Output Field Sampling ( $\hookrightarrow$ Sec. 97.1 .4$).$ |
| Spectrum of Plane Waves | Corresponds to the spectrum of plane waves propagation operator as ex- <br> plained in Sec. 93.4. The output plane sampling distance is equal to the <br> transmission plane sampling distance divided by the given pixelation factor. |

### 97.1.4 Output Plane Sampling

In this group box the output plane sampling parameters are given, which follow from the transmission plane sampling ( $\hookrightarrow$ Sec. 97.1.2) and the propagation operator settings ( $\hookrightarrow$ Sec. 97.1.3).
If the propagation operator Far Field (Angular Spectrum) is selected, by checking Use Angular Coordinates it can be determined whether the output plane sampling is to be given in degrees instead of the internally used wave number coordinates ( $1 / \mathrm{m}$ ). The calculation of the output plane parameters in degrees is done in paraxial approximation assuming a linear dependency between the angles in degrees and the angles in wave number coordinates. For non-paraxial designs the display in degrees should not be used.

### 97.1.5 Output Field Requirements

The constraints on the resulting output field as given in this group box determine the signal plane projection operator to be used for the IFTA design method.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Desired Output Field | Set or show the desired output field. For setting a new Desired Output Field, all currently open globally polarized harmonic fields can be selected in a separate dialog. This dialog also allows you to create the Optimization Region from the selection ( $\hookrightarrow$ Sec. 11.3.4) in the selected field. In case of using a harmonic field, it has to have the sampling parameters as specified in the Output Plane Sampling box. If the number of sampling points do not match, you cannot start the optimization. If the sampling distances do not match, they are set to the values shown in the Output Plane Sampling box. The wavelength and other physical parameters of the specified field are ignored. |
| Optimization Region | To Set a new Optimization Region, any currently opened region document ( $\varsigma$ Sec. 21) can be selected. The IFTA optimizes only this region of the output field to match the Desired Output Field. <br> Note that if you set an analytic region, it is sampled internally: Only those sampling points of the desired output field are optimized whose center point lies within the analytic region. $\hookrightarrow$ Fig. 692 |
| Sample Optimization Region from Desired Output Field | If checked, a sampled Optimization Region is created from all positions where the current Desired Output Field is not exactly equal to zero. |
| Allow Phase Freedom | Determines whether the phase of the Desired Output Field is significant or whether it can be set freely by the IFTA. |
| Allow Scale Freedom | If this control is checked, during each iteration the current result field is scaled by a factor $\alpha$ to match the desired output field. As a result usually the stray light decreases at the cost of also decreased conversion efficiency. Otherwise $\alpha$ is always 1 . |
| Limit Scale Factor According to Goal Efficiency | When this option is checked, a lower bound for the amplitude of the scale factor $\alpha$ is imposed, which corresponds to the given goal efficiency. This option can be helpful for increasing the achieved conversion efficiency. |
| Limit Stray Light | When this option is checked, the IFTA restricts the amplitude of the output field for positions outside of the Optimization Region to a certain upper threshold, which corresponds to the given Maximum Relative Intensity of Stray Light ( $\hookrightarrow$ Sec. 137.2). |
| Limit Feature Size | Enables imposing a limitation to the minimum feature size in the transmission using the method of [AW98]. From the given Minimum Feature Size a corresponding maximum spatial frequency in the output field is calculated. The stray light in the region with spatial frequencies higher than this maximum frequency must not exceed the Maximum Stray Light Intensity for Higher Frequencies (which is calculated analogly to the Maximum Relative Intensity of Stray Light). |



Figure 692. Effect if an elliptic optimization region (red) is applied on a sampled desired output field (gray). Only the dark gray sampling points constitute the actual optimization region because their center is within the ellipse.

### 97.2 Design Panel

The design panel is for selecting and controlling the transmission design algorithm.
When saving a transmission design document, all parameters of the used design algorithms as set in the design panel are stored. In contrast, any logging data is not saved.
The controls within the upper row of the design panel ( $\hookrightarrow$ Fig. 693) are described in the following table. The lower part of the design panel depends on the selected design algorithm (see following subsections).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Design Method | Combo box for selecting the transmission design method to be used. The <br> available design methods are documented in the following subsections. |
| Set | After clicking this button, the user is asked to select a transmission function, <br> which will be considered as the current solution of the transmission design <br> problem. This function can be used for selecting a transmission to be ana- <br> lyzed within the Analysis panel ( $\hookrightarrow$ Sec. 97.3$),$ or to be set as an initial solution <br> for the chosen optimization algorithm. |
| Show | Shows a copy of the current solution for the transmission function to be opti- <br> mized. |



Figure 693. Design panel of the standard transmission design with iterative Fourier transform algorithm approach selected as design method.

### 97.2.1 Iterative Fourier Transform Algorithm Approach

IFTA iteration has to begin with some initial transmission $\mathcal{T}_{0}$ that is created in the so-called initialization step, which has to be chosen according to the considered design problem. For beam splitting designs, $\mathcal{T}_{0}$ is typically obtained from backward propagation of the desired output field with ideal spot intensities and randomly chosen phases. For beam shaper designs other strategies for choosing $\mathcal{T}_{0}$ are used. ([AWS97]) VirtualLab Fusion supports the following methods for creating the initial transmission function $\mathcal{T}_{0}$ :

| ITEM | DESCRIPTION |
| :--- | :--- |
| Constant 1 | Constant initial transmission function $\mathcal{T}_{0} \equiv 1$. |
| Random Phase | The initial transmission $\mathcal{T}_{0}$ is chosen to have a random phase distribution <br> and the amplitude $\left\|\mathcal{T}_{0}(x)\right\| \equiv 1$. |
| Backward Propagated De-  <br> sired Output Field The initial transmission is obtained from propagating the Desired Output <br>  Field backward to the transmission plane. In this operation the phase of <br> the desired output field is not neglected, even if phase freedom is selected <br> $(\hookrightarrow$ Sec. 97.1.5). <br> Backward Propagated De- <br> sired Output Field (Ran- The initial transmission is obtained from propagating the current desired out- <br> pom field with a superimposed random phase backward to the transmission <br> domase) plane. |  |

When using the IFTA, best results are typically obtained by introducing the transmission and signal constraints step by step. In the phase synthesis step, iterations are performed without amplitude freedom. In the subsequent SNR optimization step, amplitude freedom is switched on to optimize the signal-to-noise ratio. If
quantization is necessary, one or two further iteration steps are required, which are described in the following subsection.
The rows in the table appearing in the upper part of the design panel ( $\hookrightarrow$ Fig. 693) correspond to the design steps explained above. The design steps can be switched on and off by the corresponding check boxes. For the iterative design steps the corresponding number of iterations can be specified in the second column of that table.
The controls within the Logging group box are documented in Sec. 97.2.1.1. The following table contains all remaining controls of the design panel as shown in Fig. 693:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Soft Introduction of Trans- <br> mission Constraint | Determines whether the transmission constraint is to be introduced softly by <br> using relaxed projections with projection strength $\lambda$ linearly increasing from 0 <br> to 1. This option may be useful for avoiding the creation of speckles during <br> the design of beam shapers. |
| Omit Final Transmission  <br> Projection Omitting the final transmission plane projection can be helpful for examining <br> the impact of the signal plane projection.  |  |
| Create Transmission Ani- | Creates an animation for showing the evolution of the transmission function <br> mation |
| during the design iterations. Several options are available by the Options |  |
| button ( $\hookrightarrow$ Sec. 97.2 .1 .2$).$ |  |

### 97.2.1.1 Logging

Within the logging table, the most important merit functions and some further parameters can be observed during iteration.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Enable Logging | By unchecking this option you can turn off the logging completely. This can <br> increase performance, especially in the case of many fast iterations. If this <br> option is checked, at least the total number of iteration steps is logged. <br> When logging is enabled and a design is running, a Suspend Logging button <br> is shown which allows to suspend logging for the currently running design. If <br> this button is pressed again, logging continues normally. |
| Configure | Configure which merit functions and parameters are to be logged (see below). <br> Less merit functions to log result in increased performance. |
| Show Diagram | Transfer selected columns of the table to a newly created one-dimensional <br> data array with one subset per merit function ( $\hookrightarrow$ Sec. 13.5). |
| Preserve Table | If checked, the contents of the table is not cleared when starting (or continu- <br> ing) the design by pressing Start Design. |

The following merit functions and parameters are supported for logging:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Iteration Index in Current <br> Design Step | Iteration counter for current design step. |
| Window Efficiency | The part of the paraxial power of the input field diffracted inside the signal <br> region. |
| Conversion Efficiency | The part of the paraxial power of the input field diffracted in the part of the <br> signal that is inside the signal region. Noises inside the signal region are <br> ignored. |
| Signal-to-Noise Ratio | The strength of the signal relative to the noises measured in dB. |
| Uniformity Error | The maximum deviation of the output field squared amplitude from the signal <br> field squared amplitude inside the signal region. |
| Relative ZerothOrder In- <br> tensity The squared amplitude of the zeroth order of the output field related to some- <br> what like the mean value of the intensities of the desired output orders. <br> Maximum Relative <br> sity of Stray Light The relative maximum intensity outside of the signal region. <br> Projection Strength <br> Projection strength parameter $\lambda$ which may vary due to a softly introduced <br> transmission constraint or during the quantization steps. <br> Magnitude <br> Scale Factor Optimal | Amplitude $\|\alpha\|$ of the optimal scale factor $\alpha$. |
| Argument of | Optimal |
| Scale Factor |  |$\quad$| Phase arg $\alpha \alpha]$ of the optimal scale factor $\alpha$. |  |
| :--- | :--- |
| Zeroth Order Efficiency | The part of the paraxial power of the input field diffracted into the zeroth order. |

The formulas behind the merit functions are given in Sec. 137.2.

### 97.2.1.2 Options for Creating Animations

Animations correspond to a sequence of individual bitmap images ( $\hookrightarrow \mathrm{Sec} .20$ ). The controls of the dialog shown in Fig. 694 determine how these individual bitmap images are created from the given transmissions or output fields.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Apply Interpolation | Determines whether the complex amplitude is to be interpolated before it is <br> converted to a bitmap image. The interpolation settings available via the Op- <br> tions button are described in Sec. 22.8.1. |
| Use Twin Image Repre-  <br> sentation If checked, each bitmap image is composed of two images side by side, which <br> are created from the same transmission or output field using different color <br> mapping settings (see below). <br> Edited Image Options With this item, available if the check box Use Twin Image Representation <br> is enabled, the part of the image (left or right) can be chosen for which the <br> options shall be edited. <br> Color Mapping The controls within this group are described in Sec. 5.11. |  |



Figure 694. Settings for generation of animations.

### 97.2.2 Geometrical Optics Beam Shaping

This design approach can be used only for designing continuous phase-only transmission functions using phase and scale freedom. Therefore, some of the settings in the specification panel need to have appropriate values. The energy mapping between transmission plane and signal plane can be calculated analytically (i.e. in one non-iterative step) only for one-dimensional problems. In case of two-dimensional design problems one of the following separability types has to be selected:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Cartesian Coordinates | Input field, desired output field, and the resulting transmission obey Carte- <br> sian separability. For the transmission function $\mathcal{T}(x, y)$ this means that <br>  <br>  <br>  <br> two one-dimensional functions $\mathcal{T}_{x}(x)$ and $\mathcal{T}_{y}(y)$ exist, so that $\mathcal{T}(x, y)=$ <br>  <br> $\mathcal{T}_{x}(x) \mathcal{T}_{y}(y)$. |
| Rotational Symmetry | Input field, desired output field, and the resulting transmission are rotation- <br>  <br> ally symmetric. For the transmission function $\mathcal{T}(x, y)$ this means, that a <br> one-dimensional function $\mathcal{T}_{r}(r)$ exists, so that $\mathcal{T}(x, y)=\mathcal{T}_{r}(r)$, where <br> $r=\sqrt{x^{2}+y^{2}}$. |

### 97.3 Analysis Panel



Figure 695. Analysis panel of the standard transmission design.
The analysis panel ( $\rightarrow$ Fig. 695) is used for analyzing the current solution of the transmission design problem. It supports the following features:

- Calculation of common merit functions ( $\leftrightarrows$ Sec. 74.6.2),
- Performing tolerancing analyses with respect to linear and binary mask scaling errors ( $\varsigma$ Sec. 97.3.2),
- Obtaining the optical setup which is represented by the current solution of the transmission design problem.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Show Output Field | Shows output field when recalculating values of merit functions. The output <br> field is calculated under consideration of the scale error values currently set <br> $(\hookrightarrow$ Sec. 97.3.1). |
| Recalculate | Recalculates merit functions ( $\hookrightarrow$ Sec. 74.6 .2$)$ which are checked in the table <br> on the left hand side. The merit function values are calculated under consid- <br> eration of the scale error values $(\hookrightarrow$ Sec. 97.3 .1$)$ currently set. |
| Show Optical Setup | Shows an Optical Setup $(\hookrightarrow$ Sec. 43$)$ which corresponds to the current solution <br> of the transmission design problem. |

Note that the shown output field is more or less just a Fourier Transform of the current transmission. It does not include Fresnel effects, non-paraxial distortion effects, diffraction effects; and depending on the Type of Propagation set on the Specification tab also not the pixelation effect. To see these effects you should use the optical setup created by Show Optical Setup or even convert the transmission into a real structure ( $\hookrightarrow$ Sec. 98).

### 97.3.1 Scale Errors for Phase-only Transmissions

By using the thin element approximation [WB91], phase-only transmission functions can be transformed to a corresponding height profile. Within this approximation several error types are equivalent and can be described by the linear scale error $\gamma$ :

- There are several possible reasons for linear scaling errors of the realized height profile, which can be described by the parameter $\gamma$. Examples are wrong etching times, wrong etching rates, or thermal expansion or shrinking effects when using hot embossing.
- Deviations between the actual wavelength $\lambda_{\text {act }}$ and the wavelength $\lambda_{\text {ref }}$ which was assumed during the design cause a linear scale error $\gamma=\lambda_{\text {ref }} / \lambda_{\text {act }}$.
- Deviations between the actual refractive index $n_{\text {act }}$ of the structured material and the refractive $n_{\text {ref }}$ which was assumed during the design cause a linear scale error $\gamma=n_{\text {act }} / n_{\text {ref }}$.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Impose Linear Scale Error <br> by Scale Factor | If checked, the given linear scale error is imposed. A value of 1 corresponds to <br> the ideal case of no scale error. This feature can be used only if the designed <br> transmission is phase-only. |
| Impose Binary Mask Scale | If checked, the given binary mask scale errors are imposed. This feature <br> Errors |
|  | lean be used only if the designed transmission is phase-only quantized to $2^{q}$ <br>  <br> for the up to four most important binary masks steps, corresponding to phase <br> modulations of $\pi, \pi / 2, \pi / 4$, and $\pi / 8$, can be given. Values of 1 correspond |
|  | to the ideal case of no scale errors. |

### 97.3.2 Scan Scale Error Range

By using the controls within this group box, basic tolerancing analysis can be performed by modifying the value of a selected scale error within a given range, while all other scale errors keep their value as specified by the controls within the group box Scale Errors for Phase-Only Transmissions ( $\hookrightarrow$ Sec. 97.3.1).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Modify Scale Error | Selection of scale error to be modified. All scale errors that can be entered <br> in the group box Scale Errors for Phase-Only Transmissions ( $\hookrightarrow$ Sec. 97.3.1) <br> are available for selection. |
| From | First scale error value to be considered. |
| To | Last scale error value to be considered. |
| Number of Steps | Number of values to be considered in the given value range. |
| Create Output Field Ani- | Creates an animation for showing the behavior of the output field during the <br> changing of the selected scale factor. Several options are available via the <br> Options button ( $\hookrightarrow$ Sec. 97.2 .1 .2$).$ |
| Recalculate | Recalculates the table containing the results of the tolerancing analysis. This <br> table contains rows for each considered scale error value and columns for <br> each merit function which is selected in the top left table of the analysis panel. <br> After this button has been pressed, it turns into a Stop button to cancel the <br> tolerancing analysis immediately. While an analysis is in progress, in the title <br> of the document window the progress in percent and an estimation of the <br> remaining calculation time is displayed. |
| Show Diagram | Shows a one-dimensional data array ( $\leftrightarrows$ Sec. 13.5) where each subset shows <br> the dependency of one of the selected merit functions from the modified scale <br> error. |

### 97.4 Multiple Runs of the IFTA Optimization Document



Figure 696. The dialog to start multiple runs of the IFTA optimization document.

Via the ribbon item IFTA Optimization > Multiple Runs you can run the currently open IFTA optimization
document multiple times which is useful if the IFTA design starts with a random phase. After completion of each run the resulting merit functions are being calculated and logged to a file in comma separated value (CSV) format. Furthermore, the resulting transmissions are saved into the same folder as the CSV file.
In the upper part of the corresponding dialog ( $\hookrightarrow$ Fig. 33.1) you can configure which Merit Functions are logged to the CSV file. For each merit function you can set up three different kinds of conditions:

- Between: The merit function must be between the given Minimum and Maximum value.
- Less Than: The merit function must be less than the given Maximum value.
- Greater Than: The merit function must be greater than the given Minimum value.

The Saving group box allows the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Result File Name | The file name used for the resulting transmission and the summary CSV file. <br> For the transmissions, to this file name the run number is appended. For the <br> summary file, Summary is appended as well as the date and time in brackets. <br> Keep in mind that characters like '*' and '?' are not allowed in file names. |
| Save Result to | The path where the results are stored. It can be changed with the $\quad . .-$-button. <br> If you want the results to be shown in the Windows Explorer you can click on <br> the path label. |
| Save and Log | You can choose whether All Results or Only Results Fulfilling All Conditions <br> are saved as transmission files and logged into the CSV file. <br> If all results are saved, the CSV file has an extra Conditions column indicating <br> whether the design passed all conditions or whether at least one condition |
| failed. Furthermore, passed and failed, respectively, is appended to the file |  |
| names of the transmissions. |  |

In the bottom of the dialog you can specify the Number of Runs.
If you click on the Start button it turns into a Stop button and no further settings are allowed. Clicking on Close simply closes the dialog and stops the simulations.

### 97.5 Preparing the Desired Output Field

The following ribbon items allow you to set a specific Desired Output Field.
ITEM DESCRIPTION
IFTA Optimization > 囲i $\hookrightarrow$ Sec. 97.5.1
Regular Beam Splitter Pat-
tern
IFTA Optimization $>\int_{\mathrm{g}}$ Allows you to select a harmonic field via a dialog. Then the sinc modulation
Sinc Compensation due to pixelation is compensated ( $\hookrightarrow$ Sec. 138.1.2) and the resulting field is inserted as Desired Output Field. If you want to see a copy of the resulting field, simply check Show Resulting Field.

### 97.5.1 Preparation of the Desired Output Field for Regular Patterns

By this dialog the desired output field can be set up for design of regular beam splitters, that is

- All signal orders have equal intensity,
- The signal orders are equidistant, and
- The signal orders are centered around the optical axis.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of Signal Orders | Number of signal orders in $x$ - and y-direction. This number must not be larger <br> than the number of sampling points within one period of the transmission <br> function as set in the specification panel ( $\hookrightarrow$ Sec. 97.1$).$ |
| Even Orders Missing | This can be applied if the desired output orders have got even splitting ratios. <br> By checking this option a symmetric signal order configuration is achieved, <br> where only odd output orders are used for signal orders. If this option is not |
| checked, all signal orders are consecutive. |  |
| If the desired output field has an odd number of orders in one direction and |  |
| an even number in the other direction, this symmetrization is only done for |  |
| the "even" direction ( $\hookrightarrow$ Fig. 697). |  |



Figure 697. Desired output field with $5 \times 6$ orders and Even Orders Missing. As you can see, it is symmetric to the point $(0 ; 0)$ marked with a cross.

## 98 Structure Design

A Jones matrix transmission - e. g. calculated by the standard transmission design of VirtualLab Fusion - has the additional ribbon item Design > 人哃Structure Design. It opens the structure design dialog which allows you to calculate a pixelated surface profile from this transmission using the thin element approximation [Goo68]. This means the surface profile height is proportional to the phase values of the transmission.
Smooth or micro-structured surfaces with or without discrete height steps can be created. The calculated surface profile is returned as a Sampled Surface ( $\leftrightarrows$ Sec. 35.2.11). This Sampled Surface is then placed in a Microstructure Component ( $\hookrightarrow$ Sec. 60.1) which is either added to an existing or a new Optical Setup. If the transmission is periodical, then the resulting Sampled Surface is periodized accordingly.
The edit dialog of the structure design consists of three tab pages. Each tab page contains a selection of parameters for the structure design. The following tab pages are available:

1. Target
2. Optical Setup
3. Surface Parameters

The subsequent sections describe the setting entries on each tab page.

### 98.1 Target

On the first page of the structure design dialog, the user can specify the target of the structure design. Fig. 698 shows the first page of the structure design dialog. The following targets can be selected:

| ITEM | DESCRIPTION |
| :--- | :--- |
| New Optical Setup | The output of the Structure Design can also be a New Optical Setup. You <br> can adapt the generated Optical Setup to make further simulations. (e.g. <br> tolerancing). |
| Add to Existing Optical <br> Setup | You can also add the generated Real Components to an existing Optical <br> Setup. |



Figure 698. Target page of the structure design edit dialog

### 98.2 Optical Setup

The resulting structure can either work in a transmission or a reflection Setup.
If you select Height Profile of Transparent Plate you obtain a transmission setup consisting of two components: a Curved Surface ( $\varsigma \mathrm{Sec} .58 .1$ ) with the front surface and the Microstructure Component. In this setup you have the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- | :--- |
| Substrate Medium | The medium between the two surfaces. The controls are described in <br> Sec. 34.1. |
| Surrounding Medium | The medium behind the microstructure. The controls are described in <br> Sec. 34.1. |
| Thickness of Substrate | The distance between the two surfaces. |
| Wavelength | The vacuum wavelength for which the phase function shall be translated into <br> a height profile. |

If you select Height Profile of Mirror you obtain a reflection setup containing only the Microstructure Component. In this setup you have the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Substrate Medium | The medium between behind the microstructure. This medium always con- <br> sists of the Ideal High Reflectance Material. |
| Surrounding Medium | The medium in front of the microstructure. Only used for the calculations of <br> the heights in the microstructure. The controls are described in Sec. 34.1. |
| Wavelength | The vacuum wavelength for which the phase function shall be translated into <br> a height profile. |

Fig. 699 shows the Optical Setup page of the structure design in case of Height Profile of Transparent Plate.


Figure 699. Settings for optical setup parameters of the structure design edit dialog.
The refractive index of the substrate medium must not be equal to the refractive index of the surrounding medium. Otherwise an error message is shown and the dialog is locked. The shown error message can be seen in Fig. 700.


Figure 700. Error message which is shown when the user sets up surrounding medium and substrate medium which are not valid. The dialog is also locked.

### 98.3 Surface Parameters

Fig. 701 shows the Surface Parameters tab page of the structure edit dialog.


Figure 701. The user can specify the parameters of the optical surface which shall be calculated from the given phase function.

The Surface Parameters tab has the following entries:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Unwrapping | Allows the complete or partial unwrapping of the phase in order to generate a smooth surface profile with heights larger than the height equivalent to $2 \pi$. For the unwrapping a line by line unwrapping method is used. The transmission should not contain phase dislocations. The following selections are possible: None - no unwrapping. <br> Partially (Neglecting Spherical Phase) - a partial unwrapping without considering the spherical phase factor information. If the unwrapped phase would be larger than the Modulo, it is wrapped. <br> Full (Neglecting Spherical Phase) - the phase is unwrapped completely without considering the spherical phase factor information. Not available for File Export. <br> Full (Considering Spherical Phase) - the phase is unwrapped completely while considering the spherical phase factor information. This option should be used if a transmission contains a strongly undersampled spherical phase factor. Not available for File Export. |
| Modulo | The maximum phase value in case of Partially (Neglecting Spherical Phase) unwrapping. Only multiples of $2 \pi$ are supported. |
| Enforce Quantization | If checked a hard quantization of the transmission is introduced. Enable this to calculate surface profiles with discrete height steps. |
| Number of Quantization Levels per 2 pi Phase Modulation | The number of quantization levels that should be introduced for discrete height profiles. This parameter is only active if Enforce Quantization is checked. |
| Height Modulation Depth per 2 pi | Displays the profile height corresponding to a $2 \pi$ phase modulation for the wavelength of the transmission. |
| Total Modulation Depth | Displays the total profile height. This value is for quantized, not unwrapped surface profiles always smaller than the height modulation depth per $2 \pi$. |
| Assume Smooth Height Profile <br> (Cubic 8 Point Interpolation) | Check this for non-quantized, non-periodic profiles that do not contain jumps, steps, and high frequency variations. Thus, the resulting sampled surface uses cubic 8 point interpolation. |
| Pixelated Height Profile (Nearest Neighbor Interpolation) | Check this for quantized profiles that are composed of rectangular pixels. Thus, the resulting sampled surface uses nearest neighbor interpolation. |
| Handle Fresnel Zone Transitions <br> (Fresnel Interpolation) | Check this for profiles containing jumps corresponding to $2 \pi, 4 \pi, \ldots$ phase steps. Those profiles should not contain discrete height levels. This parameter is only visible if Unwrapping is set to None or Partially (Neglecting Spherical Phase). The resulting sampled surface uses a special interpolation which avoids interpolation artifacts at the Fresnel jumps. |

## 99 Beam Shaper Design

VirtualLab Fusion offers three possibilities to design a beam shaping element (see table). They can be found in the Beam Shaper Design group of the Start > Diffractive Optics menu of the ribbon.

| DESIGN METHOD | DESCRIPTION |
| :--- | :--- |
| "Gaussian $\rightarrow$ Top Hat"" | Allows you to easily solve a subset of beam shaping design problems: <br> transforming a (super-)Gaussian input field into another super-Gaussian top <br> hat using a geometrical optics approach. Only the transmission is calcu- <br> lated which can be converted into a surface by using the structure design |
|  | ( $\hookrightarrow$ Sec. 98). The corresponding dialog is described in Sec. 99.1. |

## 99.1 "Gaussian $\rightarrow$ Top Hat" Transmission Design

The dialog for a "Gaussian $\rightarrow$ Top Hat" transmission design allows you to easily solve a subset of beam shaping design problems: transforming a (super-)Gaussian input field into another super-Gaussian top hat using a geometrical optics approach. By clicking OK you obtain the transmission for transforming the specified Input Field into the Desired Output Field, and optionally also other Output ( $\hookrightarrow$ Sec. 99.1.3).
You can select one of the following optical Setup Types:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $\mathbf{1 f - / 2 f - S e t u p ~}$ | The resulting transmission can be used both in a 1f- and a 2f-setup. The <br>  <br> Focal Length of the lens used in this setup can be given. |
| Fresnel Setup | The resulting transmission generates the desired output field in the far field. <br> The Distance between the transmission and the desired output field can be <br> given. |
| Angular Spectrum | The desired output field is generated in the far field of the resulting transmis- <br> sion. It is given in angular coordinates. |

In principal the used design approach can be used only for One-dimensional problems. In case of twodimensional design problems one of the following Symmetry types has to be selected:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Rectangular | Input field, desired output field, and the resulting transmission obey Cartesian |
|  | separability. For the resulting transmission function $\mathcal{T}(x, y)$ this means that |
|  | two one-dimensional functions $\mathcal{T}_{x}(x)$ and $\mathcal{T}_{y}(y)$ exist, so that $\mathcal{T}(x, y)=$ |
|  | $\mathcal{T}_{x}(x) \mathcal{T}_{y}(y)$. |
| Input field, desired output field, and the resulting transmission are rotationally |  |
|  | symmetric. For the resulting transmission function $\mathcal{T}(x, y)$ this means, that |
|  | a one-dimensional function $\mathcal{T}_{r}(r)$ exists, so that $\mathcal{T}(x, y)=\mathcal{T}_{r}(r)$, where |
|  | $r=\sqrt{x^{2}+y^{2} .}$ |

Depending on the symmetry type, the layout of the dialog changes.

Furthermore the Setup tab allows you to specify the Embedding Medium the beam shaper is placed in, i.e. you can Load a predefined homogeneous medium from the catalog ( $\hookrightarrow \mathrm{Sec} .33$ ), Edit the current medium ( $\hookrightarrow$ Sec. 37.3.1) or View it with the view described in Sec. 37.2. And you can choose whether you Design Transmission for Refractive Beam Shaper or Diffractive Beam Shaper. In the latter case an eventual spherical phase is sampled in the transmission.

### 99.1.1 Setting up Input Field and Desired Output Field

The Input Field and Desired Output Field tab of the dialog are quite similar. In both tab pages you can set the Waist Radius of the field referring to $1 / e^{2}$ of the maximum squared amplitude and the order of the superGaussian function ( $\hookrightarrow$ Sec. 132.2). An order of two corresponds to a Gaussian function. For the input field you can also specify the Wavelength which is also taken for the desired output field.

### 99.1.2 Setting up the Transmission

The aperture of the transmission can be adjusted with the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Setting | If checked, a reasonable aperture size of the transmission is determined au- <br> tomatically. |
| Field Size Factor | This factor is applied to the suggested transmission size computed for auto- <br> matic setting. A greater factor cuts off less of the input field. |
| Manual Setting | If checked, the aperture size has to be entered by the user. |
| Shape | The aperture may be Rectangularly or Elliptically shaped. |
| Diameter | Size of the aperture. |

The sampling of the transmission can be adjusted with the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic Sampling | If checked, the sampling parameters will be determined automatically. |
| Manual Sampling | If checked, the sampling parameters have to be entered by the user. |
| Accuracy Factor | This parameter can be entered for the Automatic Sampling mode only. A <br> greater factor increases the number of sampling points. |
| Sampling Points | In case of Manual Sampling, the number of sampling points can be entered <br> here. |
| Sampling Distance | In case of Manual Sampling, the sampling distance can be entered here. |
| Array Size | Read Only. The size of the resulting transmission. |

### 99.1.3 Output Specification

On the Output tab page you can specify that either an Optical Setup is generated by the dialog, containing a light source with the input field and a transmission storing the calculated transmission. Depending on the current Setup Type some additional Optical Setup Elements are included needed to obtain the desired output field in the target plane. If the setup type is not Angular Spectrum there is also a preconfigured diffractive optics merit functions detector inserted into the Optical Setup.
As alternative or in addition to Show Optical Setup the dialog can return input field, transmission, and desired output field as separate field documents.

### 99.2 Design of Diffractive Beam Shaper

The IFTA optimization document requires setting up input field and desired output field with correct sampling parameters. The sampling parameters of both fields depend on the optical setup and on the distance between the diffractive optical element (DOE) and the target plane. The document shown in Fig. 702 helps you setting up the IFTA optimization document for diffractive beam shapers.


Figure 702. First page of the document for setting up an IFTA optimization document for diffractive beam shapers.

The user has to specify at least the Input Field and the Desired Output Field. The user should make sure before the specification of the desired output field that there is a frame of zero-valued sampling points around the desired light distribution so that the size of the Desired Output Field is at least 4 times the size of the desired light distribution. Additionally the setup type ( $1 f-/ 2 f$-setup or Fresnel setup) and the distance between the element and the target plane can be specified in the dialog.
Further settings:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Optimization Region | The optimization of beam shapers and other diffractive optical elements (DOEs) requires the specification of a so called optimization region which describes an area in the target plane in which stray light will be minimized during optimization. Outside of this area stray light is allowed. If you select Arbitrary Optimization Region as Creation Method, you can Set any already open region document as optimization region. With the option Create from Desired Output Field an optimization region will be created containing all parts of the desired output field with amplitude values larger than $10 \%$ of the maximum amplitude. The last option Equal to Selection in Desired Output Field means that the optimization region will be generated from the rectangular selection marker ( $\hookrightarrow$ Sec. 11.3.4) which was present in the Desired Output Field at the time you have set it into the setup dialog. |
| Rectangular Pixelation | By checking this check box you indicate that the element designed by the IFTA will contain rectangular pixels after fabrication. In this case the "pixelation effect" ( $\hookrightarrow$ Sec. 138.1.2) will be simulated exactly. <br> This option is only available if the Optical Setup is set to 1 f -/2f-setup. |
| Pixelation Factor | In case of Fresnel Setup, the "pixelation effect" ( $\hookrightarrow$ Sec. 138.1.2) cannot be simulated exactly. Thus a Pixelation Factor $n_{\text {pix }}$ must be set. Consequently, each pixel in the resulting element is simulated by $n_{\text {pix }} \times n_{\text {pix }}$ sampling points. A pixelation factor <br> This option is only available if the Optical Setup is set to Fresnel Setup. |
| Determine Pixels Size Automatically | If this option is checked, the pixel size in the resulting element is determined automatically, but it is a multiple of the Pixel Size Increment of the machine used for exposure of the structures. Alternatively, you can specify an arbitrary Pixel Size. |
| Transmission Aperture | Allows you to set size and shape of the resulting transmission which represents the element. |

After specification of the parameters click the Next button. A new page will show the sampling parameters of input field, desired output field and DOE transmission. The Create Optimization Document button allows you to create the IFTA optimization document. If the optimization is finished, press Next again. The correct document should be preset. The Extract button generates a new transmission reduced to the Transmission Aperture defined on the first page.

## 100 Cells Array Design

## Availability

Toolboxes: Light Shaping Package
Accessible: Optical Setup: Optical Setup > New Cells Array Design


Figure 703. The Design tab of a Cells Array Design document if a Mirror Cells Array is to be designed.
Using this approach you can design a Cells Array ( $\hookrightarrow$ Sec. 40.1) to generate the desired light pattern for a given optical setup. To this end a random position in the light pattern is selected for each cell in the Cells Array and the outgoing direction is calculated from this position and the cell's position. The optical parameters of the cell are then determined so that the cell deflects the incoming light into the outgoing direction.

- For a Grating Cells Array ( $\hookrightarrow$ Sec. 40.1.1), Grating Period and Rotation Angle are determined so that the light of the first order is diffracted into the desired direction. A random lateral offset can be used to introduce random phases in the target plane.
- For a Prism Cells Array ( $\hookrightarrow$ Sec. 40.1.2), Tilt Angle and Rotation Angle are determined so that the incoming light is refracted into the desired direction. A random offset height can be used to introduce random phases in the target plane. The change in the resulting direction caused by different offset heights is considered correctly.
- For a Mirror Cells Array (= a Prism Cells Array used in reflection), Tilt Angle and Rotation Angle are determined so that the incoming light is reflected into the desired direction. A random offset height can be used to introduce random phases in the target plane. The change in the resulting direction caused by different offset heights is considered correctly.

The number of possible spot positions in the light pattern is taken directly from the sampling of the data defining the pattern. The design algorithm assumes that the light pattern is a binary one, i. e. every pixel with less than half the maximum amplitude is set to zero; all other pixels are set to the maximum amplitude. In this way, every spot position is illuminated by nearly the same number of cells.
A new Cells Array Design can only be created from an existing Light Shaping Optical Setup ( $\hookrightarrow$ Sec. 43.11.4). The design document window ( $\hookrightarrow$ Fig. 703) has two tab pages. The Lighting Setup tab summarizes the most essential parameters of the initial Optical Setup. The Show Initial Optical Setup allows you to show the initial Optical Setup again in case it has been closed.
The Design tab contains the following controls.

| Set | Allows you to set a data array describing the light pattern in three different ways (see below). It is assumed that the light pattern is centered around the position of the camera detector in the Optical Setup. The data array must contain only one two-dimensional subset. |
| :---: | :---: |
| Set > Load | Loads a data array from a .da file. |
| Set > Import | Imports a data array from a bitmap or text file by means of the import wizard described in Sec. 121.2. |
| Set > Select from Documents | Allows you to select an already open data array. |
| Show | Shows the current light pattern in a separate data array view ( $\rightarrow$ Sec. 13.5). |
| Variability of Spot Positions | If one certain position in the light pattern is illuminated by different cells, they all aim at the very same position. However, if you set a Variability of Spot Positions greater than zero the actual spot positions "are shook" around the pattern position. The variability can be set independently for $x$ - and $y$ direction. The given percentage refers to the distance to neighboring spots. See Fig. 704 for an example. |
| Use Seed for Spot Selection, Shaking, and Parameter Selection | A Cells Array Design uses random numbers to <br> - define which cell illuminates which position, <br> - how much the actual spot position is altered if Variability of Spot Positions is used, and <br> - to select a random lateral shift or offset height (depending on the type of the cells array). <br> Thus the design differs every time you click on Go!. If this shall not be the case, you can set a fixed arbitrary seed value with this option. |
| Apply Random Lateral Shift to Each Grating Cell | Only available for Grating Cells Arrays. <br> If checked, a random lateral shift is applied to each grating cell resulting in random linear phases in the target pattern. |
| Apply Random Offset Height to Each Prism / Mirror Cell | Only available for Prism and Mirror Cells Arrays. If checked, a random offset height is applied to each cell resulting in random phase offsets in the target pattern. |
| Maximum Offset Height | Only available for Prism and Mirror Cells Arrays. <br> If Apply Random Offset Height is checked, each cell gets a random offset height between zero and this value. Note that for technical reasons, the resulting offset height of certain cells can be slightly larger than this value. |
| Use Fabrication Constraint | If checked, you can either specify the Maximum Tilt Angle (for Mirror and Prism Cells Array) or the Minimum Grating Period (for Grating Cells Array). If this constraint is violated for one cell, the design algorithm tries up to ten times to find another random solution for that cell. |
| Go! | Starts the actual design. While the design is running, a progress bar is shown. The result is a new Optical Setup containing the designed cells array. |



| Ray Index | Position |  |  |
| :---: | :---: | :---: | :---: |
|  | X | Y | z |
| 1801 $\stackrel{\text { - }}{\text { V }}$ | -1.428598264 mm | -10.00001321 mm | 0 m |
| \# 10000 | 1 $\square$ III | $\square$ | , |


| Ray Index | Position |  |  |
| :---: | :---: | :---: | :---: |
|  | X | Y | z |
| 1슨 | 1.339880297 mm | $-4.954186822 \mathrm{~mm}$ | 0 m |
| \# 10000 | $1{ }^{\text {1 }}$ II | $\square$ | + |

Figure 704. Two diagrams of the spot positions for different Variability of Spot Positions. Left: A variability of ( $0 \%$; $0 \%$ ). Right: A variability of ( $75 \%$; $25 \%$ ).

## 101 Design of Light Guides

### 101.1 Footprint and Grating Analysis

Only available in the AR/VR/XR Package.

This design tool allows you to analyze in-depth the footprints at regions in a light guide as well as the performance of gratings with variable grating parameters per grating region. The following workflow can be realized by the provided tool:

1. Select the optical setup you like to use for analysis of footprints and grating performance. The selected optical setup can contain an arbitrary number of light guide components. Per component there can be also an arbitrary number of surfaces in it. And per surface also an arbitrary number of grating regions is supported for the analysis. The active light source within the selected system should be a plane wave, because the tool will adapt the angles defined in the plane wave for the footprint analysis. The plane wave has to be monochromatic.
2. Define a list of field of view angles (Cartesian angles) that should be used for the analysis. The tool allows an arbitrary number of angles to be defined, but at least one angle must be specified.
3. Perform footprint analysis. Here VirtualLab Fusion performs per specified field of view angle an analysis of the underlying setup and evaluates per grating region the positions (footprints) where the light interacts with the gratings. In addition also the direction vectors are evaluated and stored, under which each grating region is illuminated.
4. After the footprint analysis is done, there are several tools to investigate the evaluated information (evaluation by interactive footprint tool, heatmap visualization or access to the raw data).
5. In addition to access to the footprint data, the user has the option to evaluate the performance of gratings per region. This is supported only for regions which contain real gratings. The user can define a value
range for one or two grating parameters per region and VirtualLab Fusion will automatically calculate lookup tables which contain the Rayleigh matrices per incident angle and order. These lookup tables can be also displayed as efficiency curves for different polarization states (note: each grating interaction inside the light guide might change the polarization of the light, which is completely included in the modeling of such a device by physical optics).
6. After all lookup tables are calculated and stored on the hard disc (as 1D or 2D data array) the user can generate a new optical setup, where the grating regions might contain a grating with variable grating parameters (so called grating parameter modulation function; $\hookrightarrow$ Sec. 42.1.3). By clicking on the corresponding button the user can define the regions which should pre-configured with the corresponding grating parameter variation function. All lookup tables, which were calculated per region, will be stored within the region automatically.

The resulting optical setup can be used for further investigations and optimizations. After configuring the system in that way there is no need to do rigorous analysis of gratings even for a local grating parameter variation, because all information is already stored in the lookup tables. This enables an efficient and performant usage of the system within a parametric optimization.


Figure 705. The first page of the document window for the footprint and grating analysis.
The corresponding document window consists of two pages. On the bottom you have a Validity indicator ( $\hookrightarrow$ Sec. 5.10) which shows errors and warnings and gives you hints how to solve these issues.
On the first page ( $\hookrightarrow$ Fig. 705) you can configure the following.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Set | Allows you to set an Optical Setup either from a document window of <br>  <br>  <br>  <br> VirtualLab Fusion or from file. The Optical Setup must be a Light Guide Op- <br> tical Setup ( $\hookrightarrow$ Sec. 43.11.3) with a Plane Wave light source ( $\hookrightarrow$ Sec. 51.2). |
| Show | Shows the currently set Optical Setup. |
| Field of View Angles for | Allows you to define a set of field of view angles (in Cartesian coordinates) that <br> should be used for evaluation. This table can only be edited via the buttons <br> Design <br> next to its right side. |
| Efficiency of Zeroth Order | By default efficiencies of all gratings orders are set to 100 \%. This could lead <br> lo long computation times depending on the selected orders and maximum |
| ders | level for the light path finder. Therefore we offer the user to configure the <br> efficiencies of the zeroth order (typically used to distribute the light over an <br> area) and the other specified orders. |
| Analyze | Starts the analysis of the footprints, i.e. the positions (and also direction) <br> where the light hits the gratings. The text box below this button logs the <br> progress of this analysis. When the analysis is running this button becomes a <br> $\square$ <br> Stop button to cancel the analysis. When the analysis finishes this button is <br> disabled. It becomes enabled again when any of the above options changes. |



Figure 706. The second page of the document window for the footprint and grating analysis.

After the first page is successfully handled the next button will be enabled. The second page of the wizard consists mainly of a table with the following columns.

| COLUMN | DESCRIPTION |
| :---: | :---: |
| Status | Shows the status of the Vary column at a glance. Fig. 706 shows the four possible states. <br> - The first row in Fig. 706 has invalid lookup tables. They were calculated before, but the current configuration does not match the calculated lookup tables. A recalculation of the lookup tables solves this issue and will be done automatically if you press the Calculate Lookup Tables button. <br> - For the second row a valid lookup table has been calculated. <br> - For the third row a parameter configuration was configured but the corresponding lookup table has not been calculated yet. <br> - For the fourth and fifth row no parameter variation is specified. |
| Region | The name of the analyzed grating region. $\leftrightarrows$ Sec. 42.1. |
| View | Shows the footprints in a separate dialog. $\leftrightarrows$ Sec. 101.3 |
| Heatmap | Shows the "heatmap" of the region as separate Data Array 2D document. |
| Raw Data | Shows the raw data for both the footprints and the heat map as set of gridless data arrays. |
| Vary | This column allows you to define the variation of one or two parameters per grating. So first you have to check the box that you want to vary parameters, then choose the parameter(s) to vary in a separate dialog ( $\varsigma \mathrm{Sec}$. 101.4). When then the lookup tables have been calculated with the Calculate Lookup Tables button, you can either delete ( $\mathbb{区 N}_{\mathrm{E}}$ ) the results or show them as separate Data Array document ( $\mathrm{E}, ~ \leftrightarrows$ Sec. 101.1.1 ). For visualization of the lookup table context, the information of the calculated Rayleigh coefficients is transferred into efficiencies for different polarization states (we show the efficiency for TE, TM, left circular, right circular polarization and unpolarized). Note: The state of polarization will change while the light travels through the light guide and interacts with several gratings. |

Besides the table this page has the following controls.

ITEM
Path for Storing Lookup
Tables

DESCRIPTION
The tool stores the lookup table information (Rayleigh matrices) in form of 1D or 2D data arrays. During the calculation of the lookup tables the data arrays are stored on the hard disc. The user can define the path, where the lookup tables shall be stored.

- Calculate Lookup Ta- Starts the calculation of the selected lookup tables. The text box below this bles button logs the progress of this calculation. When the analysis is running this button becomes a Stop button to cancel the calculation.
Generate Optical Setup By pressing this button a dialog is opened, which is described in Sec. 101.1.2. with Modulation Function After the dialog is closed with Ok an optical setup is generated, which contains pre-configured grating regions with modulated grating parameters according to the parameters defined in the previous dialog.


### 101.1.1 Select Lookup Tables to Show

This dialog shows a list of all directions and order information for which the lookup tables are already calculated. This information is extracted from the folder defined in the analysis tool. The user can select an arbitrary number of directions and order combination. At least one entry in the table has to be selected to enable the OK. After pressing the OK button VirtualLab Fusion will generate one data array per selected entry, which shows the efficiency distribution over the define parameter range. The information of the lookup tables (Rayleigh matrix
per grating parameter) will be transferred to efficiency values for different polarization states. Each polarization state is stored as a subset in the generated data array. The efficiency will be calculated for TE, TM, left circular, right circular polarization as well as unpolarized light. Note: The state of polarization will change while the light travels through the light guide and interacts with several gratings, but the visualization for different "standard" polarization states give you already an insight into the performance and the dynamic range of the gratings that are analyzed. ${ }^{1}$
Fig. 707 shows a sample output of the efficiency visualization tool for different polarization states.


Figure 707. Sample output for displaying the efficiencies for different polarization states of a 1D grating parameter variation.

### 101.1.2 Select \& Configure Grating Regions

After the tool has calculated the lookup tables it can be used to generate a new optical setup, where the gratings per region might be modulated. This can be triggered by clicking on the Generate Optical Setup with Modulation Function button. A dialog is shown, where the user can configure the parameters used for the pre-configuration of the optical setup.
The dialog is shown in Fig. 708.

[^16]

Figure 708. Dialog to configure the parameters to use for generation of the optical setup with preconfigured grating parameter modulation functions.

The following parameters can be configured within the table provided in the dialog:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Modulate | Select the grating region that should be pre-configured to contain modulated grating pa- <br> rameters. |
| Region | The name of the grating region. $\lrcorner$ Sec. 42.1. |
| Points $\mathbf{X}$ | The grating parameter modulation function for each function will be initially configured to <br> be a sampled one. The number of points in x-direction can be selected here. |
| Points $\mathbf{Y}$ | The grating parameter modulation function for each function will be initially configured to <br> be a sampled one. The number of points in y-direction can be selected here. |
| Use Spline | The grating parameter modulation function for each function will be initially configured to <br> be a sampled one. The interpolation of the points can be done by nearest neighbor or <br> spline interpolation. By checking this option, the interpolation method will be set to spline. <br> This can be also changed afterward in the edit dialog of the grating parameter modulation <br> function. |

After pressing OK a new optical setup will be generated, that contains the configured grating parameter variation function.

### 101.2 Light Guide Grating Design

Only available in the AR/VR/XR Package.

With the light guide grating design wizard the user is enabled to optimize the grating parameters for a light guide setup including an eye pupil expander (EPE) grating and/or the grating region used for outcoupling. The typical initial starting point is the optical setup generated by the Layout Design Calculator ( $\leftrightarrows$ Sec. 113).
Within the wizard the user needs to first select the optical setup which should be used for optimization and identify the regions for incoupling, EPE and outcoupling. The document supports the design of ideal gratings as well as real gratings. For real gratings the wizard allow to select the grating parameters (maximum number 2) for EPE and outcoupling grating to be optimized. Furthermore the user can specify a set of field of view (FOV) angles which should be used for the optimization. Per FOV angle the user specifies the desired outcoupling efficiency in advanced. Several additional options for the EPE grating are provided, as well as a set of control parameters for the algorithm (like caching).
If the design is configured completely, VirtualLab Fusion will perform the optimization per FOV angle with the
desired outcoupling efficiency. Finally the results per FOV optimization are combined to a common solution. For the combination of all subresults a Voronoi algorithm is applied.
The resulting optical setup can be optimized further in a subsequent parametric optimization ( $\hookrightarrow$ Sec. 102).


Figure 709. The document window of the Light Guide Grating Design.

The document window of the Light Guide Grating Design ( $\hookrightarrow$ Fig. 709) is divided into several pages (which are described below). On the bottom you have a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) and buttons to navigate between the pages.
On the first page you have the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Set | Sets the Optical Setup to optimize. When you click on this button you can do the following: <br> - Load an optical setup from a file. <br> - Select from Documents allows you to select an already open optical setup. |
| Show | Shows the set optical setup in a separate document window. |
| Light Guide Component | Defines which element in the optical setup is the light guide to optimize. |
| Assign Regions | Defines which surface region of the selected light guide has which functionality (Incoupling Grating, Eye Pupil Expander, or Outcoupling Grating). |

On the second page the user can select whether you want to optimize Eye Pupil Expander and / or Outcoupling Grating. For the selected regions you then can choose one or two grating parameters to Vary with the control described in Sec. 101.4.
In the upper part of the third page you can define for which (Cartesian) angles of the field of view the design is done. In addition to the field of view angle to use for optimization, the user has to specify a desired outcoupling efficiency. If Eye Pupil Expander is set on the second page, you can set Optimization Options for Eye Pupil Expander to define its Desired Efficiency and the Allowed Stray Light inside the eye pupil expander region. Furthermore this page has the following options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Show Optimized Optical <br> Setups per Field of View <br> Angle | If checked for each angle defined in the upper part one optical setup is gen- <br> erated with which you can examine the performance of the optimized light <br> guide for this angle. |
| Use Cache During Design | If checked you can set a directory into which caching data is written. When <br> you cancel and restart the design this caching data is used whenever possible <br> to speed up the design. If you notice strange behavior during the design, it <br> might be because of inconsistent caching data. In this case simply uncheck <br> this option. By default the Path for Temporary Files defined in the Global <br> Options dialog ( $\hookrightarrow$ Sec. 6.17) is used. |

On the last page you can start the configured design using the $\square$ Go! button. As the design can be time consuming, you can first get an idea of the resulting Voronoi segmentation by clicking Analyze which runs much faster.
If you press the $\$ Go! button after the design has finished and no parameters are changed, just the resulting documents are created anew. If in this case you want to enforce a complete recalculation, click on the Reset button first.
Below these buttons there are two tabs. The Logging tab shows the progress of the design process. The Diagrams tab shows a visualization of the Eye Pupil Expander Region and/or the Outcoupling Region which you can Configure by means of the dialog described in the following section Sec. 101.3.1.

### 101.3 Footprint Diagrams

Footprint diagrams show where the light hits a grating region. For the Light Guide Grating Design ( $\rightarrow$ Sec. 101.2) they are shown directly in the design document, whereas for the Footprint and Grating Analysis ( $\leftrightarrows$ Sec. 101.1) they are shown in a separate dialog.
When you click on Configure the dialog described in Sec. 101.3.1 is shown.

### 101.3.1 Configuring a Grating Layout and Footprint Diagram



Figure 710. The edit dialog for configuring a Grating Layout and Footprint Diagram.

A Grating Layout and Footprint Diagram can be configured by a dialog ( $\hookrightarrow$ Fig. 710 ) with the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Show Segmentation | If you click this option, the Voronoi cells are show in the diagram. Their colors can be adjusted with the Segmentation Properties explained below. If this option is not used, you can only define the Region Border Color and the Region Fill Color. |
| Border Color | Only if Show Segmentation <br> The color used to draw the borders of the Voronoi cells. |
| Fill Mode | Only if Show Segmentation <br> Determines with which color the Voronoi cells are filled. Three modes are available: <br> - Footprint Colors: The Voronoi cells are filled with the color of the corresponding footprint as defined in the Footprint Properties box. To ensure a good contrast between the Voronoi cell and the footprint (if shown), you can set the Opacity of Filling. <br> - Constant: All cells are filled with the same Fill Color. <br> - Parameter Values: All cells are filled according to the selected grating parameter. The settings for this mode are explained below. This mode is only available after a design was run where at least one parameter was varied in the corresponding region. |
| Parameter to Show | Only if Fill Mode is Parameter Visualization <br> In case two parameters of the gratings are varied, you can select here which of the two parameters is used to determine the color of the distinct cells. |
| Color Table | Only if Fill Mode is Parameter Visualization <br> Depending on the value the Parameter to Show has in a certain cell, this cell is filled with the matching color from the set Color Table ( $\hookrightarrow$ Sec. 11.2.4). |
| Automatic Scaling | Only if Fill Mode is Parameter Visualization <br> If this option is checked, the minimum and maximum color of the Color Table are assigned to the minimum and maximum occurring value of the Parameter to Show, respectively. Otherwise you can set Minimum and Maximum according to your liking. |
| Footprint Properties | The center of the Voronoi cells are those positions where the center of a diffracted light beam enters the region. These positions can be marked by rings ("footprints"). This table allows you to select for which Field of View Angles you want to see the footprints (left column, the uppermost check mark allows you to select all / no angles). In the right column you can change the color of the footprints for each angle. |

101.4 Grating Parameter Variation


Figure 711. The control to configure the variation of grating parameters.
The control shown in Fig. 711 allows you to select one or two grating parameters which you want to Vary. For these parameters you can define the value range by setting the start (From) and end (To) value. The default From and To values for all parameters are their absolute minimum and maximum values - you must not enter a value outside of this range. It is possible to enter a To value which is smaller than the From value.
Furthermore you can enter either the number of Steps (which are not necessarily identical) or the Step Size. The defined value range(s) are then scanned with the resulting number of steps. See Sec. 44.2.3 for details. The first column allows you to collapse / expand all parameters of one Category. Simply click on the $\square$ and $\pm$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*).
The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensi- <br> tive. It is possible to search for multiple words and word groups embraced by <br> quotation marks, for example: "surface \#1" scaling. |
| Show Only Varied Param- <br> eters | Only rows where the Vary column is checked pass this filter. |

## 102 Parametric Optimization

The parametric optimization in VirtualLab Fusion allows you to optimize optical setups by means of nonlinear optimization algorithms. For that purpose VirtualLab Fusion supports the definition of merit functions that are to be optimized. Merit functions can take into account detector results. Further several types of parameter constraints are formulated as merit functions as well. Finally a common merit function is constructed by a weighted sum of individual merit functions.

Implementation details are given in Sec. 138.2.

### 102.1 Parametric Optimization Document

The parametric optimization document can be generated for Optical Setups ( $\hookrightarrow$ Sec. 43) containing at least one analyzer or one detector linked to the active light source which calculates a fixed number of physical values. For some detectors or analyzers this is only the case in a specific configuration. For example the Grating Order Analyzer ( $\hookrightarrow$ Sec. 84) can only be used for Parametric Optimization if at least one of the following conditions is fulfilled:

- Summed Transmission, Absorption, and Reflection is checked. Then the Overall Transmission Efficiency, the Overall Reflection Efficiency, and the Overall Reflection and Transmission Efficiency can be optimized.
- Single Order Output, but only with Order Range as Selection Strategy, as only then the number of results is known prior to the Optical Setup simulation.

If the currently active Optical Setup is consistent, a parametric optimization document can be opened via the ribbon item Optical Setup $>\mathbb{4}$ New Parametric Optimization or the Optical Setup Tool ( $\hookrightarrow$ Sec. 43.6) 兆 Create New Parametric Optimization.
As other documents in VirtualLab Fusion, the parametric optimization document is designed as a wizard. That means the user can switch between the different pages sequentially via the Next and Back buttons. The appearance of any page may depend on the settings made on preceding pages. All pages are documented in the next sections.
The parametric optimization document can be saved and loaded via the File menu of the main window of VirtualLab Fusion. The ribbon of this document is explained in Sec. 102.1.1.

## Handling of Obsolete Parameters

If you load a Parametric Optimization which has been saved in a previous version of VirtualLab Fusion, there might be some obsolete parameters still present in the parameter specification table. On the other hand, newly added parameters might not yet be available.
If no results have been calculated yet, the parameters are updated automatically. Otherwise, updating the parameters would delete the results. Then, only a warning is shown in both the Messages tab ( $\hookrightarrow$ Sec. 4.3) and the window title (" $₫$ Old Parameters $\triangle$ ").
If one of the varied parameters changed, the Parametric Optimization cannot be configured and simulated anymore. You can only analyze the results or Refresh the document via the ribbon (which deletes the results).

### 102.1.1 Ribbon

The ribbon of the Parametric Optimization document has the following entries:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Go! | Allows you to start the optimization. Only enabled if you are on the Opti- <br> mization Results page of the document window. During the optimization, the <br> button changes into a $\square$ Stop button which allows you to stop the calculation. |


| After Completion | For long running optimizations it can be useful if after completion the Para- <br>  <br> metric Optimization saves itself and optionally the computer shuts down. This <br> can be defined with this option which is also available in the property browser <br> $(\hookrightarrow$ Sec. 4.3). <br> If the Parametric Optimization has not been saved before it is saved at \{Path <br> for User Settings $\} \backslash$ Autosaved Files. The Path for User Settings can be <br> set on the Saving tab of the Global Options dialog ( $\hookrightarrow$ Sec. 6). Below this <br> combo box the used file name is displayed. <br> Note that Save \& Shutdown Computer can lead to data loss if there are <br> unsaved documents but the Parametric Optimization for which this op- <br> tion is set. |
| :--- | :--- |
| Refresh | Refreshes the document to use the current set of parameters. Note that this <br> deletes existing results. See also the note on handling of obsolete parameters <br> on page 832. |

## Show Optical Setup This button has three sub-entries:

- Show Initial Optical Setup: Shows the Optical Setup from which the Parametric Optimization was originally created. This can be invoked directly if the upper part of the Show Optical Setup button is clicked.
- Show Optical Setup for Certain Simulation Step...: Shows the Optical Setup with the parameters of a certain simulation step which can be selected in a separate dialog.
- Show Optimized Optical Setup: Shows an Optical Setup with the optimal values of free parameters (that is the values yielding the minimum target function value) and with the start values of the fixed parameters. The start values of fixed parameters usually equal the initial values, but they might also be edited in the Start Value column of the constraint table ( $\leftrightarrows$ Sec. 102.1.4). If there are two or more simulation steps with the same target function value, the first one is taken automatically.

| No Logging During Execution | If you press this button, the results of the individual simulation steps are only written after the optimization has finished. This improves performance especially in case of many fast simulation steps. If this button is not pressed the results are written as soon as they are available. Note that this button is disabled during an ongoing optimization and that it can also be changed via the Property Browser. |
| :---: | :---: |
| Create Output from Selection | If you click this button, for each table row of the current selection a combined output is generated, i.e. a separate one-dimensional data array where the data in this row is plotted versus the simulation step. During the output creation, the button changes into a $\quad$ Stop Output Creation button which allows you to stop the calculation. <br> Double clicking on a row header is a short cut for selecting this row completely and clicking ${ }_{\text {空 }}$ Create Output from Selection. It is also possible to generate the combined output out of the current selection via the context menu or the $\rightarrow$ Create Output from Selection button of the results table. |

### 102.1.2 Parameter Selection Page

If you change the Parameter Selection page, the results table is cleared.

By clicking Next on the welcome page of the document the parameter selection page ( $\hookrightarrow$ Fig. 712) is shown. This page lists the parameters of the underlying Optical Setup that may be varied by the optimization algorithm. Via the Vary column the user determines if a parameter shall be variable (checked) or fix (unchecked). At least one parameter must be variable.
For your information also the Original Values of all parameters are given.


Figure 712. Parameter selection page of the parametric optimization document. The parameter Distance Before has been declared as variable for the optimization.

The first column allows you to collapse/expand all parameters of an Optical Setup Element or its categories. Simply click on the $\square$ and $\mp$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*).
If at least one parameter has been checked, the Next button is enabled. By clicking Next one switches to the detector specification page ( $\hookrightarrow$ Sec. 102.1.3).
The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensi- <br> tive. It is possible to search for multiple words and word groups embraced by <br> quotation marks, for example: "surface \#1" scaling. |
| Show Only Varied Param- <br> eters | Only rows where the Vary column is checked pass this filter. |

### 102.1.3 Detecting Device Specifications Page

If you change the Detecting Device Specifications page, the results table is cleared and the constraints page needs to be updated again.

This page is the same as the corresponding page for the Parameter Run ( $\hookrightarrow \mathrm{Sec} .44 .4)$ with the following exceptions.

- For a Parametric Optimization, you can only check one out of Ray Results Profile, General Profile, and Classic Field Tracing.
- Only detectors or analyzers which output physical values can be optimized and are thus shown in the corresponding tables. For the same reason, the check boxes 3D View and Modeling Analyzer are disabled.

If the Next button is clicked, the constraint specification page will be displayed ( $\hookrightarrow$ Sec. 102.1.4).

### 102.1.4 Constraint Specification Page

If you change the Constraint Specification page, the results table is cleared.

The constraint specification page ( $\hookrightarrow$ Fig. 713) lists the constraints ( $\hookrightarrow$ Sec. 138.2.1) that have been implicitly defined on the previous pages of the document in a table. By means of that table the user defines the composition of the target function ( $\hookrightarrow$ Sec. 138.2.1).


Figure 713. Constraint specification page containing parameter constraints, merit function constraints and general constraints

Each row stands for a constraint, whereupon the constraints are sorted into their classes:

1. The parameter constraints are listed with light blue background color. Every free parameter, which was selected on the parameter selection page ( $\hookrightarrow$ Sec. 102.1.2), implies a parameter constraint on this page.
2. The merit function constraints appear with light orange color. A merit function constraint is created for each detector merit function that gets evaluated during optimization. Note that the set of evaluated merit functions can be adjusted by editing or enabling/disabling of detectors. This is possible either in the initial Optical Setup or later on the detector specification page of the created optimization document ( $\leftrightarrows$ Sec. 102.1.3)
3. If there are general constraints predefined in the Optical Setup, they will be listed with light turquoise background color.

The constraint table consists of the following columns:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Constraint Host | The Optical Setup Element that hosts the parameter(s) or the merit function, <br> respectively, of the constraint. This column is read-only. |
| Constraint Name | The name of the constraint. This column is read-only. |
| Use | One can enable or disable constraints via this column. |
| Weight | Here the constraint weights $g_{i}$ can be specified for the target function <br> ( $\hookrightarrow$ Sec. 138.2.1). |
| Constraint Type | On this column one specifies the constraint type, which triggers the kind of <br> contribution to the target function. Via clicking on a cell one can choose <br> among Lower Limit, Upper Limit, Range and Target Value ( 4 Sec. 138.2.1.2). |
| Target Value is not available for parameter constraints. |  |

Furthermore, the following controls buttons are available below the table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Tools | Opens a menu containing the optimization tools (see below). |
| Target Function Value | Here the current value of the target function $F$ (Eq. (138.4)) is displayed. |
| Update | Updates the Start Value and Contribution column if values got invalid (sym- <br> bolized via $N / A)$. |

The following optimization tools are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Reset Start to Initial Val- <br> ues | Start values of all parameters (whether they are currently free or not) will be <br> reset to their initial values that are stored in the initial Optical Setup. |
| Set Optimized Start Val- <br> ues | Parameter values that were found by the last run of the optimization algorithm <br> (appearing in the last column of the results table [ $\hookrightarrow$ Fig. 717]) will be set as <br> start values for another optimization run. |
| Set Values from Certain <br> Simulation Step | Parameter values from any already calculated simulation step will be set as <br> start values for another optimization run. Via a dialog you can select from <br> which simulation step the values are taken. |
| Distribute Contributions | Weights of constraints with a contribution greater zero will be adapted to get <br> an uniform distribution of contribution. |
| Uniformly | Opens a dialog for setting a new target contribution of a single con- <br> straint whereupon the ratio of the other contributions remain unchanged <br> ( $\hookrightarrow$ Sec. 102.1.4.1). This command is only available if the current contribu- |
| tions are up-to-date. If not, one has to press Update before. |  |

### 102.1.4.1 Target Contribution Dialog

Via this dialog the user is able to set a new contribution for one of the constraints whose current contributions are unequal zero. To achieve the specified contribution the weights of all constraints will be adapted appropriately.

| Set Target Contribution for Single Constraint |  | $\times$ |
| :---: | :---: | :---: |
| Choose Constraint from List: |  |  |
| Constraint Host | Constraint Name | Select |
| Beam Parameters \#600 | Diameter X | $\square$ |
|  | Diameter $Y$ | $\square$ |
|  | Waist Diameter X | $\square$ |
|  | Waist Diameter $Y$ | $\square$ |
|  | Full Divergence Angle $X$ | $\square$ |
|  | Full Divergence Angle $Y$ | $\square$ |
|  | Waist Distance X | $\square$ |
|  | Waist Distance $Y$ | $\square$ |
|  | M 2 -Parameter in x -Direction | $\square$ |
|  | M 2 -Parameter in y-Direction | $\square$ |
| Lens System \#2 | Aspherical Interface \#1 \| Minimal Local Radius | $\square$ |
|  | Aspherical Interface \#2 \| Minimal Local Radius | $\square$ |
| Enter Target Contribution: | 10\% |  |
|  | Ok Apply | Help |

Figure 714. Dialog for setting a target contribution for a selected constraint

The available constraints are listed in a table. Like on the constraint specification page of the optimization document ( $\hookrightarrow$ Sec. 102.1.4) the constraints are sorted into parameter constraints, merit function constraints and general constraints (each group with different background color). The table has three columns:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Constraint Host | The Optical Setup Element that hosts the parameter(s) or the merit function, <br> respectively, of the constraint. This column is read-only. |
| Constraint Name | The name of the constraint. This column is read-only. |
| Select | Herewith the user selects the constraint, for that a certain target contribution <br> shall be achieved. There is only a single selection possible. |

Below the constraint table the target contribution can be input:

ITEM
Enter Target Contribution

DESCRIPTION
For the selected constraint the current contribution (as shown in the optimization document, too) is displayed. The user can specify the wanted contribution in percent here. Please note that one has to press OK or Apply to validate the current input. Otherwise, the currently entered value will be forgotten if one selects another constraint.

If OK or Apply is pressed, the weights of all constraints are recalculated to achieve the wanted contribution for the selected constraint. Thereby the ratios of the other constraint's contributions among each other remain unchanged. The constraint table of the underlying optimization document is updated immediately.

### 102.1.5 General Settings Page

If you change the General Settings page, the results table is cleared.

On this page general settings concerning the optimization algorithm that is used for minimizing the target function ( $\hookrightarrow$ Sec. 138.2.1) can be adjusted.


Figure 715. General settings page of the parametric optimization document

First of all one should decide on the Optimization Strategy:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Local Optimization | If selected, one of the local optimization algorithms is applied. |
| Global Optimization | If selected, the global optimization method of simulated annealing <br> $(\hookrightarrow$ Sec. 102.1.5.1) is applied. |

Local optimization algorithms are fast but their success in finding the global minimum strongly depends on the choice of the start value - at least for functions that are not strictly convex in the area of interest. Therefore, in cases where no good start values are known, global optimization should be preferred ( $\hookrightarrow$ Sec. 102.1.5.1). Currently, three nonlinear local algorithms for minimizing a multivariate function are provided:

- Downhill Simplex method of Nelder and Mead [NM65]
- Powell's method [Pow64]
- Levenberg-Marquardt algorithm [Lev44][Mar63]

The first two methods do not make use of the derivatives of the target function, the third one calculates the derivatives numerically.
For local algorithms the following settings (Local Optimization Settings) are available:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Optimization Algorithm | Choose one of the three optimization algorithms given above. |
| Maximal Number of Itera- <br> tions | Here the maximal number of iterations. The algorithm stops when either the <br> estimated error is less than the Maximal Tolerance, or the maximal number of <br> iterations is reached. Please consider that the number of function evaluations <br> is higher than the number of iterations. |
| Maximal Tolerance | Herewith the stop criterion for the algorithm is specified. The algorithm stops <br> when either the estimated error is less than the specified value $\varepsilon_{\text {max }}$, or Max- <br> imal Number of Iterations was reached. See Sec. 138.2 .2 for the definition of <br> the estimated error. |
| Initial Step Width Scale | Via this factor the step widths from the start values to the first iteration values <br> of all free parameters are scaled. Thereby the user can control the search <br> area around the start value. The step widths also depend on the constraint <br> types and constraint values of the corresponding parameter constraints. |

The iteration process of a local algorithm stops when either the estimated error $\varepsilon$ is less than the tolerance $\varepsilon_{\max }$, or the maximum number of iterations is reached.

### 102.1.5.1 Simulated Annealing

The simulated annealing method is based on an analogy from materials science and enables the global search for the minimum by an random temperature term $t$ that is added to the current target function value. It is obtained from

$$
\begin{equation*}
t=T \log r \tag{102.1}
\end{equation*}
$$

where $r$ is a random value between 0 and 1. $T$ is the temperature, which is gradually decreased according to an annealing schedule, which is specified on the Global Optimization Settings group box ( $\hookrightarrow$ Fig. 716). The selected local optimization algorithm is applied to the adapted target function at each annealing step. Currently, the downhill simplex algorithm is the only possible choice for the applied local optimization algorithm.

The following Global Optimization Settings can be specified:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Optimization Algorithm | The global optimization method. Only Simulated Annealing is available. |
| Number of Annealing | The number of steps $n$ at which the temperature is evenly decreased by <br> Steps <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br>  <br> Number of Iterations of the applied local optimizer is reached or if the esti- <br> mated error is less than the tolerance, but typically this only occurs during the <br> final step, when the temperature is zero. |
| Start Temperature | Temperature $T_{S}$ at which the annealing process is started. |



Figure 716. Group box with global optimization settings. Only visible if Global Optimization strategy is chosen.
For locating the global minimum successfully, appropriate values for Start Temperature and Number of Annealing Steps must be chosen. Unfortunately, this is something of a trial and error process in most cases. Generally, it is a good idea to do some iterations via a Parameter Run ( $\leftrightarrows$ Sec. 44) within the considered parameter range for better understanding the target function value range. If the start temperature is too low the algorithm will possibly get stuck in the surrounding of a local minimum. On the other hand, temperature values that are too high will increase the probability for "jumping out" of the surrounding of an already detected global minimum.

### 102.1.6 Optimization Results Page



Figure 717. Optimization results page of the parametric optimization document
On this page the optimization can be started or stopped via the $\downarrow$ Go! button or the Parametric Optimization > $\downarrow$ Go! ribbon item and one can track the advance in the optimization progress via the results table ( $\varsigma$ Fig. 717). The table shows the following information per simulation step:

- The resulting target function value of each simulation step (Optimizer Logging row). Sec. 138.2.1 explains how this value is calculated.
- The values of all varied parameters in the Parameter Constraints row.
- All enabled general constraints in the General Constraints row.
- All enabled merit functions.

Each simulation step, which is equal to an evaluation of the target function by the optimization algorithm, is logged in a new column. Note, that in general the simulation step number does not equal the iteration number. E. g. in Powell's method the target function can be evaluated more than 100 times during one iteration [Pow64]. If the optimization algorithm stops or is stopped by the user, the last column will always show the optimized parameters (for which the smallest target function value was obtained).
The appearance and the handling of this page is very similar to the results page of the parameter run document ( $\leftrightarrows$ Sec. 44.5), but it has less output options.
You can select a subset of all results by clicking on the column or row headers or by directly selecting a cell range. This selection can be copied to the Windows ${ }^{\text {TM }}$ clipboard via the context menu or the shortcut $\mathrm{Ctrl}+\mathrm{C}$.

\begin{tabular}{|c|c|}
\hline ITEM \& DESCRIPTION <br>
\hline Create Output from Selection \& If you click this button, for each table row of the current selection a combined output is generated, i.e. a separate one-dimensional data array where the data in this row is plotted versus the simulation step. This button has the same functionality as the corresponding ribbon button ( $\leftrightarrows$ Sec. 44.1). <br>

\hline Filter Rows by ... \& | Applies a search string to the table. Only rows matching the given string are shown, whereas the following rules apply: |
| :--- |
| - The search is not case sensitive, i.e. lens, Lens, and LENS yield the same results. |
| - It is possible to search for multiple words and word groups embraced by quotation marks. Rows containing at least one of these words or word groups in any of their cells are shown. |
| - A - in front of a word or word group means 'not', e.g. -lens shows all lines not containing 'lens'. |
| - Expressions in quotation marks are searched as entered. For example ${ }^{\prime}-2.5$ ' ' searches for the number -2.5 , not for rows not containing 2.5. And '`Lens System' ' searches for rows containing directly "lens system", not for rows containing "lens" or "system". | <br>

\hline
\end{tabular}

The following options for the result table are available in the Property Browser ( $\leftrightarrows$ Sec. 4.3).

## ITEM

DESCRIPTION

| Always Plot versus Simulation Step | If you create a combined output of the values in a table row, usually these values are plotted versus the Simulation Step (= the column headers). But if there are only one or two parameter constraints and you do not create a combined output for these constraints, then you can choose to plot versus these constraints instead by setting the option Always Plot versus Simulation Step in the Property Browser to False. $\hookrightarrow$ Sec. 44.5.1.1 |
| :---: | :---: |
| Log Contributions | If this option is enabled, not only the target function ( $\hookrightarrow$ Sec. 138.2.1) is logged for each optimization step, but also the contribution of each merit function to it. In this way you can easily recognize when one merit function dominates the optimization process. |
| No Logging During Optimization | Provides the same functionality as the No Logging During Execution ribbon item ( $\hookrightarrow$ Sec. 102.1.1). |
| Sort Rows | By default the rows are sorted alphanumerically by the Detector and the Subdetector. Using this option you can ensure the same order as in the Parameter Selection and the Constraint Specification page is used. |
| After Completion | For long running optimizations it can be useful if after completion the optimization document saves itself and optionally the computer shuts down. This can be defined with this option which is also available in the ribbon ( $\leftrightarrows$ Sec. 102.1.1). <br> If the document has not been saved before it is saved at \{Path for User Settings $\} \backslash$ Autosaved Files. The Path for User Settings can be set on the Saving tab of the Global Options dialog ( $\hookrightarrow$ Sec. 6). <br> Note that Save \& Shutdown Computer can lead to data loss if there are unsaved documents but the Parameter Run for which this option is set. |
| Automatic Saving | Here you can enable or disable that the document is saved periodically after a certain time interval. |
| Interval for Automatic Saving | Only if Automatic Saving is true. <br> The time interval after which the document is saved automatically. |
| Number of Digits | The number of digits of the shown values. The default is taken from the Number of Digits of the Global Options dialog ( $\hookrightarrow$ Sec. 6.5). |
| Show Physical Units | With this option you can convert all values to their respective base unit and omit all units. For example, " 1 nm " will then be shown as " $1 \mathrm{e}-9$ " and " $180^{\circ}$ " will be shown as "3.1416". This simplifies using copied values in external programs. |

### 102.1.6.1 Additional Information in the Table

If only one parameter constraint is optimized, it might happen that the same parameter value is used in distinct simulation steps. Such duplicate simulations are not shown in the table.
If the optimizer chooses parameters which result in an inconsistent Optical Setup (e. g. negative thicknesses), the target function is set to NaN (an indicator for invalid values). If any of the chosen parameters violates its specified constraints it is marked with red font color. Both such simulation steps can be hidden by setting Show Only Valid Simulation Steps in the Property Browser to False.
Merit functions where the specified constraint is fulfilled are marked with green font color.

The currently best result(s), i. e. the simulation step(s) with the minimum target function value, are marked with golden background.

## 103 optiSLang Package

The optiSLang Optimization in VirtualLab Fusion allows you to optimize optical setups with additional optimizing algorithms. Just like Parametric Optimization ( $\hookrightarrow$ Sec. 102), in optiSLang Bridge defined merit functions are to be optimized. Merit functions can consider detector results. Many types of parameter constraints are formulated as merit functions as well. Parameters available for parametric optimization are marked with a ${ }^{\mathrm{PV}}$ in this manual ( $\hookrightarrow$ Sec. 43.5).

## 103.1 optiSLang Optimization Document

The optiSLang optimization document can be generated for Optical Setups ( $\hookrightarrow$ Sec. 43) containing at least one analyzer or one detector linked to the active light source which calculates a fixed number of physical values. For some detectors or analyzers this is only the case in a specific configuration. For example the Grating Order Analyzer ( $\hookrightarrow$ Sec. 84) can only be used for optiSLang Optimization if at least one of the following conditions is fulfilled:

- Summed Transmission, Absorption, and Reflection is checked. Then the Overall Transmission Efficiency, the Overall Reflection Efficiency, and the Overall Reflection and Transmission Efficiency can be optimized.
- Single Order Output, but only with Order Range as Selection Strategy, as only then the number of results is known prior to the Optical Setup simulation.

If the currently active Optical Setup is consistent, an optiSLang Optimization document can be opened via the ribbon item Optical Setup $>$ Optimize with optiSLang.
As other documents in VirtualLab Fusion, the optiSLang Optimization document is designed as a wizard. That means the user can switch between the different pages sequentially via the Next and Back buttons. The appearance of any page may depend on the settings made on preceding pages. All pages are documented in the next sections.
The optiSLang Optimization document can be saved and loaded via the File menu of the main window of VirtualLab Fusion. The ribbon of this document is explained in Sec. 102.1.1.

## Handling of Obsolete Parameters

If you load an optiSLang Optimization which has been saved in a previous version of VirtualLab Fusion, there might be some obsolete parameters still present in the parameter specification table. On the other hand, newly added parameters might not yet be available.
If no results have been calculated yet, the parameters are updated automatically. Otherwise, updating the parameters would delete the results. Then, only a warning is shown in both the Messages tab ( $\hookrightarrow$ Sec. 4.3) and the window title (" $\triangle$ Old Parameters $\triangle$ ").
If one of the varied parameters changed, the optiSLang Optimization cannot be configured and simulated anymore. You can only analyze the results or Refresh the document via the ribbon (which deletes the results).

### 103.1.1 Ribbon

The ribbon of the optimization document has the following entries:

| Go！ | Allows you to start the optimization．Only enabled if you are on the results page of the document window．During the optimization，the button changes into a Stop button which allows you to stop the calculation． |
| :---: | :---: |
| After Completion | For long running optimizations it can be useful if after completion the Para－ metric Optimization saves itself and optionally the computer shuts down．This can be defined with this option which is also available in the property browser （ $\leftrightarrows$ Sec．4．3）． <br> If the Parametric Optimization has not been saved before it is saved at \｛Path for User Settings\}\Autosaved Files. The Path for User Settings can be set on the Saving tab of the Global Options dialog（ $\rightarrow$ Sec．6）．Below this combo box the used file name is displayed． <br> Note that Save \＆Shutdown Computer can lead to data loss if there are unsaved documents but the Parametric Optimization for which this op－ tion is set． |
| $\bigcirc$ Refresh | Refreshes the document to use the current set of parameters．Note that this deletes existing results．See also the note on handling of obsolete parameters on page 843. |
| 毘 Show Optical Setup | This button has three sub－entries： <br> －Show Initial Optical Setup：Shows the Optical Setup from which the optiSLang Optimization was originally created．This can be invoked directly if the upper part of the Show Optical Setup button is clicked． <br> －Show Optical Setup for Certain Simulation Step．．．：Shows the Op－ tical Setup with the parameters of a certain simulation step which can be selected in a separate dialog． <br> －Show Best Design Optical Setups：Allows you to select one of setups regarded as best designs from optiSLang． |
| No Logging During Execution | If you press this button，the results of the individual simulation steps are only written after the optimization has finished．This improves performance es－ pecially in case of many fast simulation steps．If this button is not pressed the results are written as soon as they are available．Note that this button is disabled during an ongoing optimization and that it can also be changed via the Property Browser． |
| Create Output from Selection | If you click this button，for each table row of the current selection a combined output is generated，i．e．a separate one－dimensional data array where the data in this row is plotted versus the simulation step．During the output cre－ ation，the button changes into a Stop Output Creation button which allows you to stop the calculation． <br> Double clicking on a row header is a short cut for selecting this row completely and clicking 胥 Create Output from Selection．It is also possible to generate the combined output out of the current selection via the context menu or the $\rightarrow$ 酸 Create Output from Selection button of the results table． |

### 103.1.2 Parameter Selection and Simulation Engine Selection Page

If you change this page, the results table is cleared.

When you create a new document the parameter selection page ( $\hookrightarrow$ Fig. 718) is shown.
The upper part of this page with simulation engine drop down lets you select the simulation engine ( $\hookrightarrow$ Sec. 43.4) or analyzer ( $\hookrightarrow$ Part XII) that is used for the optimization process. Analyzers can be edited using the Edit button.


Figure 718. Parameter selection page of the optiSLang optimization document. The parameter Distance Before has been declared as variable for the optimization.

The middle part of this page lists the parameters of the underlying Optical Setup that may be varied by the optimization algorithm. Via the Vary column the user determines if a parameter shall be variable (checked) or fix (unchecked). At least one parameter must be variable.
The Short Name of the varied parameters is by default the last part of the Parameter Name ${ }^{1}$. However, it must be unique for the varied parameters so you can change it if needed.
For your information also the Original Values of all parameters are given.
The first column allows you to collapse / expand all parameters of an Optical Setup Element or its categories. Simply click on the $\square$ and $\oplus$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*).
The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensi- <br> tive. It is possible to search for multiple words and word groups embraced by <br> quotation marks, for example: "surface \#1" scaling. |
| Show Only Varied Param- <br> eters | Only rows where the Vary column is checked pass this filter. |

If at least one parameter has been checked, the Next button is enabled. By clicking Next one switches to the constraints specification page ( $\hookrightarrow$ Sec. 103.1.3).
A validity indicator ( $\leftrightarrows$ Sec. 5.10) shows errors if for example

- the Optical Setup does not have merit functions for the currently selected Simulation Engine. This can happen if all detectors are in a state that they cannot be used for the optiSLang optimization, e.g. they are inconsistent or do not calculate physical values in the current configuration,
- no parameter to Vary is selected, or
- the value range of one varied parameter is too large


### 103.1.3 Constraint Specification Page

If you change the constraint specification page, the results table is cleared.

The constraint specification page ( $\hookrightarrow$ Fig. 713) lists the constraints ( $\hookrightarrow$ Sec. 138.2.1) that have been implicitly defined on the previous page of the document in a table. By means of that table the user defines the composition of the target function ( $\hookrightarrow$ Sec. 138.2.1).


Figure 719. Constraint specification page containing parameter constraints and merit function constraints.
Each row stands for a constraint, whereupon the constraints are sorted into their classes:

1. Every free parameter, which was selected on the parameter selection page ( $\hookrightarrow$ Sec. 102.1.2), implies a parameter constraint on this page. They are listed with gray background color because they cannot be edited in this table.
2. The merit function constraints appear with light orange color. A merit function constraint is created for each detector merit function that gets evaluated during optimization.

The constraint table consists of the following columns:

[^17]| COLUMN | DESCRIPTION |
| :--- | :--- |
| Parameter Host | The Optical Setup Element that hosts the parameter(s) or the merit function, <br> respectively, of the constraint. This column is read-only. |
| Parameter Name | The name of the parameter. This column is read-only. |
| Use | One can enable or disable merit functions via this column, but not parameters. <br> Parameter Type <br> On this column one specifies the constraint type only for merit functions, which <br> triggers the kind of contribution to the target function. Via clicking on a cell <br> one can choose among Lower Limit, Upper Limit, and Target Value. |
| Value 1 | For parameters the minimum allowed value is shown here. For merit func- <br> tions, the Lower Limit, Upper Limit, or Target Value can be entered here. |
| Value 2 | For parameters the maximum allowed value is shown here. For merit func- <br> tions this column is unused by OptiSLang Optimization Document. |
| Start Value | Here the user can see the start values of both parameters and merit functions. <br> The values for the merit functions can be calculated by clicking the Update <br> button. |

### 103.1.4 General Settings Page

On this page the optimization algorithm that is used for minimizing the target function can be defined. In the moment only the global optimization method Evolutionary Algorithm (EA 10000, $\hookrightarrow$ Sec. 138.2.3.2) is available.


Figure 720. General settings page of the optiSLang Optimization Document.

### 103.1.5 Results Page

On this page the optimization can be started or stopped via the $>$ Go! button or the optiSLang Optimization > Go! ribbon item and one can track the advance in the optimization progress via the results table ( $\hookrightarrow$ Fig. 717). The table shows the following information per simulation step:

- The values of all varied parameters in the Parameter Constraints row.
- All enabled merit functions.


Figure 721. Optimization results page of the parametric optimization document
The appearance and the handling of this page is very similar to the results page of the parameter run document ( $\leftrightarrows$ Sec. 44.5), but it has less output options. Each simulation done by optiSLang is logged into a new column. You can select a subset of all results by clicking on the column or row headers or by directly selecting a cell range. This selection can be copied to the Windows ${ }^{\text {TM }}$ clipboard via the context menu or the shortcut Ctrl + C.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Create Output from Se- | If you click this button, for each table row of the current selection a combined |
| output is generated, i. e. a separate one-dimensional data array where the |  |
| data in this row is plotted versus the simulation step. This button has the |  |
| same functionality as the corresponding ribbon button ( $\hookrightarrow$ Sec. 44.1). |  |

The following options for the result table are available in the Property Browser ( $\hookrightarrow$ Sec. 4.3).
$\left.\begin{array}{ll}\hline \begin{array}{ll}\text { Always Plot versus Simu- } \\ \text { lation Step }\end{array} & \begin{array}{l}\text { If you create a combined output of the values in a table row, usually these } \\ \text { values are plotted versus the Simulation Step (= the column headers). But } \\ \text { if there is only one parameter constraint and you do not create a combined }\end{array} \\ \text { output for this constraint, then you can choose to plot versus this constraint in- } \\ \text { stead by setting the option Always Plot versus Simulation Step in the Property } \\ \text { Browser to False. }\end{array}\right\}$

## XV Calculators

VirtualLab Fusion offers various calculators which implement formulas and algorithms often used in optics. Usually, they can be found in the Calculators menu of the Start ribbon.

| CALCULATOR | DESCRIPTION |
| :---: | :---: |
| ABCD Law Calculator | Allows you to define a rotationally symmetric optical system and to calculate how a laser beam is altered by this system. The ABCD law is used to this end. $\leftrightarrows$ Sec. 104 |
| Coherence Time \& Length Calculator | Calculates the coherence time and the coherence length for different spectra. $\rightarrow$ Sec. 105 |
| Debye-Wolf Integral Calculator | With this calculator one can easily calculate the field in or near the focus of an ideal lens which is illuminated with collimated light. $\hookrightarrow$ Sec. 106 |
| Diffraction Angle Calculator | Calculates the diffraction angles for a given period, wavelength and angle of incidence. $\lrcorner$ Sec. 107 |
| Direction Converter | Converts between Cartesian and spherical angles as well as wave numbers and spatial frequencies. $\leftrightarrows$ Sec. 108 |
| Fiber Mode Calculator | Calculates the (linearly polarized) modes inside an optical fiber. $\rightarrow$ Sec. 109 |
| Fresnel Effects Calculator | Calculates the Fresnel effects at a material transition for different wavelengths and angles of incidence. $\hookrightarrow$ Sec. 110 |
| k-Layout Visualization | Shows the k-Layout diagram for a given grating setup. Available via the Start $>$ Light Guide ribbon item. $\hookrightarrow$ Sec. 111 |
| Laser Beam Calculator | A simple calculator which helps you to determine all fundamental parameters of a Gaussian beam from given parameters. $\leftrightarrows$ Sec. 112. |
| Layout Design | Creates an optical setup with a light guide fulfilling the given specifications. In particular, the grating regions have the correct positions and sizes. Available via the Start > Light Guide ribbon item. $\lrcorner$ Sec. 113 |
| Memory Calculator | Calculates how much memory a certain field needs (depending on number of sampling points, polarization state, and so on). $\lrcorner$ Sec. 114 |
| Modulation Depth Calculator | Allows you to calculate the modulation depth of a Diffractive Optical Element (DOE) generating a phase difference of $2 \pi$. $\lrcorner$ Sec. 115 . |
| Rigorous Analysis of Slanted Gratings | Slanted gratings are an important sub-class of gratings but can be analyzed only inefficiently by the Fourier Modal Method. So this calculator allows you to analyze them by the Integral Method, and for reference also by the Fourier <br> Modal Method. $\hookrightarrow$ Sec. 116 |
| Spherical Lens Calculator | This calculator can be used for paraxial calculations based on the lens maker's equation as well as on the imaging equation of a spherical lens. <br> $\rightarrow$ Sec. 117 |
| Vector \& Coordinate System Viewer | This tool visualizes coordinate system base vectors which are rotated in relation to a reference coordinate system in the 3D space. $\leftrightarrows$ Sec. 118. |

## 104 ABCD Law Calculator

ABCD matrices give an easy way to describe the transformation of a Gaussian beam in radially symmetric optical systems without limiting apertures. Therefor the complex radius of curvature $q$ of a Gaussian beam is defined as follows:

$$
\begin{equation*}
\frac{1}{q(z)}=\frac{1}{R(z)}-i \frac{\mathrm{M}^{2} \lambda}{\pi w(z)^{2}} \tag{104.1}
\end{equation*}
$$

$R(z)$ is the Phase Radius at a certain position $z$ and $w(z)$ is the Beam Radius at the same position $z$. Furthermore, $\mathrm{M}^{2}$ is the $M^{2}$ Parameter of the Gaussian beam and $\lambda$ its Wavelength. See also Sec. 51.1 for reference. The complex radius of curvature $q_{\text {in }}$ of the Input Gaussian Beam is transformed by an ABCD matrix $\mathcal{M}$ into the complex radius of curvature $q_{\text {out }}$ of the Output Gaussian Beam by the so-called ABCD law [ST91]:

$$
\begin{equation*}
q_{\mathrm{out}}=\frac{A q_{\mathrm{in}}+B}{C q_{\mathrm{in}}+D} \tag{104.2}
\end{equation*}
$$



Figure 722. The ABCD Law Calculator
The dialog of this calculator is shown in Fig. 722 and has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Input Gaussian Beam | Allows you to enter Wavelength $\lambda, M^{2}$ Parameter, Beam Radius $w(z)$, and <br> Phase Radius $1 / e^{2} R(z)$ of the input beam. It is assumed that both beam and <br> phase radius are given at the same position $z$. |
| ABCD Matrix Control | Allows you to define the system ABCD matrix by composing it of an arbitrary <br> number of optical elements. $\hookrightarrow$ Sec. 5.16 |
| Resulting ABCD Matrix | Shows the automatically calculated ABCD Matrix of the combination of the <br> optical elements. |
| Output Gaussian Beam | Displays Beam Radius $1 / e^{2}$ and Phase Radius if the input beam has been <br> propagated through the optical system represented by the ABCD matrix. |

## 105 Coherence Time \& Length Calculator

This calculator calculates the coherence time and the coherence length for different spectra. It has the following controls which can be set in the dialog shown in Fig. 723.


Figure 723. Coherence Time \& Length Calculator

ITEM

| Ambient Material | Allows you to define the material in which the spectrum is defined. $\hookrightarrow$ Sec. 34.3 |
| :--- | :--- |
| Gaussian Spectrum / <br> Lorentzian Spectrum | The type of the spectrum. |
| Peak Wavelength | Allows you to set the peak (vacuum) wavelength $\lambda$ of the spectrum. |
| Bandwidth (Wavelength) | Allows you to set the bandwidth $\Delta \lambda$ of the spectrum in the wavelength domain. |
| Peak Frequency | Shows the corresponding frequency $v$ of the peak wavelength. |
| Bandwidth (Frequency) | Shows the bandwidth $\Delta v$ of the spectrum in the frequency domain. <br> $\Delta v=c \Delta \lambda / \lambda^{2}$ where $c$ is the speed of light in the ambient material. |
| Coherence Time | Shows the coherence time $\tau=s / \pi \Delta v . s$ is 2 for a Gaussian spectrum and 1 <br> for a Lorentzian one. |
| Coherence Length | Shows the coherence length $l=c \cdot \tau$. |
| Validity | This control ( $\hookrightarrow$ Sec. 5.10$)$ indicates whether there are issues with the current <br> configuration, which happens for example if the wavelength is not valid for <br> the given ambient material. In such a case, no calculated values are shown. <br> You then can click on the 固-button for further information. |

## 106 Debye-Wolf Integral Calculator

With the Debye-Wolf Integral ( $\hookrightarrow$ Sec. 139.1) one can easily calculate the field in or near the focus of an ideal lens which is illuminated with collimated light.


Figure 724. The Debye-Wolf Integral Calculator

VirtualLab Fusion offers a calculator to easily evaluate this integral ( $\hookrightarrow$ Fig. 724). It is separated into three tabs (see below). Furthermore it contains the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Create Results | Starts the generation of the results. The electromagnetic field $\left(E_{x}, E_{y}\right.$, and <br> $\left.E_{z}\right)$ and the electric energy density are calculated. <br>  <br> After clicking, this button turns into a Stop button which allows you to cancel <br> a long lasting calculation. |
| Validity | This control $(\hookrightarrow$ Sec. 5.10$)$ indicates whether there are issues with the current <br> configuration. If this is the case you can click on the <br> information. |

The Light Source tab allows you to set the Wavelength and polarization of the incident collimated light. For setting the polarization the control described in Sec. 48.3 is used.
The Optical Setup tab has the following controls.
ITEM
DESCRIPTION

| Ambient Material | Allows you to define the material around the focusing lens. $\hookrightarrow$ Sec. 34.3 |
| :--- | :--- |
| Numerical Aperture | The numerical aperture of the focusing lens. |
| Focal Length | The focal length of the lens. |
| Distance from Focal Plane | You can calculate the field in the focus (if this value is zero) or slightly out of <br> to Result Field |

The Numerical Parameters tab contains those settings with which you can reduce the accuracy of the results to achieve faster calculations.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Field Size | The lateral extension of the results. |
| Estimate Field Size | Estimates the field size $F$ according to |
|  | $F=6 \cdot(0.61 \lambda \cdot N A+\|d\| \cdot \tan (\arcsin N A / n))$ |
|  | with the Wavelength $\lambda$, the Numerical Aperture NA, the Distance from Focal |
|  | Plane to Result Field $d$, and the refractive index $n$ of the Ambient Material. |
| Sampling Points | The number of sampling points in the result fields. |
| Number of Directions | The Debye-Wolf integral over all angles ( $\hookrightarrow$ Sec. 139.1$)$ is approximated by a |
|  | sum over a certain number of discrete angles. This number can be set here. |

## 107 Diffraction Angle Calculator

This calculator is a visualization of the grating equation given in Sec. 139.5. Only a one-dimensional intersection $(y=0)$ is shown and thus only the angles $\alpha$ are given.
The Grating Period $P_{\mathrm{x}}$, the Incident Angle $\alpha_{\text {in }}$ (out of which the incident wave vector is calculated), and the Wavelength $\lambda$ can be entered directly. The refractive indices $n_{\text {in }}$ and $n_{\text {out }}$ can be specified by setting the First Material and the Second Material using the control described in Sec. 34.3. Incident wave and reflected orders are in the first material, the transmitted orders are in the second material. If a material has no refractive index data for the given wavelength, a refractive index of 1 is used.
Using the Switch Materials button you can swap the two materials easily.
In the Diffraction Orders box, you can change the Maximum Shown Order. This parameter determines how many propagating orders you will see - evanescent orders are not shown in this diagram. The minimum and maximum propagating order, both for reflection and transmission, are shown as Reflected Orders Range and Transmitted Orders Range, respectively.
The results are visualized in a Diffraction Orders Diagram ( $\hookrightarrow$ Sec. 19). If you want to save or manipulate this diagram, you can generate a Separate Diagram document.

## 108 Direction Converter

| 32: Direction Converter |  | $\square$ 回 |
| :---: | :---: | :---: |
| Vacuum Wavelength |  | 532 nm |
| Homogeneous Medium |  |  |
| Name Non-Dispersive Material ( $\mathrm{n}=1$ ) |  | Q |
| Defined by Constant Refractive Index |  | $\checkmark \quad 1$ |
| State of Matter | Gas or Vacuum | $\checkmark$ |
| Direction <br> Cartesian Angles |  |  |
|  |  |  |
| Alpha |  | -0.2 |
| Beta |  | $1^{\circ}$ |
| $\bigcirc$ Spherical Angles |  |  |
| Phi |  | 101.31 ${ }^{\circ}$ |
| Theta |  | $1.0198^{\circ}$ |
| O Wave Vector Components |  |  |
| X Component (kx) |  | -412311/m |
| Y Component (ky) |  | $2.0618 \mathrm{E}+051 / \mathrm{m}$ |
| $\bigcirc$ Spatial Frequencies |  |  |
| X Component (u) |  | -6562.2 1/m |
| Y Component (v) |  | 32814 1/m |
|  | Close | Help |

Figure 725. Direction Converter

There are different ways how angles can be specified. This calculator converts between the following four representations using the equations given in Sec. 139.3:

- Cartesian Angles
- Spherical Angles
- Wave Vector Components and
- Spatial Frequencies

The independent parameters vacuum wavelength $\lambda_{\text {vac }}$ and refractive index $n$ have to be specified in the dialog:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vacuum Wavelength | Vacuum wavelength $\lambda_{\text {vac }}$ to calculate the wave number $k$ from. |
| Homogeneous Medium | Defines the medium that provides the refractive index $n\left(\lambda_{\text {vac }}\right)$ for the calcu- <br> lation of the wave number $k$. This control is described in Sec. 34.3. |

## 109 Fiber Mode Calculator

| [1: Fiber Mode Calculator |  |  |  |  | $\square$ 回 $x^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mode Type | Linearly Polarized Bessel | Azimuthal Order L | Radial Order M | Propagation Const... | Effectiv... |
|  |  | 0 | 1 | $1.7951 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5199 |
| Wavelength | 532 nm | 0 | 2 | $1.795 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5199 |
|  |  | 0 | 3 | $1.795 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5198 |
| Core Diameter | $100 \mu \mathrm{~m}$ | 0 | 4 | $1.7949 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5198 |
| Core Material |  | 0 | 5 | $1.7948 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5197 |
| Name ${ }^{\text {N-BK7_Schott_2015 }}$ |  | 0 | 6 | $1.7947 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5196 |
|  |  | 0 | 7 | $1.7946 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5195 |
|  |  | 0 | 8 | $1.7944 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5193 |
| Catalog Material |  | 0 | 9 | $1.7942 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5192 |
| State of Matter | Solid | 0 | 10 | $1.794 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.519 |
| State of Matter | Solid | 1 | 1 | $1.7951 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5199 |
| Cladding Material |  | 1 | 2 | $1.795 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5199 |
|  |  | 1 | 3 | $1.795 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5198 |
| Name Fused_Silica |  | 1 | 4 | $1.7949 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5197 |
|  |  | 1 | 5 | $1.7948 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5196 |
| Catalog Material |  | 1 | 6 | $1.7946 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5195 |
| State of Matter |  | 1 | 7 | $1.7945 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5194 |
|  | Solid | 1 | 8 | $1.7943 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5193 |
| Maximum Azimuthal Index |  | 1 | 9 | $1.7941 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5191 |
|  | 1* | 1 | 10 | $1.7939 \mathrm{E}+07 \mathrm{~m}^{-1}$ | 1.5189 |
| Maximum Radial Index | 10) - |  |  |  |  |
| Output of Additional Data Arrays |  |  |  |  |  |
| - Create Mode Fields | Show 1 |  |  |  |  |
| Validity: ${ }^{\text {a }}$ |  |  |  | Close | Help |

Figure 726. The document window of the Fiber Mode Calculator.

The Fiber Mode Calculator calculates the propagation constants, effective refractive indices and field distributions of the modes in a fiber.
It has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Mode Type | Allows you to select between Linearly Polarized Bessel modes which occur <br> in step-index fibers and Linearly Polarized Laguerre modes which occur in <br> gradient index fibers. |
| Wavelength | The wavelength $\lambda$ of the modes. |
| Core Diameter | The core diameter $d$ of the fiber. |
| Core Material | Allows you to set the material in the fiber core with the control described in <br> Sec. 34.3. Only the real-valued refractive index $n_{\text {core }}(\lambda)$ is used. |
| Cladding Material | OnLY FOR LINEARLY PoLARIZED BESSEL MODEs <br> Allows you to set the material of the fiber cladding with the control described <br> in Sec. 34.3. Only the real-valued refractive index $n_{\text {cladding }}(\lambda)$ is used. |
| Gradient Constant | OnLY FOR LINEARLY PoLARIZED LAGUERRE MoDES |
|  | For gradient index fibers the refractive index distribution is given by |

## 110 Fresnel Effects Calculator

The Fresnel Effects calculator enables you to get the complex Fresnel Coefficients according to Fresnel's equations given in Sec. 139.4:
There is the possibility to get all coefficients at a glance for a given wavelength and incidence angle, but there is also the possibility to get a diagram of the dependencies on wavelength and angle of incidence. These
both kinds of output (Tables $\hookrightarrow$ Sec. 110.2 and Diagram $\hookrightarrow$ Sec. 110.3) are described in the following, after the description of the materials setup of the calculator (Sec. 110.1).

### 110.1 Materials and Coating Setup



Figure 727. The controls for the setup of the materials and an optional coating.

The controls of the dialog are explained in detail in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| First Material | Material in front of the surface to examine the Fresnel coefficients for. For the <br> usage of the control see Sec. 34.3. |
| Switch Materials | Sets the First Material as Second Material and vice versa. |
| Second Material | Material behind the surface to examine the Fresnel coefficients for. For the <br> usage of the control see Sec. 34.3. |
| Coating | A coating to be considered for the calculation. For the usage of the control <br> see Sec. 34.2. |

The image in the bottom of Fig. 727 shows the sequence of the materials, the coating and the surface. Solid material is symbolized by $/ / / /$, liquid by $\bar{\equiv}$, and gaseous material or vacuum by $\because \circ$. Which side of the surface is coated is shown by the symbols \|\| and \|.

### 110.2 Tables Output Panel



Figure 728. The calculator's panel with the output of all Fresnel coefficients for one wavelength and one incidence angle at a glance.

The controls of the dialog are explained in detail in the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | Wavelength $\lambda$ to do the calculation for. |
| Angle of incidence | Angle of incidence $\theta$ to do the calculation for. |
| Intensity Coefficients | Reflectance $R$ and transmittance $T$. |
| Complex Fresnel Coeffi- <br> cients | Reflection coefficient $\rho$ and transmission coefficient $\tau$ in Amplitude/Phase no- <br> tation. |

### 110.3 Diagram Output Panel



Figure 729. The calculator's panel with the output of a diagram with wavelength or angular dependency.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Abscissa(e) | What dependency shall be shown in the diagram? Dependency on Wave- <br> length, Incidence Angle, Energy, or Wavelength and Angle? <br> Wavelength/Energy <br> Angle of Incidence <br> Wavelength $\lambda$ or wavelength range (energy range in case of Energy depen- <br> dence) to do the calculation for. |
| Angle of incidence $\theta$ or angle range to do the calculation for. |  |

## 111 k-Layout Visualization

Only available in the AR/VR/XR Package.

This calculator generates a k-Layout diagram for the specified grating setup. Its document window ( $\hookrightarrow$ Fig. 730) has two tabs, a zoomable diagram, and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ).


Figure 730. The document window of the $k$-Layout Visualization.
The Physical Settings tab has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | The (vacuum) wavelength for which the k-Layout is generated. |
| Surrounding Medium | Defines the surrounding medium by means of the control described in <br> Sec. 34.1. |
| Light Guide Medium | Defines the light guide medium by means of the control described in <br> Sec. 34.1. |
| Width $\mathbf{x}$ Height | The extension of the field of view in degrees for both x - and y -direction. |
| Offset | The offset of the field of view from perpendicular incidence in degrees for both <br> x -and y -direction. |
| Grating Parameters | Period, Rotation Angle, and Grating Order of the three involved gratings: In- <br> coupling Grating, Eye Pupil Expander, and Outcoupling Grating. |

The View Settings tab has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Colors | All colors to be used in the diagram can be set here. |
| Fill Field of View Boxes | Defines whether the "field of view boxes" are drawn filled or just as outline. |
| Opacity of Field of View <br> Boxes  | In case of filled boxes, the opacity of the filling can be set here. The maximum <br> value of 1 means full opacity. |

## 112 Laser Beam Calculator

The Laser Beam Calculator ( $\leftrightarrows$ Fig. 731) allows you to calculate all parameters of a laser beam ( $\mathrm{M}^{2}$, waist radius, divergence, Rayleigh length, waist distance, and beam radius) if only some of these parameters are known. To this end the equations given in Sec. 132.1 are used.

This calculator is designed as document, i.e. you can open more than one document and and then open a Gaussian generator dialog ( $\hookrightarrow$ Sec. 51.1) to import the data there.


Figure 731. Laser Beam Calculator
The following parameters can be specified:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Type | You can choose among different types of a laser beam. Depending on the type the document windows slightly changes. The following types are available: <br> - For an Arbitrary Laser Beam, the $\mathrm{M}^{2}$ value can be set freely. <br> - For a Fundamental Gaussian Mode $\mathrm{M}^{2}$ is always 1. But in this case you can choose whether you want to enter $1 / \mathrm{e}^{2}$, FWHM, or HWHM values. <br> - For a Hermite-Gaussian Mode and a Laguerre-Gaussian Mode, the M ${ }^{2}$ value is calculated from the given order(s). |
| Parameters | Only for the Fundamental Gaussian Mode <br> Defines which parameters you actually set: <br> - $1 / e^{2}$ Waist Radius, Divergence Half Angle: The beam radius is determined by a relative intensity decay by $1 / \mathrm{e}^{2}$ for a Gaussian beam. The divergence angle is measured between the optical axis and the $1 / \mathrm{e}^{2}$ decay of the intensity. <br> - $1 / e^{2}$ Waist Diameter, Divergence Full Angle: The beam diameter is determined by a relative intensity decay by $1 / \mathrm{e}^{2}$ for a Gaussian beam. The divergence angle is measured between the $1 / \mathrm{e}^{2}$ decays of the intensity. <br> - FWHM Waist and Divergence Angle: The waist and the divergence angle are defined as full width half maximum (FWHM) of the laser beam intensity. The conversion factor from $1 / \mathrm{e}^{2}$ radius / half angle to FWHM is $\sqrt{2 \ln 2}$. <br> - HWHM Waist and Divergence Angle: The waist and the divergence angle are defined as half width half maximum (FWHM) of the laser beam intensity. |


| Order | OnLY FOR A HERMITE-GAUSSIAN MODE OR LAGUERRE-GAUSSIAN MODE <br> Order O corresponds to the fundamental Gaussian mode. For a Laguerre- <br> Gaussian mode, the left text box refers to the radial order while the right box <br> specifies the angular order. |
| :--- | :--- |
| $\mathbf{M}^{\mathbf{2}}$ Parameter | $\mathrm{M}^{2}$ parameter of the beam. Can be set only for Arbitrary Laser Beams. Oth- <br> erwise it is fixed to 1 (Fundamental Gaussian Mode) or calculated from the <br> Order. |
| Reference $\quad$ Wavelength <br> (Vacuum) | Vacuum wavelength of the Gaussian wave. |
| Waist Radius | Beam size in waist position. |
| Divergence Angle | The divergence angle in the far field. |
| Rayleigh Length | Rayleigh length of the Gaussian wave. |
| Longitudinal $\quad$ Waist |  |
| tance | Dis- |
| Distance from the waist used for the calculation of Beam Radius and Phase |  |
| Radius. |  |

## 113 Layout Design Calculator

Only available in the AR/VR/XR Package.

This calculator creates an optical setup with a light guide fulfilling the given specifications. In particular, the grating regions have the correct positions and sizes.


Figure 732. The document window of the Layout Design Calculator.
Its document window ( $\hookrightarrow$ Fig. 732) has three tabs, a button Create Result which creates the optical setup and the corresponding k-layout ( $\hookrightarrow$ Fig. 111), and a validity indicator ( $\hookrightarrow$ Sec. 5.10 ).
The Incident Light tab has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | The (vacuum) wavelength of the incident light. |
| Beam Size | The beam size in $x$ - and $y$-direction. |
| Distance Source to Light | The distance between the source and the light guide component. |
| Guide | The medium outside of the light guide. The controls are described in <br> Surrounding Medium <br> Sec. 34.1. |
| The extension of the field of view in degrees for both $x$ - and $y$-direction. |  |
| Offset | The offset of the field of view from perpendicular incidence in degrees for both <br> $x-$ and $y$-direction. |

The Light Guide tab contains the specification of the actual light guide.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Absolute Position | The lateral position of the center of the incoupling grating relative to the internal coordinate system ( $\leftrightarrows$ Sec. 43.8.1.1) of the light guide component. |
| Position Outcoupling Grating | The lateral position of the outcoupling grating (and thus the output channel) relative to the center of the incoupling grating. |
| Thickness of Light Guide | The thickness of the light guide. |
| Design for Reflection | If this option is checked, the light leaves the light guide on the same side as the incident light. |
| Light Guide Medium | The medium within the light guide. The controls are described in Sec. 34.1. |
| Orientation Incoupling Grating | A value of $0^{\circ}$ means that the incident light is deflected along the $x$-axis. |
| Fixed Incoupling Period | Determines whether the Period Incoupling Grating or the Mode Density is determined by the user. |
| Period Incoupling Grating | Only if Fixed Incoupling Period is checked. The period of the incoupling grating. |
| Desired Maximum Distance of Outcoupling Beams | Only if Fixed Incoupling Period is not checked. <br> The period of the incoupling grating is determined so that the desired maximum distance for the outcouplping beams is reached. The maximum distance of the outcoupling beams is calculated for the field of view mode which has the smallest density. In case no period could be calculated for the entered value an error message will be displayed. |
| Deflection Angle Eye Pupil Expander | Specifies by how many degrees the Eye Pupil Expander changes the lateral direction of the light. |

The Outgoing Light tab has the following controls.
DESCRIPTION
Distance Light Guide to The distance between light guide and eye (represented by a Camera DetecEye tor).

Size of Eye Box
The size of the eye box (represented by the window size of the detector).

## 114 Memory Calculator

The Memory Calculator ( $\hookrightarrow$ Fig. 733) allows you to calculate how much memory a certain field needs (depending on number of sampling points, polarization state, and so on).


Figure 733. Memory Calculator

The required memory depends on the following parameters.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Sampling Points | The number of sampling points of a field. |
| Real-Valued / | In contrast to Real-Valued numbers, Complex-Valued numbers store two |
| Complex-Valued | numbers per pixel (real and imaginary part). |
| Globally Polarized / In contrast to a Globally Field, a Locally Polarized field contains two field <br> Locally Polarized components $\left(E_{x}\right.$ and $\left.E_{y}\right)$. |  |

## 115 Modulation Depth Calculator

The Modulation Depth Calculator ( $\rightarrow$ Fig. 734) allows you to calculate the modulation depth of a Diffractive Optical Element (DOE) generating a phase difference of $2 \pi$. To this end the Thin Element Approximation (TEA) is used.

| 1. Modulation Depth Calculator |  |  |  |  | 回 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Setup |  | Height Profile of Transparent Plate |  |  |  |
| Substrate Medium <br> Fused_Silica in Homogeneous Medium |  |  | Surrounding Medium <br> Air in Homogeneous Medium |  |  |
|  |  |  |  |  |  |
| $\square$ Load | $\int$ Edit | Q View | Load | / Edit | Q Vie |
| Wavelength <br> Number of Quantization Levels per 2 pi Phase Modulation |  |  |  |  | 532 |
|  |  |  |  |  |  |
| Height Modulation Depth per 2 pi |  |  |  |  | 1.1544 |
| Modulation Depth of Quantized Surface |  |  |  |  | 1.0823 |
| Validity: |  |  |  | ose | Help |

Figure 734. Modulation Depth Calculator
The following parameters can be specified:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Setup | The user can specify whether the modulation depth shall be calculated for a <br> transparent plate which works in transmission, or for a Height Profile of Mirror. |
| Substrate Medium | The medium of the substrate block of the DOE. Note that the substrate can <br> only be configured if the optical setup Height Profile of Transparent Plate is <br> selected, otherwise it is set to $l$ deal Mirror. |
| Surrounding Medium | The surrounding medium of the DOE. |
| Wavelength | The vacuum wavelength for which the modulation depth shall be calculated. |
| Number of Quantization <br> Levels per $\mathbf{2}$ pi Phase <br> Modulation | The number of quantization levels that are used to generate a phase modu- <br> lation of $2 \pi$. |
| Height Modulation Depth <br> per 2 pi | Displays the profile height $h$ corresponding to a $2 \pi$ phase modulation. <br> For a transparent plate this height is $h=\lambda / \Delta n$, where $\lambda$ is the Wavelength, <br> and $\Delta n$ is the (positive) difference of the refractive indices of the two media. <br> For a mirror this height is $h=\lambda / 2 n_{\mathrm{s}}$ where $n_{\mathrm{s}}$ is the refractive index of the <br> Surrounding Medium. |
| Modulation <br> Quantized Surface | The highest level of a quantized surface never corresponds to a phase differ- <br> ence of $2 \pi$ as then it would have the same effect as the lowest level. Thus <br> the overall Modulation Depth of Quantized Surface $h_{\mathrm{q}}$ is only $h_{\mathrm{q}}=h \cdot(l-1) / l$ <br> where $l$ is the Number of Quantization Levels. |

The refractive index of the substrate medium must not be equal to the refractive index of the surrounding medium. Otherwise no results are displayed and the validity indicator in the bottom left corner shows an error message.

## 116 Rigorous Analysis of Slanted Gratings

Only available for Virtuallab Fusion Advanced.

Slanted gratings are an important sub-class of gratings but can be analyzed only inefficiently by the Fourier Modal Method ( $\hookrightarrow$ Sec. 96.3). So this calculator allows you to analyze them by the Integral Method ([SK11]), and for reference also by the Fourier Modal Method.


Figure 735. Calculator for Rigorous Analysis of Slanted Gratings
Its document window ( $\hookrightarrow$ Fig. 735) has the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength | The (vacuum) wavelength for which the analysis is done. |
| Surrounding Medium | Defines the medium in front of the grating. This control is described in <br> Sec. 34.1. |
| Substrate Medium | Defines the medium behind the grating. This control is described in Sec. 34.1. |
| Period | The period of the grating. |
| Fill Factor | The width of the grating ridges relative to the period. |
| Slant Angle <br> Polarization | The angle of the left and the right flank of the grating, respectively. <br> Order to Analyze |
| Whather the analysis is done for the TE Polarization or the TM Polarization. |  |
| cies for Transmission | with this checkbox you can switch between analysis of transmitted and re- |
| flected orders. |  |
| Range of Curvatures | This calculator models the slanted grating with rounded edges of a certain <br> curvature. More precisely a range of curvatures is scanned. |
| Number of Steps for Anal- | Defines how many curvatures in the given Range of Curvatures are analyzed. |
| ysis | Defines whether the gratings are analyzed by the Integral Method and/or the <br> Analyze by ... |

## 117 Spherical Lens Calculator

This calculator can be used for paraxial calculations based on the lens maker's equation as well as on the imaging equation of a spherical lens.

### 117.1 Lens Definition

In this page ( $\hookrightarrow$ Fig. 736), a spherical lens can be defined by using the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Embedding Medium | The medium the lens is supposed to be used in. |
| Lens Medium | The medium the lens is made of. |
| First Surface Type | The type (convex, concave, or planar) of the first lens surface. |
| First Surface Radius | The curvature radius of the first spherical lens surface. |
| Center Thickness | The center thickness of the lens, i.e. the distance of one surface vertex to the <br> other. |
| Second Surface Type | The type (convex, concave, or planar) of the second lens surface. |
| Second Surface Radius | The curvature radius of the second spherical lens surface. |



Figure 736. The Lens Definition page of the Spherical Lens Calculator
In the lower area of the dialog, some characteristic distances will be given for a certain Design Wavelength. These distances are:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Effective Focal Length | The effective focal length of the lens if used with the given Design Wavelength <br> inside the given Embedding Medium. |
| Front Focal Length | The distance from the front vertex to the front focal point. For a converging <br> lens, this will be negative. |
| Back Focal Length | The distance from the back vertex to the back focal point. For a converging <br> lens, this will be positive. |
| $\mathbf{V}_{\mathbf{1}} \mathbf{P}_{\mathbf{1}}$ | The distance of the front principal point measured from the front vertex. |
| $\mathbf{e}$ | The distance of the two principal points to each other. <br> $\mathbf{V}_{\mathbf{2}} \mathbf{P}_{\mathbf{2}}$ |

The calculations are based on the lens maker's equation:

$$
\begin{equation*}
1 / f=(n-1)\left(\frac{1}{r_{1}}-\frac{1}{r_{2}}\right)+\frac{d(n-1)^{2}}{n r_{1} r_{2}} \tag{117.1}
\end{equation*}
$$

with $f$ being the effective focal length, $n$ the ratio of the refractive indices of the lens medium and the embedding medium, $r_{1}$ the curvature radius of the first surface (positive if convex), $r_{2}$ the curvature radius of the second surface (positive if concave), and $d$ being the center thickness.

### 117.1.1 Setting a New Focal Length

If a certain effective, back, or front focal length shall be realized, the corresponding lens parameters can be calculated. By clicking Set to the right of the respective Effective/Back/Front Focal Length text box, a new dialog ( $\hookrightarrow$ Fig. 737) will open.


Figure 737. Dialog for setting a new focal length for the Spherical Lens Calculator

New Effective / Back / The desired focal length can be entered here.
Front Focal Length
Curvature Radius of the If this option is chosen and one of the surfaces is defined to be planar then Surfaces / Non-planar Sur- the curvature radius of the other surface which will realize the desired focal face length will be calculated.

If it is chosen and none of the surfaces is planar, the curvature radii of a symmetric lens will be calculated.

| Center Thickness | IN CASE OF A DESIRED EFFECTIVE FOCAL LENGTH, THIS OPTION IS AVAILABLE |
| :--- | :--- |
|  | ONLY IF BOTH OF THE LENS SURFACES ARE NON-PLANAR. |
|  | IN CASE OF A DESIRED BACK FOCAL LENGTH, THIS OPTION IS AVAILABLE ONLY |
|  | IF THE FRONT LENS SURFACE IS NON-PLANAR. |
|  | IN CASE OF A DESIRED FRONT FOCAL LENGTH, THIS OPTION IS AVAILABLE ONLY |
|  | IF THE BACK LENS SURFACE IS NON-PLANAR. |
|  | If this option is chosen, the center thickness which will realize the desired |
| effective focal length will be calculated. |  |

### 117.2 Paraxial Imaging with a Lens

Two equations are important for calculating distances and sizes for paraxial imaging.
The imaging equation describes the relation between the focal length $f$, the object distance $s_{0}$, and the image distance $s_{i}$ :

$$
\begin{equation*}
\frac{1}{f}=\frac{1}{s_{i}}-\frac{1}{s_{0}} \tag{117.2}
\end{equation*}
$$

while the magnification $y_{i} / y_{0}$ (i.e. the ratio of the image size $y_{i}$ to the object size $y_{o}$ ) is related to the object and image distance as follows:

$$
\begin{equation*}
y_{i} / y_{o}=\frac{s_{i}}{s_{0}} \tag{117.3}
\end{equation*}
$$

All possible dependencies of these four quantities $f, s_{0}, s_{i}$, and $y_{i} / y_{0}$ can be analyzed in the Imaging page of the calculator ( $\hookrightarrow$ Fig. 738).


Figure 738. The Imaging page of the Spherical Lens Calculator
There are two modes for using the calculations in this page:

- If Retrieve from Lens Definition is checked, the Effective Focal Length is copied from the Lens Definition page and cannot be altered here. If one of the three other quantities is changed, the two remaining values are calculated.
- If Retrieve from Lens Definition is unchecked, the button Select Constants allows to decide which two of the four quantities shall be kept constant while a new value is entered.


## 118 Vector \& Coordinate System Viewer

This tool serves the visualization of coordinate system base vectors which are rotated in relation to a reference coordinate system in the 3D space. It allows to understand the effect that has any value for any angle that belongs to any type of orientation definition. For an overview of all available orientation definition types see Sec. 139.2.


Figure 739. Vector \& Coordinate System Viewer

The following parameters can be specified:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Longitude/Latitude | The view direction can be set via the values of Longitude and Latitude. An <br> alternative is the rotation of the view by dragging via mouse inside the view. |
| Definition Type | The orientation definition type (see Sec. 139.2) can be chosen here. |
| Angle Phi / Theta / Alpha | The angles which belong to the definition types Spherical Angles, Direction |
| / Beta / Gamma / Rho / | Angles, and Cartesian Angles, resp. All these angles are used in order to <br> Sigma / Tau |
| define the orientation of the new z'-axis. The new directions of the x'- and <br> y'-axis are defined by rotating the original x-y-z-system about the node line <br> (marked blue in the view). The node line is the normal to the plane which is |  |
| spanned by the old z- and the new z'-axis. |  |

## 119 Waveplate Calculator

If a waveplate shall be designed with the objective of creating a certain phase retardation for polarized light of a given wavelength, then the correct thickness of the plate has to be known. The waveplate calculator (as shown in Fig. 740) serves that purpose.


Figure 740. Calculator for determining the thickness of a waveplate.
The following parameters have to be specified:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Design Wavelength The vacuum wavelength the waveplate shall be designed for. <br> Retardation <br> or Phase Difference can be set in the text-box as the desired value of retar- <br> dation. Otherwise, a pre-defined value can be set here: A Half Wave can be <br> chosen as well as a Quarter Wave which correspond to the well-known types <br> of common waveplates. <br> Medium The uniaxial, anisotropic medium the waveplate shall consist of. |  |
| Use Minimum Thickness | If checked, a minimum thickness for the waveplate can be defined. <br> In case a certain minimum thickness is given, the "absolute retardation" will <br> describe the absolute phase effect of a waveplate of the calculated thickness <br> on polarized light. This may be an integer multiple of the defined Retardation. |
| Calculated Thickness | The thickness a waveplate of the given Medium must have in order to produce <br> the desired Retardation. |

Please note: The formula for calculating the thickness is an approximation in that it only takes into account the optical path length differences for a single transition of light. Resonance effects due to multiple reflections are thus not included, although they naturally have an effect on the polarization of the transmitted light.

## XVI Export and Import

Different programs use different file formats. This part of the manual explains the most important file formats which can be imported into / exported from VirtualLab Fusion.

In the following all supported file formats are listed, grouped by the VirtualLab Fusion objects which can handle them.

| VIRTUALLAB FUSION OBJECT | SUPPORTED FILE FORMATS |
| :---: | :---: |
| Animations | - Export the current frame to various raster graphics formats (*.bmp, *.png, *.jpg). <br> - Export the whole animation as an animated GIF file (*.gif). $\hookrightarrow$ Sec. 123.1 <br> - Export the whole animation as a video file (*.avi). <br> - Create an overview image of all frames (*.bmp; *.jpg; *.png; *.tif). $\rightarrow$ Sec. 123.2 |
| Boundary Operators | - Export of Grating Cells Arrays to text file (*.csv) or GDSII Data (*.gds). $\rightarrow$ Sec. 126.1 <br> - Export of Prism or Mirror Cells Arrays to text file (*.csv) or stereolithography format (*.stl). $\leftrightarrows$ Sec. 126.2 |
| Coatings | Import of Macleod Coatings. $\hookrightarrow$ Sec. 128 |
| Chromatic Fields Sets | - Export to Field Information format (*.fin). $\lrcorner$ Sec. 122.1 <br> - Import of various raster graphics formats (*.bmp, *.png, *.jpg). $\leftrightarrows$ Sec. 122.2 |
| Data Arrays | - Export to text file (*.txt, *.csv). $\leftrightarrows$ Sec. 121.1 <br> - Import of various raster graphics formats (*.bmp, *.gif, *.png, *.jpg, ${ }^{*} . \mathrm{pcx}$, *.tif) and of text files (*.txt, *.csv, *.fin). $\lrcorner$ Sec. 121.2 |
| Harmonic Fields | - Export and import to various raster graphics formats (*.bmp, *.png, *.jpg, *.tiff). $\hookrightarrow$ Sec. 120.1 <br> - Export of current view to vector format (*.emf) <br> - Export and import of Field Information format (*.fin). $\hookrightarrow$ Sec. 120.2.1 <br> - Export and import of "ASCII" format (*.txt; *.csv). $\hookrightarrow$ Sec. 120.2.2 <br> - Export and import of "Code V" format (*.dat). $\hookrightarrow$ Sec. 120.2.3 <br> - Export and import of "Plain Text" format (*.ptf). $\hookrightarrow$ Sec. 120.2.4 <br> - Import of "Zemax OpticStudio® BeamFile" binary format (*.zbf). $\rightarrow$ Sec. 120.3 |
| Harmonic Fields Sets | - Export and import of Field Information format (*.fin). $\hookrightarrow$ Sec. 120.2.1 <br> - Export to various raster graphics formats (*.bmp, *.png, *.jpg). $\hookrightarrow$ Sec. 120.1.2 <br> - Import of various raster graphics formats (*.bmp, *.png, *.jpg). $\hookrightarrow$ Sec. 120.1.3.3, $\lrcorner$ Sec. 120.1.3.4 |
| Materials | Import from Zemax OpticStudio® Glass Catalogs (*.agf). $\hookrightarrow$ Sec. 129 |
| Optical Setups | - Export to XML / Batch Mode files / optiSLang Project $\lrcorner$ Sec. 124.1 <br> - Import Parameters from XML. $\hookrightarrow$ Sec. 43.6 <br> - Import of optiSLang Results. $\lrcorner$ Sec. 124.2 <br> - Export to JCMsuite format. $\hookrightarrow$ Sec. 124.3 <br> - Export to stereolithography format (*.stl) and to the IGES format (*.igs) via the 3D View. $\hookrightarrow$ Sec. 5.15 <br> - Import of Zemax OpticStudio® Lens File format (*.zmx, *.zos) and archive format (*.zar). $\hookrightarrow$ Sec. 124.4 |


| Real Components | - Export to stereolithography format ( ${ }^{*}$.stI) and to the IGES format ( ${ }^{*}$.igs) via |
| :--- | :--- |
|  | the 3D View. $\lrcorner$ Sec. 5.15 |

- An additional section Sec. 130 summarizes which obsolete VirtualLab Fusion files can be imported into which objects.
- Some dialogs allow an import / export to their own specific formats which are explained in the corresponding sections (e.g. snippets, $\hookrightarrow$ Sec. 7.3).
- The file formats native of VirtualLab Fusion are given in Sec. 4.1.


## 120 Export and Import of Field Data

### 120.1 Image Formats

## Restrictions of Image Formats

There are in principal two kinds of raster graphics images supported by VirtualLab Fusion:

- 24 bit RGB: 8 bit or 256 different levels per color channel (red, green, blue). Thus altogether more than 16 million colors are possible.
- 16 bit grayscale: 24 bit RGB images can only contain 256 gray levels, whereas 16 bit gray scale images support 65536 gray levels.
The maximum size of an image file is 4 gigabytes, which restricts the image size to roughly $36000 \times$ 36000 pixels for 24 bit RGB images and $44000 \times 44000$ pixels for 16 bit grayscale images.


### 120.1.1 Export Harmonic Fields to Images

When you export a Harmonic Field you are first asked for the file name and which of the three export variants you want (each leading to different possible file formats).

| IMAGE TYPE | DESCRIPTION |
| :---: | :---: |
| 24 bit RGB Raster Graphics | Exports the field into a red-green-blue color image. Supports the following file formats: Windows Bitmap file ( ${ }^{*}$.bmp); Portable Network Graphic ( ${ }^{*}$.png); JPEG File Interchange Format (*.jpg, *.jpeg); and Tagged Image File Format (*.tif, *.tiff). Opens the dialog described in Sec. 120.1.1.1. |
| 16 bit Grayscale Raster Graphics | 16 bit grayscale supports 65536 gray levels. Such a file can only be saved as Portable Network Graphic (*.png) or Tagged Image File Format (*.tif, *.tiff). This export uses the dialog described inSec. 120.1.1.1. |
| Vector Graphics | Exports the currently visible view to an Enhanced Windows Metafile (*.emf), a vector format. In this case a dialog to adjust export settings analog to Fig. 11.6.1 appears. |

### 120.1.1.1 Dialog for Export to Raster Graphics



Figure 741. The dialog for exporting a harmonic field to a raster graphics file.

The Field Quantity of one Vectorial Component will be exported but not the Light View. If you want to export the latter, please use the Copy View to Clipboard function ( $\hookrightarrow$ Sec. 11.6.1) instead. If you export a phase distribution, an analytical spherical phase radius is not exported.
If a 24 bit RGB image is to be generated you can configure the color mapping via the control described in $\hookrightarrow$ Sec. 5.11.
Additionally a preview is available which can be updated with the Preview button.
The bitmap size is automatically calculated from the number of sampling points of the field. The resolution of the resulting bitmap file is set according to the sampling distance.

### 120.1.2 Export Harmonic Fields Sets to Images

If the Light View ( $\hookrightarrow$ Sec. 12.2.1) is visible it will be exported to the specified file. If the Data View ( $\hookrightarrow$ Sec. 12.2.2) is visible the current Harmonic Field is exported as described in Sec. 120.1.1.

### 120.1.3 Import Harmonic Field Data from Bitmap Files

| Image Import Type |
| :--- |
| Select Type of Image Import |
| O Monochromatic (LUT based) |
| ORGB (False Color) |
| ORGB (Real Color) |
| OK |

Figure 742. Dialog to select how a bitmap shall be imported.
If you want to import a RGB raster graphics file, you can choose between three options:

| ITEM |  | DESCRIPTION |
| :---: | :---: | :---: |
| Monochromatic based) | (LUT | With the help of a so-called look-up table (LUT) the RGB values of the bitmap are converted to values of the selected field quantity and vectorial component. $\rightarrow \text { Sec. 120.1.3.1 }$ <br> There is also a special variant for importing an intensity distribution into the Diffractive Optics Package, $\leftrightarrows$ Sec. 120.1.3.2. |
| RGB (False Color) |  | The bitmap is imported into a polychromatic Harmonic Fields Set. Each of the channels R, G, and B is stored into one Harmonic Field. Their wavelengths can be set and weighted freely. $\rightarrow$ Sec. 120.1.3.3 |
| RGB (Real Color) |  | The bitmap is imported into a polychromatic Harmonic Fields Set in a way that guarantees the best color fidelity when viewed in the light view (in display mode Visual Perception). $\hookrightarrow$ Sec. 120.1.3.4 |

The following image formats are supported: Windows Bitmap file (*.bmp); Portable Network Graphic (*.png); JPEG File Interchange Format (*.jpg, *.jpeg); and Tagged Image File Format (*.tif, *.tiff). If you import a 16 bit grayscale image, the Monochromatic (LUT based) is started automatically.
The sampling distance of the resulting Harmonic Fields Set is calculated from the resolution stored in the file. For example the bitmap export of VirtualLab Fusion sets this value according to the original sampling distance. If no resolution is stored in the bitmap file the resolution of the screen is taken.

### 120.1.3.1 Importing Monochromatic Images

In order to understand then input parameters needed, the following technical details have to be considered. For importing a bitmap as one field quantity of a harmonic field, it is necessary to project a three-dimensional color vector to an one-dimensional subspace of the color space (here referred to as Color Scale). This allows a mapping of all values along the color scale to numerical values in an interval to be specified.
The color scale which determines the mapping from bitmap colors to numerical values has to be specified by the user. A gray scale is predefined, but the best result will be achieved if the same color scale will be used the bitmap has been created with.
Furthermore, using a middle color can have the effect that one color is assigned to two different values which yields unexpected results.


Figure 743. Options dialog for monochromatic bitmap import.
\(\left.$$
\begin{array}{ll}\text { ITEM } & \text { DESCRIPTION } \\
\hline \text { Vectorial Component } & \text { The vectorial component which is encoded in the bitmap data. } \\
\hline \text { Field Quantity } & \begin{array}{l}\text { The field quantity which is encoded in the bitmap data. After import, the se- } \\
\text { lected Field Quantity is shown by default. }\end{array} \\
\hline \text { Start Value } & \begin{array}{l}\text { The smallest value of the Field Quantity. The color at the left of the color scale } \\
\text { is assumed to be this value. }\end{array} \\
\hline \text { End Value } & \begin{array}{l}\text { The largest value of the Field Quantity. The color at the right of the color scale } \\
\text { is assumed to be this value. }\end{array} \\
\hline \text { Use Middle Color } & \begin{array}{l}\text { If checked, you can set a middle color for the color scale if the bitmap to be } \\
\text { imported is given in a three-color scale. }\end{array} \\
\text { Ouvelength } & \begin{array}{l}\text { The wavelength the generated harmonic field will have. } \\
\text { defined Table }\end{array}
$$ <br>
\hline If selected, the color table in the output's data view can be specified indepen- <br>

dently from the color scale used for the input mapping color \rightarrow value.\end{array}\right]\)| OnLY AVAILABLE IF OuTPUT CoLors FROM PREDEFINED TABLE HAS BEEN SE- |
| :--- |
| Output Colors From Input |
| Mapping | | LECTED. |
| :--- |
| If selected, the color scale used for the input mapping will be used as color |
| table in the output's data view as well. |

### 120.1.3.2 Importing Monochromatic Images as Intensity Distribution

For importing a bitmap as an intensity distribution, it is necessary to project a three-dimensional color vector $c$ to an one-dimensional subset of the color space (here referred to as Color Scale).
It is strongly recommended to use a color scale other than the predefined gray scale (i.e. luminance scale) only, if the bitmap has been created with the same color scale. Furthermore, using a middle color can have the effect that one color is assigned to two values which yields unexpected results.


Figure 744. Options dialog for importing intensities from a bitmap.
This import is only available for the Arbitrary Array Beam Splitter Session Editor as well as the Pattern Generating Diffuser Session Editor of the Diffractive Optics Package. It has the dialog shown in Fig. 744 with the following options.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Start Value | The smallest intensity. The color at the left of the color scale is assumed to be this value. |
| End Value | The largest intensity. The color at the right of the color scale is assumed to be this value. |
| Use Middle Color | If checked, you can set a middle color for the color scale if the bitmap to be imported is given in a three-color scale. |
| Mirror Horizontally | Applies transformation $f(x, y) \rightarrow f(-x, y)$, that is the data is mirrored horizontally by a mirror that corresponds to the y -axis. |
| Mirror Vertically | Applies transformation $f(x, y) \rightarrow f(x,-y)$, that is the data is mirrored vertically by a mirror that corresponds to the x -axis. |
| Transpose | Applies transformation $f(x, y) \rightarrow f(y, x)$, that is the data is mirrored by a mirror that corresponds to a diagonal in the $\mathrm{x}-\mathrm{y}$-plane. |
| Light Pattern Dimension | Only for Pattern Generating Diffuser Session Editor Allows you to specify the physical size of the imported light pattern. This can be done either by Specification of Sampling Distance of Light Pattern or by Specification of Size of Light Pattern. |
| Preview | If this button is pressed, a preview of the bitmap is (re)calculated. Recalculation is not done automatically as this can be very time-consuming. |

### 120.1.3.3 Importing False Color RGB Images

The result of the import process is a polychromatic harmonic fields set with three fields of three different wavelengths. These wavelengths can be determined and weighted by the user.


Figure 745. Options dialog for false color bitmap import.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Vectorial Component | The vectorial component the bitmap information shall be converted to. |
| Field Quantity | The field quantity the bitmap values stand for. |
| Wavelength $\mathbf{1 / 2 / 3}$ | The wavelengths of the three harmonic fields the bitmap channels are <br> matched with. |
| Weight | The (intensity) weight the channel is multiplied with. |
| Default RGB Values | By clicking this button the Wavelengths and Weights are set to the default <br> values. These are values which produce the most natural false color image. |
| Preview | By clicking this button you can see how the light view of the imported image (in <br> display mode Visual Perception) will look like using the current parameters. |

### 120.1.3.4 Importing Real Color RGB Images

The result of the import process is a polychromatic harmonic fields set with three fields of three different wavelengths. These wavelengths are determined from the used color system if Automatic is chosen. Then the light view (in display mode Visual Perception only, see Sec. 12.2.1) reproduces Hue and Saturation (H and S in the HSV color system) of the original image exactly (if no gamut errors occur). The Value (V in the HSV color system) may differ slightly due to the interpolation. This real color import is based upon a color transform from the bitmap's color space to the color space used in VirtualLab Fusion(usually 'VirtualLab Color Space').

| Image Import Type |  | $\times$ |
| :---: | :---: | :---: |
| Select Type of Image Import Monochromatic (LUT based) RGB (False Color) RGB (Real Color) <br> Real Color Import Wavelengths Automatic User Defined <br> Wavelength 1 $\square$ 700 nm <br> Wavelength 2 $\square$ 530 nm <br> Wavelength 3 <br> - $\square$ |  |  |
| OK | Help |  |

Figure 746. Options dialog for real color bitmap import.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic | Use three wavelengths that are suitable for the color system used for display, <br> so that minimal out-of-gamut errors occur. |
| User Defined | Choose three wavelengths (Wavelength $1 / 2 / 3)$ for the color space conver- <br> sion. Warning: There is a very high probability for out-of-gamut errors while <br> converting if these values differ from the automatically determined ones, so <br> the result's colors may look strange. |

### 120.2 Text Formats

### 120.2.1 Field Information Format

The Field Information format is the only text format capable of storing the complete field information (all modes and all field quantities).
It contains a header at the beginning of the file into which for example the wavelength, the embedding material, and the sampling distance are written. Each header line starts with a specific character, the header indicator. Then follows the field data whereas a complex number is written per sampling point. One row in the field data is written to one line of the resulting text file.
If the file to be exported is a harmonic fields sets with multiple modes or a locally polarized field, the data is split into multiple files bearing the same base file name followed by either "Mode\#\{number\}_\{wavelength\}" or "_Ex" / "_Ey".
The export and the import dialog for this format are explained in the following subsections.

### 120.2.1.1 Export Dialog



Figure 747. The export dialog for the field information format.

The export dialog ( $\hookrightarrow$ Fig. 747) for the Field Information format ( $\leftrightarrows$ Sec. 120.2.1) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Decimal Separator | You can either choose point or comma as decimal separator or enter an arbitrary character. |
| Column Separator | You can either choose one of the various predefined column separators or enter an arbitrary character. |
| Header Indicator | The first character of lines with additional information (e.g. the wavelength or the embedding material). |
| Format of Complex Numbers | The following formats are supported: <br> - Real Part / Imaginary Part: \{real part\} + i\{imaginary part\} <br> - Amplitude / Phase: \{amplitude\}• $\exp (\{$ phase $\} \cdot$ i) <br> - MATLAB, a more compact variant of the Real Part / Imaginary Part format: $\{$ real part $\}+\{i m a g i n a r y ~ p a r t\} i$ <br> - PTF, a format used for the PTF export ( $\neg$ Sec. 120.2.4): (\{real part\}, \{imaginary part\}) |
| Validity | This control ( $\leftrightarrows$ Sec. 5.10) shows a red-white cross and an info button if you enter an invalid decimal separator, column separator, or header indicator. |

### 120.2.1.2 Import Dialog



Figure 748. The import dialog for the field information format.

The import dialog ( $\hookrightarrow$ Fig. 748) for the Field Information format ( $\hookrightarrow$ Sec. 120.2.1) has the following controls.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Decimal Separator | You can either choose point or comma as decimal separator or enter an arbitrary character. |
| Column Separator | You can either choose one of the various predefined column separators or enter an arbitrary character. |
| Header Indicator | The first character of lines with additional information (e.g. the wavelength or the embedding material). |
| Format of Complex Numbers | The following formats are supported: <br> - Real Part / Imaginary Part: \{real part\} + i\{imaginary part\} <br> - Amplitude / Phase: \{amplitude\}•exp(\{phase\}•i) <br> - MATLAB, a more compact variant of the Real Part / Imaginary Part format: \{real part\}+\{imaginary part\}i <br> - PTF, a format used for the PTF export ( $\hookrightarrow$ Sec. 120.2.4): (\{real part\}, \{imaginary part\}) |
| 目 (View Text File) | Opens an additional dialog allowing you to take a look into any of the files to be imported. In this way you can for example see what column separator is the correct one ("»" indicates a tab character). |

At the top of the dialog the base file name is given. All files starting with the base file name are imported.

### 120.2.2 ASCII Format

Text files in "ASCII" format must consist of separated real numbers.
A single field quantity of a harmonic field can be exported to an "ASCII" text file. Every line of the exported ASCII text consist of separated real numbers which represent one row of the complex amplitude. Several header lines may be prepended with the following information.

- file creation date and time
- complex amplitude type (Harmonic Field or Jones Matrix Transmission)
- number of sampling points and sampling distance (Introduction of Part VIII)
- whether the complex amplitude has an imaginary component or not
- spherical phase radius ( $\hookrightarrow$ Sec. 12.1.1)
- the wavelength of the harmonic field
- the stored field component ( $\hookrightarrow$ Sec. 12.2.2.2) and field quantity ( $\hookrightarrow$ Sec. 11.1)

The first character on header lines is always "\#".

### 120.2.2.1 Export Dialog

The following options can be adjusted in the dialog displayed in Fig. 749.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Create header | Forces creation of a prepending header as described above. |
| Decimal Separator | Choose between "." and ",". <br> Column Separator <br> Choose either from a list of predefined characters or choose an arbitrary col- <br> umn separator by selecting Other. |
| Sets the field quantity to be exported from the harmonic field or transmission. |  |


| {Export to ASCII-File D: $\$ Example.trt} & $\times$ |  |  |
| :---: | :---: | :---: |
| Style of Exported ASCII File |  |  |
| $\square$ Create Header |  |  |
| Decimal Separator . (dot) |  |  |
| Column Separator tab | $\checkmark \square$ |  |
| Complex Amplitude Export Parameters |  |  |
| Vectorial Component | Ex | $\checkmark$ |
| Field Quantity | Real Part | $\checkmark$ |
| $\square$ Transpose Complex Amplitude |  |  |
| Remove Spherical Phase Factor from Sampling Points before Export |  |  |
| Ok | Cancel | Help |

Figure 749. Dialog to adjust options for ASCII export.

### 120.2.2.2 Import Dialog

There is a dialog offering several options to alter the way ASCII text is parsed ( $\hookrightarrow$ Fig. 750).

| ITEM | DESCRIPTION |
| :---: | :---: |
| $\begin{aligned} & \text { \{Complex Amplitude } \\ & \text { Type\} } \end{aligned}$ | Destination type of import: Transmission or Complex Amplitude Field. |
| Wavelength | Wavelength of the imported complex amplitude. |
| Complex Data | If checked the resulting complex amplitude stores real and imaginary part of the imported data. Otherwise only the real part is stored and the imaginary part is assumed to be zero. |
| Default Parameters | Resets the options above to their default values. |
| Vectorial Component Field Quantity | The data can be imported either to the Ex Component or the Ey Component. Choose the field quantity of the complex amplitude to be imported. After import, the selected Field Quantity is shown by default. Note that you can import e. g. phase values even if Complex is switched off: the imported values are written into the phase of complex numbers from which then only the real part is stored. |
| Transpose | The imported data is transposed, i.e. the rows in the data represent the $y$ dimension of the imported data and the columns in the data represent the $x$-dimension. |
| Skip Header Lines | Feature to skip a given number of lines at the beginning of the file. |
| Skip Lines Starting with | Feature to skip lines starting with the given character. |
| Decimal Separator | Choose between "." and ",". |
| Column Separator | Choose form list of predefined characters or enter custom one. |
| Preview | A preview panel supports the user to verify settings. It shows the currently selected Field Quantity. |
| \{First Lines of Imported File\} | Table showing the first lines of the imported text file as parsed by VirtualLab Fusion. Cells that cannot be parsed are marked red. |



Figure 750. Dialog to adjust options for ASCII import.

### 120.2.2.3 Dialog for Import of Intensities



Figure 751. Options dialog for importing intensities from an ASCII file.

This import is only available for the Arbitrary Array Beam Splitter Session Editor as well as the Pattern Generating Diffuser Session Editor of the Diffractive Optics Package. It has the dialog shown in Fig. 751 with the following options.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Skip Header Lines | Feature to skip a given number of lines at the beginning of the file. |
| Skip Lines Starting with | Feature to skip lines starting with the given character. |
| Decimal Separator | Choose between "." and ",". |
| Column Separator | Choose form list of predefined characters or enter custom one. |
| Mirror Horizontally | Applies transformation $f(x, y) \rightarrow f(-x, y)$, that is the data is mirrored hori- <br> zontally by a mirror that corresponds to the y-axis. |
| Mirror Vertically | Applies transformation $f(x, y) \rightarrow f(x,-y)$, that is the data is mirrored verti- <br> cally by a mirror that corresponds to the x-axis. |
| Transpose | Applies transformation $f(x, y) \rightarrow f(y, x)$, that is the data is mirrored by a <br> mirror that corresponds to a diagonal in the x-y-plane. |
| Light Pattern Dimension | OnLY FOR PATTERN GENERATING DIFFUSER SESsIoN EDITOR |
|  | Allows you to specify the physical size of the imported light pattern. This can <br> be done either by Specification of Sampling Distance of Light Pattern or by <br> Specification of Size of Light Pattern. |
| Preview | If this button is pressed, a preview of the bitmap is (re)calculated. Recalcula- <br> tion is not done automatically as this can be very time-consuming. |
| \{Preview of First Lines of | Table showing the first lines of the imported text file as parsed by VirtualLab <br> Imported File |

### 120.2.3 Code V Format

Code V files consist of two parts: the header contains information like data type and wavelength and so on, and the following second part contains the actual data. Lines starting with a '!' are ignored.
The header lines include the following information:

- creation date and exported field components as comments
- data type
- wavelength
- real part of the complex refractive index of the medium in which the harmonic field is embedded.
- grid spacing (in VirtualLab Fusion: sampling distance)
- array size (in VirtualLab Fusion: sampling points)

Note that the data is always exported as Code V DataType VGridSpatial, i. e. with 6 values per sampling point (real and imaginary part of $E_{x}, E_{y}$, and $E_{z}$, respectively). Each row of the field data in VirtualLab Fusion is exported to one line in the Code V file.
There is neither an export nor an import dialog for this text format.

### 120.2.4 Plain Text Format

PTF files use a special format to store complex or real fields: The first three lines contain header information including the date of creation. The first character on header lines is always "\#". The fifth line indicates the size of the field; for instance "128 128". All following lines until end of file store sampling points; beginning at the bottom left and ending at the top right corner of the complex amplitude. There are two different formats for representing either real or complex sampling points:

- Complex values $\rightarrow(\operatorname{Re}($ value $), \operatorname{Im}($ value $))$.
- Real values $\rightarrow$ value.

Of course, all elements of a file must have the same representation.

During import a dialog asks for the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| \{Complex Amplitude <br> Type\} | Destination type of import: Transmission or Complex Amplitude Field. |
| Wavelength | Wavelength of the imported complex amplitude. |
| Complex Data | If checked the resulting complex amplitude stores real and imaginary part of <br> the imported data. Otherwise only the real part is stored and the imaginary <br> part is assumed to be zero. |
| Default Parameters | Resets the options above to their default values. |

### 120.3 Zemax OpticStudio® Beam File Binary Format

Zemax OpticStudio® Beam Files are stored either in text format or in binary format. VirtualLab Fusion is able to import beam files in binary format. After importing the data of a *.zbf file into a harmonic field, some additional data are written into the messages tab. Furthermore, there is the possibility to let VirtualLab Fusion calculate the irradiance ( $\leftrightarrows$ Sec. 137.5.3) for the imported field data.

## 121 Export and Import of Data Arrays

### 121.1 Export of Data Arrays

One subset of a VirtualLab Fusion Data Array can be exported to a text file in "ASCII" format ( $\leftrightarrows$ Sec. 120.2.2). Fig. 752 shows the configuration dialog for this export. The current implementation of VirtualLab Fusion supports only the export of 1D and 2D data arrays that are equidistant.
Export Data Array
File Name
C:IProgramDatalWyrowski PhotonicsIVirtualLab Fusionl2
Data Array Export Parameters
Subset to Export
Quantity to Export
Real Part
Text Export Settings
Decimal Separator
Column Separator
Header Indicator

Figure 752. The dialog to specify the text export for data arrays.
The following parameters can be specified:

| ITEM | DESCRIPTION |
| :--- | :--- |
| File Name | The user can specify the file name which shall be used to export the selected <br> subset and the selected quantity. |
| Subset to export | You can specify which subset shall be exported. This option is only available <br> if the data array has more than one subset. Otherwise the single subset within <br> the data array will be exported. |
| Quantity to export | If the selected data subset is complex the user can specify which quantity shall <br> be used for the export. The user can select between real part, imaginary part, <br> amplitude, phase or squared amplitude. |
| Decimal Separator | You can either choose period or comma as decimal separator or enter an <br> arbitrary character. |
| Column Separator | You can either choose one of the various predefined column separators or <br> enter an arbitrary character. |
| Header Indicator | The ASCII export allows you to export additional information of the data ar- <br> ray. These information (including sampling distance and number of sampling <br> points) are shown at the beginning of the resulting text file in lines starting <br> with the specified Header Indicator. |

This dialog uses a validity indicator ( $\hookrightarrow$ Sec. 5.10 ) which shows a red-white cross and an info button if you enter an invalid decimal separator, column separator, or header indicator. Furthermore it shows a warning if the specified file already exists.

### 121.2 Import of Data Arrays

VirtualLab Fusion allows you to import one or more bitmap and text files into one object called Numerical Data Array (this general data storage concept is explained in Sec. 13). The following bitmap formats are supported:

- Windows bitmap files (*.bmp)
- Graphics Interchange Format files (*.gif)
- JPEG file interchange format (*.jpg, *.jpeg)
- Portable network graphics (*.png)
- Picture exchange files (*.pcx)
- Tagged Image File Format files (*.tif, ${ }^{*} . t i f f ;$ can also be 16 bit grayscale images)

A text file may have the extensions .txt, .csv, or .fin but must be a one- or two-dimensional array of real numbers. For the import, a wizard dialog has to be used. It provides the settings explained in the following:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Wl\| Save Import Settings | Allows you to store the current settings so that you can re-use them on another computer or after a restart of VirtualLab Fusion. |
| Load Import Settings | Loads previously stored import settings. |
| (3) Reset Dialog | Resets the dialog to its initial state. |
| Dimensionality | On the first page, you can set up whether you want to import One-Dimensional or Two-Dimensional data. Furthermore, it has to be specified whether the Data are Complex-Valued or Data are Real-Valued. |
| Subset import table | Data arrays may consist of more than one subset ( $\rightarrow$ Sec. 13). Each subset can be configured individually with the table on the second page (see Fig. 753). This table including the Add Subset and Delete Last Subset buttons is described in Sec. 121.2.1. |
| x-Axis / <br> $y$-Axis | These controls on the third page allow you to set up the coordinate axes of the data array. It is assumed that equidistant coordinates are used. See Sec. 121.2.3 for details on these controls. For one-dimensional data arrays only the $x$-Axis control is shown. |
| Next > 1 <br> Finish | Switches to the next page or starts the actual import (on the last page). In the case any settings in the dialog are incorrect, this button is disabled until the error is corrected. |

121.2.1 Import of Subsets


Figure 753. The table containing the import settings of the individual data files. An error message is shown here, because one file is still to be defined.

Data arrays can consist of more than one subset ( $\leftrightarrows$ Sec. 13). The subsets can be real- or complex-valued (either all are real-valued or all are complex). In the latter case, two data files are needed to describe either the Amplitude / Phase or the Real / Imaginary part of the complex values. Thus, the import of a data array can require the import of several data files. The table control shown in Fig. 753 comprises one row per data file and the following columns.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Subset \# | The index for each of the subsets. |
| Description | This column allows you to give a (short) description for the imported data, for <br> example "Ex field data". |
| Physical Property | The physical property (e. g. Electrical Field Strength) of the imported data. If <br> the complex Interpretation is set to Amplitude / Phase, the phase data has <br> always the physical property Angle (Rad). |
| Interpretation | In case of complex-valued data, you can specify the interpretation of the files <br> to be imported. If you select Amplitude / Phase, the first row of the subset will <br> contain the amplitude data and the second row the phase data. If you select <br> Real / Imaginary, the first row of the subset will contain the data for the real <br> part of the complex values and the second row for the imaginary part. |
| File Import | Opens a dialog for choosing a file and configuring the import settings for either <br> text or bitmap files. See Sec. 121.2 .2 for details. The same dialog is shown <br> automatically if a new file needs to be imported, i.e. <br> • this table control is shown for the first time or <br> • a new subset is added. |
| File Name | This read-only column gives the name of the file containing the actual data. |
| Fata Points your information, this read-only column gives the number of data points |  |
| which are extracted from the given file. This value must be the same for all |  |
| rows of the table. Otherwise an error message will be shown beneath the |  |
| table. |  |

Below the table, there are two buttons to add a new subset or to delete the last subset from the table. If the already imported data are inconsistent, an error message is shown beneath the table.

### 121.2.2 Import Settings for one Data Array Subset



Figure 754. The dialog comprising the settings needed to import a (bitmap) file to a data array. (The imported image was provided by Ricardo Cancho Niemietz via English Wikipedia as public domain.)

The dialog to import a file to a data array ( $\hookrightarrow$ Fig. 754) contains the following sections.

| ITEM | DESCRIPTION |
| :--- | :--- |
| File Name | Shows the file name and allows you to change it via the -button. |
|  | Supported file extensions: .txt, .csv, .jpeg, .jpg, .bmp, .png, .pcx, .gif, .tif, .tiff. |
|  | Text files must be a one- or two-dimensional array of real numbers. |
| Specific import settings | The settings specific for bitmap files are described in subsection <br>  <br>  <br>  <br>  <br>  <br> Sec. 121.2.2.1. <br> The settings specific for text files are described in subsection Sec. 121.2.2.2. |
|  | The preview on the right part of the dialog is actually a data array view de- <br> scribed in Sec. 13.5. Initially no preview is shown - you must click Refresh <br>  <br>  <br> Preview to create the preview, which may take some time. |

### 121.2.2.1 Specific Import Settings for Bitmap Files



Figure 755. The specific import settings for bitmaps (with annotations).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Color Range | You can configure the Color Scale of the imported file by clicking the color but- <br> tons for the Start Color and End Color, respectively. If you have checked Use <br>  <br> Additional Middle Color you can also configure a Middle Color. It is strongly <br> recommended to use a color scale other than the predefined gray scale (i. e. <br> luminance scale) only, if the bitmap has been created with the same color <br> scale. Furthermore, using a middle color can have the effect that one color is <br> assigned to two values which yields unexpected results. |
| Corresponding | ValueA pixel having exactly the Start Color is assigned the Start Value of the value  <br> Range range. In the same manner, a pixel having exactly the End Color is assigned <br> the End Value of the value range. Other colors within the color range get a <br>  corresponding value between Start Value and End Value. Colors outside of <br> the specified color scale are first projected to the nearest point of the color <br> scale (in RGB space). |

### 121.2.2.2 Specific Import Settings for Text Files



Figure 756. The specific import settings for text files.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Number of Header Lines <br> to Skip | The specified number of lines on the beginning of the document (which may <br> contain header information) are skipped. |
| Skip Lines Starting with | If checked, any line starting with the specified character is skipped. It is rec- <br> ommended to not combine this option with Number of Header Lines to Skip. |
| Decimal Separator | You can either choose period or comma as decimal separator or enter an <br> arbitrary character. |
| Column Separator | You can either choose one of the various predefined column separators or <br> enter an arbitrary character. |

Note that the row separator is always a line break. Numbers can be either given in normal format (e.g. 1234 or in scientific format (e.g. 1.234e3). If in a non-skipped row there is any character which is not a number, a space, a decimal separator or a column separator, the import will fail. Multiple consecutive column separators (e. g. spaces) will be treated as one.

### 121.2.3 Control for Configuring an Axis of a Data Array



Figure 757. Control for configuring one axis of a data array.

The control for defining the coordinate axis of a data array (Fig. 757) has the following settings.

| ITEM | DESCRIPTION |
| :---: | :---: |
| Description | The caption of the coordinate axis. |
| Physical Property | The physical property (e.g. Length) of the coordinates. An overview of all supported physical properties and the corresponding units is given in Sec. 5.1. |
| Interpolation Method | The type of interpolation which is used if a value between adjacent sampling points has to be interpolated. The available interpolation methods are listed in Sec. 13.2.2. |
| Dimensions | The dimensions along the axis can be determined either via Sampling Distance, Array Size, or Coordinate Extent. |
| Sampling Distance | The distance between two adjacent coordinates. |
| Array Size <br> Coordinate Extent | The distance between the coordinates of the first and the last data point. <br> Available only if the Interpolation Method is set to Nearest NeighBOR. <br> The distance between the lower boundary of the nearest neighbor interval of the first data point and the upper boundary of the interval of the last data point. |
| Positioning | The position of the axis can be determined either via entering a Start Coordinate or by defining that the axis range shall be centered. This can be done referring to the exact center (Center Around Zero) or to the coordinate of the data point which has the next higher coordinate to the exact center (Center Around Zero Node). |
| Center Around Zero | If chosen, the coordinate range will be centered around 0 . |
| Center Around Zero Node | For an odd number of sampling points, this will be the same as CenterAround Zero. If chosen for an even number $N$ of sampling points, the coordinate range will be set in the following way: That sampling point whose (zero based!) index equals $N / 2$ will get the coordinate 0 . |
| Start Coordinate | The coordinate of the first sampling point. |
| Equals minimum boundary of first interval | Available only if the Positioning mode is set to Sampling Distance and the Interpolation Method is set to Nearest Neighbor. <br> If checked, the start coordinate refers to the lower boundary of the nearest neighbor interval of the first data point instead of the coordinate of the first data point itself. |

## 122 Export and Import of Chromatic Fields Sets

### 122.1 Field Information Format for Chromatic Fields Sets

Chromatic Fields Sets can be exported into a slightly modified Field Information format ( $\hookrightarrow$ Sec. 120.2.1). It contains a header at the beginning of the file into which for example the wavelength and the sampling distance are written. Each header line starts with a specific character, the header indicator.
Then follows the actual data whereas a number (the squared amplitude) is written per sampling point. One row in the field data is written to one line of the resulting text file.
Distinct wavelengths are exported into distinct file bearing the same base file name followed by the wavelength. The export dialog for this format is explained in the following subsection.

### 122.1.1 Export Dialog

| Export Chromatic Fields Set |  |  |
| :---: | :---: | :---: |
| File Name |  |  |
| C:IProgramData\Wyrowski PhotonicsiVirtualLab Fusion\C... |  |  |
| Chromatic Fields Set Export Parameters |  |  |
| Data to Export | Single Wavelength | $\checkmark$ |
| Wavelength to Export | 473 nm | $\checkmark$ |
| Text Export Settings |  |  |
| Decimal Separator | (period) | $\checkmark$ |
| Column Separator | (tab) | $\checkmark$ |
| Header Indicator | \# |  |
| Validity: () | Cancel | Help |

Figure 758. The export dialog for Chromatic Fields Sets.

The export dialog ( $\hookrightarrow$ Fig. 758) for the Field Information format ( $\hookrightarrow$ Sec. 122.1) has the following controls.

| ITEM | DESCRIPTION |
| :--- | :--- |
| File Name | Shows the current file name. Via the button you can browse to the place <br> where you want to store the file and change the actual file name. |
| Data to Export | OnLY FOR ChROMATIC FIELDS SET WITH MORE THAN ONE WAVELENGTH <br> You can either export All Wavelengths into separate files, select a Single <br> Wavelength to export or export the (incoherent) Summation of the data of <br> all wavelengths. |
| Wavelength to Export | OnLY In Summation mODE FOR CHROMATIC FIELDS SET wITH MORE THAN ONE <br> WAVELENGTH <br> Allows you to select one distinct wavelength of the Chromatic Fields Set to <br> export. |
| Decimal Separator | You can either choose period or comma as decimal separator or enter an <br> arbitrary character. |
| Column Separator | You can either choose one of the various predefined column separators or <br> enter an arbitrary character. |
| Header Indicator | The first character of lines with additional information (e.g. the wavelength or <br> the sampling distance). |
| Validity | This control ( $\leftrightarrows$ Sec. 5.10$)$ shows a red-white cross and an info button if you <br> enter an invalid decimal separator, column separator, or header indicator. |

### 122.2 Import a Chromatic Fields Set from Bitmap Files



Figure 759. Dialog to select how a bitmap shall be imported.

If you want to import a bitmap file into a Chromatic Field Set, you can choose between two options:

| ITEM | DESCRIPTION |
| :--- | :--- |
| RGB (False Color) | Each of the channels R, G, and B is stored into one subset of the Chromatic |
|  | Fields Set. Their wavelengths can be set and weighted freely. $\hookrightarrow$ Sec. 122.2.1 |
| RGB (Real Color) | The bitmap is imported in a way that guarantees the best color fidelity <br> when the resulting Chromatic Fields Set is viewed in the real color mode. <br>  <br> $\hookrightarrow$ Sec. 122.2.2 |

Three bitmap formats are supported: Windows bitmap files (.bmp), JPEG images (.jpg, .jpeg), and portable network graphics (.png).
The sampling distance of the resulting Chromatic Fields Set is calculated from the resolution stored in the file. For example the bitmap export of VirtualLab Fusion sets this value according to the original sampling distance. If no resolution is stored in the bitmap file the resolution of the screen is taken.

### 122.2.1 Importing False Color RGB Images

The result of the import process is a Chromatic Fields Set with three fields of three different wavelengths. These wavelengths can be determined and weighted by the user.


Figure 760. Options dialog for false color bitmap import.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Wavelength $\mathbf{1 / 2 / 3}$ | The wavelengths of the three harmonic fields the bitmap channels are <br> matched with. |
| Weight | The (intensity) weight the channel is multiplied with. |
| Default RGB Values | By clicking this button the Wavelengths and Weights are set to the default <br> values. These are values which produce the most natural false color image. |
| Preview | By clicking this button you can see how the real color view ( $\hookrightarrow$ Sec. 14.2) of <br> the imported image will look like using the current parameters. |

### 122.2.2 Importing Real Color RGB Images

The result of the import process is a Chromatic Fields Set with three fields of three different wavelengths. These wavelengths are determined from the used color system if Automatic is chosen. Then the real color view ( $\hookrightarrow$ Sec. 14.2) reproduces Hue and Saturation (H and S in the HSV color system) of the original image exactly (if no gamut errors occur). The Value (V in the HSV color system) may differ slightly due to the interpolation. This real color import is based upon a color transform from the bitmap's color space to the color space used in VirtualLab Fusion(usually 'VirtualLab Color Space').


Figure 761. Options dialog for real color bitmap import.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Automatic | Use three wavelengths that are suitable for the color system used for display, <br> so that minimal out-of-gamut errors occur. |
| User Defined | Choose three wavelengths (Wavelength 1/2/3) for the color space conver- <br> sion. Warning: There is a very high probability for out-of-gamut errors while <br> converting if these values differ from the automatically determined ones, so <br> the result's colors may look strange. |

## 123 Export of Animations

Via File > Export you can

- export the current frame of the animation to a bitmap, .png, or .jpg file
- export the whole animation as an animated GIF file ( $\hookrightarrow$ Sec. 123.1)
- export the whole animation as an .avi video file. Note that for technical reasons the frames per second set up in the options dialog ( $\hookrightarrow$ Sec. 20.3) are rounded internally to the next integer or
- create an overview image of all frames ( $\hookrightarrow$ Sec. 123.2).


### 123.1 Export as Animated GIF

Animated GIF files have two limitations:

1. The GIF format uses a color palette of 256 colors only, so the bitmaps in the animation (which use true colors) have to be converted. Thus if you start the export to animated GIF files, you are first asked whether you want to use an Adaptive color scale which generates a palette of 256 colors so that the converted bitmaps differ as little as possible from the original ones - or a Grayscale which uses 256 shades of gray, i. e. only the brightness information of the bitmaps in the animation is maintained.
2. The frame duration is taken from the animation options ( $\leftrightarrows$ Sec. 20.3). However, GIF is limited to frame durations being a multiple of 10 milliseconds. If this is not the case rounding is done automatically and a warning is shown.

After deciding about the color scale you can specify the name of the exported file.

### 123.2 Overview Image of an Animation



Figure 762. Edit dialog for creating an overview image of an animation.

Via File > Export > Overview Image you can create an image which shows all (or some, depending on the configuration) frames of an animation side by side - like an index print. In the corresponding edit dialog ( $\hookrightarrow$ Fig. 762) you can configure the following.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Layout | As an information, the number of frames in the animation is shown and the size of <br> the resulting image. You can set the general Layout, i. e. the number of columns <br> and rows into which the frames are written. If the number of frames does not match <br> the number of columns times the number of rows, a warning is shown by the Validity <br>  <br> Control in the bottom left corner of the dialog ( $\hookrightarrow$ Sec. 5.10$).$ |
|  | Furthermore you can define an additional Space Between Frames to separate the <br> columns and rows. It is filled with an transparent color. |
| Stitching Order | Defines the order in which the individual frames are written into the columns and <br> rows. A table below illustrates the different settings. <br> Stitch Horizontally First means that one row is filled before a new row is started. <br> Stitch Vertically First means that one column is filled before a new column is started. <br> Start at Top / Bottom defines whether first the top most row is filled or the bottom <br> most one. |
| Result is saved at... | With the $/$ button you can set the path and name of the resulting overview image. <br> The extension of the file name defines the used image codec (bitmap, PNG with <br> lossless compression, JPG with lossy compression, or TIF). |

The following table illustrates how the different stitching orders influence the location of 6 frames on a $3 \times 2$ layout.

|  | Stitch Horizontally First | Stitch Vertically First |
| :--- | :--- | :--- |
| Start at Top | $1 ; 2 ; 3$ | $1 ; 3 ; 5$ |
|  | $4 ; 5 ; 6$ | $2 ; 4 ; 6$ |
| Start at Bottom | $4 ; 5 ; 6$ | $2 ; 4 ; 6$ |
|  | $1 ; 2 ; 3$ | $1 ; 3 ; 5$ |

## 124 Export and Import of Optical Setups

Optical Setups can be used easily from within other programs using the batch mode described in Sec. 9. Sample batch mode files can be generated using File > Export > Create Batch Mode Files. The menu File > Export contains also various exports to specific target applications which are described in the following subsections. Optical Setups can also be exported into the stereolithography format (*.stl) via the 3D View ( $\hookrightarrow$ Sec. 5.15).

### 124.1 Export Parameters to XML

Most parameters of an Optical Setup can be exported to an XML file. Some of these are changeable, which means they can be re-imported into VirtualLab Fusion when changed in the XML file. And some of the changeable numerical parameters are also variable which means their value can be varied within a certain range. See also the chapter about Parameter Extraction Sec. 43.5.
For each parameter the following information is exported.

| TAG | DESCRIPTION |
| :--- | :--- |
| Name | Name and category of the parameter. If changed, re-import into VirtualLab <br> Fusion might fail. |
| ID | OnLY FOR CHANGEABLE PARAMETERS <br> Facilitates re-import into VirtualLab Fusion. |
| ShortName | OnLY FOR VARIABLE PARAMETERS <br> User-specified short name, e.g. set in the dialog described in Sec. 124.1.1. <br>  <br>  <br> Not used during re-import. |
| Value | OnLY FOR VARIABLE PARAMETERS <br> Indicates a parameter preselected by the user, e.g. via the dialog described <br> in Sec. 124.1.1. Not used during re-import. |
| PhysicalProperty | The value of the parameter. |
| OnLY FOR PHYSICAL vALUES |  |
| Min | The physical property of the value. Not used during re-import. |
| OnLY FOR VARIABLE VALUES |  |
| The minimum of the range in which the value can be varied. Can be set in |  |
| the dialog described in Sec. 124.1.1. Not used during re-import. |  |

In addition at the begin of the XML document the notes ( $\hookrightarrow$ Sec. 43.1) and all available simulation engines ( $\hookrightarrow$ Sec. 43.4) of the Optical Setup are given. As the available parameters depend on the selected simulation engine, the selected engine is marked by an Used tag.
The XML export can be triggered in three different ways.

## RIBBON ITEM

File > Export > Export as Exports all parameters. You only have to specify path and name of the XML XML

File > Export > Create Creates a parameters.xml file in the specified path and a sample batch file

## DESCRIPTION

 file. for external execution of VirtualLab Fusion. See Sec. 9 for details on the available command line arguments. The XML file contains only changeable parameters of Optical Setup Elements which are connected to the active light source (with index "0").File > Export > Export to Special variant of the batch mode export specifically tailored for optiSoptiSLang Project

Lang. Only variable parameters are exported from Optical Setup Elements which are connected to the active light source (with index "0"). The Optical Setup is executed during export to generate initial results. A special dialog ( $\hookrightarrow$ Sec. 124.1.1) is used to configure the export.

The parameter values in an XML file can be re-imported into an Optical Setup using an Optical Setup Tool ( $\hookrightarrow$ Sec. 43.6).

### 124.1.1 Export to optiSLang Project



Figure 763. Edit dialog for the export to an optiSLang project.
If you click on File > Export > Export to optiSLang Project the dialog shown in Fig. 763 opens where you can configure the export.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Export Folder | The folder into which the files needed for the optimization in optiSLang are ex- <br> ported. It is recommended that this folder is empty. The path can be changed <br> with the <br> you can click on the path label. |
| Simulation Engine | Allows you to select the simulation engine to be used for the optimization in <br> optiSLang. |
| Export Only Varied Param- |  |
| eters | If checked only the varied parameters are exported. This yields a much <br> smaller parameter file and thus much faster execution times. |
| \{Parameter Table\} | See below. |
| Validity | This control ( $\hookrightarrow$ Sec. 5.10 ) indicates whether there are issues with the current <br> configuration. If this is the case you can click on the <br> information. |

The table lists all Parameters of all Objects which can be altered in optiSLang. Often, a Category column is available to group similar parameters.
For each parameter you can specify a Short Name identifying that parameter.
In the Vary column you must select one or more parameters which you want to alter in optiSLang. For these parameters you can define the value range by setting the start (From) and end (To) value. The default From and To values for all parameters are their absolute minimum and maximum values - you must not enter a value outside of this range. It is possible to enter a To value which is smaller than the From value. For your information also the Original Values of all parameters are given.
The first column allows you to collapse/expand all parameters of an Optical Setup Element or its categories. Simply click on the $\square$ and $\boxplus$ symbols, respectively. At the top of this column you can select to collapse all levels (1), collapse only the Category level (2) or show all levels (*).

The table can be filtered with the following controls. Only rows passing all filters are shown.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Filter Table by | All rows containing the given string either in the Object, Category (if applica- <br> ble) or the Parameter column pass this filter. The matching is case insensi- <br> tive. It is possible to search for multiple words and word groups embraced by <br> quotation marks, for example: "surface \#1" scaling. |
| Show Only Varied Param- <br> eters | Only rows where the Vary column is checked pass this filter. |

### 124.2 Import optiSLang Results

If you click on File > Import > Import optiSLang Results a dialog opens where you can either enter a path directly or browse for it using the $\square$-button. This path must contain a system.lpd and a matching parameters. xml in the format used for the data exchange with optiSlang and the batch mode ( $\leftrightarrows$ Sec. 9). The parameters of the Optical Setup are then changed to the values in the parameters.xml and the resulting Optical Setup is shown as new document in VirtualLab Fusion.
Using this import you can re-import Optical Setups optimized by optiSLang.

### 124.3 Export to JCMsuite Format

Grating Optical Setups can be converted to JCMsuite files. These files allow you to analyze the structures rigorously by using the finite element method within JCMsuite. (In case of 2D-periodic structures, only the plane at $y=0$ is exported.)

| Settings for Export to JCMsuite Format | $\times$ |
| :---: | :---: |
| Output Path |  |
| C:\ProgramData $\backslash$ Wyrowski Photonics $\backslash$ VirtualLab Fusion\} | $\square$ |
| $\checkmark$ Assume Periodic Structure Definition |  |
| OK Cancel | Help |

Figure 764. The dialog for configuring the export to JCMsuite files.
This feature can be accessed via File > Export > Export to JCMsuite Format if a Grating Optical Setup is active. This menu item opens the dialog shown in Fig. 764 and offers the following settings.

| ITEM | DESCRIPTION |
| :--- | :--- |
| Output Path | Specifies the path where the resulting JCMsuite files are stored. You can <br> either enter the path directly. If the path does not exist, it is created on in- <br> quiry. Or you can access the default Windows ${ }^{T M}$ folder selection dialog via <br> the |
| Assume |  |
| ture Definition |  |$\quad$| JCMsuite can assume the outside of the structure to be either periodic or |
| :--- |
| transparent. With this setting you can switch between these two possibilities. |

### 124.4 Import of Zemax OpticStudio® Lens Files and Archive Files

File > Import > Import 'Zemax OpticStudio®' Lens File imports the surface data from a *.zmx, *.zos, or *.zar file into an Optical Setup.

## Zemax OpticStudio® license needed

The import of *.zmx or *.zar files requires a valid Zemax OpticStudio® license of version '19.4 SP2' or newer. Importing *.zos files requires a version '21.3' or newer. It has to be a 'Professional' or 'Premium' edition in any case, a 'Standard' edition will not work.
If no valid license can be found or the Global Options are configured accordingly ( $\hookrightarrow$ Sec. 6.16), VirtualLab Fusion may use a rudimentary import algorithm on *.zmx files which may produce unsatisfactory results. Import features which are not supported by the rudimentary algorithm are marked with the symbol zos Lic.

A new Optical Setup will be created by the import algorithm. It contains a light source, a Camera Detector as well as a Spot Size detector. All surfaces except for the object plane, the image plane and coordinate breaks will be imported into a VirtualLab Fusion component each (see below for a list of supported surface types). The media between the Optical Setup Elements are set to "Air (Zemax OS)" but the materials which are connected to the surfaces in the lens file are imported to VirtualLab Fusion materials (Sec. 124.4.2) and are used as subsequent media. Temperature and pressure are copied from the Zemax OpticStudio® lens file to the Optical Setup too (Sec. 124.4.3).
The type of the light source in the imported Optical Setup depends on the distance behind the object plane. If it is infinite, a Plane Wave light source is used, otherwise a Spherical Wave light source is inserted. The material behind the object plane determines the embedding medium of this source. The wavelengths of the light source are set to the wavelengths as found in the file after converting to vacuum. The field size is taken from the entrance pupil diameter. The ray pattern and the ray density for a ray tracing source are copied from a spot diagram, if there is one in the lens file.

### 124.4.1 Supported Zemax OpticStudio® Surface Types

VirtualLab Fusion can import some types of optical surfaces from a Zemax OpticStudio® lens file. The supported surface types are summarized in the following table:

## SURFACE TYPE IN ZEMAX REPRESENTATION IN VIRTUALLAB FUSION OPTICSTUDIO®

| Biconic | Anamorphic Surface |
| :---: | :---: |
| Binary 1 | A Combined Surface, consisting of a Plane or Aspherical Surface and a Polynomial Surface. The latter may be height-scaled, see 124.4.1.1 for more information. |
| Binary 2 | Two cases have to be distinguished: |
|  | - Valid OpticStudio® license present ${ }^{[205 L T}$ and Flat Lens Package present and import called from main menu (instead of using the Lens System tool as described in Sec. 125.2): VirtualLab Fusion tries to determine whether the Binary 2 surface forms a diffractive lens together with its preceding or its subsequent surface by evaluating the involved materials. Both surfaces will be represented by a Diffractive Lens component ( $\leftrightarrows$ Sec. 60.2) in the imported optical setup. The Binary 2 surface will be a surface whose channel operator represents the diffractive properties of the Binary 2. |
|  | - Else: The import creates a Combined Surface, consisting of a Plane or Aspherical Surface and an Aspherical Surface. The latter may be height-scaled, see 124.4.1.1 for more information. |


| Coordinate Break ${ }^{\text {Z20sLl }}$ | N/A <br> (Coordinate breaks are not imported because they are not needed in the imported Optical Setup. All positions and orientations of the surfaces are set correctly without referring to theses virtual planes.) |
| :---: | :---: |
| Even Asphere Surface | Aspherical Surface |
| Extended Asphere | Aspherical Surface |
| Odd Asphere Surface | Aspherical Surface |
| Q-Type Asphere <br> Standard Surface | Forbes Surface <br> A Conical Surface or Plane Surface, depending on the radius of the Standard Surface. |
| Tilted Surface | Plane Surface |
| Toroidal | A couple of cases have to be distinguished: $\begin{array}{l\|l} Z>0 & Z=0 \end{array}$ |
|  | $R \neq 0$ CS: Toroidal + Zernike Standard Toroidal Surface <br> $R=0$ CS: Cylindrical + Zernike Standard Cylindrical Surface <br> with $R$ being the Radius of Rotation and $Z$ being the number of Zernike coefficients given in the lens file. 'CS' stands for Combined Surface. |
| Zernike Fringe Sag ${ }^{\text {ZOSLIC }}$ | Available only if the Zernike decenter values are zero. <br> A Combined Surface, consisting of a Plane or Aspherical Surface and a Zernike Fringe Surface |
| Zernike Standard Phase | A Combined Surface, consisting of a Plane or Conical Surface and a Zernike Standard Surface. The latter may be height-scaled, see 124.4.1.1 for more information. |
| Zernike <br> Standard Sag ${ }^{\boxed{2 O S} \text { LIO }}$ | Available only if the Zernike decenter values are zero. <br> A Combined Surface, consisting of a Plane or Aspherical Surface and a Zernike Standard Surface |

Surfaces of unsupported types are considered to be Plane Surfaces.

### 124.4.1.1 Handling of Surfaces Which Define Phase Variations Directly

In the case of Binary 1, Binary 2 (if no OpticStudio® license present) and Zernike Standard Phase, the phase functions given in Zemax OpticStudio® are transformed into a height profile in VirtualLab Fusion. This height profile is always the second of the two sub-surfaces in the imported Combined Surface.
The height profile is computed using the thin element approximation [Goo68]. This means that the surface profile height is proportional to the phase values. To this end, the wavelength and the refractive indices of the media before and behind the surface are calculated from the data in the Zemax OpticStudio® lens file. (The refractive indices are relative to the Air (Zemax OS), in order to resemble the behavior of Zemax OpticStudio®.) If necessary, the z-scaling of the height profile in VirtualLab Fusion can be used to compensate side effects, caused e. g. by using only the first wavelength of the Zemax OpticStudio® lens file.

### 124.4.2 Importing Materials from Zemax OpticStudio® Lens Files

There are different kinds of specifications for material data in Zemax OpticStudio®. The following specification types are supported by VirtualLab Fusion:

- MIL Number Glasses and
- Model Glasses are interpreted as representing a simple dispersion formula as described in the Zemax OpticStudio® user manual.
- The material MIRROR is imported as being an idealized material with a constant refractive index of 1 and a very high constant absorption coefficient of $10^{15} 1 / \mathrm{m}$, leading to an almost perfect reflection behavior.
- All table glasses (file extension *.ztg) as well as
- all catalog glasses (file extension *.agf) are expected to be stored in the subdirectory "Glasscat" of the Path for 'Zemax OpticStudio®' User Data. This search path can be specified in the Global Options dialog ( $\hookrightarrow$ Sec. 6.17) .

Please note: Although Model Glasses as well as MIL Number Glasses are defined via Abbe number $v_{d}$ and refractive index $n_{d}$, these kinds of materials are not imported to a Virtual Lab material using the Abbe Number (vd) dispersion formula. Regarding Model Glasses, the reason is the additional partial dispersion parameter $\Delta P_{g^{F}}$ which can be defined there. MIL Number Glasses just use a different dispersion formula in Zemax OpticStudio® compared to our formula ( $\hookrightarrow$ Sec. A.4.1). So, a special programmable material is used for the import of Model Glasses and MIL Number Glasses.

### 124.4.3 Handling of the Environment Conditions

In Zemax OpticStudio®, all specified wavelengths are defined in air. The dispersion of this air is defined by an environment temperature and pressure. To fully represent this behavior in VirtualLab Fusion, the following steps are done during import:

1. A new material is defined using the Edlén equation given in Sec.38.2.1. For the temperature and pressure which are parameters of this equation the values from the Zemax OpticStudio® lens file are used. This new material is hence referred to as Air (Zemax OS).
2. The vacuum wavelength $\lambda_{\text {vac }}$ is calculated by solving the equation $\lambda_{\text {air }}=\frac{\lambda_{\text {vac }}}{n_{\text {air }}}$ for $\left.\lambda_{\text {vac }}\right)$. $n_{\text {air }}$ is the refractive index of the Air (Zemax OS) and $\lambda_{\text {air }}$ is the first wavelength in the Zemax OpticStudio® lens file.
3. The reference material ( $\hookrightarrow$ Sec. 38.2.1) of all imported materials is set to the Air (Zemax OS).

### 124.4.4 Combining Imported Surfaces

Each surface of the Zemax OpticStudio® lens file (except for object plane, image plane and coordinate breaks) is imported to a Curved Surface component. Subsequent to the actual import, the user is asked whether to combine these surfaces to one or more Lens System component(s). If desired, this combination will be tried as described in Sec. 43.6.3.2.

### 124.4.5 Handling Unpacked Data From ZAR Archives

In case a Zemax *.zar archive file shall be imported ${ }^{\text {ZOSLCO }}$, the contained files of the archive will be extracted into a temporary folder. The unpacked lens file will be used for the actual import then. The extraction folder will be deleted after VirtualLab Fusion has closed.
In case the unpacked data shall be stored for later use anyway, the files can be saved to a different, permanent folder via the dialog shown in Fig. 765.


Figure 765. Dialog for handling the extracted data from a Zemax *.zar archive.

Clicking the underlined link will open the temporary folder, while pressing the Yes, Save Now button allows to specify a different, permanent folder for storing the data to.

## 125 Export and Import of Real Components

### 125.1 Stereolithography Format

All real components can be exported into the stereolithography format (*.stl) via their 3D View ( $\hookrightarrow$ Sec. 5.15).

### 125.2 Import of Zemax OpticStudio® Lens Files into a Lens System Component

A tool in the edit dialog of the Lens System component ( $\hookrightarrow$ Sec. 57.1) allows importing Zemax OpticStudio® lens file data into a lens system.

## Zemax OpticStudio® license needed

The import of *.zmx or *.zar files requires a valid Zemax OpticStudio® license of version '19.4 SP2' or newer. Importing *.zos files requires a version '21.3' or newer. It has to be a 'Professional' or 'Premium' edition in any case, a 'Standard' edtion will not work.
If no valid license can be found or the Global Options are configured accordingly ( $\leftrightarrows$ Sec. 6.16), VirtualLab Fusion may use a rudimentary import algorithm on *.zmx files which may produce unsatisfactory results.

At first, VirtualLab Fusion checks whether or not the surface data in the file fulfill the restrictions of a Lens System component. Most important are the following conditions:

- All positions have to be on one line which is considered to be the optical axis of the system to be imported.
- No surface, except for standard surfaces with infinite radius (considered to be plane surfaces), may be tilted to the optical axis.

All other properties of the import algorithm are explained in Sec. 124.4.
The imported surfaces are appended at the end of the current surface sequence. To maintain the overall structure, surfaces which could not be imported are replaced by a Plane Surface and materials which could not be imported are replaced by the "Air (Zemax OS)".

### 125.3 Import of Zemax OpticStudio® Lens Files into a Diffractive Lens or Meta Lens

The edit dialogs for diffractive and meta lenses have a button Import from 'Zemax OpticStudio®' System on their Structure page. Using this button, a .zmx, .zos or .zar file can be selected via 'file open' dialog. This file will be searched for surfaces of type 'Binary 2'.

- If no 'Binary 2' surface can be found, an error message will be given.
- If there is exactly one 'Binary 2' surface contained in the lens file, it will be imported automatically into the diffractive or meta lens component.
- If more than one 'Binary 2' surface are found, the user will be asked which of them is to be imported.


## 126 Export of Cells Arrays

### 126.1 Export of Grating Cells Arrays

The grating parameters can be exported by pressing on the 目-button on the bottom of the edit dialog of the Grating Cells Array. This triggers the Export Grating Cells Array dialog, which can be used for configuring the export parameters of the set up Grating Cell Array. The export to CSV (comma separated values) and GDSII is supported for the GCA.

| Export Grating Cells Array |  |  |  |
| :---: | :---: | :---: | :---: |
| Grating Type | Sawtooth G | Grating | $\checkmark$ |
| $\square$ Calculate Binary Masks |  |  |  |
| Number of Discrete Height Levels |  | 6 |  |
| Height Profile Storage |  |  |  |
| $\square$ Text File (".csv) | $\square$ GDSII Data (*.gds) |  |  |
| CSV Parameters |  |  |  |
| Decimal separator |  | (period) |  |
| Column separator |  | (comma) |  |
| OK | Cancel |  | Help |

Figure 766. The dialog to set up the export parameters for a Grating Cells Array.

Fig. 766 shows the edit dialog to export a Grating Cells Array. It has the following settings:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Grating Type | For the export of the Grating Cells Array data the grating type need to be <br> specified. Currently on sawtooth grating is supported for the fabrication ex- <br> port. |
| Calculate Binary Masks | The export allow to calculate binary masks. Checking this option allow the <br> export to GDSII format. If this option is not selected, only CSV format is <br> available. |
| Number of Discrete Height | The export supports also a quantization of the gratings. Therefor the user <br> Levels to specify the number of discrete height levels which he will use for the <br> fabrication process. |
| Text File (*.csv) | The user can select to export the parameters of the Grating Cells Array into a <br> comma separated value format. Within this format the analytic parameters of <br> all grating cells are written into a text file in matrix form. The different grating <br> parameters are written in three different blocks within the text file. The blocks <br> are arranged under each other. Additional information about the GCA as the |
|  | number of cells and the cell size are written in the header of the csv file. The <br> csv format can be easily opened with a text editor or a spreadsheet. |
| VirtualLab Fusion offers the possibility to export the Grating Cells Parameter |  |
| into the GDSII format. Therefor the element has to be factorized into binary |  |
| masks. The GDSII option is only available if the Calculate Binary Masks op- |  |
| tion is checked. The element within the GDSII format is not pixelated. This |  |
| reduces the storage effort and increases the specification accuracy. Fig. 767 |  |



Figure 767. The Grating Cells Array can be exported to GDSII.
After pressing the OK button the user needs to specify the location and file name for both the .csv and the GDSII file.

### 126.2 Export of Prism Cells Arrays

The prism parameters can be exported by pressing on the $\boldsymbol{l}^{2}$-button on the bottom of the edit dialog of the Prism Cells Array (PCA). This triggers the Export Prism Cells Array dialog, which can be used for configuring the export parameters of the set up Prism Cell Array. The export to CSV (comma separated values) text files and to the STL format is supported for PCAs.


Figure 768. The dialog to set up the export parameters for a Prism Cells Array. Here the settings for STL export are shown.


Figure 769. A Prism Cells Array extruded to a solid.
The following settings can be done within the Export Prism Cells Array dialog ( $\rightarrow$ Fig. 768):

| ITEM | DESCRIPTION |
| :---: | :---: |
| Text File (*.csv) | The user can select to export the parameters of the Prism Cells Array into a comma separated value format. Within this format the analytic parameters of all prism cells are written into a text file in matrix form. The different grating parameters are written in three different blocks within the text file. The blocks are arranged under each other. Additional information about the PCA as the number of cells and the cell size are written in the header of the CSV file. The CSV format can be easily opened with a text editor or a spreadsheet. |
| STL (*.stl) | VirtualLab Fusion offers the possibility to export the whole Prism Cells Parameter into the standard STL format. |
| Decimal Separator | ONLY AVAILABLE FOR THE TEXT FILE EXPORT. <br> Allows the user to choose either ',' or '.' as decimal separator or to enter a custom one. |
| Column Separator | OnLy AVAILABLE FOR THE TEXT FILE EXPORT. <br> Allows the user to choose either among distinct customized column separators like space, tab stop, semicolon, ...; or to enter a custom one. |
| Extrude STL Mesh | Only available for the STL export. <br> For the STL format you can extrude the surface to a real solid. To this end an additional plane surface is added at Extrusion Distance below the actual surface, $\hookrightarrow$ Fig. 769. With this checkbox you can switch the extrusion on or off. |
| Extrusion Distance | OnLy available for the STL EXPORT. <br> The additional plane surface is perpendicular to the optical axis and placed at a certain distance $z$ from the negative z-extension of the actual surface (the "lowermost point"). This distance $z$ is the Extrusion Distance which can be set by the user. |
| X-Y-Z Scaling Factor | Only available for the STL Export. <br> You can use this factor to apply an overall scaling on the exported data if necessary. |

At the bottom of the dialog the minimum and the maximum height of the Prism Cells Array are given. After clicking on the OK button the user needs to specify the location and file name for both the CSV and the STL file.

The exported STL file will have slightly smaller numerical values for the minimum and the maximum height value of the full structure. This is due to the fact that some STL reading programs have problems if VirtualLab Fusion exports the edges from one prism cell to the next with ideal $90^{\circ}$; so the actual prism surface is reduced a tiny bit so that instead of totally vertical edges slightly slanted ones are exported. The difference is negligible for the optical effect.

## 127 Export and Import of Optical Surfaces

In VirtualLab Fusion, optical surfaces are exported by first sampling the height profile with a given pixel size. This pixelated height profile can then be exported either directly into a single file. Or the height profile can be decomposed into several masks: One mask stores the binary information whether or not half the total profile
height shall be removed from the substrate, another mask stores whether or not a fourth of the total profile height shall be removed and so on.
The height level data can be exported to various text and binary formats. In addition to the actual data files, always a summary file in a specific XML format ( $\leftrightarrows$ Sec. 127.4) is created containing additional metadata, for example the pixel size. This summary file can additionally be generated as HTML, text, or rich text file. Together with the XML file always a file summary.xslt is saved which ensures that the XML file is shown in a more human-readable form if opened with a web browser.
All these formats (but the point cloud and the stereolithography (*.stl) format) can be imported into a Sampled Surface ( $\hookrightarrow$ Sec. 35.2.11) if a XML file in the format as specified in Sec. 127.4 is provided.
Sec. 127.1 explains the export dialog in detail.

### 127.1 Export Dialog (for Standard Surfaces)



Figure 770. The dialog for configuring the export of a surface (here: General Parameters tab).
To configure the export to your needs a dialog opens during the export ( $\hookrightarrow$ Fig. 770). This dialog comprises up to three tab pages which are explained in the following subsections. Furthermore it contains a button for starting and stopping the actual export as well as a progress bar indicating the progress of the current export step (which is shown in a label below the progress bar).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Export | Starts the actual export. After the export has been started this button turns <br> into a Stop button, allowing you to cancel the current export process. Fur- <br> thermore, the Close button is disabled during the export. |

### 127.1.1 General Parameters

The General tab page ( $\hookrightarrow$ Fig. 770) contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Path | The path into which the resulting files are saved. This path can be changed with the Select button. If you want to open that path in the Windows ${ }^{\text {TM }}$ Explorer, you can click on the path label. |
| File Names | Allows you to set the file name used for all data and summary files (without the specific file extensions). Summary files are supplemented by "_summary" and data files representing masks are supplemented by "_MASK_\#", where \# is the number of the mask. The file name also defines the name of the main structure in GDSII and CIF files. It must not contain any of the following characters: V: *? < > \|. |
| Export Binary Masks | This option is only enabled for a surface with $2^{n}$ discrete height levels. $n$ is the number of resulting masks (which is given in brackets) and can be in the range from 1 to 12. |
| File Name Convention | If Export Binary Masks is checked, one data file per mask is created. If you choose Ascending then the file . . . _MASK_1 contains the binary mask with the smallest height modulation. Otherwise it contains the largest height modulation - half the total profile height. |
| Export as ... | This group box allows you to select the file format(s) for the resulting data files. It is ensured that at least one format is selected. Not all file formats are always available: <br> - Bitmap files can only be generated if the surface contains discrete height levels, but no more than 256. <br> - CIF and GDSII format are only available if Export Binary Masks is checked. <br> - The Point Cloud, the STL, and the 16-bit grayscale format are only available if Export Binary Masks is not checked. <br> Sec. 127.3 gives some annotations for the used file formats. |
| Summary Files | At least a XML file with additional metadata is always generated, as this file is needed if you want to re-import the data into VirtualLab Fusion. But you can select HTML, text, and rich text as additional, more human-readable, formats. Sec. 127.4 explains the structure of the summary files and lists the metadata written during the export of surfaces. Sec. 127.3 gives some annotations for the used file formats. |

### 127.1.2 Export Parameters



Figure 771. The General Parameters tab for exporting a surface.

The Export Parameters tab page ( $\hookrightarrow$ Fig. 771) contains the following controls:

| ITEM | DESCRIPTION |
| :--- | :--- |
| Export Whole Surface / <br> Export Only One Period | This item is only enabled if the surface is set to be periodic ( $\hookrightarrow$ Sec. 35.1.1). <br> If you choose to Export Whole Surface then a rectangle with the size of the <br> outer definition area is exported. Otherwise, only one period is exported. |
| Oversampling Factor | If the surface is already pixelated you can specify an integer oversampling <br> factor. The pixel size used for the export is then the original pixel size of the <br> surface divided by that oversampling factor. |
| Pixel Size | As all export formats support only pixelated data, a pixel size must be speci- <br> fied. If the surface is already pixelated, you cannot set the Pixel Size directly <br> but only an Oversampling Factor as explained above. For one-dimensional <br> pixelated surfaces the pixel size in the unmodulated direction is always equal <br> to the overall size of the surface. Note that the internally used pixel size is <br> always a multiple of 1 nm. |
| All heights are inverted. For the export of binary masks that means that if this <br> option is not checked the written data (= the white areas in a bitmap) describes <br> what remains after the production process. In contrast, if the heights are <br> inverted the written data describes what is removed, e.g. etched away. |  |

Additionally to these controls there is an info label giving the size of the exported region as well as the number of pixels in the resulting data files.

### 127.1.3 GDSII/CIF Settings



Figure 772. The specific settings for the GDSII and the CIF export.

If GDSII or CIF are selected as output format, you have the following options on an additional tab ( $\hookrightarrow$ Fig. 772).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Compression | For GDSII or CIF export a compression can be selected. In this case, the <br> individual shapes are combined to $1 \times n$ Rectangular Shapes. Fig. 773 shows <br> an example. This can lead to file sizes reduced by a factor 10 or more. |
| Structure Name from File | The structure name is used in a GDSII/CIF file to group the shapes which <br> represent the structure. If the user checks this option the structure name is <br> the file name specified by the user, succeeded by "MASK_" and the mask <br> number. |
| Custom | If the user checks this option, he can specify an arbitrary structure name. In <br> this case, the same structure name is used for all masks. |



Figure 773. Illustration for the effect of the Compression for GDSII or CIF export.
Left: Stored shapes if None ( $1 \times 1$ Square Shapes) are used.
Right: Stored shapes for the same region if $1 \times \mathrm{n}$ Rectangular Shapes are used.

See also notes on allowed file and structure names for GDSII in Sec. 127.3.

### 127.1.4 STL Settings



Figure 774. The specific settings for the STL export.


Figure 775. A toroidal surface extruded to a solid.

For the STL format you can extrude the surface to a real solid. To this end an additional plane surface is added at a certain position below the actual surface. Fig. 775 shows an example. There are two settings for this extrusion on a separate tab page ( $\hookrightarrow$ Fig. 774).

| ITEM | DESCRIPTION |
| :--- | :--- |
| Extrude to Solid | With this checkbox you can switch the extrusion or or off. |
| Extrusion Distance | The additional plane surface is perpendicular to the optical axis and placed <br> at a certain distance $z$ from the negative z-extension of the surface (the "low- <br> ermost point"). This distance $z$ is the Extrusion Distance which can be set by <br> the user. |

### 127.2 Export Dialog for Diffractive Structures



Figure 776. The dialog for exporting a diffractive structure as polygons.

In contrast to the export dialog for standard surfaces, this dialog ( $\hookrightarrow$ Fig. 776) allows not only the export of pixelated data but also of polygons. It contains the following controls:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Path | The path into which the resulting files are saved. This path can be changed with the Select button. If you want to open that path in the Windows ${ }^{\text {TM }}$ Explorer, you can click on the path label. |
| File Names | Allows you to set the file name used for all data and summary files (without the specific file extensions). Summary files are supplemented by "_summary" and the data files representing masks are supplemented by "_MASK_\#", where \# is the number of the mask. The file name also defines the name of the main structure in GDSII and CIF files. It must not contain any of the following characters: V : *? < > \|. |
| Invert | Flag whether the masks shall be inverted. That means for example that you replace a positive resist by a negative one. |
| File Name Convention | One data file per mask is created. If you choose Ascending then the file ..._MASK_1 contains the binary mask with the smallest height modulation. Otherwise it contains the largest height modulation - half the total profile height. |
| Export Type | The user can define whether pixelated data or polygons are exported. After selecting the export type the dialog offers specific settings for the selected type. |
| Sampling Distance | Only for Pixelated Data Export. <br> The pixel size that should be used for the export. |
| Polygon Detection Accuracy | Only for Polygon Data Export. <br> The user can specify an integer value $i$. This integer value is used to calculate the accuracy of the polygon detection relative to the wavelength. The total accuracy (= maximum lateral distance between level curve and polygon line) is calculated by the formula $(\lambda / i)$. |
| Maximum Number of Points per Polygon | Only for Polygon Data Export. <br> The user can specify the maximum number of points for a polygon. The default value for this option is 8000 which is admissible for both CIF and GDSII. Furthermore, the lower limit is 100 . |
| Export as ... | By defining the export types the user can specify in which format the files shall be exported. In case of pixelated data export the module supports the export to: bitmap, ASCII and plain text, GDSII and CIF format. For the polygon data export the formats GDSII and CIF are available. At least one of the data export file types has to be selected. Sec. 127.3 gives some annotations for the used file formats. |
| Summary Files | At least a XML file with additional metadata is always generated, as this file is needed if you want to re-import the data into VirtualLab Fusion. But you can select HTML, text, and rich text as additional, more human-readable, formats. Sec. 127.4 explains the structure of the summary files and lists the metadata written during the export of surfaces. Sec. 127.3 gives some annotations for the used file formats. |
| \{Export Progress\} | During the export the dialog informs you about the progress of the current export step. The current export step is displayed in the info label below the progress bar. |


| Go! | Starts (and stops) the export. |
| :--- | :--- |
| 390 Preview | Shows a preview of the structure to be exported in the 3D view explained in |
|  | Sec. 5.15. |

See also notes on allowed file names in Sec. 127.3.

## Tip

Export of polygons is much faster when done for rotationally symmetric surfaces. Thus if you export for example a Diffractive Lens ( $\hookrightarrow$ Sec. 60.2), ensure that the surface is a non-periodic Aspherical, Conical, or untilted Plane Surface with a circular definition area.

### 127.3 Annotations for the Various File Formats

| FILE FORMAT | ANNOTATION |
| :---: | :---: |
| Bitmap | In this case an indexed Windows bitmap file with 256 gray values is created ( 8 bits per pixel). Its header contains the color definition for every height level and additional data. The color definition allows to display the bitmap in every painting program. <br> After the header a byte matrix follows which contains the height levels directly as hexadecimal data. For example, if you have exported an element with eight height levels a byte value of 00 corresponds to the smallest height level and 07 to the largest one. The real height can be calculated by multiplying the height level with the height level difference given in the summary file. White is associated with the largest height, black with the lowest one. However, the gray values assigned to the height levels might not be equidistant. Thus, if you want to export the real heights from the bitmap, use the height levels directly, not the gray values. |
| ASCII format | The heights in meters are stored. The file contains a matrix of numbers with $N_{x}$ columns and $N_{y}$ rows ( $N_{x}$ and $N_{y}$ being the number of sampling points in $x$ - and $y$-direction, respectively). The columns are separated by a space. It is recommended to use ASCII instead of the Plain text format because ASCII files are smaller (roughly $33 \%$ for binary masks) and they can be generated up to 5 times faster. |
| Plain text format | The height values in meters are stored. A line contains the data of one single pixel. The header contains information about the number of sampling points in x - and y -direction, respectively. |


| GDSII format | As explained in Sec. 127.1.3, both GDSII and CIF format use a structure name to identify the main structure which contains the actual data. However, the GDSII format only supports the following characters: a. . .z, A. . .Z, 0. . .9, underscore, question mark, and dollar sign. This means that the structure name can only contain these characters. Consequently, the File Names can only contain a. . .z, A. . .Z, 0. . .9, and underscore if the option Structure Name from File Name is used as described in Sec. 127.1.3. |
| :---: | :---: |
| Point Cloud format | This format stores the x - and y -positions in $\mu \mathrm{m}$ along with the corresponding height, also in $\mu \mathrm{m}$. Not that the data is transformed so that only positive values occur. |
| STL format | This format often used for stereolithography stores a triangular mesh. Due to technical reasons, more than $3860 \cdot 3860 \approx 15 \cdot 10^{6}$ pixels cannot be exported with the STL format. |
| Rich Text Format | The rich text format only supports the characters of the Windows-1252 character set natively. Thus the Path and the File Names must not contain other characters than these if you want to use the rich text format as summary file |

### 127.3.1 Annotations for Binary Masks

If a standard surface is exported with the Calculate Binary Masks option ( $\leftrightarrows$ Sec. 127.1.1), some file formats are used a bit differently:

- Bitmap files use only 1 bit per pixel to store a black/white image of the mask.
- ASCII format and plain text format do not store height levels but " 1 " and " 0 " to indicate the binary mask information.


### 127.4 Metadata Summary Files

VirtualLab Fusion provides a general XML format for storing additional metadata for exported data files. The main idea of this format is that the XML file contains several metadata entries (which can be grouped) for a collection of data files (which can also be grouped). The metadata are stored as description (e. g. "Total Profile Height") / value (e.g. 532 nm ) pairs.
Up to now, such summary files are only used for the export of surfaces. In this case the following metadata is stored:

- Metadata Group "Element Parameters"
- Element Size
- Element Shape (elliptic / rectangular)
- Height Outside Element
- Absorbing Material Outside Element
- Total Profile Height
- Exported Binary Masks (yes/no)
- Number of Height Levels (only if the surface Contains Discrete Height Levels)
- Height Level Difference (only if the surface Contains Discrete Height Levels)
- Pixel Size
- Data Represents Only One Period ("yes": Export Only One Period was selected during export; "no": Export Whole Surface was selected during export)
- Number of Exported Pixels
- Metadata Group "Period Parameters" (only if Data Represents Only One Period)
- Size of One Period
- Resulting Repetitions (Element Size / Size of One Period)
- Size of Inner Definition Area
- Shape of Inner Definition Area
- Height Outside Inner Definition Area
- Absorbing Material Outside Inner Definition Area
- Metadata Group "Mask Information" (only if Exported Binary Masks is "yes")
- Number of Masks
- Height Modulation of Mask \# 1
- Height Modulation of Mask \# 2
- ...
- Metadata Group "Specific Export Settings"
- Invert Profile
- Compression for GDSII / CIF (only if GDSII / CIF have been generated)


## 128 Import of Macleod Coatings

VirtualLab Fusion supports importing Macleod coatings in the following two ways.

1. You can import the data directly into VirtualLab Fusion's coatings catalog by clicking on the 首 Import Macleod Coating Data button, which is located within the Catalog Tools of the catalog. After the import you are prompted for a name and categories to insert the imported coating into the User Defined catalog (see also Sec. 33.1).
2. In the edit catalog of a coating you can replace the current data with the imported Macleod data by clicking the 党-button.

The order of the layer sequence of an optical thin film coating is important for its optical properties. When applied to any surface between a solid and a non-solid medium in automatic coating application mode, VirtualLab Fusion will put layer \#1 automatically as the very next one to the solid substrate. As this convention is not used within Macleod, a dialog asks you to confirm the imported layer sequence for non-symmetrical layer structures. If necessary the order of the layer sequence can be inverted in the dialog in question.
Furthermore Macleod files contain also the substrate and the surrounding material. During the import you are prompted whether these two materials are to be saved into VirtualLab Fusion's material catalog. If you want to do so, the dialog in Fig. 777 is shown.


Figure 777. Import dialog for Macleod substrate and surrounding material.
In the upper part of this dialog there is a table with the following columns:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Import | Allows you to select which materials shall be imported. If the selected item <br> is marked red then its name is not unique, already present in the file for user <br> defined entries, or empty. If it is marked green the file can be imported. |
| Name | Shows the name of the material and allows you to change it. |
| State of Matter | Macleod materials have no state of matter. Thus you can set it in this column <br> whereas VirtualLab Fusion already provides an educated guess. |

The lower part of the catalog defines the categories in which all entries are stored. You can add a new category with the
If you press $O k$ the chosen materials will be saved to the user defined materials catalog.

## 129 Import of Materials from Zemax OpticStudio® Glass Catalogs

Via the Catalog Tools of the catalog main form (Sec. 33) for materials you can Import 'Zemax OpticStudio®' Glass Catalogs.


Figure 778. Import dialog for a Zemax OpticStudio® glass catalog with some inconsistent entries.

This catalog tool first shows the standard Windows dialog for opening one or more files with the file extension .agf. The preselected path in this dialog is the GlassCat folder in the Path for 'Zemax OpticStudio®' User Data as specified in the Global Options dialog. The selected files are then imported with the dialog shown in Fig. 778. In the upper part of this dialog there is a table with the following columns:

| COLUMN | DESCRIPTION |
| :--- | :--- |
| Import | Allows you to select which materials shall be imported from the Ze- <br> max OpticStudio® glass catalog. Materials whose name is not unique, al- <br> ready present in the user defined catalog, or empty cannot be imported. If <br> such a material is selected the corresponding row is marked red. Otherwise, <br> it is marked green and OK is shown in the Status column. |
| Shows the name of the material and allows you to change it. |  |$\quad$| Saterials imported from Zemax OpticStudio® have no state of matter. By |
| :--- |
| State of Matter |
| default they are assumed to be solids, but you can change it in this column. |

By clicking on a column caption, you can sort by this column.
The Selection Tools allow you to either Select All materials in the table or to Unselect All.

The lower part of the catalog defines the categories into which all materials are stored. You can add a new category with the -button and remove a category with the X -button.

## 130 Import of Obsolete VirtualLab Fusion Files

The following document types are no longer supported by VirtualLab Fusion but can still be imported into newer document types.

| DOCUMENT TYPE | ANNOTATIONS |
| :--- | :--- |
| Materials and material cat- <br> alogs <br> (*.mtr, *.mct) | Can be imported into the Materials catalog. $\hookrightarrow$ Sec. 33.4. |
| Coatings and coating cat- | Can be imported into the Coatings catalog. $\hookrightarrow$ Sec. 33.4. |
| alogs |  |
| (*.ctg, *.cct) | Surfaces and media contained in a Spread Sheet can be imported into a Lens <br> Spread Sheets <br> (*.ops) <br> Import via File > Import > Import Old VirtualLab Files is also possible. In <br> this case, an Optical Setup is created containing one Lens System with the |
| surfaces and media contained in the Spread Sheet. |  |


|  | PIXELATED INTERPOLATION | SPLINE INTERPOLATION IN DIA- |
| :--- | :--- | :--- |
|  | IN DIAGRAM | GRAM |
| Resulting interpolation method <br> for equidistant Data Arrays | Nearest Neighbor | Linear (Real/Imaginary) |
| Resulting interpolation method <br> for non-equidistant Data Arrays | Constant Interval | Linear (Real/Imaginary) |

Instead of using File > Import > Import Old VirtualLab Files you can also drag importable document types into the main window of VirtualLab Fusion.

### 130.1 Import of VirtualLab Fusion 1.x Complex Amplitude

Complex amplitudes saved in VirtualLab Fusion 1.x lack some information in comparison with VirtualLab Fusion, namely wavelength, wave parameters, spherical phase factor and support for different complex amplitude types. Complex numbers are always stored using float numbers. Local polarization is not supported. Some of this missing parameters must be specified by an input dialog with the following parameters:

| ITEM | DESCRIPTION |
| :--- | :--- |
| \{Complex Amplitude <br> Type | Destination type of import: Transmission or Complex Amplitude Field. |
| Wavelength | Wavelength of the imported complex amplitude. |
| Complex Data | If checked the resulting complex amplitude stores real and imaginary part of <br> the imported data. Otherwise only the real part is stored and the imaginary <br> part is assumed to be zero. |
| Default Parameters | Resets the options above to their default values. |

## XVII Algorithm Manual

This part of the manual gives physical and mathematical background information to the topics covered in the previous parts of the manual.

## 131 Field Data

For locally polarized harmonic fields the two electric field components $E_{x}$ and $E_{y}$ are stored, from which all other field components can be reconstructed. For globally polarized fields, only the scalar field $U(x, y)$ and the Jones vector $J$ ( $\hookrightarrow$ Sec. 131.1) are stored.
The field data are stored as field values on an equidistantly sampled grid. The number of sampling points in x- and y-direction, $N_{x}$ and $N_{y}$ can be chosen freely in the x - and y-direction respectively. For storing twodimensional fields both $N_{x}$ and $N_{y}$ are greater than 1. One-dimensional fields are typically stored with $N_{y}=1$. For each sampling point a complex number is stored by two double precision numbers for the real and imaginary part. This corresponds to a memory requirement of $2 \times 8$ bytes per sampling point. It is also possible that only the real part is stored.
In VirtualLab Fusion $E_{z}$ is calculated according to

$$
\begin{equation*}
E_{z}(x, y)=\left[\mathcal{F}^{-1}\left(-\frac{1}{k_{z}}\left(k_{x} \cdot\left[\mathcal{F} E_{x}(x, y)\right]\left(k_{x}, k_{y}\right)+k_{y} \cdot\left[\mathcal{F} E_{y}(x, y)\right]\left(k_{x}, k_{y}\right)\right)\right)\right](x, y) \tag{131.1}
\end{equation*}
$$

where $\mathcal{F}$ denotes a Fourier transform and $\mathcal{F}^{-1}$ an inverse Fourier transform.
The components of the magnetic field are calculated with the following formulas:

$$
\begin{align*}
& H_{\mathrm{x}}=a_{0}\left(k_{\mathrm{y}} E_{z}-k_{\mathrm{z}} E_{y}\right)  \tag{131.2}\\
& H_{\mathrm{y}}=a_{0}\left(k_{\mathrm{z}} E_{x}-k_{\mathrm{x}} E_{z}\right)  \tag{131.3}\\
& H_{\mathrm{z}}=a_{0}\left(k_{\mathrm{x}} E_{y}-k_{\mathrm{y}} E_{x}\right) \tag{131.4}
\end{align*}
$$

with

$$
\begin{equation*}
a_{0}=\frac{1}{k} \sqrt{\frac{\epsilon_{0}}{\mu_{0}}} \tag{131.5}
\end{equation*}
$$

### 131.1 Global and Local Polarization

If the ratio of the two field components $E_{x}\left(x, y, z_{j}\right) / E_{y}\left(x, y, z_{j}\right)$ is independent of the position $(x, y)$, we obtain

$$
\begin{equation*}
f\left(x, y, z_{j}\right)=J U\left(x, y, z_{j}\right) \tag{131.6}
\end{equation*}
$$

with the Jones vector $J=\left[J_{x}, J_{y}\right]$. Those fields are uniformly or globally polarized in the $x$-y-plane.
All other harmonic fields are locally polarized, that is only locally they are of the form shown in Eq. (131.6).
VirtualLab Fusion deals with both states of polarization and handles the change from global to local polarization automatically.

### 131.2 Spherical Phase Radius

Sampling of a large spherical phase (e.g. a lens with short focal length) would require a very small sampling distance and thus many sampling points for correctly sampling the spherical phase in the border areas of the field. Therefore, VirtualLab Fusion can handle the spherical phase radius as a separate factor multiplied to the sampled aberrations of the spherical phase. This means that the sampling distance has to be chosen only for accurate sampling of the aberrations.
Many of the internal operations of VirtualLab Fusion, as for example the homogeneous medium propagation operators, take into account the stored spherical phase radius.
In harmonic fields sets, a separate spherical phase radius is stored for each harmonic field. Thus, spherical phase radius functions are not available in the light view of harmonic fields sets.
For newly created harmonic fields, VirtualLab Fusion detects and stores the spherical phase radius automatically.

### 131.3 Propagation in Positive Z-Direction?

Part of a complete definition of a harmonic field at a position $z^{\prime}$ is the sign of the z-component of its principal propagation direction $\operatorname{sgn}\left(k_{z}\right)$. It determines whether the field propagates principally to the positive or the negative z -direction. For an example of the importance of this distinction see Fig. 779.


Figure 779. Phase of Spherical Wave. Left: Propagating in Positive Z-Direction, Right: Propagating in Negative ZDirection.

Fields resulting from an Optical Setup ( $\hookrightarrow$ Sec. 43) always propagate in positive z-direction.

### 131.4 Interpolation Methods for Equidistant Data

The appropriate interpolation method has to be chosen according to the physical meaning of the data which shall be interpolated, and according to the acceptable computational effort. If the data represents a harmonic field, the standard reconstruction method is based on the Sinc interpolation [Goo68]. Unfortunately this method is typically connected with a relatively high computational effort. If the data represents a diffractive optical element, nearest neighbor interpolation is recommended.
The following interpolations for equidistant data are supported in VirtualLab Fusion:

| ITEM | DESCRIPTION |
| :---: | :---: |
| Nearest Neighbor Interpolation | Each sampling point of the resultant field is set to the complex amplitude of the nearest sampling point of the original field. |
| Linear (Amplitude/Phase) | Linear interpolation with respect to the 2 (one-dimensional case) or 4 (twodimensional case) adjacent sampling points. This interpolation is performed independently for amplitude and phase. |
| Linear (Real/Imaginary Part) | Linear interpolation with respect to the 2 (one-dimensional case) or 4 (twodimensional case) adjacent sampling points. This interpolation is performed independently for real and imaginary part. |
| Cubic 4 Point | Complex cubic interpolation with respect to the 4 (one-dimensional case) or $4 \times 4$ (two-dimensional case) neighboring sampling points of the original field. $\hookrightarrow \text { Fig. } 780$ |
| Cubic 6 Point | Complex cubic interpolation with respect to the 6 (one-dimensional case) or $6 \times 6$ (two-dimensional case) neighboring sampling points of the original field. $\rightarrow$ Fig. 780 |


| Cubic 8 Point | Complex cubic interpolation with respect to the 8 (one-dimensional case) or $8 \times 8$ (two-dimensional case) neighboring sampling points of the original field. $\rightarrow$ Fig. 780 |
| :---: | :---: |
| Sinc (Fourier Transform) | Using this interpolation method finer sampling is achieved by embedding in the Fourier space. This interpolation method is equivalent to the following steps: <br> 1. Remove the spherical phase radius (if present). $\leftrightarrows$ Sec. 12.1.1 <br> 2. Do a physical backward Fourier transformation. $\leftrightarrows$ Sec. 31.1 <br> 3. Embed the field according to the desired new sampling distance. $\rightarrow$ Sec. 22.7 <br> 4. Do a physical forward Fourier transformation. $\hookrightarrow$ Sec. 31.1 <br> 5. Embed or extract the field to achieve the desired new field size. $\rightarrow$ Sec. 22.7 <br> 6. Superimpose the previously removed spherical phase radius. $\rightarrow$ Sec. 22.5.1 |
| Windowed Sinc | Variant of the Sinc Interpolation (Fourier Transform), which does the embed or extract to the desired new field size before the first Fourier transform. This reduces the required computational effort if only a part of the original field should be interpolated but yields only a slightly approximated result. More precisely, first a little bit larger part (larger by 6 sampling points) is extracted out of the original field in order to reduce numerical errors on the borders of the interpolated field; the additional sampling points are then removed in a final step. |
| Accelerated Sinc | If you interpolate to a new field size $(x ; y)$, then the original field is first truncated to $(t \cdot x ; t \cdot y)$ using a soft aperture of that size. $t$ is the Field Size Truncation Factor for Accelerated Sinc Interpolation of the Global Options dialog ( $\leftrightarrows$ Sec. 6.13). Afterwards a Sinc Interpolation (Fourier Transform) is performed on the truncated field. |
| Sinc (Pointwise) | Sinc interpolation using pointwise superposition of sinc functions, that is for each sampling point of the resulting field a summation is performed over the sinc functions of all sampling points of the original field. This interpolation method can be significantly slower but less memory consuming than Sinc Interpolation (Fourier Transform), although besides of numerical errors it yields the same result. |
| Truncated Sinc | Approximation to the interpolation method Sinc Interpolation (Pointwise) in which the extent of the sinc function is limited to 6 sampling points. |
| Combined | Depending on the physical extension of the resultant field either cubic 6 point interpolation (small size) or Windowed Sinc Interpolation (larger size) is used. The cubic interpolation is used if the extension of the resultant field is smaller than three sampling points of the original field. |



Figure 780. Illustration which neighbor points are used for a Cubic n Point Interpolation.

## 132 Sources

VirtualLab Fusion provides a growing set of source models. Each model describes an electromagnetic field in a plane. The source generation results in a discretized field that is represented by a data array (sampled field) and additional parameters including, e. g., wavelength(s), physical coordinates and others, see below.
The fields resulting from the source generation are described in the input plane with $z=0$. A source field can be represented by one or more complex amplitude fields. Each of those fields is globally polarized and is described by

$$
\begin{equation*}
E_{\mathrm{xy}}(x, y, 0)=J U(x, y, 0) \tag{132.1}
\end{equation*}
$$

where $J$ denotes the Jones vector and $U(x, y, 0)$ is a scalar complex function.
In order to handle arbitrary fields $U(x)$ numerically, $U(x)$ has to be sampled with a finite number of $\left(N_{x} ; N_{y}\right)$ sampling points. In VirtualLab Fusion an equidistant sampling with the sampling distance ( $\delta x ; \delta y$ ) corresponds to sampling points at the positions $\left(\mathrm{x}_{\text {min }}, \mathrm{x}_{\text {min }}+\delta x, \ldots, \mathrm{x}_{\text {min }}+\left(N_{x}-1\right) \delta x, \mathrm{y}_{\min }, \mathrm{y}_{\text {min }}+\delta y, \ldots, \mathrm{y}_{\min }+\left(N_{y}-1\right) \delta y\right)$ with

$$
\begin{equation*}
\mathrm{x}_{\min }=-\left\lfloor\frac{N_{x}}{2}\right\rfloor \delta x, \quad \mathrm{y}_{\min }=-\left\lfloor\frac{N_{y}}{2}\right\rfloor \delta y \tag{132.2}
\end{equation*}
$$

where $\lfloor\cdot\rfloor$ denotes the rounding down operation.

### 132.1 Gaussian Wave

### 132.1.1 Formulas for an Ideal Gaussian Wave

An ideal one-dimensional Gaussian field is defined by

$$
\begin{equation*}
U_{\mathrm{G}}(x)=\exp \left[-\frac{x^{2}}{w^{2}(z)}\right] \exp \left[i\left(-\frac{k z}{2}-k \frac{x^{2}}{2 R(z)}+\frac{1}{2} \arctan \left(\frac{z}{z_{\mathrm{R}}}\right)\right)\right] \tag{132.3}
\end{equation*}
$$

The variable $k=2 \pi / \lambda$ refers to the wave number; $\lambda$ is the medium wavelength. $z$ is the Distance to Input Plane. In contrast to the "Laser Beam Calculator" ( $\hookrightarrow$ Sec. 112), you cannot enter the beam radius $w(z)$ directly in the generator dialog. It is calculated via

$$
\begin{equation*}
w(z)=w_{0} \sqrt{1+\left(\frac{z}{z_{\mathrm{R}}}\right)^{2}} \tag{132.4}
\end{equation*}
$$

$w_{0}$ is the Waist Radius and $z_{\mathrm{R}}$ is the Rayleigh length

$$
\begin{equation*}
z_{\mathrm{R}}=\frac{\pi w_{0}^{2}}{\lambda} \tag{132.5}
\end{equation*}
$$

Further fundamental parameters of a Gaussian beam are the Phase Radius $R(z)$ as well as the Half Angle of Divergence $\frac{\alpha}{2}$. These parameters can be calculated by the following equations.

$$
\begin{align*}
R(z) & =z\left[1+\left(\frac{z_{\mathrm{R}}}{z}\right)^{2}\right]  \tag{132.6}\\
\frac{\alpha}{2} & =\frac{\lambda}{\pi w_{0}} \quad \text { valid in the far field }\left(z \gg z_{\mathrm{R}}\right) \tag{132.7}
\end{align*}
$$

For all the equations above, waist radius and half angle of divergence are referring to the point where the squared amplitude is reaching $e^{-2}(\approx 0.135)$ times the maximum squared amplitude.
A two-dimensional Gaussian field can be constructed by multiplying two one-dimensional fields:

$$
\begin{equation*}
U_{\mathrm{G}}(x, y)=U_{\mathrm{G}}(x) \cdot U_{\mathrm{G}}(y) \tag{132.8}
\end{equation*}
$$

whereas the beam parameters may be different for both directions. Different waist distances $z$ lead to an astigmatic Gaussian field.

### 132.1.2 Beam Quality and Higher Order Modes

The Gaussian wave generator ( $\hookrightarrow$ Fig. 476) can also be used to generate fields that represent Hermite-Gaussian or Laguerre- Gaussian modes. A two-dimensional Hermite-Gaussian is derived by:

$$
\begin{equation*}
U_{\mathrm{H}}(x, y)=U_{\mathrm{G}}(x, y) \cdot \exp \left[ \pm i(m+n) \arctan \left(\frac{z}{z_{\mathrm{R}}}\right)\right] \cdot \mathcal{H}_{m}\left(\frac{\sqrt{2} x}{w(z)}\right) \cdot \mathcal{H}_{n}\left(\frac{\sqrt{2} y}{w(z)}\right) \tag{132.9}
\end{equation*}
$$

where $m$ and $n$ are the order for $x$ - and $y$-direction, respectively. $\mathcal{H}_{j}$ is the Hermite polynomial for the order $j$. The $M^{\wedge} 2$ Parameter of a Hermite-Gaussian is calculated by

$$
M^{2}= \begin{cases}2 m+1 & \text { x-direction }  \tag{132.10}\\ 2 n+1 & \text { y-direction }\end{cases}
$$

A two-dimensional Laguerre-Gaussian is derived by:

$$
\begin{equation*}
U_{\mathrm{L}}(x, y)=U_{\mathrm{G}}(x, y) \cdot \exp \left[ \pm i\left(l \arctan \left(\frac{y}{x}\right)+M^{2} \arctan \left(\frac{z}{z_{\mathrm{R}}}\right)\right)\right] \cdot \mathcal{L}_{p}^{|l|}\left(\frac{2\left(x^{2}+y^{2}\right)}{w(z)^{2}}\right) \tag{132.11}
\end{equation*}
$$

where $p$ is the radial order and $l$ is the angle order. $\mathcal{L}_{p}^{|l|}$ is an associated Laguerre polynomial. The $M^{\wedge} 2$ Parameter of a Laguerre-Gaussian is calculated by

$$
\begin{equation*}
M^{2}=2 p+|l|+1 \tag{132.12}
\end{equation*}
$$

Further explanations for these formulas can be found for instance in [ST91].

### 132.2 Super-Gaussian Wave

This source model allows you to generate isotropic and separable super-Gaussian fields.
An isotropic super-Gaussian field $U(x, y)$ is given by

$$
\begin{equation*}
U(x, y)=\exp \left[-\left(\frac{r}{w_{0}}\right)^{m}\right] \tag{132.13}
\end{equation*}
$$

where $w_{0}$ denotes the waist radius at the amplitude level of $1 / e, m$ denotes the order of the super Gaussian ( $m=2$ corresponds to a regular Gaussian) and

$$
\begin{equation*}
r=\sqrt{x^{2}+y^{2}} \tag{132.14}
\end{equation*}
$$

A separable super Gaussian field $U(x, y)$ is defined by

$$
\begin{equation*}
U(x, y)=\exp \left[-\left(\frac{x}{w_{0, x}}\right)^{m_{x}}-\left(\frac{y}{w_{0, y}}\right)^{m_{y}}\right] \tag{132.15}
\end{equation*}
$$

where order and waist radius are given for both $x$ - and $y$-direction.
It is possible to define the waist radius $w$ at any (amplitude or intensity) level $k$ above the minimum edge level, i.e. different from $w_{0}$ as defined in Eq. (132.13). This waist radius $w$ is connected to $w_{0}$ by

$$
\begin{equation*}
w_{0}=\frac{w}{\sqrt[m]{-\ln k}} \tag{132.16}
\end{equation*}
$$

where the amplitude level $0<k<1$ is given as fraction of the maximum amplitude of the super Gaussian in its center.
If you want to create a field with a Top-Hat-like light distribution where only the "sharpness" of the edges is known but not the required order of the super Gaussian, then it is possible to enter the width $\Delta r_{e}$ of the edge between a lower (minimum) and an upper (maximum) level ( $y_{l}$ and $y_{u}$ ). The relation between edge width and order of the super Gaussian is

$$
\begin{equation*}
\Delta r_{e}=w\left(\sqrt[m]{\frac{\ln y_{l}}{\ln k}}-\sqrt[m]{\frac{\ln y_{u}}{\ln k}}\right) \tag{132.17}
\end{equation*}
$$

The meaning of all these parameters $w$ (waist radius), $k$ (definition level for waist radius), $\Delta r_{e}$ (edge width), $y_{l}$ (minimum level of the edge) and $y_{u}$ (maximum level of the edge) is shown in the sketch in Fig. 781.


Figure 781. Definition of a Super Gaussian by Edge Width and Waist Radius.


Figure 782. Isotropic Super Gaussian Field as 3D View.

### 132.3 Gaussian Type Planar Source

This generator can be used to simulate LEDs and Excimer lasers. The details of the model will be described in a separate paper which can be distributed on request.
The model is based on using a set of fundamental modes. In this case, Gaussian modes are used. The modes are laterally shifted across the emitting surface. The model assumes a dense set of modes. The computational model requires a finite set of modes which has to be defined by the user. Currently, the modes are scaled with the factor $1 / \sqrt{n}$, where $n$ is the number of lateral positions.
This source can be described by its divergence, by the coherence length or by the waist of the fundamental modes. Let us discuss the relationship between these values.
A single fundamental mode is a Gaussian field. The complex amplitude $U$ in its waist plane $(z=0)$ is given by

$$
\begin{equation*}
U(x, y, z=0)=U_{0} \exp \left(-\rho^{2} / w_{0}^{2}\right) \tag{132.18}
\end{equation*}
$$

with $\rho^{2}=x^{2}+y^{2}$. The waist radius $w_{0}$ defines the radius for which the value of $U$ is decreased by a factor of $1 / \mathrm{e}$. Therefore, the squared amplitude is decreased by $1 / \mathrm{e}^{2}$. In paraxial approximation a propagated Gaussian remains Gaussian and possesses the $1 / \mathrm{e}$-beam radius $w(z)$. We may then define the half-width $1 / \mathrm{e}$ (HWE) angle divergence of the beam by

$$
\begin{equation*}
\theta_{\mathrm{HWE}}=\lim _{z>\infty} \arctan \left(\frac{w(z)}{z}\right)=\arctan \left(\frac{w_{0}}{z_{0}}\right) \tag{132.19}
\end{equation*}
$$

with the Rayleigh length

$$
\begin{equation*}
z_{0}=\pi w_{0}^{2} / \lambda . \tag{132.20}
\end{equation*}
$$

Finally we obtain

$$
\begin{equation*}
\theta_{\mathrm{HWE}}=\arctan \left(\frac{\lambda}{\pi w_{0}}\right) \tag{132.21}
\end{equation*}
$$

Because the derivation uses a paraxial assumption, the angles are small and the arctan is often omitted in literature. It is important to note, that the arctan in Eq. (132.21) does not ensure its validity in the non-paraxial domain.
If we consider non-paraxial beams, the definition of the waist $w_{0}$ remains unchanged. But for the definition of the divergence we must consider the far field of the beam in form of the radiant intensity which takes the form

$$
\begin{equation*}
J(\theta, \phi)=4 \pi^{4} w_{0}^{4} k^{2} \cos ^{2} \theta \exp \left(-\frac{1}{2}\left(k w_{0}\right)^{2} \sin ^{2} \theta\right) \tag{132.22}
\end{equation*}
$$

For small angles we have $\sin \theta \approx \theta$ and $\cos \theta=1$ and Eq. (132.22) reduces to the intensity of a paraxial far field, which is a Gaussian. The divergence is now defined by the extent of $J$ in terms of $\theta$. Obviously it makes no sense to define a 1 /e value, because of the $\cos ^{2} \theta$ term. Thus, the half-width at half-maximum (HWHM) angle of $J(\theta)$ is defined as the divergence half-angle $\theta_{\text {HWHM }}$. Evaluation of Eq. (132.22) results in the relationship between the waist $w_{0}$ and the divergence $\theta_{\text {HWHM }}$ according to

$$
\begin{equation*}
w_{0}=\lambda \frac{\sqrt{\ln \left(2 \cos ^{2} \theta_{\mathrm{HWHM}}\right)}}{\sqrt{2} \pi \sin \theta_{\mathrm{HWHM}}} . \tag{132.23}
\end{equation*}
$$

The relation between waist and coherence length is given by

$$
\begin{equation*}
w_{0}=\sqrt{2} \cdot \text { coherence length. } \tag{132.24}
\end{equation*}
$$

### 132.4 Far Field Source

The far field source allows you to define a spatially partially coherent light source by its far field.
$\left\{{ }_{u} V_{\ell}(\rho, z ; \omega)\right\}_{u}$ refers to one vectorial component $\ell$ of a single mode $u$ out of many uncorrelated modes. It is defined by

$$
\begin{equation*}
\left\{{ }_{u} V_{\ell}(\rho, z ; \omega)\right\}_{u}=\left\{\alpha_{u} D_{\ell}(\theta, \phi) \frac{e^{i k r}}{r}\right\}_{u} \tag{132.25}
\end{equation*}
$$

The following symbols are used in Eq. (132.25).

- $\omega=\frac{2 \pi c}{\lambda}$ : Angular frequency.
- $k$ : Wave number.
- $\rho$ : The lateral position $(x ; y)$.
- $r=\sqrt{x^{2}+y^{2}+z^{2}}$
- $\alpha_{u}$ is the weight of the mode.
- The complex direction weight functions $D_{\ell}(\theta, \phi)$.
- The braces with index $u$ indicate the use of the mode coordinate system shifted by $\rho_{u}$.


### 132.5 Spectrum Generators

### 132.5.1 Black Body Spectrum

The black body power spectrum uses the energy density distribution law in dependence on the wavelength $\lambda$

$$
S(\lambda)=\frac{8 \pi h c}{\lambda^{5}} \frac{1}{e^{\left(\frac{h c}{\lambda k T}\right)}-1}
$$

where $T$ is the temperature in Kelvin, $h$ denotes the Planck constant ( $6.6260755 \cdot 10^{-34} \mathrm{Js}$ ), $k$ is the Boltzmann constant ( $1.3806505 \cdot 10^{-23} \mathrm{~J} / \mathrm{K}$ ), and $c$ stands for the vacuum speed of light ( $299792458 \mathrm{~m} / \mathrm{s}$ ).

### 132.5.2 Gaussian Spectrum

A Gaussian spectrum arises in Doppler broadening of a spectral line.
Its dependence on the angular frequency $\omega$ is given by the formula

$$
\begin{equation*}
S(\omega)=S_{0} \exp \left(-\ln 2 \cdot \frac{\left(\omega-\omega_{0}\right)^{2}}{\Delta \omega^{2}}\right) \tag{132.26}
\end{equation*}
$$

where $\omega_{0}$ is the central angular frequency, $\Delta \omega$ the half width at half-maximum of the distribution. In transforming the density to a function of the wavelength, the relations

$$
\begin{gathered}
\omega_{0}=2 \pi c / \lambda_{0}, \\
\Delta \omega=-\omega_{0} / \lambda_{0} \cdot \Delta \lambda,
\end{gathered}
$$

were used.
If wavelengths with a minimal intensity $S_{\text {min }}$ (relative to the peak intensity) shall limit the sampled wavelength interval, then corresponding lowest and highest angular frequencies are computed from

$$
\begin{gathered}
\omega_{\min }=\omega_{0}+\Delta \omega \cdot \sqrt{\frac{-\ln S_{\min }}{\ln 2}}, \\
\omega_{\max }=2 \omega_{0}-\omega_{\min },
\end{gathered}
$$

and the equivalent wavelengths follow from $\lambda=2 \pi c / \omega$.

### 132.5.3 Lorentzian Spectrum

The Lorentzian power spectrum arises in natural lifetime and collision broadening of a spectral line. Its dependence on the angular frequency $\omega$ is given by the formula

$$
S(\omega)=\frac{S_{0}}{\left(\omega-\omega_{0}\right)^{2}+\Delta \omega^{2}},
$$

where $\omega_{0}$ is the central angular frequency, $\Delta \omega$ the half width at half-maximum of the distribution.
In transforming the density to a function of the wavelength, the relations

$$
\begin{gathered}
\omega_{0}=2 \pi c / \lambda_{0}, \\
\Delta \omega=-\omega_{0} / \lambda_{0} \cdot \Delta \lambda,
\end{gathered}
$$

were used.
If wavelengths with a minimal intensity $S_{\min }$ (relative to the peak intensity) shall limit the sampled wavelength interval, then corresponding lowest and highest angular frequencies are computed from

$$
\begin{gathered}
\omega_{\min }=\omega_{0}+\Delta \omega \cdot \sqrt{1 / S_{\min }-1} \\
\omega_{\max }=2 \omega_{0}-\omega_{\min }
\end{gathered}
$$

and the equivalent wavelengths follow from $\lambda=2 \pi c / \omega$.

## 133 Optical Components

### 133.1 Surfaces

### 133.1.1 Approximated Function Domain of Surfaces

Internally all surfaces have an Approximated Function Domain, which is either elliptical or rectangular. If you extend the (inner) definition area of the surface beyond this limit, you may noticed unwanted "bends" or too large values for the following reasons.

- The formula used to describe the surface really becomes invalid beyond this range. Most likely reason is that the radicand of a square root in the formula becomes less than zero. These invalid values are then replaced by the Position of Surrounding Plane ( $\varsigma$ Sec. 35.1.1.1). Example: Conical Surface ( $\leftrightarrows$ Sec. 35.2.4).
- The formula used to describe the surface becomes invalid somewhere beyond this range, but the exact shape of the boundary between valid and invalid values is unknown due to mathematical reasons. Then an Approximated Function Domain is used which for sure contains only valid values. Invalid values are replaced by the Position of Surrounding Plane ( $\leftrightarrows$ Sec. 35.1.1.1). This is the case for the Toroidal Asphere Surface ( $\rightarrow$ Sec. 35.2.12).
- The formula used to describe the surface is a polynomial which was designed to deliver height values within a certain range as long as you are in the Unit Radius. But outside of the unit radius the height values tend towards infinity. For these surfaces like the Zernike \& Seidel Surface ( $\leftrightarrows$ Sec. 35.2.14) the unit radius defines the Approximated Function Domain.
- You exceed the range of given data for data-based surfaces like the Sampled Surface ( $\leftrightarrows$ Sec. 35.2.11). Then extrapolation ( $\leftrightarrows$ Sec. 13.3) is used, which can lead to overshooting in case of cubic interpolation of the data.
- Programmable Surfaces ( $\rightarrow$ Sec. 35.2.9) always have an infinite Approximated Function Domain. But in case your snippet yields invalid values ( NaNs ), they are replaced by the Position of Surrounding Plane ( $\rightarrow$ Sec. 35.1.1.1).

If along the boundary of the (inner) definition area there are only invalid values, the boundary minimum and maximum is regarded as zero.

### 133.1.2 Height Discontinuities and Rescaling of Surfaces

VirtualLab Fusion allows to scale any surface in $x$-, $y$-, and $z$-direction, respectively. Furthermore, VirtualLab Fusion offers three mathematical operations which introduce height discontinuities into the height profile of an optical surface.

1. Pixelation introduces rectangular pixels. The height within one pixel remains constant. $\hookrightarrow$ Sec. 133.1.2.1.
2. Height Quantization introduces a limited number of equidistant discrete height levels. The height at a certain position is set to the nearest height level. $\leftrightarrows$ Sec. 133.1.2.2.
3. Using Fresnel zones, the height profile is wrapped so that all height values lie within a certain interval. $\rightarrow$ Sec. 133.1.2.3.
The following equation shows how and in which order these surface manipulations are applied.

$$
\begin{equation*}
h(x, y)=\mathcal{Q}\left(\alpha \mathcal{R}\left(h^{\prime}\left[\mathcal{P}\left(\frac{x}{\beta}\right), \mathcal{P}\left(\frac{y}{\gamma}\right)\right]\right)\right) \tag{133.1}
\end{equation*}
$$

$h^{\prime}(x, y)$ is the original height profile, e.g. that of a conical surface. $h(x, y)$ is the height profile after applying the aforementioned manipulations. $\beta, \gamma$ and $\alpha$ represent a scaling in x -direction, scaling in y -direction, and scaling in z-direction, respectively.
The scaling in $x$-direction and the scaling in $y$-direction effect the domain of definition of the surface function ( $\varsigma$ Sec. 35.1.1). Thus, you cannot enter values which are so small that the current size of the definition area exceeds the domain of definition of the surface function. The scaling in z-direction must not be zero, a negative scaling in z-Direction means that the height profile is inverted.
$\mathcal{P}(a)$ refers to the pixelation operator ( $\leftrightarrows$ Sec. 133.1.2.1), $\mathcal{Q}(h)$ to the quantization operator ( $\leftrightarrows$ Sec. 133.1.2.2), $\mathcal{R}(h)$ to the fresnelization operator ( $\leftrightarrows \mathrm{Sec} .133 .1 .2 .3$ ).

### 133.1.2.1 Pixelation

The pixelation function $p(a)$ introduces discrete rectangular pixels in the height profile and is defined as

$$
p(a)= \begin{cases}\operatorname{round}\left(\frac{a}{\Delta a}\right) \Delta a & ; \text { If pixelation is used. }  \tag{133.2}\\ a & ; \text { else }\end{cases}
$$

$\Delta a$ represents the pixel size along the x - or y -axis. The pixel size is in general different along both axes. Note, according to Eq. (133.1), the resulting pixelation effect (the size of a region for which the height is constant) is influenced by the scaling parameters $\beta$ (scaling in $\mathbf{x}$-direction) and $\gamma$ (scaling in $\mathbf{y}$-direction).

The Sampled Surface contains discrete, equidistantly sampled height values with sampling distances $\delta x$ and $\delta y$ along the $x$ - and $y$-axis, respectively. An additional interpolation method creates a continuous surface profile from these sampling points. If Nearest Neighbor is the interpolation method set in the sampled surface, rectangular pixels will always appear. Hence pixelation cannot be disabled then and the pixel sizes are fixed to $\delta x \cdot \delta y$.

### 133.1.2.2 Use Discrete Height Levels (Height Quantization)

The function $q(h)$ introduces discrete height levels in an optical surface and is defined as

$$
q(h)= \begin{cases}h & \text { If quantization is not used. }  \tag{133.3}\\ q_{\min } & \text { if } h_{\min } \leq h<q_{\min } \\ q_{\max } & \text { if } q_{\max }<h \leq h_{\max } \\ \text { round }\left(\frac{h-q_{\min }}{\Delta h}\right) \Delta h+q_{\min } & \text { else }\end{cases}
$$

$q_{\text {min }}$ and $q_{\text {max }}$ are the minimum and the maximum height level of the discretized height profile, respectively. $\Delta h$ is the height difference between two consecutive height levels and is defined as

$$
\begin{equation*}
\Delta h=\frac{q_{\max }-q_{\min }}{n-1} \tag{133.4}
\end{equation*}
$$

$h_{\text {min }}$ represents the minimum height of the original non-discretized surface and $h_{\text {max }}$ its maximum height. $n$ is the Number of Discrete Height Levels between and including $q_{\min }$ and $q_{\max }$. The function round $(x)$ returns the integer value closest to $x$.

## Quantization Function $q(h)$



Min-Max-Riser



User Defined


Figure 783. Illustration of the three quantization modes supported by VirtualLab Fusion. The top row shows the respective quantization functions $q(h)$ and the bottom row shows the effect if this quantization function is applied on a sample height profile.

The quantization mode Min-Max-Tread ensures that the z-extension does not change. To this end, $q_{\text {min }}$ is set to the original minimum height $h_{\text {min }}$ and $q_{\text {max }}$ is set to the original maximum height $h_{\text {max }}$. As you can see in the left part of Fig. 783, the "stairway" representing the quantization function starts with a tread (a horizontal region).
However, the Min-Max-Tread mode has a maximum quantization error $q(h)-h$ of $\frac{h_{\text {max }}-h_{\text {min }}}{2(n-1)}$. If one resigns the conservation of the z-extension, this error can be reduced to $\frac{h_{\max }-h_{\min }}{2 n}$. To this end, the mode Min-Max-Riser is available where $q_{\text {min }}=h_{\text {min }}+\frac{h_{\max }-h_{\text {min }}}{2 n}$ and $q_{\max }=h_{\text {max }}-\frac{h_{\text {max }}-h_{\text {min }}}{2 n}$. As you can see in the middle part of Fig. 783, the "quantization stairway" starts with a riser (a vertical line).
A third quantization mode named User Defined Min- and Max-Levels allows you to set arbitrary $q_{\text {min }}$ and $q_{\text {max }}$ values.
The following table summarizes the three modes.

| QUANTIZATION MODE | $Q_{\text {MIN }}$ | $Q_{\text {max }}$ |
| :---: | :---: | :---: |
| Min-Max-Tread | $h_{\text {min }}$ | $h_{\text {max }}$ |
| Min-Max-Riser | $h_{\text {min }}+\frac{h_{\text {max }}-h_{\text {min }}}{2 n}=h_{\text {min }}+\frac{\Delta h}{2}$ | $h_{\text {max }}-\frac{h_{\text {max }}-h_{\text {min }}}{2 n}=h_{\text {max }}-\frac{\Delta h}{2}$ |
| User Defined Min- and MaxLevels | User Defined | User Defined |
| $h_{\text {min }} \leq q_{\text {min }}<q_{\text {max }} \leq h_{\text {max }}$ |  |  |

The default quantization mode for new surfaces is Min-Max-Riser, with the exception of those surfaces which are by default restricted to a discrete number of height levels (Rectangular Grating Surface, Sampled Surface, and Transition Point List Surface). Those surfaces are set to Min-Max-Tread quantization by default so that quantization does not change the predefined height levels (if they are equidistant). Furthermore, a Rectangular Grating Surface is always discretized to two height levels.

### 133.1.2.3 Fresnel Zones

If you use Fresnel zones the height profile is "folded" so that all height values lie in the interval $-p \cdot h_{t} \ldots$ ( $1-$ $p) h_{\mathrm{t}}$. $h_{\mathrm{t}}$ refers to the Fresnel Height and $p$ refers to the Relative Position on $z$-Axis.
Thus, if the Relative Position on z-Axis is set to $0 \%$ the height values range from 0 to $+h_{t}$. This is the recommended setting for a height profile containing only positive height values (e.g. a conical surface with positive radius of curvature).
Vice versa, a Relative Position on z-Axis of $100 \%$ is recommended for surfaces with only negative height values as then the height values are in the range $-h_{t} \ldots 0$.
Any intermediate relative position is of course also feasible. Fig. 784 shows an example for the effect of the relative position.


Figure 784. A cylindrical surface with positive radius of curvature and Fresnel zones. The subfigures illustrate the effect of different values for the Relative Position on z-Axis $p$.
Left: $p=0 \%$. Height values range from 0 to 2 mm . Middle: $p=50 \%$. Height values range from -1 to 1 mm . Right: $p=99.99 \%$. Height values range from -2 to (nearly) 0 mm .

Note that the scaling in z-direction is applied after introducing the Fresnel zones. Thus the scaling in z-direction does not influence the positions of the Fresnel "jumps" but the total profile height of a surface with Fresnel "jumps" is the scaling factor $\alpha$ times the set Fresnel Height.

### 133.2 Coatings

The properties of a real coating naturally depend on the conditions of the process it was produced in. First of all, its thickness depends on the deposition parameters, like the flow direction of the material. Therefore VirtualLab Fusion allows you to specify some of these parameters, to produce more realistic coatings. The thickness $t_{c}$ of a coating at the position $\left(x_{c}, y_{c}, z_{c}\right)$ is modified by a factor $F_{\mathrm{HK}}$ that is derived from the Hertz-Knudsen-Law (Please read [BE04] or [Bun82] for more information about the deposition of thin films for producing coatings.):

$$
\begin{equation*}
t_{c}\left(x_{c}, y_{c}, z_{c}\right)=t_{0} \cdot F_{\mathrm{HK}}=t_{0} \cdot \cos \alpha \cos \Theta \cdot 1 / r_{S}^{2} \tag{133.5}
\end{equation*}
$$

In this equation, $t_{0}$ is the thickness of the coating as specified, that means without consideration of the processing parameters. The angle $\Theta$ is measured between the normal vector $n$ of the optical surface at position $\left(x_{c}, y_{c}, z_{c}\right)$ and the direction of the particle flow from the source at this point. $\alpha$ means the angle between this current flow and the direction of the maximum density flow $f$. The ratio of the distances $d_{0} / d_{c}$ equals $r_{S}$ (where $d_{0}$ denotes the distance of the particle source to the origin of the coordinate system, where the optical axis intersects the surface; and $d_{c}$ is measured from the particle source to the current position $\left(x_{c}, y_{c}, z_{c}\right)$ ). Please see also Fig. 785. As you can see, the Hertz-Knudsen-Law assumes a flux density, decreasing laterally with a cosine law, and decreasing axially with an $1 / r^{2}$-law.


Figure 785. Sketch of the meaning of the processing parameters of coatings.

### 133.3 Media

### 133.3.1 Scaling and Periodization of Media

Inhomogeneous optical media in VirtualLab Fusion define an arbitrary refractive index distribution $n(x, y, z)$. From this index distribution one can derive a new index distribution $n^{\prime}(x, y, z)$ that includes scaling and periodization along the $\mathrm{x}-, \mathrm{y}$ - , and z -direction.

$$
\begin{equation*}
n^{\prime}(x, y, z)=n\left(\frac{x \% P_{x}}{S_{x}}, \frac{y \% P_{y}}{S_{y}}, \frac{z \% P_{z}}{S_{z}}\right) \tag{133.6}
\end{equation*}
$$

$S_{x}, S_{y}$ and $S_{z}$ represent a Scaling in x-Direction, Scaling in y-Direction, and Scaling in z-Direction, respectively. $\chi \% P$ is a modulo operator performing the operation $\chi^{\prime}=\chi \pm \ell P ; \ell \in \mathbb{Z}$ whereas the resulting $\chi^{\prime}$ lies in the (cuboid shaped) elementary cell. This elementary cell is defined as ( $-P_{x} / 2 \ldots+P_{x} / 2 ;-P_{y} / 2 \ldots+P_{y} / 2 ; 0 \ldots P_{z}$ ).

### 133.3.2 GRIN Medium

A GRIN medium is described by a base material and an analytical formula which alters the refractive index of this base material.
There are several equations to describe the refractive index modulation. The following formulas are implemented:

$$
\begin{align*}
& n(s)=n_{0}+\sum_{i=1}^{N} n_{i} s^{i}  \tag{133.7}\\
& n(s)=\sqrt{n_{0}+\sum_{i=1}^{N} n_{i} s^{i}}  \tag{133.8}\\
& n(s)= \begin{cases}n_{0} \sqrt{1-2 \Delta\left(\frac{s}{b}\right)^{p}} & , s \leq b \\
n_{1}=n_{0} \sqrt{1-2 \Delta} & , s>b\end{cases}  \tag{133.9}\\
& n(s)=n_{0}\left(1-\frac{g^{2}}{2} s^{2}\right) \tag{133.10}
\end{align*}
$$

$n_{0}$ is the wavelength dependent complex refractive index of the base material. In the first two cases you define the maximum order $N$ and the individual parameters $n_{i}$.

## Annotations

- $n_{0}$ is the wavelength dependent complex-valued refractive index of the base material.
- The actual meaning of $s$ depends on the chosen symmetry. You can define a GRIN lens with either rotational symmetry $\left(s=\sqrt{x^{2}+y^{2}}\right.$ ) or with cylindrical symmetry ( $s=|x \cos \alpha+y \sin \alpha|$ with the rotation angle $\alpha$ ). $\alpha=0^{\circ}$ refers to modulation in x-direction only and $\alpha=90^{\circ}$ refers to modulation in $y$-direction only.
- For the Polynomial (Eq. (133.7)) and the Square Root of Polynomial (Eq. (133.8)) you define the maximum order $N$ and the individual parameters $n_{i}$.
- The Power Law Index Profile is usually used to describe an optical fiber with a GRIN profile. Then the border $b$ is equal to the core radius of the fiber. The decrease $\Delta$ describes how much the refractive index is decreased till the border. Alternatively one can use the refractive index $n_{1}$ at and outside of the border. The two values are related via $n_{1}=n_{0} \sqrt{1-2 \Delta}$. The (positive) exponent $p$ of the equation is close to 2 for common GRIN fibers and infinity for step-index fibers. This formula is taken from [Nat].
- Approximation of sech(s) (Eq. (133.9)) is a commonly used formula to characterize GRIN media, whereas the parameter $g$ is referred to as gradient constant. The also-used equation $n(\xi)=n_{0} \cdot \operatorname{sech}(g r)$ yields nearly identical results for real GRIN lenses. Instead of the gradient constant $g$ also the "pitch length" $P_{L}=2 \pi / g$ can be used. In a lens with a length equal to the pitch length, light exits at the same position as it has entered the lens ( $\hookrightarrow$ Fig. 786). Manufacturers usually do not give the pitch length $P_{L}$ but the length $z$ of the lens and its "pitch" $P$.

$$
\begin{align*}
P & =\frac{z}{P_{L}} \quad \text { and thus }  \tag{133.11}\\
g & =\frac{2 \pi P}{z} \tag{133.12}
\end{align*}
$$



Figure 786. Effect of a GRIN lens on collimated incident light. The pictured lens has a pitch of approximately 1.1. As you can see, a GRIN lens with a pitch of 0.25 would focus collimated light immediately after the lens.

### 133.3.3 Volume Grating Medium

The volume grating medium is designed for analyzing interferograms recorded into a photosensitive Holographic Material. In VirtualLab Fusion the interferograms can be synthesized by the superposition of an arbitrary number of plane waves.
Mathematically, the x-period of the volume grating medium is the least common multiple of all subperiods $P_{n m}=2 \pi /\left(k_{x, n}-k_{x, m}\right)$. As given angles $\alpha_{n}$ and $\alpha_{m}$ do not transfer linearly into wave numbers $k_{x, n}$ and $k_{x, m}$, even the simple case of three interfering waves with angles $\alpha$ of $0^{\circ}, 10^{\circ}$, and $20^{\circ}$ would lead to a period of far more than one meter. As periods this large are not used in reality, you can specify a Limit Period which leads to quantized wave numbers. The smaller the Test Period the larger the difference between original and quantized angles can become. Under certain conditions the resulting Structure Period of Quantized Medium can be $\frac{1}{n}$ the test period, where $n$ is an integer. This period is used in simulations, as smaller periods lead to less computational effort.

The interference pattern can be described as local time-averaged energy density $\bar{w}(x, y, z)$.

$$
\begin{equation*}
\bar{w}(x, y, z)=\epsilon_{0} n_{\text {base }}^{2}\left(\sum_{n} E_{n} e^{i \Phi_{n}(x, y, z)}\right)^{2} \tag{133.13}
\end{equation*}
$$

The phase function $\Phi_{n}(x, y, z)$ depends on the incident angle and wavelength of the $n^{\text {th }}$ wave. It is assumed that only waves of exactly the same wavelength will interfere with each other.
$E_{n}$ is the amplitude of the $n^{\text {th }}$ wave. It is calculated as follows:

$$
\begin{equation*}
E_{n}=\sqrt{\frac{F_{n}}{\sum_{n} F_{n}} \frac{w_{\max }}{\epsilon_{0} n_{\mathrm{base}}^{2}}} \tag{133.14}
\end{equation*}
$$

$w_{\text {max }}$ is the overall energy density of all superposing plane waves. $F_{n}$ is the Weight factor of the $n^{\text {th }}$ wave. Eqs. (133.13)-(133.14) follow from Maxwell's equations assuming $n=\sqrt{\epsilon}$ and $\mu=1$.

### 133.3.3.1 Index Modulation

The following equations specify how the local electrical field density $\bar{w}(x, y, z)$ ( $\hookrightarrow$ Eq. (133.13)) is converted into a change of the refractive index. The volume grating medium offers three different modes therefor:

## (a) Direct

In this case you just specify the desired Refractive Index Modulation $\Delta n$. The refractive index $n(x, y, z)$ at a certain position is then calculated via

$$
\begin{equation*}
n(x, y, z)=n_{\text {holo }}+\frac{\bar{w}(x, y, z)}{w_{\max }} \cdot \Delta n \tag{133.15}
\end{equation*}
$$

$w_{\text {max }}$ can be an arbitrary value, as it cancels out in this case (see Eqs. (133.13)-(133.14)). $n_{\text {holo }}$ is the refractive index of the Holographic Material.

## (b) Simulate Exposition Process

In this case you simulate the real exposition process. This means you can set up the overall Power Density $P$ of all superposing waves, the Exposure Time $t_{\exp }$ and the Material Response.

Then, the overall energy density is calculated as follows:

$$
\begin{equation*}
w_{\max }=P \cdot t_{\exp } \tag{133.16}
\end{equation*}
$$

You can choose between three equations how the Dose to Refractive Index Modulation is modeled:

DOSE TO REFRACTIVE EQUATION

## PARAMETERS

INDEX MODULATION

| Linear | $n(x, y, z)=n_{\text {holo }}+l \bar{w}(x, y, z)$ | $l$ : Linear Factor |
| :--- | :--- | :--- |
| Quadratic | $n(x, y, z)=\quad n_{\text {holo }}+l \bar{w}(x, y, z)+$ | $l$ : Linear Factor |
|  | $p \bar{w}(x, y, z)^{2}$ | $p:$ Squared Factor |
| Asymptotic | $n(x, y, z)=n_{\text {holo }}+\Delta n-\frac{\Delta n}{1+\left(\bar{w}(x, y, z) / w_{0}\right)^{\gamma}}$ | $\Delta n:$ Refractive Index Modulation |
|  |  | $w_{0}:$ Average Energy Density |
|  |  | $\gamma:$ Modulation Exponent |
|  |  | $\hookrightarrow$ Fig. 787 |
|  |  |  |



Figure 787. The refractive indices $n(w)$ if asymptotic dose to refractive index modulation is chosen. The blue curve has the smallest modulation exponent and the red curve the largest.

## (c) Photonic Crystals

In this case it is assumed that above a certain energy density $w_{\mathrm{t}}$ the original Holographic Material is replaced by a second material. In VirtualLab Fusion you enter the relative Threshold, i. e. $\frac{w_{t}}{w_{\text {max }}}$.

### 133.4 Materials

The following dispersion formulas are implemented in VirtualLab Fusion to describe the wavelength dependency of the real part of the refractive index analytically:

## FORMULA NAME EQUATION

## Sellmeier 1

$$
n=\sqrt{\frac{K_{1} \cdot \lambda^{2}}{\lambda^{2}-L_{1}}+\frac{K_{2} \cdot \lambda^{2}}{\lambda^{2}-L_{2}}+\frac{K_{3} \cdot \lambda^{2}}{\lambda^{2}-L_{3}}+1}
$$

## Sellmeier 2

$$
n=\sqrt{A+\frac{B_{1} \cdot \lambda^{2}}{\lambda^{2}-\lambda_{1}^{2}}+\frac{B_{2}}{\lambda^{2}-\lambda_{2}^{2}}+1}
$$

## Sellmeier 3

$$
n=\sqrt{\frac{K_{1} \cdot \lambda^{2}}{\lambda^{2}-L_{1}}+\frac{K_{2} \cdot \lambda^{2}}{\lambda^{2}-L_{2}}+\frac{K_{3} \cdot \lambda^{2}}{\lambda^{2}-L_{3}}+\frac{K_{4} \cdot \lambda^{2}}{\lambda^{2}-L_{4}}+1}
$$

## Sellmeier 4

$$
n=\sqrt{A+\frac{B \cdot \lambda^{2}}{\lambda^{2}-C}+\frac{D \cdot \lambda^{2}}{\lambda^{2}-E}}
$$

## Sellmeier 5

$$
n=\sqrt{\frac{K_{1} \cdot \lambda^{2}}{\lambda^{2}-L_{1}}+\frac{K_{2} \cdot \lambda^{2}}{\lambda^{2}-L_{2}}+\frac{K_{3} \cdot \lambda^{2}}{\lambda^{2}-L_{3}}+\frac{K_{4} \cdot \lambda^{2}}{\lambda^{2}-L_{4}}+\frac{K_{5} \cdot \lambda^{2}}{\lambda^{2}-L_{5}}+1}
$$

## Schott

$$
n=\sqrt{A_{0}+A_{1} \cdot \lambda^{2}+\frac{A_{2}}{\lambda^{2}}+\frac{A_{3}}{\lambda^{4}}+\frac{A_{4}}{\lambda^{6}}+\frac{A_{5}}{\lambda^{8}}}
$$

This formula is no longer used by Schott itself but by many other glass manufacturers.

## Herzberger

$$
n=A+B \cdot L+C \cdot L^{2}+D \cdot \lambda^{2}+E \cdot \lambda^{4}+F \cdot \lambda^{6} \quad \text { with } L=\frac{1}{\lambda^{2}-0.028}
$$

The Herzberger formula is mainly used in the infrared spectrum.

## Conrady

$$
n=n_{0}+\frac{A}{\lambda}+\frac{B}{\lambda^{3.5}}
$$

Useful formula to fit data with only few data points.

## Handbook Optics 1

$$
n=\sqrt{A+\frac{B}{\lambda^{2}-C}-D \cdot \lambda^{2}}
$$

## Handbook Optics 2

$$
n=\sqrt{A+\frac{B \cdot \lambda^{2}}{\lambda^{2}-C}-D \cdot \lambda^{2}}
$$

## Cauchy

$$
n=A+\frac{B}{\lambda^{2}}+\frac{C}{\lambda^{4}}+\frac{D}{\lambda^{6}}
$$

## Edlén 1994 (for Air)

$n=1+\frac{p\left(n_{s t}-1\right)}{96095.43} \cdot \frac{1+10^{-8}(0.601-0.00972 T) p}{1+0.0036610 \cdot T}-f\left(3.7345-0.0401 \frac{1}{\lambda^{2}}\right) \cdot 10^{-10}$
with
$n_{s t}=8.34254 \cdot 10^{-5}+0.02406147 /\left(130-\frac{1}{\lambda^{2}}\right)+1.5998 \cdot 10^{-4} /\left(38.9-\frac{1}{\lambda^{2}}\right)+1$,
$p$ being the atmospheric pressure in $\mathrm{Pa}, T$ being the temperature in ${ }^{\circ} \mathrm{C}$, and $f$ being the Partial Pressure of Water Vapor in Pa. While the latter can be entered in the dialog, the pressure and temperature are taken from the Optical Setup which is simulated.

## Edlén 1953 (for Air)

$$
n=1+\frac{n_{s t}-1}{1+0.0034785 \cdot(T-15)} \cdot p / 101325-55 \cdot 10^{-9} \cdot 0.0075 f /(1+0.00367 \cdot T)
$$

with

$$
n_{s t}=6.4328 \cdot 10^{-5}+0.0294981 /\left(146-\frac{1}{\lambda^{2}}\right)+2.554 \cdot 10^{-4} /\left(41-\frac{1}{\lambda^{2}}\right)+1
$$

$p$ being the atmospheric pressure in $\mathrm{Pa}, T$ being the temperature in ${ }^{\circ} \mathrm{C}$, and $f$ being the Partial Pressure of Water Vapor in Pa. While the latter can be entered in the dialog, the pressure and temperature are taken from the Optical Setup which is simulated.

## Power Series

$$
n=\sqrt{\sum_{i=0}^{3} A_{i} \cdot \lambda^{2 i}+\sum_{k=1}^{6} A_{k+3} \cdot \lambda^{-2 k}}
$$

## Abbe Number ( $v_{d}$ )

$$
n(\lambda)=A+\frac{B}{\lambda^{2}}
$$

with

$$
B=\frac{n_{\mathrm{d}}-1}{v_{\mathrm{d}}\left(\lambda_{\mathrm{F}}^{-2}-\lambda_{\mathrm{C}}^{-2}\right)}
$$

and

$$
A=n_{\mathrm{d}}-\frac{B}{\lambda_{\mathrm{d}}^{2}}
$$

$v_{\mathrm{d}}$ being the (classic) Abbe number, $n_{\mathrm{d}}$ the refractive index at the Fraunhofer line $\mathrm{d}\left(\lambda_{\mathrm{d}}=587.5618 \mathrm{~nm}\right)$. Additionally, the Fraunhofer lines F and $\mathrm{C}\left(\lambda_{\mathrm{F}}=H_{\beta}=\right.$ $486.134 \mathrm{~nm} ; \lambda_{\mathrm{C}}=H_{\alpha}=656.281 \mathrm{~nm}$ ) are used.

## Abbe Number ( $v_{e}$ )

$$
n(\lambda)=A+\frac{B}{\lambda^{2}}
$$

with

$$
B=\frac{n_{\mathrm{e}}-1}{v_{\mathrm{e}}\left(\lambda_{\mathrm{F}}^{-2}-\lambda_{\mathrm{C}^{\prime}}^{-2}\right)}
$$

and

$$
A=n_{\mathrm{e}}-\frac{B}{\lambda_{\mathrm{e}}^{2}}
$$

$v_{\mathrm{e}}$ being the (alternative) Abbe number, $n_{\mathrm{e}}$ the refractive index at the Fraunhofer line e $\left(\lambda_{\mathrm{e}}=546.07 \mathrm{~nm}\right)$. Additionally, the Fraunhofer lines F' and $\mathrm{C}^{\prime}\left(\lambda_{\mathrm{F}}{ }^{\prime}=\right.$ $479.99 \mathrm{~nm} ; \lambda_{\mathrm{C}^{\prime}}=643.85 \mathrm{~nm}$ ) are used.

## 134 Functions

### 134.1 ABCD Matrix Simulation

ABCD matrices give an easy way to describe transformations in radial symmetric optical systems without limiting apertures, in paraxial approximation. Given a vector $r_{\text {in }}=(x, \alpha)^{T}$ describing the distance $x$ to the optical axis and the direction component $\alpha$ (direction cosine) of an incoming (local) plane wave it is transformed by an ABCD matrix $\mathcal{M}$ to the vector $r_{\text {out }}$ :

$$
r_{\mathrm{out}}=\binom{x^{\prime}}{\alpha^{\prime}}=\mathcal{M} \cdot r_{\mathrm{in}}=\left(\begin{array}{ll}
A & B  \tag{134.1}\\
C & D
\end{array}\right)\binom{x}{\alpha}
$$

Simple optical elements can be described by specific matrices e.g. ( $\left(\begin{array}{ll}1 & d \\ 0 & 1\end{array}\right)$ for a free space propagation of distance $d$, or $\left(\begin{array}{cc}1 & 0 \\ -f^{-1} & 1\end{array}\right)$ for an infinitely extensive, thin lens with focal length $f$. A system consisting of several optical elements is described by the product of their matrices (where the order of multiplication depends on the order in which the elements are passed by the light):

$$
\begin{equation*}
\boldsymbol{\mathcal { M }}_{\text {system }}=\mathcal{M}_{n-1} \times \mathcal{M}_{n-2} \times \cdots \times \mathcal{M}_{0} \tag{134.2}
\end{equation*}
$$

In this equation $\mathcal{M}_{0}$ is the first of $n$ elements passed through, $\mathcal{M}_{n-1}$ is the last.
Collins [Col70] described a way to use ABCD matrices for wave optics by giving the following equation (Collins Integral, here simplified for one dimension),

$$
\begin{align*}
& U_{\mathrm{out}}\left(x^{\prime}\right)=-\frac{i k}{2 \pi B} \exp \left(i k L_{0}\right) \\
& \qquad \int_{-\infty}^{\infty} U_{\text {in }}(x) \exp \left[\frac{i k}{2 B}\left(A x^{2}-2 x x^{\prime}+D x^{\prime 2}\right)\right] \mathrm{d} x \tag{134.3}
\end{align*}
$$

where $L_{0}$ is the axial optical distance of the system. Please note that Collins used a differing notation for the matrix elements, where A and D are interchanged as well as B and C. From the given equation (134.3), which can be understood as a kind of Fresnel transform, the propagation of spectrum of plane waves as well as the Rayleigh-Sommerfeld convolution can be derived. All three propagation types are physically equivalent (and paraxial approximations(!), due to the nature of ABCD matrix representations) and differ only in the numerical accuracy. For more information about the propagation types and their application read Sec. 93.
Important: As it is not possible to enter the axial optical distance $L_{0}$, the phase of the result of Eq. (134.3) has got a constant offset to the real phase, except the case of $B=0$, that means the geometrical and optical axial distance is $=0$.

Furthermore, ABCD matrices give an easy way to describe the transformation of a Gaussian beam in radially symmetric optical systems without limiting apertures. Therefor the complex radius of curvature $q$ of a Gaussian beam is defined as follows:

$$
\begin{equation*}
\frac{1}{q(z)}=\frac{1}{R(z)}-i \frac{\mathrm{M}^{2} \lambda}{\pi w(z)^{2}} \tag{134.4}
\end{equation*}
$$

$R(z)$ is the Phase Radius at a certain position $z$ and $w(z)$ is the Beam Radius at the same position $z$. Furthermore, $\mathrm{M}^{2}$ is the $M^{2}$ Parameter of the Gaussian beam and $\lambda$ its wavelength. See also Sec. 132.1 for reference. The complex radius of curvature $q_{\text {in }}$ of the input Gaussian beam is transformed by an ABCD matrix $\mathcal{M}$ into the complex radius of curvature $q_{\text {out }}$ of the output Gaussian beam by the so-called ABCD law [ST91]:

$$
\begin{equation*}
q_{\mathrm{out}}=\frac{A q_{\mathrm{in}}+B}{C q_{\mathrm{in}}+D} \tag{134.5}
\end{equation*}
$$

### 134.2 Zernike \& Seidel Aberrations

### 134.2.1 Zernike Polynomials

Zernike Polynomials are usually defined in normalized polar coordinates $(\rho, \theta)$, where $0 \leq \rho \leq 1 ; 0 \leq \theta \leq 2 \pi$. Thus the radii $r=\sqrt{x^{2}+y^{2}}$ have to be converted into $\rho=r / r_{\text {max }}$ where $r_{\text {max }}$ is the maximum radial extent of all positions.
Zernike polynomials are defined in standard form in Born and Wolf [BW83] as follows

$$
\begin{equation*}
Z_{n}^{m}(\rho, \theta)=N_{n}^{m} R_{n}^{m}(\rho) \Theta_{m}(\theta) \tag{134.6}
\end{equation*}
$$

The normalization constant is

$$
\begin{equation*}
N_{n}^{m}=\sqrt{\frac{2(n+1)}{1+\delta_{m 0}}} \tag{134.7}
\end{equation*}
$$

the radial polynomial is

$$
\begin{equation*}
R_{n}^{m}(\rho)=\sum_{s=0}^{\frac{n-|m|}{2}} \frac{(-1)^{s}(n-s)!}{s!\left(\frac{n+m}{2}-s\right)!\left(\frac{n-m}{2}-s\right)!} \rho^{n-2 s} \tag{134.8}
\end{equation*}
$$

and azimuthal component is given by

$$
\Theta_{m}(\theta)= \begin{cases}\cos (|m| \theta) & \text { for } m \geq 0 \\ \sin (|m| \theta) & \text { for } m<0\end{cases}
$$

$m$ is the azimuthal order and $n$ is the radial order. The following table lists the first 36 Zernike polynomials whereas the index $i$ is the sequential OSA / ANSI standard index ${ }^{1}$. Fig. 788 illustrates the relation between the indices $i, m$, and $n$ for the first 91 Zernike polynomials.

[^18]| $i$ | $n$ | $m$ | $Z_{i}(r, \theta)=Z_{n}^{m}(r, \theta)$ | Name |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 0 | 1 | Piston |
| 2 | 1 | -1 | $2 \rho \sin \theta$ | Tilt Y |
| 3 | 1 | 1 | $2 \rho \cos \theta$ | Till X |
| 4 | 2 | -2 | $\sqrt{6} \rho^{2} \sin 2 \theta$ | Astigmatism Y |
| 5 | 2 | 0 | $\sqrt{3}\left(2 \rho^{2}-1\right)$ | Defocus |
| 6 | 2 | 2 | $\sqrt{6} \rho^{2} \cos 2 \theta$ | Astigmatism X |
| 7 | 3 | -3 | $\sqrt{8} \rho^{3} \sin 3 \theta$ | Trefoil Y |
| 8 | 3 | -1 | $\sqrt{8}\left(3 \rho^{3}-2 \rho\right) \sin \theta$ | Coma Y |
| 9 | 3 | 1 | $\sqrt{8}\left(3 \rho^{3}-2 \rho\right) \cos \theta$ | Coma X |
| 10 | 3 | 3 | $\sqrt{8} \rho^{3} \cos 3 \theta$ | Trefoil $X$ |
| 11 | 4 | -4 | $\sqrt{10} \rho^{4} \sin 4 \theta$ | Tetrafoil Y |
| 12 | 4 | -2 | $\sqrt{10}\left(4 \rho^{4}-3 \rho^{2}\right) \sin 2 \theta$ | Secondary Astigmatism Y |
| 13 | 4 | 0 | $\sqrt{5}\left(6 \rho^{4}-6 \rho^{2}+1\right)$ | Spherical |
| 14 | 4 | 2 | $\sqrt{10}\left(4 \rho^{4}-3 \rho^{2}\right) \cos 2 \theta$ | Secondary Astigmatism X |
| 15 | 4 | 4 | $\sqrt{10} \rho^{4} \cos 4 \theta$ | Tetrafoil X |
| 16 | 5 | -5 | $\sqrt{12} \rho^{5} \sin 5 \theta$ | Pentafoil Y |
| 17 | 5 | -3 | $\sqrt{12}\left(5 \rho^{5}-4 \rho^{3}\right) \sin 3 \theta$ | Secondary Trefoil Y |
| 18 | 5 | -1 | $\sqrt{12}\left(10 \rho^{5}-12 \rho^{3}+3 \rho\right) \sin \theta$ | Secondary Coma Y |
| 19 | 5 | 1 | $\sqrt{12}\left(10 \rho^{5}-12 \rho^{3}+3 \rho\right) \cos \theta$ | Secondary Coma X |
| 20 | 5 | 3 | $\sqrt{12}\left(5 \rho^{5}-4 \rho^{3}\right) \cos 3 \theta$ | Secondary Trefoil $X$ |
| 21 | 5 | 5 | $\sqrt{12} \rho^{5} \cos 5 \theta$ | Pentafoil $X$ |
| 22 | 6 | -6 | $\sqrt{14} \rho^{6} \sin 6 \theta$ | Hexafoil Y |
| 23 | 6 | -4 | $\sqrt{14}\left(6 \rho^{6}-5 \rho^{4}\right) \sin 4 \theta$ | Secondary Tetrafoil Y |
| 24 | 6 | -2 | $\sqrt{14}\left(15 \rho^{6}-20 \rho^{4}+6 \rho^{2}\right) \sin 2 \theta$ | Tertiary Astigmatism Y |
| 25 | 6 | 0 | $\sqrt{7}\left(20 \rho^{6}-30 \rho^{4}+12 \rho^{2}-1\right)$ | Secondary Spherical |
| 26 | 6 | 2 | $\sqrt{14}\left(15 \rho^{6}-20 \rho^{4}+6 \rho^{2}\right) \cos 2 \theta$ | Tertiary Astigmatism X |
| 27 | 6 | 4 | $\sqrt{14}\left(6 \rho^{6}-5 \rho^{4}\right) \cos 4 \theta$ | Secondary Tetrafoil $X$ |
| 28 | 6 | 6 | $\sqrt{14} \rho^{6} \cos 6 \theta$ | Hexafoil $X$ |
| 29 | 7 | -7 | $4 \rho^{7} \sin 7 \theta$ | Heptafoil Y |
| 30 | 7 | -5 | $4\left(7 \rho^{7}-6 \rho^{5}\right) \sin 5 \theta$ | Secondary Pentafoil $Y$ |
| 31 | 7 | -3 | $4\left(21 \rho^{7}-30 \rho^{5}+10 \rho^{3}\right) \sin 3 \theta$ | Tertiary Trefoil Y |
| 32 | 7 | -1 | $4\left(35 \rho^{7}-60 \rho^{5}+30 \rho^{3}-4 \rho\right) \sin \theta$ | Tertiary Coma Y |
| 33 | 7 | 1 | $4\left(35 \rho^{7}-60 \rho^{5}+30 \rho^{3}-4 \rho\right) \cos \theta$ | Tertiary Coma X |
| 34 | 7 | 3 | $4\left(21 \rho^{7}-30 \rho^{5}+10 \rho^{3}\right) \cos 3 \theta$ | Tertiary Trefoil X |
| 35 | 7 | 5 | $4\left(7 \rho^{7}-6 \rho^{5}\right) \cos 5 \theta$ | Secondary Pentafoil $X$ |
| 36 | 7 | 7 | $4 \rho^{7} \cos 7 \theta$ | Heptafoil X |



Figure 788. This figure shows the first 91 Zernike polynomials and their corresponding radial order $n$ and azimuthal or$\operatorname{der} \theta$. The black numbers in the squares give the OSA / ANSI standard index $i$. The red numbers give the index of the corresponding Zernike fringe aberrations. Those Zernike polynomials which can be converted into Seidel aberrations are marked by a green frame.

### 134.2.2 Zernike Fringe and Seidel Aberrations

Zernike fringe aberrations are a commonly used subset of 37 Zernike polynomials ( $\hookrightarrow$ Fig. 788) whereas for Zernike fringe aberrations the normalization constant $N_{n}^{m}$ in Eq. (134.6) always equals 1.

There are six Seidel aberrations:

| NAME | FORMULA |
| :--- | :--- |
| Piston | $M_{P}$ |
| Distortion | $M_{\mathrm{D}} \cdot \rho \cos \left(\theta-\theta_{\mathrm{D}}\right)$ |
| Field Curvature | $M_{\mathrm{F}} \cdot \rho^{2}$ |
| Astigmatism | $M_{\mathrm{A}} \cdot \rho^{2} \cos ^{2}\left(\theta-\theta_{\mathrm{A}}\right)$ |
| Coma | $M_{\mathrm{C}} \cdot \cos \left(\theta-\theta_{\mathrm{C}}\right)$ |
| Spherical Aberration | $M_{\mathrm{S}} \cdot \rho^{4}$ |

The $M_{\text {? }}$ and $\theta_{\text {? }}$ give the magnitude and the orientation angle of the corresponding Seidel aberrations. They can be derived out of the coefficients of the first nine Zernike fringe aberrations using the formulas given in table $\vee$ of [WC92].

## 135 Manipulations

### 135.1 Array - Array Operations

There are four basic arithmetic operations for arrays: addition, subtraction, multiplication, and division and additionally the convolution.
In the case that the two arrays of a array-array operation have not the same sampling distance or the same array size, at least one of the fields or transmissions has to be resampled before the calculation, because the underlying operation works pointwise.
The following table shows which parameter has to be adjusted in what case for each operation. The second and the third column show how the sampling distance $\Delta_{\text {new }}$ and the array size $S_{\text {new }}$ of the resulting array are determined by the sampling parameters of the operands (indices 1 and 2). Before starting the calculation, the $\operatorname{array}(s)$ that has got sampling parameters different from that of the result field must be resampled.

Important: The sampling parameters for the directions x and y are checked and adjusted independently!

| Operation | $\Delta_{\text {new }}$ | $S_{\text {new }}$ |
| :--- | :---: | :---: |
| Addition | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |
| Subtraction | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |
| Multiplication | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\min \left(S_{1}, S_{2}\right)$ |
| Division | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\min \left(S_{1}, S_{2}\right)$ |
| Convolution | $\Delta_{\text {new }}=\min \left(\Delta_{1}, \Delta_{2}\right)$ | $S_{\text {new }}=\max \left(S_{1}, S_{2}\right)$ |

### 135.1.1 Basic Arithmetic Operations

Different types of Complex Amplitude Documents (Harmonic Field vs. Transmission) cannot be used as operands in every possible combination. A summary of all combinable types and their result for all operations is shown in the following tables 135.1-135.3. The used abbreviations are (GP) for globally polarized fields and (LP) for locally polarized fields.
Note: If the normalization factor of the Jones vector $J^{\prime}$ is zero, the resulting field is set to zero and the Jones vector to $(1,0)^{T}$. If for one sampling point a division by zero occurs, then the result is set to zero too.

| $1^{\text {st }}$ Operand | $2^{\text {nd }}$ Operand |  |  |
| :---: | :---: | :---: | :---: |
|  | Transmission | Harmonic Field (GP) | Harmonic Field (LP) |
| Transmission | Result: Transmission $\begin{aligned} & t=t_{1} \pm t_{2} \\ & \mathcal{J}=\mathcal{J}_{\mathbf{1}} \end{aligned}$ | - | - |
| Harmonic Field (GP) | - | $\text { if } J_{1}=J_{2}$ <br> Result: Harmonic Field (GP) $\begin{aligned} & J=J_{1} \\ & U=U_{1} \pm U_{2} \end{aligned}$ <br> else <br> Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=J_{1, x} U_{1} \pm J_{2, x} U_{2} \\ & E_{y}=J_{1, y} U_{1} \pm J_{2, y} U_{2} \end{aligned}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=J_{1, x} U_{1} \pm E_{2, x} \\ & E_{y}=J_{1, y} U_{1} \pm E_{2, y} \end{aligned}$ |
| Harmonic Field (LP) | - | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} \pm J_{2, x} U_{2} \\ & E_{y}=E_{1, y} \pm J_{2, y} U_{2} \end{aligned}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} \pm E_{2, x} \\ & E_{y}=E_{1, y} \pm E_{2, y} \end{aligned}$ |

Table 135.1: Addition or Subtraction of two Complex Amplitudes

| $1^{\text {st }}$ Operand | $2^{\text {nd }}$ Operand |  |  |
| :---: | :---: | :---: | :---: |
|  | Transmission | Harmonic Field (GP) | Harmonic Field (LP) |
| Transmission | Result: Transmission $\begin{aligned} & t=t_{1} \cdot t_{2} \\ & \mathcal{J}=\mathcal{J}_{1} \times \mathcal{J}_{2} \end{aligned}$ | Result: Harmonic Field (GP) ${ }^{\dagger}$ $\begin{aligned} & U=t_{1} \cdot U_{2} \cdot\left\|\mathcal{J}_{1} \times \boldsymbol{J}_{\mathbf{2}}\right\| \\ & \boldsymbol{J}=\left(\mathcal{J}_{\mathbf{1}} \times \boldsymbol{J}_{\mathbf{2}}\right) /\left\|\mathcal{J}_{\mathbf{1}} \times \boldsymbol{J}_{\mathbf{2}}\right\| \end{aligned}$ | Result: Harmonic Field (LP) ${ }^{\dagger}$ $\boldsymbol{E}_{\mathrm{xy}}=\left(\mathcal{J}_{\mathbf{1}} \times \boldsymbol{E}_{\mathrm{xy}, 2}\right) t_{1}$ |
| Harmonic Field (GP) | Result: Same as for Transmission times Harmonic Field (GP), i.e. the operands are swapped internally. ${ }^{\dagger}$ | Result: Harmonic Field (GP) $\begin{aligned} U & =U_{1} \cdot U_{2} \\ J_{x} & =J_{1, x} J_{2, x} /\left\|J^{\prime}\right\| \\ J_{y} & =J_{1, y} J_{2, y} /\left\|J^{\prime}\right\| \end{aligned}$ <br> with $\left\|J^{\prime}\right\|=\sqrt{\left\|J_{1, x} J_{2, x}\right\|^{2}+\left\|J_{1, y} J_{2, y}\right\|^{2}}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=\left(J_{1, x} \cdot U_{1}\right) E_{2, x} \\ & E_{y}=\left(J_{1, y} \cdot U_{1}\right) E_{2, y} \end{aligned}$ |
| Harmonic Field (LP) | Result: Harmonic Field (LP) ${ }^{\dagger}$ $\boldsymbol{E}_{\mathrm{xy}}=\left(\mathcal{J}_{2} \times \boldsymbol{E}_{\mathrm{xy}, 1}\right) t_{2}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x}\left(J_{2, x} \cdot U_{2}\right) \\ & E_{y}=E_{1, y}\left(J_{2, y} \cdot U_{2}\right) \end{aligned}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} \cdot E_{2, x} \\ & E_{y}=E_{1, y} \cdot E_{2, y} \end{aligned}$ |

Table 135.2: Multiplication of two Complex Amplitudes.
$\times$ refers to a matrix multiplication.
${ }^{\dagger}$ Please note: There is a global option ( $\hookrightarrow$ Sec. 6.12) which allows to embed the result of a multiplication of harmonic field and transmission into an additional frame of zeros.

| $1{ }^{\text {st }}$ Operand | $2^{\text {nd }}$ Operand |  |  |
| :---: | :---: | :---: | :---: |
|  | Transmission | Harmonic Field (GP) | Harmonic Field (LP) |
| Transmission | Result: Transmission $\begin{gathered} t=t_{1} / t_{2} \\ \mathcal{J}=\mathcal{J}_{1} \end{gathered}$ | - | - |
| Harmonic Field (GP) | - | Result: Harmonic Field (GP) $\begin{aligned} U & =U_{1} / U_{2} \\ J_{x} & =\left(J_{1, x} / J_{2, x}\right) /\left\|J^{\prime}\right\| \\ J_{y} & =\left(J_{1, y} / J_{2, y}\right) /\left\|J^{\prime}\right\| \end{aligned}$ <br> with $\left\|J^{\prime}\right\|=\sqrt{\left\|J_{1, x} / J_{2, x}\right\|^{2}+\left\|J_{1, y} / J_{2, y}\right\|^{2}}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=\left(J_{1, x} \cdot U_{1}\right) / E_{2, x} \\ & E_{y}=\left(J_{1, y} \cdot U_{1}\right) / E_{2, y} \end{aligned}$ |
| Harmonic Field (LP) | - | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} /\left(J_{2, x} \cdot U_{2}\right) \\ & E_{y}=E_{1, y} /\left(J_{2, y} \cdot U_{2}\right) \end{aligned}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} / E_{2, x} \\ & E_{y}=E_{1, y} / E_{2, y} \end{aligned}$ |

Table 135.3: Division of two Complex Amplitudes

### 135.1.2 Convolution

The convolution of two Complex Amplitude Documents $U_{1}$ and $U_{2}$ is calculated by

$$
\begin{equation*}
U_{1} \star U_{2}=\mathcal{F}^{-1}\left[\left(\mathcal{F} U_{1}\right) \cdot\left(\mathcal{F} U_{2}\right)\right] \tag{135.1}
\end{equation*}
$$

What types of Complex Amplitude Documents (Harmonic Field vs. Transmission) can be combined as operands and their result for all operations is shown in the following table 135.4. The used abbreviations are (GP) for globally polarized fields and (LP) for locally polarized fields.
Note: If the normalization factor of the Jones vector $J^{\prime}$ is zero, the resulting field is set to zero and the Jones vector to $(1,0)^{T}$.

| $1{ }^{\text {st }}$ Operand | $2^{\text {nd }}$ Operand |  |  |
| :---: | :---: | :---: | :---: |
|  | Transmission | Harmonic Field (GP) | Harmonic Field (LP) |
| Transmission | Result: Transmission $\begin{gathered} t=t_{1} \star t_{2} \\ \mathcal{J}=\mathcal{J}_{\mathbf{1}} \end{gathered}$ | - | - |
| Harmonic Field (GP) | - | Result: Harmonic Field (GP) $\begin{aligned} U & =U_{1} \star U_{2} \\ J_{x} & =J_{1, x} J_{2, x} /\left\|J^{\prime}\right\| \\ J_{y} & =J_{1, y} J_{2, y} /\left\|J^{\prime}\right\| \end{aligned}$ <br> with $\left\|J^{\prime}\right\|=\sqrt{\left\|J_{1, x} J_{2, x}\right\|^{2}+\left\|J_{1, y} J_{2, y}\right\|^{2}}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=\left(J_{1, x} \cdot U_{1}\right) \star E_{2, x} \\ & E_{y}=\left(J_{1, y} \cdot U_{1}\right) \star E_{2, y} \end{aligned}$ |
| Harmonic Field (LP) | - | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} \star\left(J_{2, x} \cdot U_{2}\right) \\ & E_{y}=E_{1, y} \star\left(J_{2, y} \cdot U_{2}\right) \end{aligned}$ | Result: Harmonic Field (LP) $\begin{aligned} & E_{x}=E_{1, x} \star E_{2, x} \\ & E_{y}=E_{1, y} \star E_{2, y} \end{aligned}$ |

Table 135.4: Convolution of two Complex Amplitudes

### 135.2 Jones Matrix Multiplication

Some optical elements and devices influence the polarization state of light. Mathematically this process can be described by a change of the electric field vector by a matrix, called Jones matrix $\mathcal{J}$

$$
\begin{equation*}
E_{\mathrm{xy}}^{\text {out }}=\mathcal{J} \cdot \boldsymbol{E}_{\mathrm{xy}}^{\text {in }} . \tag{135.2}
\end{equation*}
$$

For globally polarized fields, this means a change of the Jones vector:

$$
\begin{equation*}
J_{\text {out }}=\mathcal{J} \cdot J_{\text {in }} . \tag{135.3}
\end{equation*}
$$

Since Transmissions contain their own Jones matrix $\mathcal{J}^{(T)}$, the effect of a Jones Matrix Multiplication can be "added" to the transmission by applying former to the latter, which corresponds to the mathematical operation

$$
\begin{equation*}
\mathcal{J}_{\text {out }}^{(T)}=\mathcal{J} \cdot \mathcal{J}_{\text {in }}^{(T)} . \tag{135.4}
\end{equation*}
$$

For your convenience, the four important cases of Linear Polarization, Phase Shift, Retardation, and Rotation are implemented as separate manipulations in VirtualLab Fusion.

- Linear Polarization: A linear polarizer is a kind of optical filter that will pass only that part of $E_{x y}$ which oscillates in a certain direction. If this direction is given by an angle $\alpha$, the corresponding Jones matrix is given by

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos ^{2} \alpha & \sin \alpha \cos \alpha  \tag{135.5}\\
\sin \alpha \cos \alpha & \sin ^{2} \alpha
\end{array}\right) .
$$

- Phase Shift: A phase shift adds a phase difference $\phi$ to both $E_{x}$ and $E_{y}$. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
\exp (i \phi) & 0  \tag{135.6}\\
0 & \exp (i \phi)
\end{array}\right)
$$

- Retardation: Retarders as e.g. quarter-wave plates or half-wave plates "retard" $E_{y}$ against $E_{x}$ by a phase difference $\phi$. Thereby linearly polarized light can be transformed into circularly polarized and vice versa, for example. The appropriate Jones matrix is

$$
\mathcal{J}=\left(\begin{array}{cc}
1 & 0  \tag{135.7}\\
0 & \exp (-i \phi)
\end{array}\right)
$$

- Rotation: The angle of rotation $\theta$ of the plane of polarization determines the Jones matrix as follows

$$
\mathcal{J}=\left(\begin{array}{cc}
\cos \theta & -\sin \theta  \tag{135.8}\\
\sin \theta & \cos \theta
\end{array}\right)
$$

### 135.3 Quantization

Quantization of a complex amplitude field means to introduce discrete amplitude and phase levels.

### 135.3.1 Hard Quantization

You can enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively.
The quantization is performed independently for amplitude and phase. For each position $(x, y)$ the original field value $u(x, y)=A \exp [i \phi]$ is replaced by $A^{\prime} \exp \left[i \phi^{\prime}\right]$, where

$$
A^{\prime}= \begin{cases}A & \text { if } q=0  \tag{135.9}\\ A_{\max } & \text { if } q=1 \\ \frac{A_{\max }}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\max }}\right\rceil & \text { otherwise }\end{cases}
$$

(where $\lfloor\cdot\rceil$ denotes the rounding-to-nearest-integer operation) and

$$
\phi^{\prime}= \begin{cases}\phi & \text { if } Q=0  \tag{135.10}\\ \frac{2 \pi}{Q} \cdot\left\lfloor\frac{Q(\phi+\pi)}{2 \pi}\right\rceil-\pi & \text { otherwise }\end{cases}
$$

$A_{\max }$ is the maximum amplitude within the input field. Compared to the definition of the phase quantization operator $\Pi_{\text {quant, } Q}$ used during IFTA optimization (Sec. 97), which corresponds to the case of $q=1$, the definition given in this section allows simultaneous amplitude and phase quantization. Furthermore, the special cases for $q=0$ and $Q=0$ have been included for maintaining the original amplitude and phase, respectively. In cases of $q=1$ the amplitude is set to one. If $Q=1$, the resulting field has a zero phase.

### 135.3.2 Soft Quantization

You can enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively. Furthermore a projection strength $\lambda$ can be entered.
The quantization is performed independently for amplitude and phase. For each position $(x, y)$ the original field value $u(x, y)=A \exp [i \phi]$ is replaced by $A^{\prime} \exp \left[i \phi^{\prime}\right]$. The amplitude $A^{\prime}$ is obtained by

$$
A^{\prime}= \begin{cases}A & \text { if } q=0  \tag{135.11}\\ A_{\max } & \text { if } q=1 \wedge C_{1}=\text { true } \\ \frac{A_{\max }}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\max }}\right\rceil & \text { if } q>1 \wedge C_{2}=\text { true } \\ A & \text { otherwise }\end{cases}
$$

with the Boolean terms

$$
\begin{align*}
C_{1} & =\left(\left|\frac{A}{A_{\max }}-1\right| \geq 0.5 \lambda\right)  \tag{135.12}\\
C_{2} & =\left(\left|\frac{A}{A_{\max }}-\frac{1}{q-1} \cdot\left\lfloor(q-1) \frac{A}{A_{\max }}\right\rceil\right| \geq \frac{\lambda}{2(q-1)}\right) \tag{135.13}
\end{align*}
$$

The phase $\phi^{\prime}$ is calculated from

$$
\phi^{\prime}= \begin{cases}\phi & \text { if } Q=0 \vee C_{3}=\text { true }  \tag{135.14}\\ \frac{2 \pi}{Q} \cdot\left\lfloor\frac{Q(\phi+\pi)}{2 \pi}\right\rceil-\pi & \text { otherwise }\end{cases}
$$

with the Boolean term

$$
\begin{equation*}
C_{3}=\left(Q>0 \wedge\left|\phi-\frac{2 \pi}{Q} \cdot\lfloor Q /(2 \pi) \phi\rceil\right|>\lambda \pi / Q\right) \tag{135.15}
\end{equation*}
$$

$A_{\text {max }}$ is the maximum amplitude within the complex amplitude field.
Compared to the definition of the phase quantization operator $\Pi_{\text {softquant }, Q}^{\lambda}$ used during IFTA optimization ( $\hookrightarrow$ Sec. 97), which corresponds to the case of $q=1$, the definition given in this section allows for simultaneous amplitude and phase quantization. Furthermore, the special cases for $q=0$ and $Q=0$ have been included for maintaining the original amplitude and phase, respectively. If $Q=1$, the resulting field has a zero phase.

### 135.3.3 Floyd-Steinberg Quantization

You can enter the numbers $q$ and $Q$ of amplitude and phase levels, respectively.
The result of the Floyd-Steinberg quantization contains only field values from the set

$$
\begin{equation*}
M_{(q, Q)}=\left\{A \exp [i \phi]: A \in M_{q} \wedge \exp [i \phi] \in M_{Q}\right\} \tag{135.16}
\end{equation*}
$$

where the sets $M_{q}$ and $M_{Q}$ are given by

$$
\begin{equation*}
M_{q}=\left\{\frac{j A_{\max }}{q-1}: j=0 \ldots q-1\right\} \tag{135.17}
\end{equation*}
$$

and

$$
\begin{equation*}
M_{Q}=\left\{\exp \left[-i \pi\left(-1+\frac{2 \pi j}{Q}\right)\right]: j=0,1, \ldots, Q-1\right\} \tag{135.18}
\end{equation*}
$$

$A_{\text {max }}$ is the maximum amplitude within the complex amplitude field.
In contrast to the quantization types described in the previous two sections, the Floyd-Steinberg quantization is not a pointwise operation. That is, the quantization result at a position $(x, y)$ does not depend only on the field value $u(x, y)$ but also on the field values on neighboring positions. The basic idea of the Floyd-Steinberg quantization is to distribute the error, which was made by the quantization at a certain position, to the neighboring positions.
During the application of the Floyd-Steinberg quantization an iteration through all field positions is performed row by row, whereby within each row positions are considered consecutively from left to right. At a considered position $(x, y)$ firstly a hard quantization is performed ( $\hookrightarrow$ Sec. 135.3.1). After that the quantization error is calculated from the difference between $u(x, y)$ and the obtained quantization value.
This difference is spread using the weighting factors shown in Fig. 789 to four neighboring positions, which are considered in following iterations.


Figure 789. Weighting factors for distribution of quantization errors to neighboring positions during Floyd-Steinberg quantization.

### 135.4 Dimension Separation

You can separate a two-dimensional complex array or recombine the parts of a previously separated array. A two-dimensional separable array $u_{\text {sep }}(x, y)$ fulfills the property

$$
\begin{equation*}
u_{\operatorname{sep}}(x, y)=u_{x}(x) u_{y}(y) \tag{135.19}
\end{equation*}
$$

with the one-dimensional arrays $u_{x}$ and $u_{y}$ which are calculated from the (not necessarily separable) current array $u(x, y)$ by

$$
\begin{align*}
& u_{x}(x)=f_{x} u_{x}^{\prime}(x)  \tag{135.20}\\
& u_{y}(y)=f_{y} u_{y}^{\prime}(y) \tag{135.21}
\end{align*}
$$

with

$$
\begin{align*}
& u_{x}^{\prime}(x)=\sum_{j=0}^{N_{y}-1} u\left(x, y_{j}\right)  \tag{135.22}\\
& u_{y}^{\prime}(y)=\sum_{i=0}^{N_{x}-1} u\left(x_{i}, y\right) \tag{135.23}
\end{align*}
$$

and

$$
\begin{align*}
& f_{x}=\sqrt{f_{0} \frac{N_{x}}{N_{y}}}  \tag{135.24}\\
& f_{y}=\sqrt{f_{0} \frac{N_{y}}{N_{x}}} \tag{135.25}
\end{align*}
$$

where $N_{x}$ and $N_{y}$ denote the number of sampling points and $f_{0}$ is calculated as

$$
\begin{equation*}
f_{0}=\frac{\sum_{j=0}^{N_{y}-1} \sum_{i=0}^{N_{x}-1} u\left(x_{i}, y_{j}\right) \overline{u_{x}\left(x_{i}\right) u_{y}\left(y_{j}\right)}}{\sum_{j=0}^{N_{y}-1} \sum_{i=0}^{N_{x}-1}\left\|u_{x}\left(x_{i}\right) u_{y}\left(y_{j}\right)\right\|^{2}} . \tag{135.26}
\end{equation*}
$$

### 135.5 Fourier Transforms

### 135.5.1 Fourier Transform (Space)

The Fourier transform has many applications in wave-optical simulations. Examples are the usage in free space propagation operators ( $\hookrightarrow$ Sec. 93) and the simulation of Fourier transforming optical setups ( $\hookrightarrow$ Sec. 31.1.1). There are four different Fourier transforms:

- (Physical) Forward: $x \rightarrow k$,
- (Physical) Backward: $\mathrm{k} \rightarrow \mathrm{x}$,
- Numerical Forward: $x \rightarrow k$, and
- Numerical Backward: $\mathrm{k} \rightarrow \mathrm{x}$

The numerical and the "normal" or physical Fourier transform differ in their scaling: The numerical variants ensure that the summed norm of the field ( $\hookrightarrow$ Sec. 75.4 .7 ) is not changed by the transform. This leads to the effect that if you embed the Fourier transform of a field in a zeroized frame and then perform the backward transform, the power and maximum amplitude of the field has changed. This is circumvented if you use the physical transforms.
The mathematical equations for the Fourier transform and its inverse operation are:
Fourier transform $\mathcal{F}$ :

$$
\begin{equation*}
[\mathcal{F} U(x, y)](\hat{x}, \hat{y})=\iint_{-\infty}^{\infty} \mathrm{d} x \mathrm{~d} y \exp [-i 2 \pi(x \hat{x}+y \hat{y})] U(x, y) \tag{135.27}
\end{equation*}
$$

Its inverse operation $\mathcal{F}^{-1}$ :

$$
\begin{equation*}
\left[\mathcal{F}^{-1} U(\hat{x}, \hat{y})\right](x, y)=\iint_{-\infty}^{\infty} \mathrm{d} \hat{x} \mathrm{~d} \hat{y} \exp [i 2 \pi(x \hat{x}+y \hat{y})] U(\hat{x}, \hat{y}) \tag{135.28}
\end{equation*}
$$

The used implementations of the Fourier transform and its inverse operation are using the technique of the Fast Fourier Transform (FFT) [Bra65] which is based on the discrete Fourier transform [Goo68]. They are given in the following subsections.

### 135.5.1.1 Forward: $\mathbf{x} \rightarrow \mathbf{k}$

The discrete Fourier transform $\mathcal{F}$ calculates a complex array in the spectral representation with wave number coordinates $\left(k_{x}, k_{y}\right)$ from an array with spatial coordinates $(x, y)$ using the equation

$$
\begin{equation*}
[\mathcal{F} u(x, y)]\left(k_{x}, k_{y}\right)=S \cdot \sum_{x} \sum_{y} \exp \left[-i\left(x k_{x}+y k_{y}\right)\right] u(x, y) \tag{135.29}
\end{equation*}
$$

with the scaling factor

$$
S= \begin{cases}\frac{1}{\sqrt{N_{x} N_{y}}} & \text { for the numerical variant }  \tag{135.30}\\ \frac{\delta x \delta y}{2 \pi} & \text { for the physical variant and two-dimensional fields } \\ \frac{\delta x}{\sqrt{2 \pi}} & \text { for the physical variant and one-dimensional fields }\end{cases}
$$

The two sums are calculated over the $\left(N_{x} ; N_{y}\right)$ sampling points at a grid, which is defined by the sampling distance $(\delta x ; \delta y)$. For constructing the resultant field, Eq. (135.29) is evaluated at ( $N_{x} ; N_{y}$ ) sampling points
with a sampling distance $\left(\delta k_{x} ; \delta k_{y}\right)$ given by

$$
\begin{align*}
\delta k_{x} & =\frac{2 \pi}{N_{x} \delta x} \quad \text { and }  \tag{135.31}\\
\delta k_{y} & =\frac{2 \pi}{N_{y} \delta y} \tag{135.32}
\end{align*}
$$

### 135.5.1.2 Backward: $k \rightarrow \mathbf{x}$

The inverse discrete Fourier transform $\mathcal{F}^{-1}$ calculates a complex array in spatial representation from an array in spectral representation using the equation

$$
\begin{equation*}
\left[\mathcal{F}^{-1} u\left(k_{x}, k_{y}\right)\right](x, y)=S \cdot \sum_{k_{x}} \sum_{k_{y}} \exp \left[i\left(x k_{x}+y k_{y}\right)\right] u\left(k_{x}, k_{y}\right) \tag{135.33}
\end{equation*}
$$

with the scaling factor

$$
S= \begin{cases}\frac{1}{\sqrt{N_{x} N_{y}}} & \text { for the numerical variant }  \tag{135.34}\\ \frac{\delta k_{x} \delta k_{y}}{2 \pi} & \text { for the physical variant and two-dimensional fields } \\ \frac{\delta k_{x}}{\sqrt{2 \pi}} & \text { for the physical variant and one-dimensional fields }\end{cases}
$$

The sampling parameters of the two fields are related in the same way as stated above (Eqs. (135.31)-(135.32)).

## 136 Propagations

### 136.1 Free Space Operators

### 136.1.1 Propagation between Optical Setup Elements

Generally, the propagation of a field between Optical Setup Elements is equivalent to propagating the field between two arbitrarily positioned planes. These planes are related to the Optical Setup Elements involved and are called transfaces. This is a special shortcut for "transfer interface" and means the location of the field transfer between two kinds of operators. The output transface $\tau_{1}$ of the start element is the plane where the output of the propagation through this element is given to the homogeneous medium free space operator. The input transface $\tau_{2}$ of the target element is the plane where the output of the free space operator is given to the propagation operator of the second element.
The position and orientation of the output transface - the starting point for the homogeneous medium free space operator - is determined by the propagation through the start element and the type of the reference output coordinate system chosen for this element (but the output coordinate system does not have to be identical to this transface's position and orientation). It is stored after the element's propagation in the coordinate system of the field itself: the origin of this coordinate system is identical to the position of the transface and the orientation is given by the coordinate system's $x-y$-plane.
The position and orientation of the input transface - the end point for the homogeneous medium free space operator - is determined by the geometry of the target element and, of course, the relative position of the target element to the start element.
There are two general cases to be distinguished for the propagation between Optical Setup Elements, related to two different algorithms used for propagating the field from output transface $\tau_{1}$ to input transface $\tau_{2}$ :

1. The planes $\tau_{1}$ and $\tau_{2}$ are parallel. The algorithm used for this configuration is shown in Fig. 790.
2. The planes $\tau_{1}$ and $\tau_{2}$ are not parallel. The algorithm used for this configuration is shown in Fig. 791.

Please note: this case cannot be simulated with 1D fields.


Figure 790. Algorithm for the propagation between Optical Setup Elements where output transface and input transface are parallel. There are two operations at most: the actual free space propagation followed by a lateral shift.


Figure 791. Algorithm for the propagation between Optical Setup Elements where output transface and input transface are not parallel. The operators 1: actual free space propagation and 3: rotation operation can be configured by the user.

### 136.1.2 Far Field Operator

The far field propagation simulates the propagation of a field $U(x, y)$ with a wavelength $\lambda$ by a distance $\Delta z$ through an infinite homogeneous medium with a given refractive index $n$. A propagation can be simulated from the waist to the far field, from the far field to the waist and from one far field distance to another. The far field propagation is the far field approximation of the Rayleigh Sommerfeld propagation integral [MW95] (see also

Sec. 136.1.4). Thus it contains no paraxial approximation. The propagation is defined as:

$$
\begin{align*}
{\left[\mathcal{P}_{\Delta z}^{\text {FarField }} U(x, y)\right]\left(x^{\prime}, y^{\prime}\right) } & \sim-\frac{i k z}{2 \pi r} \frac{e^{i k r}}{r} \iint_{-\infty}^{\infty} \mathrm{d} x \mathrm{~d} y U(x, y) e^{-\frac{i k}{r}\left(x x^{\prime}+y y^{\prime}\right)}  \tag{136.1}\\
\text { with } \quad r & =\sqrt{x^{\prime 2}+y^{\prime 2}+\Delta z^{2}}  \tag{136.2}\\
\text { and } \quad k & =\frac{2 \pi n}{\lambda} \tag{136.3}
\end{align*}
$$

For the estimation of the sampling distance Eq. (136.20) is used if the propagation mode is Waist to Far Field or Far Field to Waist. For the propagation mode Far Field to Far Field the sampling distance is calculated by

$$
\begin{equation*}
\Delta x^{\prime}=\Delta x \frac{\Delta z+\Delta z_{\mathrm{sph}}}{\Delta z_{\mathrm{sph}}} \tag{136.4}
\end{equation*}
$$

$\Delta z_{\text {sph }}$ is the radius of the spherical phase factor which in the far field equals the distance from the waist of the field. This means that a spherical phase radius (Sec. 131.2) must be set if you use the Far Field to Far Field mode.
In the paraxial case the following approximation (far field approximation of Eq. (136.17)) is used:

$$
\begin{align*}
& {\left[\mathcal{P}_{\Delta z}^{\text {FarField-P }} U(x, y)\right]\left(x^{\prime}, y^{\prime}\right)=\frac{A}{i} \exp (i k \Delta z) \exp \left(\frac{i k}{2 \Delta z}\left(x^{\prime 2}+y^{\prime 2}\right)\right)} \\
& {[\mathcal{F}(U(x, y))]\left(\frac{k}{2 \pi \Delta z} x^{\prime}, \frac{k}{2 \pi \Delta z} y^{\prime}\right)} \tag{136.5}
\end{align*}
$$

where $A$ denotes a real-valued factor. The definitions of $k$ and $\mathcal{F}$ correspond to those in Sec. 136.1.3.

### 136.1.3 Spectrum of Plane Waves Operator

The spectrum of plane waves propagation operator $\mathcal{P}_{\Delta z}^{\mathrm{SPW}}$ is used for simulating the propagation of a field $U(x, y)$ with a wavelength $\lambda$ by a distance $\Delta z$ through an infinite homogeneous medium with a given refractive index $n$ [MW95],

$$
\begin{equation*}
\mathcal{P}_{\Delta z}^{\mathrm{SPW}} U=\mathcal{F}^{-1}\left(\exp \left[i 2 \pi \sqrt{\frac{n^{2}}{\lambda^{2}}-\hat{x}^{2}-\hat{y}^{2} \Delta z}\right] \mathcal{F} U(x, y)\right) \tag{136.6}
\end{equation*}
$$

where $\hat{x}$ and $\hat{y}$ are spatial frequencies, i.e. pixel coordinates of the Fourier transformed field.
For more details about the Fourier transform used in this equation see Sec. 135.5.1.
The spectrum of plane waves propagation operator $\mathcal{P}_{\Delta z}^{S P W}$ as given in Eq. (136.6) can be derived without using any physical approximations, that is its accuracy is limited only by numerical errors.
The main reason for these numerical errors is the sampling of the phase term in Eq. (136.6) by a finite sampling distance $\delta x$, which can cause sampling problems during the numerical evaluation of Eq. (136.6). These issues vanish if the propagation distance $\Delta z$ is sufficiently small. The following formula gives an approximate maximum value $\Delta z_{\text {max }}$ for the propagation distance, that is in case of $\Delta z<\Delta z_{\max }$ the numerical error in the application of $\mathcal{P}_{\Delta z}^{\mathrm{SPW}}$ is often negligible,

$$
\begin{equation*}
\Delta z_{\max }=\frac{1}{2}\left[\sqrt{\left(\frac{n}{\lambda}\right)^{2}-\left(U_{0}-\delta U\right)^{2}}-\sqrt{\left(\frac{n}{\lambda}\right)^{2}-U_{0}^{2}}\right]^{-1} \tag{136.7}
\end{equation*}
$$

where $U_{0}=1 /(2 \delta x)$ and $\delta U=1 /\left(N_{x} \delta x\right)$. It should be mentioned that in general the numerical error for all propagation distances $\Delta z>0$ is never zero but just decreases with decreasing propagation distance.
The numerical error can be decreased for a given propagation distance $\Delta z$ by appending sampling points (with value zero) at the borders of the field. The number of sampling points is increased from $N_{x}$ to $N_{x, \text { min }}$ by doing so. The recommended value for $N_{x, \min }$ can be calculated approximately by

$$
\begin{equation*}
N_{x, \min }=\frac{2}{1-2 \delta x \sqrt{\left(\frac{n}{\lambda}\right)^{2}-a^{2}}} \tag{136.8}
\end{equation*}
$$

where

$$
\begin{equation*}
a=\frac{1}{2 \Delta z}+\sqrt{\left(\frac{n}{\lambda}\right)^{2}-\left(\frac{1}{2 \delta x}\right)^{2}} \tag{136.9}
\end{equation*}
$$

For the estimation of the number of sampling points Eq. (136.8) is used.

### 136.1.4 Rayleigh Sommerfeld Operator

The propagation integral used in Rayleigh Sommerfeld propagation simulates the propagation of a field $U(x, y)$ with a wavelength $\lambda$ by a distance $\Delta z$ through an infinite homogeneous medium with a given refractive index $n$. It is defined by [MW95] as:

$$
\begin{equation*}
\left[\mathcal{P}_{\Delta z}^{\mathrm{RS}} U(x, y)\right]\left(x^{\prime}, y^{\prime}\right)=\frac{1}{2 \pi} \int_{-\infty}^{\infty} \mathrm{d} x \mathrm{~d} y U(x, y) \frac{\partial \exp (i k R) / R}{\partial z} \tag{136.10}
\end{equation*}
$$

where

$$
\begin{equation*}
\frac{1}{2 \pi} \frac{\partial \exp (i k R) / R}{\partial z}=\frac{z \exp (i k R)(1-i k R)}{2 \pi R^{3}} \tag{136.11}
\end{equation*}
$$

and

$$
\begin{equation*}
R=\sqrt{\left(x-x^{\prime}\right)^{2}+\left(y-y^{\prime}\right)^{2}+\Delta z^{2}} \tag{136.12}
\end{equation*}
$$

The Rayleigh Sommerfeld propagation integral can be derived without any physical approximation. Actually the propagation integral is a convolution of a harmonic field and a spherical phase function. It is possible to solve this convolution by using fast Fourier transforms. In this case the propagation integral has a form

$$
\begin{equation*}
\left[\mathcal{P}_{\Delta z}^{\mathrm{RS}} U(x)\right]\left(x^{\prime}\right)=\mathcal{F}\left[\mathcal{F}^{-1}\left(\frac{z \exp (i k R)(1-i k R)}{2 \pi R^{3}}\right) \mathcal{F}^{-1} U(x)\right] \tag{136.13}
\end{equation*}
$$

If the convolution is evaluated by fast Fourier transforms it is also called Rayleigh Sommerfeld Convolution. In contrast the integral can also be numerically evaluated by simple summation. In difference to the calculation of the convolution by fast Fourier transforms, the pure summation is much more time consuming but has the advantage of a free choice of the number of sampling points and the sampling distance of the propagated field. This propagation method is accurate for large propagation distances. For smaller distances numerical errors will occur because of an undersampling of the spherical phase function in Eq. (136.12). The critical distance $\Delta z_{\text {min }}$ can be estimated by

$$
\begin{equation*}
\Delta z_{\min }=\frac{n}{\lambda} \sqrt{\left[\left(\frac{\lambda}{2 n}\right)^{2}-x_{0}^{2}-\left(x_{0}-\delta x\right)^{2}\right]^{2}-4 x_{0}^{2}\left(x_{0}-\delta x\right)^{2}} \tag{136.14}
\end{equation*}
$$

$x_{0}$ is the radius of the field and is defined as $x_{0}=\frac{N_{x}}{2} \Delta x$. It should be mentioned that for all propagation distances $\Delta z \neq 0$ the numerical errors never vanish but just decrease more and more with increasing distance. For propagation distances $\Delta z<\Delta z_{\text {min }}$, numerical errors can be reduced by interpolating the harmonic field before the propagation. The necessary sampling distance $\delta x_{\text {min }}$ can be estimated by

$$
\begin{equation*}
\delta x_{\min }=\frac{\pi}{k x_{0}} \sqrt{x_{0}^{2}+(\Delta z)^{2}} \tag{136.15}
\end{equation*}
$$

where

$$
\begin{equation*}
k=\frac{2 \pi n}{\lambda} \tag{136.16}
\end{equation*}
$$

For the estimation of the sampling distance Eq. (136.15) is used.

### 136.1.5 Fresnel Propagation Operator

The Fresnel propagation operator $\mathcal{P}_{\Delta z}^{\text {Fresnel }}$ for simulating the propagation of a field $U(x, y)$ with a wavelength $\lambda$ by a distance $\Delta z$ through an infinite homogeneous medium with a given refractive index $n$ can be derived using the paraxial Fresnel approximation [Goo68]:

$$
\begin{align*}
& {\left[\mathcal{P}_{\Delta z}^{\text {Fresnel }} U(x, y)\right]\left(x^{\prime}, y^{\prime}\right)=\frac{A}{i} \exp (i k \Delta z) \exp \left(\frac{i k}{2 \Delta z}\left(x^{\prime 2}+y^{\prime 2}\right)\right) .} \\
& {\left[\mathcal{F}\left(U(x, y) \exp \left[\frac{i k}{2 \Delta z}\left(x^{2}+y^{2}\right)\right]\right)\right]\left(\frac{k}{2 \pi \Delta z} x^{\prime}, \frac{k}{2 \pi \Delta z} y^{\prime}\right),} \tag{136.17}
\end{align*}
$$

where $A$ denotes a real-valued factor. The definitions of $k$ and $\mathcal{F}$ correspond to those in Sec. 136.1.3.
In contrast to the spectrum of plane waves operator ( $\hookrightarrow$ Sec. 136.1.3), for the application of the Fresnel propagation operator the numerical errors become larger for shorter propagation distances $\Delta z$ because of the quadratic phase term in Eq. (136.17). The critical minimum distance $\Delta z_{\text {min }}$ for a field with ( $N_{x} ; N_{y}$ ) sampling points and a sampling distance $(\delta x ; \delta y)$ can be estimated by

$$
\begin{equation*}
\Delta z_{\min }=\frac{(\delta x)^{2} n N_{x}}{\lambda} \tag{136.18}
\end{equation*}
$$

It should be mentioned that for all propagation distances $\Delta z \neq 0$ the numerical errors never vanish but just decrease more and more with increasing distance.
For propagation distances $\Delta z<\Delta z_{\text {min }}$ numerical errors can be reduced by interpolating the field before the propagation to a smaller sampling distance $\delta x_{\min }$, which can be calculated approximately by

$$
\begin{equation*}
\delta x_{\min }=\frac{N_{x} \delta x}{2}-\sqrt{\left(\frac{N_{x} \delta x}{2}\right)^{2}-\frac{\Delta z \lambda}{n}} . \tag{136.19}
\end{equation*}
$$

In difference to most of the other homogeneous medium propagation algorithms, the sampling distance of the field is scaled during the Fresnel propagation. The sampling distance of the propagated field follows from

$$
\begin{equation*}
\Delta x^{\prime}=\frac{\lambda \Delta z}{n N_{x} \Delta x} \tag{136.20}
\end{equation*}
$$

For the estimation of the sampling distance Eq. (136.19) is used.

### 136.1.6 Combined SPW / Fresnel Operator

This propagation operator combines automatically the spectrum of plane waves propagation ( $\hookrightarrow$ Sec. 136.1.3) and the Fresnel propagation ( $\hookrightarrow$ Sec. 136.1.5) to achieve an efficient propagation of paraxial waves free of numerical errors. For propagation of harmonic fields close to the waist of a wave, spectrum of plane waves is used. For larger distances the Fresnel propagation is used. Since the Fresnel propagation is more efficient the automatic paraxial propagation tries always to use the Fresnel propagation if the distance from the waist is larger than the minimum distance $\Delta z_{\min }$ ( $\hookrightarrow$ Eq. (136.18)). If the spectrum of plane wave propagation is used the harmonic field will be automatically embedded in order to reduce numerical errors.
In general a combination of both propagation methods is necessary depending on the distances from the waist of the wave $\Delta z_{w, \text { start }}$ of the harmonic field before the propagation and $\Delta z_{w, \text { end }}$ of the harmonic field after the propagation. The following table shows which combinations of propagation operators may occur.
DISTANCE $\left|\Delta Z_{W, S T A R T}\right|$ DISTANCE $\left|\Delta Z_{W, E N D}\right|$ USED PROPAGATION ALGORITHMS

| $=0$ | $<\Delta z_{\min }$ | SPW |
| :--- | :--- | :--- |
| $=0$ | $\geq \Delta z_{\min }$ | FRT |
| $<\Delta z_{\text {min }}$ | $<\Delta z_{\text {min }}$ | SPW |
| $<\Delta z_{\min }$ | $\geq \Delta z_{\min }$ | SPW to waist and FRT |
| $\geq \Delta z_{\min }$ | $\geq \Delta z_{\min }$ | FRT to waist and FRT |
| $\geq \Delta z_{\min }$ | $<\Delta z_{\text {min }}$ | FRT to waist and SPW |

### 136.1.7 Rayleigh Expansion Propagation

The Rayleigh coefficients $\mathcal{R}\left(k_{x}, k_{y}\right)$ calculated by the Fourier Modal Method correspond to the complex amplitudes of the individual grating orders. Thus a kind of SPW propagation ( $\hookrightarrow$ Sec. 136.1.3) can be used to calculate the near field in a certain propagation distance $\Delta z$.

$$
\begin{equation*}
\mathcal{P}_{\Delta z}^{N F} \boldsymbol{E}\left(x, y, z_{0}+\Delta z\right)=\sqrt{N_{x} N_{y}} \mathcal{F}^{-1}\left(\exp \left[i k_{z} \Delta z\right] \mathcal{R}\left(k_{x}, k_{y}\right)\right) \tag{136.21}
\end{equation*}
$$

$\mathcal{R}\left(k_{x}, k_{y}\right)$ are the Rayleigh coefficients for $E_{x}$ - and $E_{y}$-component of the field. $N_{x}$ and $N_{y}$ are the sampling points in $x$ - and y-direction, respectively. The factor $\sqrt{N_{x} N_{y}}$ is due to the fact that $\mathcal{R}\left(k_{x}, k_{y}\right)$ is not exactly $\mathcal{F} E(x, y)$ as in VirtualLab Fusion the Fourier transform is defined with a factor $1 / \sqrt{N_{x} N_{y}}(\hookrightarrow$ Sec. 135.5.1.1).

## Notes

- To use geometrical optics alongside with the Rayleigh expansion propagation, the harmonic field calculated by the geometrical optics is transformed to Rayleigh coefficients first.
- As the Rayleigh coefficients represent ideal plane waves with infinite size, you are always in the near field, regardless of the set $\Delta z$. Thus you never see separate orders if you use the near field propagation.
- The Output Field Oversampling Factor of the Rayleigh Expansion Propagation is considered by an embedding prior to the inverse Fourier transform. The result is the same as if a sinc interpolation ( $\hookrightarrow$ Sec. 13.2.2) was applied.
- The Number of Periods parameter of the Rayleigh Expansion Propagation is considered by a zeroized oversampling prior to the inverse Fourier transform, i. e. by surrounding each pixel with a suitable amount of zeros.
- $x, y, z_{0}$, and $\Delta z$ in Eq. (136.21) refer to the coordinate system of the grating, not the coordinate system of the incoming light.


### 136.2 Propagation Operators for Real Components

### 136.2.1 Thin Element Approximation

The thin element approximation can be used for propagating through surfaces, homogeneous and inhomogeneous (index modulated) media. It is assumed that paraxial/parabasal conditions hold. The paraxial mode is documented by [Goo68]. Using the paraxial mode, the method is identical to the mode AI/All of the geometrical optics operator, see Sec. 96.1.
In principle the propagation of a field $E$ by a distance $\Delta z$ from $z$ to $z+\Delta z$ is based on:

$$
\begin{equation*}
E(z+\Delta z)=Q \cdot E(z) \tag{136.22}
\end{equation*}
$$

where

$$
\begin{equation*}
Q=\exp \left\{-i k_{0} I(n(x, y, \tilde{z}))\right\} \tag{136.23}
\end{equation*}
$$

Here $k_{0}$ is the wavenumber with respect to the base-material (without index modulation), and $I(n(x, y, z))$ is the integral value of $n(x, y, z)$ along the propagation path, i. e. from $\tilde{z}=z$ to $\tilde{z}=z+\Delta z$. In case of surfaces, the propagation is applied for each medium (in front and behind the surface) separately, i.e. two consecutive propagation steps are applied. For the integration a summed trapezoidal rule (Romberg integration) with at most 4 integration points is used. Hence, only weak modulation of the refractive index along the propagation path are taken into account. In the case of stronger modulation along the z-variable, the split step propagation method ( $\hookrightarrow$ Sec. 136.2.2) is to be preferred.

### 136.2.2 Split Step (BPM) Propagation

This propagation operator is applicable for inhomogeneous media with small refractive index modulation $\delta n \ll$ $n$. Furthermore, paraxial conditions are assumed to hold and the influence of reflected waves is assumed to be negligible. The operator is based on the classical ideas of paraxial beam propagation methods, see e.g. [YL92] and [TY82]. The field is propagated through a medium by sequence of two alternating propagation steps: a step assuming a homogeneous medium and a correction step taking into account the index modulation. Using the notation of [TY82] we can write for the propagation of a field $E$ by distance $\Delta z$ from $z$ to $z+\Delta z$ :

$$
\begin{equation*}
E(z+\Delta z)=P \cdot Q \cdot P \cdot E(z) \tag{136.24}
\end{equation*}
$$

where

$$
\begin{equation*}
P=\exp \left\{-i\left(\frac{z}{2}\right) \nabla_{\perp}^{2} /\left[\left(\nabla_{\perp}^{2}+k^{2}\right)^{1 / 2}+k\right]\right\} \tag{136.25}
\end{equation*}
$$

and

$$
\begin{equation*}
Q=\exp \left\{-i \Delta z k_{0} \delta n(x, y)\right\} \tag{136.26}
\end{equation*}
$$

The effect of the operator $P$ is to propagate the field through a distance $\Delta z / 2$ in homogeneous medium of refractive index $n_{0}$. The operator $Q$ subsequently imposes a phase change on the propagating field equal to $\Delta z k_{0} \delta n$ taking into account the index modulation $\delta n(x, y)$. After that the field is propagated by another step of $\Delta z / 2$ in homogeneous medium. This is repeated $n$-times, until the total propagation distance $Z=n \Delta z$ is reached.
Note, the z-dependence of $\delta n(x, y, z)$ is taken into account by the splitting along the z-distance which corresponds to a piecewise trapezoidal integration rule of $\delta n(x, y, z)$ with respect to the variable $z$.

## 137 Detectors

### 137.1 Beam Parameters

For calculating the beam parameters of a globally polarized complex amplitude field we use a method based on the calculation of the second order momenta ( $\hookrightarrow$ Sec. 137.8). The ten momenta used to calculate the beam parameters are $\left\langle x^{2}\right\rangle,\left\langle y^{2}\right\rangle,\left\langle x \theta_{x}\right\rangle,\left\langle\theta_{x}^{2}\right\rangle,\langle x y\rangle,\left\langle x \theta_{y}\right\rangle,\left\langle y \theta_{x}\right\rangle,\left\langle\theta_{x} \theta_{y}\right\rangle,\left\langle y \theta_{y}\right\rangle$, and $\left\langle\theta_{y}^{2}\right\rangle$.
Beam parameters are well defined for harmonic fields having some finite lateral extension.
The calculation of beam parameters from the momenta is described by the following table:

| ITEM | DESCRIPTION |
| :--- | :--- |
| $w_{x}\left(z_{x}\right)=4 \sqrt{\left\langle x^{2}\right\rangle}$ | Diameter in x-direction at the measured plane of the beam |
| $w_{y}\left(z_{y}\right)=4 \sqrt{\left\langle y^{2}\right\rangle}$ | Diameter in y-direction at the measured plane of the beam |
| $w_{x}^{0}=4 \sqrt{\left\langle x^{2}\right\rangle^{\prime}}$ | Waist diameter in x-direction of the beam |
| $w_{y}^{0}=4 \sqrt{\left\langle y^{2}\right\rangle^{\prime}}$ | Waist diameter in y-direction of the beam |
| $\theta_{x}=4 \sqrt{\left\langle\theta_{x}^{2}\right\rangle}$ | Full divergence angle of the beam in x-direction |
| $\theta_{y}=4 \sqrt{\left\langle\theta_{y}^{2}\right\rangle}$ | Full divergence angle of the beam in y-direction |
| $M_{x}^{2}=4 \frac{\pi}{\lambda} \sqrt{\left\langle x^{2}\right\rangle^{\prime}\left\langle\theta_{x}^{2}\right\rangle^{\prime}}$ | $M^{2}$ parameter for the x-axis |
| $M_{y}^{2}=4 \frac{\pi}{\lambda} \sqrt{\left\langle y^{2}\right\rangle^{\prime}\left\langle\theta_{y}^{2}\right\rangle^{\prime}}$ | $M^{2}$ parameter for the y-axis |
| $z_{x}^{R}=\left(w_{x}^{0}\right)^{2} \frac{\pi}{\lambda}$ | Rayleigh Length of the beam in x-direction |
| $z_{y}^{R}=\left(w_{y}^{0}\right)^{2} \frac{\pi}{\lambda}$ | Rayleigh Length of the beam in y-direction |
| $\frac{1}{2} \arctan \frac{2\langle x y\rangle}{\left\langle x^{2}\right\rangle-\left\langle y^{2}\right\rangle}$ | Rotation angle of the principal axis |

### 137.1.1 Calculation of the Momenta in the Waist

With the help of ABCD matrices, it is possible to calculate the beam parameters in the waist position of the beam. The changing of the momenta during a propagation is described by Eq. (137.39). The associated ABCD matrix

$$
\left(\begin{array}{ll}
A & B  \tag{137.1}\\
C & D
\end{array}\right)=\left(\begin{array}{cc}
1 & z_{x / y} \\
0 & 1
\end{array}\right)
$$

is used to simulate a free space propagation from the waist plane (marked with an apostrophe) to the measured plane of the beam. Using this matrix, there follows according to [Mär]

$$
\begin{align*}
\left\langle x^{2}\right\rangle^{\prime} & =\left\langle x^{2}\right\rangle+2 z_{x}\left\langle x \theta_{x}\right\rangle+z_{x}^{2}\left\langle\theta_{x}^{2}\right\rangle  \tag{137.2}\\
\langle x y\rangle^{\prime} & =\langle x y\rangle+z_{a}\left\langle x \theta_{y}\right\rangle+z_{b}\left\langle y \theta_{x}\right\rangle+z_{a} z_{b}\left\langle\theta_{x} \theta_{y}\right\rangle  \tag{137.3}\\
\left\langle y^{2}\right\rangle^{\prime} & =\left\langle y^{2}\right\rangle+2 z_{y}\left\langle y \theta_{y}\right\rangle+z_{y}^{2}\left\langle\theta_{y}^{2}\right\rangle  \tag{137.4}\\
\left\langle x \theta_{x}\right\rangle^{\prime} & =\left\langle x \theta_{x}\right\rangle+z_{x}\left\langle\theta_{x}^{2}\right\rangle  \tag{137.5}\\
\left\langle y \theta_{y}\right\rangle^{\prime} & =\left\langle y \theta_{y}\right\rangle+z_{y}\left\langle\theta_{y}^{2}\right\rangle  \tag{137.6}\\
\left\langle\theta_{x}^{2}\right\rangle^{\prime} & =\left\langle\theta_{x}^{2}\right\rangle  \tag{137.7}\\
\left\langle\theta_{x} \theta_{y}\right\rangle^{\prime} & =\left\langle\theta_{x} \theta_{y}\right\rangle  \tag{137.8}\\
\left\langle\theta_{y}^{2}\right\rangle^{\prime} & =\left\langle\theta_{y}^{2}\right\rangle \tag{137.9}
\end{align*}
$$

The parameters $z_{x}$ and $z_{y}$ are the distances from the plane of the measured beam to the waist plane of the beam. The z parameters can be calculated from equations Eq. (137.5) and Eq. (137.6). It follows

$$
\begin{align*}
& z_{x}=-\frac{\left\langle x \theta_{x}\right\rangle}{\left\langle\theta_{x}^{2}\right\rangle}  \tag{137.10}\\
& z_{y}=-\frac{\left\langle y \theta_{y}\right\rangle}{\left\langle\theta_{y}^{2}\right\rangle} . \tag{137.11}
\end{align*}
$$

$z_{a}$ and $z_{b}$ can be calculated with the following two equations from [Mär].

$$
\begin{align*}
& z_{a}=-\frac{\left\langle x \theta_{y}\right\rangle^{\prime}}{\left\langle\theta_{x} \theta_{y}\right\rangle}  \tag{137.12}\\
& z_{b}=-\frac{\left\langle y \theta_{y}\right\rangle^{\prime}}{\left\langle\theta_{x} \theta_{y}\right\rangle} \tag{137.13}
\end{align*}
$$

### 137.1.2 Rotating Momenta according to Principal Axes

If the momentum $\langle x y\rangle$ is non-zero then the X and Y axes are not the principal axes of the beam. To calculate the beam parameters in the principal axes, a rotation of the momenta is necessary. The rotation angle can be calculated by

$$
\begin{equation*}
\phi=\frac{1}{2} \arctan \left(\frac{2\langle x y\rangle}{\left\langle x^{2}\right\rangle-\left\langle y^{2}\right\rangle}\right) \tag{137.14}
\end{equation*}
$$

With the help of the rotation matrix

$$
N=\left(\begin{array}{ccc}
\cos ^{2} \phi & 2 \sin \phi \cos \phi & \sin ^{2} \phi  \tag{137.15}\\
-\sin \phi \cos \phi & \cos ^{2} \phi-\sin ^{2} \phi & \sin \phi \cos \phi \\
\sin ^{2} \phi & -2 \sin \phi \cos \phi & \cos ^{2} \phi
\end{array}\right)
$$

the rotated momenta in the principal axis are

$$
\begin{align*}
& \left(\begin{array}{ccc}
\left\langle x^{2}\right\rangle_{r} & \left\langle x \theta_{x}\right\rangle_{r} & \left\langle\theta_{x}^{2}\right\rangle_{r} \\
\langle x y\rangle_{r} & \left(\left\langle x \theta_{y}\right\rangle_{r}+\left\langle y \theta_{x}\right\rangle_{r}\right) / 2 & \left\langle\theta_{x} \theta_{y}\right\rangle_{r} \\
\left\langle y^{2}\right\rangle_{r} & \left\langle y \theta_{y}\right\rangle_{r} & \left\langle\theta_{y}^{2}\right\rangle_{r}
\end{array}\right)= \\
& N\left(\begin{array}{ccc}
\left\langle x^{2}\right\rangle & \left\langle x \theta_{x}\right\rangle & \left\langle\theta_{x}^{2}\right\rangle \\
\langle x y\rangle & \left(\left\langle x \theta_{y}\right\rangle+\left\langle y \theta_{x}\right\rangle\right) / 2 & \left\langle\theta_{x} \theta_{y}\right\rangle \\
\left\langle y^{2}\right\rangle & \left\langle y \theta_{y}\right\rangle & \left\langle\theta_{y}^{2}\right\rangle
\end{array}\right) . \tag{137.16}
\end{align*}
$$

The momenta marked with the subscript $r$ are the momenta rotated in the principal axis. Now it is possible to calculate all beam parameters in relation to the principal axis by substituting all unrotated momenta in Sec. 137.1 and in Sec. 137.1.1 by the associated rotated ones.

### 137.2 Diffractive Optics Merit Functions

This section lists all merit functions and their defining equations which are used for the design and analysis of diffractive structures in VirtualLab Fusion.
In the equations, it is assumed that the output intensity at position $x^{\prime}$ is proportional to $\left|U_{\text {out }}\left(x^{\prime}\right)\right|^{2}$. This assumption is only valid in paraxial approximation.
The symbols $\alpha, U_{\text {in }}, U_{\text {out }}, U_{\text {sig }}$, and $\mathcal{W}_{\text {sig }}$ are defined in Sec. 138.1.1.

- The window efficiency $\eta_{\text {win }}$ is defined as the ratio between the power of the output field in the evaluation region $\mathcal{W}_{\text {sig }}$ and the power of the incident field:

$$
\begin{equation*}
\eta_{\mathrm{win}}=\frac{\int_{x^{\prime} \in \mathcal{W}_{\text {sig }}} \mathrm{d} x^{\prime}\left|U_{\text {out }}\left(x^{\prime}\right)\right|^{2}}{\int_{-\infty}^{\infty} \mathrm{d} \xi\left|U_{\text {in }}(\xi)\right|^{2}} . \tag{137.17}
\end{equation*}
$$

- The idea for calculating the conversion efficiency $\eta_{\text {conv }}$ is to measure the portion of the incident field's power which flows into the Desired Output Field [WA98]. Its value is calculated by

$$
\begin{equation*}
\eta_{\mathrm{conv}}=|\alpha|^{2} \frac{\int_{x^{\prime} \in \mathcal{L}_{\text {sig }}} \mathrm{d} x^{\prime}\left|U_{\text {sig }}\left(x^{\prime}\right)\right|^{2}}{\int_{-\infty}^{\infty} \mathrm{d} \xi\left|U_{\text {in }}(\xi)\right|^{2}}, \tag{137.18}
\end{equation*}
$$

- The signal-to-noise ratio (SNR) measures the correspondence between a (complex-valued) desired function (here: $\alpha U_{\text {sig }}$ ) and a function which possesses errors in addition (here: $U_{\text {out }}$ ). The SNR is calculated by

$$
\begin{equation*}
\mathrm{SNR}=\frac{\int_{x^{\prime} \in \mathcal{W}_{\text {sig }}} \mathrm{d} x^{\prime}\left|U_{\text {out }}\left(x^{\prime}\right)\right|^{2}}{\int_{x^{\prime} \in \mathcal{W}_{\text {sig }}} \mathrm{d} x^{\prime}\left|U_{\text {out }}\left(x^{\prime}\right)-\alpha U_{\text {sig }}\left(x^{\prime}\right)\right|^{2}} . \tag{137.19}
\end{equation*}
$$

The numerical value of the SNR is often given in dB . For getting the corresponding dB value, the decadic logarithm of the result of Eq. (137.19) has to be multiplied by 10.

- Whereas during the calculation of the SNR all positions $x^{\prime} \in \mathcal{W}_{\text {sig }}$ have influence on the result, the uniformity error is determined only by the positions with the maximum deviations between resulting and desired output field.

If we denote the largest and smallest occurring values of the quotients between output intensity and (scaled) desired output intensity by $\widehat{I}_{\text {max }}$ and $\widehat{I}_{\text {min }}$, respectively, that is

$$
\begin{equation*}
\widehat{I}_{\max }=\max _{x^{\prime} \in \mathcal{W}_{\text {sig }}} \frac{\left|U_{\text {out }}\left(x^{\prime}\right)\right|^{2}}{\left|\alpha U_{\text {sig }}\left(x^{\prime}\right)\right|^{2}}, \tag{137.20}
\end{equation*}
$$

and

$$
\begin{equation*}
\widehat{I}_{\text {min }}=\min _{x^{\prime} \in \mathcal{W}_{\mathrm{sig}}} \frac{\left|U_{\mathrm{out}}\left(x^{\prime}\right)\right|^{2}}{\left|\alpha U_{\mathrm{sig}}\left(x^{\prime}\right)\right|^{2}} \tag{137.21}
\end{equation*}
$$

then the uniformity error $E_{\text {unif }}$ can be calculated by [Ben97]

$$
\begin{equation*}
E_{\text {unif }}=\frac{\widehat{I}_{\max }-\widehat{I}_{\min }}{\widehat{I}_{\max }+\widehat{I}_{\min }} \tag{137.22}
\end{equation*}
$$

- The relative zeroth order intensity $I_{0}$ is calculated by

$$
\begin{equation*}
I_{0}=\frac{\left|U_{\mathrm{out}}(0)\right|^{2}}{|\alpha|^{2}} \tag{137.23}
\end{equation*}
$$

- The zeroth order efficiency $\eta_{0}$ is defined by

$$
\begin{equation*}
\eta_{0}=\frac{\left|U_{\mathrm{out}}(0)\right|^{2}}{\int_{-\infty}^{\infty} \mathrm{d} \xi\left|U_{\mathrm{in}}(\xi)\right|^{2}} \tag{137.24}
\end{equation*}
$$

- The maximum relative intensity of stray light $I_{\text {stray }}$ is calculated by

$$
\begin{equation*}
I_{\text {stray }}=\max _{x^{\prime} \notin \mathcal{W}_{\text {sig }}} \frac{\left|U_{\mathrm{out}}\left(x^{\prime}\right)\right|^{2}}{|\alpha|^{2}} \tag{137.25}
\end{equation*}
$$

- The complex optimal scale factor $\alpha$ is defined in Eq. (138.1).


### 137.3 Fiber Coupling Efficiency

The coupling efficiency of an arbitrary harmonic field into a single mode fiber can be obtained by calculating the complex overlap integral between the fiber mode and the harmonic field. The overlap integral is defined by

$$
\begin{align*}
\eta_{\text {coupl }} & =\eta_{\mathrm{x}, \text { coupl }}+\eta_{\mathrm{y}, \text { coupl }}  \tag{137.26}\\
& =\frac{1}{\int_{\mathbb{R}^{2}}\left|E_{\mathrm{xy}, \text { in }}\right|^{2} \mathrm{~d} x \mathrm{~d} y}\left[\frac{\left[\int_{\mathbb{R}^{2}} E_{x, \text { out }} E_{x, \mathrm{sig}}^{*} \mathrm{~d} x \mathrm{~d} y\right]^{2}}{\int_{\mathbb{R}^{2}}\left|E_{x, \text { sig }}\right|^{2} \mathrm{~d} x \mathrm{~d} y}+\frac{\left[\int_{\mathbb{R}^{2}} E_{y, \text { out }} E_{y, \text { sig }}^{*} \mathrm{~d} x \mathrm{~d} y\right]^{2}}{\int_{\mathbb{R}^{2}}\left|E_{y, \text { sig }}\right|^{2} \mathrm{~d} x \mathrm{~d} y}\right] .
\end{align*}
$$

$E_{\mathrm{xy} \text {, in }}$ is the complex amplitude of the incident field, $\binom{E_{x, \text { out }}}{E_{y, \text { out }}}$ is the complex amplitude of the field where the coupling efficiency should be calculated from and $\binom{E_{x, \text { sig }}^{*}}{E_{y, \text { sig }}^{*}}$ is the complex conjugate of the reference field - this means the harmonic field of the fiber mode. Typically as the reference field the Gaussian base mode of the fiber should be used.

### 137.4 Polarization

This detector plots either the azimuthal component $E_{\phi}$ or radial component $E_{\rho}$ (please see Fig. 792 for the meaning) of a harmonic field into a data array.
The conversion from $E_{x}$ and $E_{y}$ to $E_{\phi}$ and $E_{\rho}$ is done by the following equation:

$$
\begin{equation*}
\binom{E_{\rho}(\rho, \phi, z)}{E_{\phi}(\rho, \phi, z)}=\binom{\cos \phi \sin \phi}{-\sin \phi \cos \phi} \cdot\binom{E_{x}(x, y, z)}{E_{y}(x, y, z)} \tag{137.27}
\end{equation*}
$$



Figure 792. Decomposition of the electric field vector E into Cartesian components (blue) and polar coordinate components (green).

The polar coordinates are given by $\rho=\sqrt{x^{2}+y^{2}}$ and $\phi=\operatorname{atan} 2 \frac{y}{x} .{ }^{1}$

### 137.5 Radiometry and Photometry

In the field of optics there are several physical properties considering the energy sent out by a light source or received by a detector or a surface.
At first let us define the radiant flux $\Phi_{r}$ (in watts) through an area $A$, which is a power value:

$$
\begin{equation*}
\Phi_{r}=\int S \mathrm{~d} A, \quad \text { where } \quad S=E \times H \quad \text { the Poynting vector. } \tag{137.28}
\end{equation*}
$$

Especially this applies for the total power sent out by a source:

$$
\Phi_{r, t o t}=\oint S \mathrm{~d} A
$$

If the light is polychromatic, you have to distinguish between spectral (wavelength dependent) and integral (wavelength independent) values. They are connected by a relation of the form $\Phi_{r}=\int_{0}^{\infty} \Phi_{r}(\lambda) \mathrm{d} \lambda$, in this example $\Phi_{r}$ means the integral radiant flux and $\Phi_{r}(\lambda)=\frac{d \Phi_{r}}{\mathrm{~d} \lambda}$ the spectral radiant flux.
Furthermore these physical properties are divided into two kinds of values: physical (radiometric, subscript $r$ ) and psycho-physical (photometric, subscript $p$ ) values. For every radiometric value exists a photometric equivalent, which can be calculated from the first one (given in spectral form) by using the spectral luminous efficiency function $y_{\lambda}$. Here for instance the (spectral) radiant flux $\Phi_{r}(\lambda)$ and its photometric equivalent, the luminous flux $\Phi_{p}$ :

$$
\begin{equation*}
\Phi_{p}=680 \mathrm{Im} / \mathrm{W} \int_{0}^{\infty} y_{\lambda} \Phi_{r}(\lambda) \mathrm{d} \lambda \tag{137.29}
\end{equation*}
$$

### 137.5.1 Radiant Intensity

If you want to know what power is sent out by a point light source into a specific solid angle $\Omega$, you have to calculate its radiant intensity ( $\hookrightarrow$ Fig. 793). This is defined by

$$
\begin{equation*}
I_{r}=\frac{\mathrm{d} \Phi_{r}}{\mathrm{~d} \Omega} \tag{137.30}
\end{equation*}
$$

For the detection the distance to the source has to be known.

[^19]

Figure 793. Principle of Detecting the Radiant Intensity. $d$ is the Distance to the Point Light Source.

### 137.5.2 Radiance

For a non point source emission the radiance gives you the angular and spatial characteristics of the light source or reflecting area ( $\hookrightarrow$ Fig. 794). It is defined by

$$
\begin{equation*}
L_{r}=\frac{\mathrm{d}^{2} \Phi_{r}}{\cos \theta \mathrm{~d} \Omega \mathrm{~d} A}=\frac{\mathrm{d} S}{\mathrm{~d} \Omega} \tag{137.31}
\end{equation*}
$$

where $\Omega$ gives the solid angle and $A$ the radiating area you want the radiance to know for. $\theta$ is the angle between the Poynting vector $S$ and the normal vector $A$.
To use this detector, its position related to the light source or the reflecting area has to be known, as well as the directionality of the source. This is a curve, giving the dependency of the relative intensity ( $\frac{I}{I_{0}}$, where $I_{0}=I(\theta=0)$ ) from the angle of radiation $\theta$. A special case is a so called Lambert characteristic, which has the form $\frac{I}{I_{0}}=\cos \theta$, and which leads to an angular independent radiance.


Figure 794. Principle of Detecting the Radiance. $(x, y, z)$ is the detector position.

### 137.5.3 Irradiance

The irradiance is the total power going through an area $A$ perpendicularly ( $\hookrightarrow$ Fig. 795) and it is defined by:

$$
\begin{equation*}
E_{r}=\frac{\mathrm{d} \Phi_{r}}{\cos \theta \mathrm{~d} A}=S_{\perp} \tag{137.32}
\end{equation*}
$$

where $S_{\perp}$ is the magnitude of the component of the Poynting vector perpendicular to $A$.


Figure 795. Principle of Detecting the Irradiance

### 137.5.4 Luminous Intensity

Luminous Intensity is the photometric, i. e. psycho-physical equivalent to the Radiant Intensity ( $\hookrightarrow$ Sec. 137.5.1) and is calculated from it analog to Eq. (137.29). Under daylight conditions a different spectral luminous efficiency function $y_{\lambda}$ has to be used than for night conditions. This is due to the brightness dependency of the spectral sensitivity of the human eye.

### 137.5.5 Luminance

Luminance is the photometric, i.e. psycho-physical equivalent to the Radiance ( $\hookrightarrow$ Sec. 137.5.2) and is calculated from it analog to Eq. (137.29). Under daylight conditions a different spectral luminous efficiency function $y_{\lambda}$ has to be used than for night conditions. This is due to the brightness dependency of the spectral sensitivity of the human eye.

### 137.5.6 Illuminance

Illuminance is the photometric, i.e. psycho-physical equivalent to the Irradiance ( $\hookrightarrow$ Sec. 137.5.3) and is calculated from it analog to Eq. (137.29). Under daylight conditions a different spectral luminous efficiency function $y_{\lambda}$ has to be used than for night conditions. This is due to the brightness dependency of the spectral sensitivity of the human eye.

### 137.6 Spherical Phase

One important function is the detection of spherical phase from the phase information.
A correct detection is only possible if the sampled phase information is not undersampled. The detection is performed using a two step fitting process. A fitting is complicated due to the fact that the phase is generally in a modulo $2 \pi$ representation. And since the additional aberrations to the spherical phase factor may contain dislocations, an unwrapping of the phase and a fitting of the unwrapped phase is not always possible. Therefore not the fitting of the phase $\phi(x, y)$ but the fitting of the phase derivatives $\frac{\partial \phi(x, y)}{\partial x}=\phi^{x}(x, y)$ and $\frac{\partial \phi(x, y)}{\partial y}=\phi^{y}(x, y)$ instead is performed. For the fitting a least squares method is used. Since an analytical fitting of the spherical phase by a least squares method is not possible in a first step, a quadratic phase is fitted. For the radius $r_{\text {quad }}$ of the quadratic phase follows analytically

$$
\begin{equation*}
r_{\text {quad }}=\frac{k \sum_{i=0, j=0}^{N_{x}, N_{y}}\left(x_{i, j}^{2}+y_{i, j}^{2}\right)}{\sum_{i=0, j=0}^{N_{x}, N_{y}}\left(\phi_{i, j}^{x} x_{i, j}+\phi_{i, j}^{y} y_{i, j}\right)} \tag{137.33}
\end{equation*}
$$

with $k=\frac{2 \pi n}{\lambda}$ and n is the real part of the refractive index. In a second step an iterative fit of a spherical phase $\phi=k r$ with $r=\sqrt{x^{2}+y^{2}+r_{\text {spher }}^{2}}$ follows, starting with the result of the quadratic phase fit for $r_{\text {spher }}$. Therefore $r_{\text {spher }}$ has to be optimized in order to minimize the function

$$
\begin{equation*}
G=\sum_{i=0, j=0}^{N_{x}, N_{y}}\left[\left(\phi_{i, j}^{x}-\frac{k x_{i, i}}{r_{i, j}}\right)+\left(\phi_{i, j}^{y}-\frac{k y_{i, i}}{r_{i, j}}\right)\right] . \tag{137.34}
\end{equation*}
$$

This optimization is done numerically.

### 137.7 Field Components

### 137.7.1 Magnetic Field (H-Field)

In VirtualLab Fusion the components of the magnetic field vector $\boldsymbol{H}(r, t)$ are calculated by the following equations:

$$
\begin{align*}
& H_{x}(x, y, z)=-\frac{1}{k_{0}} \sqrt{\frac{\varepsilon_{0}}{\mu_{0}}}\left[\mathcal{F}^{-1}\left(\frac{1}{k_{z}}\left(k_{x} k_{y}\left[\mathcal{F} E_{x}(x, y)\right]+\left(k_{y}^{2}+k_{z}^{2}\right)\left[\mathcal{F} E_{y}(x, y)\right]\right)\right)\right]  \tag{137.35}\\
& H_{y}(x, y, z)=\frac{1}{k_{0}} \sqrt{\frac{\varepsilon_{0}}{\mu_{0}}}\left[\mathcal{F}^{-1}\left(\frac{1}{k_{z}}\left(\left(k_{x}^{2}+k_{z}^{2}\right)\left[\mathcal{F} E_{x}(x, y)\right]+k_{x} k_{y}\left[\mathcal{F} E_{y}(x, y)\right]\right]\right)\right]  \tag{137.36}\\
& H_{z}(x, y, z)=-\frac{1}{k_{0}} \sqrt{\frac{\varepsilon_{0}}{\mu_{0}}}\left[\mathcal{F}^{-1}\left(k_{y}\left[\mathcal{F} E_{x}(x, y)\right]-k_{x}\left[\mathcal{F} E_{y}(x, y)\right]\right)\right] . \tag{137.37}
\end{align*}
$$

with $k_{0}=\frac{2 \pi}{\lambda}$,
$k_{x}=k_{0} \sin (\theta) \cos (\varphi)=2 \pi u$,
$k_{y}=k_{0} \sin (\varphi)=2 \pi v$,
$k_{z}=k_{0} \cos (\theta) \cos (\varphi)=2 \pi w$ and $w=\sqrt{\frac{n^{2}}{\lambda^{2}}-u^{2}-v^{2}}$.

### 137.7.2 Poynting Vector

In VirtualLab Fusion the components of the time averaged Poynting vector $<\operatorname{Sr}(t)>$ are calculated by:

$$
\begin{aligned}
& <S_{x}(t)>_{t}=\frac{1}{2}\left[\operatorname{Re}\left[E_{y} \cdot H_{z}^{*}\left(E_{x}, E_{y}\right)\right]-\operatorname{Re}\left[E_{z}\left(E_{x}, E_{y}\right) \cdot H_{y}^{*}\left(E_{x}, E_{y}\right)\right]\right] \\
& <S_{y}(t)>_{t}=\frac{1}{2}\left[\operatorname{Re}\left[E_{z}\left(E_{x}, E_{y}\right) \cdot H_{x}^{*}\left(E_{x}, E_{y}\right)\right]-\operatorname{Re}\left[E_{x} \cdot H_{z}^{*}\left(E_{x}, E_{y}\right)\right]\right] \\
& <S_{z}(t)>_{t}=\frac{1}{2}\left[\operatorname{Re}\left[E_{x} \cdot H_{y}^{*}\left(E_{x}, E_{y}\right)\right]-\operatorname{Re}\left[E_{y} \cdot H_{x}^{*}\left(E_{x}, E_{y}\right)\right]\right]
\end{aligned}
$$

with $k_{0}=\frac{2 \pi}{\lambda}$,
$k_{x}=k_{0} \sin (\theta) \cos (\varphi)=2 \pi u$,
$k_{y}=k_{0} \sin (\varphi)=2 \pi v$,
$k_{z}=k_{0} \cos (\theta) \cos (\varphi)=2 \pi w$ and $w=\sqrt{\frac{n^{2}}{\lambda^{2}}-u^{2}-v^{2}}$.

### 137.8 Momentum

The momentum theory is very useful to determine the beam parameters ( $\hookrightarrow$ Sec. 137.1) of an arbitrary wave with global polarization.
The momenta of a globally polarized harmonic field $U(x, y)$ are defined by

$$
\begin{equation*}
\left\langle x^{n}, y^{m}, \theta_{\mathrm{x}}^{k}, \theta_{\mathrm{y}}^{l}\right\rangle=\frac{(-i \bar{\lambda})^{k+l}}{2 P} \cdot\left(I_{1}+I_{2}\right) \tag{137.38}
\end{equation*}
$$

with

$$
\begin{aligned}
& I_{1}=\iint d x d y x^{n} y^{m}\left[u(x, y) \frac{\partial^{k}}{\partial x^{k}} \frac{\partial^{l}}{\partial y^{l}} u^{*}(x, y)\right] \\
& I_{2}=(-1)^{(k+l)} \iint d x d y x^{n} y^{m}\left[u^{*}(x, y) \frac{\partial^{k}}{\partial x^{k}} \frac{\partial^{l}}{\partial y^{l}} u(x, y)\right] \\
& P=\iint d x d y u(x, y) u^{*}(x, y) \\
& \bar{\lambda}=\frac{\lambda}{2 \pi}
\end{aligned}
$$

In a paraxial optical system the changing of the momenta during the propagation of the wave can be described by ABCD matrices ( $\leftrightarrows$ Sec. 104) in the following way.

$$
\begin{align*}
& \left\langle x^{n}, y^{m}, \theta_{x}^{k}, \theta_{y}^{l}\right\rangle^{\prime}  \tag{137.39}\\
= & \left\langle\left(A x+B \theta_{x}\right)^{n},\left(A y+B \theta_{y}\right)^{m},\left(C x+D \theta_{x}\right)^{k},\left(C y+D \theta_{y}\right)^{l}\right\rangle .
\end{align*}
$$

## 138 Design

### 138.1 Iterative Fourier Transform Algorithm

### 138.1.1 Basic Concept and Terminology

The basic idea of the Iterative Fourier Transform Algorithm (IFTA) is to design a transmission $\mathcal{T}$ which transforms an Input Field $U_{\text {in }}$ into a Desired Output Field $U_{\text {sig }}$. The real Output Field $U_{\text {out }}$ will differ from $U_{\text {sig }}$, these differences can be measured with Diffractive Optics Merit Functions ( $\hookrightarrow$ Sec. 137.2). The IFTA optimizes these merit functions.
To make the design task easier and e.g. obtain larger structures in the resulting transmission, you can allow three types of design freedom in the output plane.

1. In the case of amplitude freedom, the correspondence between output field and desired output field is only measured within a given lateral region $x^{\prime} \in \mathcal{W}_{\text {sig }}$, which is denoted as evaluation region or optimization region.
2. In the case of phase freedom, only the amplitudes of output field and desired output field are of concern, which mathematically corresponds to the substitutions $U_{\text {out }} \rightarrow\left|U_{\text {out }}\right|$ and $U_{\text {sig }} \rightarrow\left|U_{\text {sig }}\right|$.
3. In the case of scale freedom, $U_{\text {sig }}$ can be scaled by a complex-valued factor $\alpha$ for getting a better correspondence to $U_{\text {out }}$. This optimal scale factor $\alpha$ is calculated by

$$
\begin{equation*}
\alpha=\frac{\int_{x^{\prime} \in \mathcal{W}_{\text {sig }}} \mathrm{d} x^{\prime} U_{\text {out }}^{*}\left(x^{\prime}\right) U_{\text {sig }}\left(x^{\prime}\right)}{\int_{x^{\prime} \in \mathcal{W}_{\text {sig }}} \mathrm{d} x^{\prime}\left|U_{\text {sig }}\left(x^{\prime}\right)\right|^{2}} \tag{138.1}
\end{equation*}
$$

$U_{\text {out }}^{*}$ is the complex conjugate of $U_{\text {out }}$.

### 138.1.2 Sinc Modulation due to Pixelation

VirtualLab Fusion allows an analytical simulation and compensation of a sinc effect in the far field of pixelated transmissions.
This feature can be used to correct a desired output field prior to a transmission design and to simulate the pixelation effect of a transmission after the design.
Pixelation of a transmission function means that every discrete sampling point can be understood as a rectangular pixel. In a mathematical sense this is a convolution between a rect-function and the transmission function

$$
\begin{equation*}
\mathcal{T}_{\mathrm{pix}}\left(x^{\prime}, y^{\prime}\right)=\iint \mathcal{T}(x, y) \operatorname{rect}\left(x-x^{\prime}, \frac{\Delta x}{2}\right) \operatorname{rect}\left(y-y^{\prime}, \frac{\Delta y}{2}\right) d x d y \tag{138.2}
\end{equation*}
$$

In the far field this convolution gives a multiplication between a sinc-function and the far field of the transmission

$$
\begin{equation*}
\mathcal{F}\left(\mathcal{T}_{\text {pix }}\left(x^{\prime}, y^{\prime}\right)\right)=\mathcal{F}(\boldsymbol{\mathcal { T }}(x, y)) \operatorname{sinc}\left(\frac{u \pi}{\Delta x}\right) \operatorname{sinc}\left(\frac{v \pi}{\Delta y}\right) \tag{138.3}
\end{equation*}
$$

$\Delta x$ and $\Delta y$ are the pixel sizes in $x$ - and $y$ - direction of the transmission. If a sinc-compensation is performed, VirtualLab Fusion divides the far field by a sinc-function in order to avoid a modulation of the far field due to a pixelation.

### 138.2 Parametric Optimization

The parametric optimization in VirtualLab Fusion allows you to optimize optical systems by means of nonlinear optimization algorithms. For that purpose VirtualLab Fusion supports the definition of merit functions that are to be optimized. Merit functions can take into account detector results. Further several types of parameter constraints are formulated as merit functions as well. Finally a common merit function is constructed by a weighted sum of individual merit functions.

### 138.2.1 Definition of the Target Function

Basically, the target function is a summed combination of constraints. Constraints are functions of the parameter vector $\mathbf{x}=\left(x_{1}, \ldots, x_{t}\right)^{T}$ that can represent ranges or target values of

- the parameters itself (parameter constraints),
- merit functions calculated by detectors (merit function constraints) or
- general (arbitrary) functions (general constraints).

Let $\left\{f_{i}(\mathbf{x})\right\}_{i=1, \ldots, n}$ be the set of user-defined constraints. Then the target function $F(\mathbf{x})$ is defined as the weighted sum over all constraints:

$$
\begin{equation*}
F(\mathbf{x})=\sum_{i=1}^{n} g_{i} f_{i}(\mathbf{x}) \tag{138.4}
\end{equation*}
$$

where $g_{i}$ is the weight for the i -th constraint.
Each constraint $f_{i}(\mathbf{x})$ is a composition of an inner function $\sigma_{i}(\mathbf{x})$ and outer function $\hat{f}_{i}(s)$ which conveys the actual constraint type.

$$
\begin{equation*}
f_{i}(\mathbf{x})=\hat{f}_{i}\left(\sigma_{i}(\mathbf{x})\right) \tag{138.5}
\end{equation*}
$$

$\hat{f}_{i}(s)$ yields an positive value, if the constraint is violated and 0 , if not.

### 138.2.1.1 Definition of the Inner Function $\sigma(\mathbf{x})$

The inner function $\sigma_{i}\left(x_{1}, \ldots, x_{t}\right)$ of the parameter constraint that corresponds to the $k$-th parameter $(1 \leq k \leq t)$ is the identity function with respect to this parameter:

$$
\begin{equation*}
i d^{k}\left(x_{1}, \ldots, x_{t}\right)=x_{k} \tag{138.6}
\end{equation*}
$$

The inner functions of merit function constraints are the underlying detector merit functions. An inner function $\sigma(\mathbf{x})$ of a general constraint can be an arbitrary function. Such a function, also called general structure parameter, is evaluated only during parametric optimization.
Each inner function is evaluated in SI derived units.

### 138.2.1.2 Definition of the Outer Function $\hat{f}(s)$

The outer function $\hat{f}_{i}(s)$ of a constraint $f_{i}$ is quadratic in regions of constraint violation and constant zero if constraints are fulfilled. $\hat{f}_{i}(s)$ is continuous anyway. The actual definition depends on the constraint type. There are 4 different constraint types:

- Lower Limit, i.e. $\hat{f}_{i}(s)$ yields a positive value if $s=\sigma\left(x_{1}, \ldots, x_{t}\right)$ is smaller than $s_{\text {min }}$ :

$$
\begin{align*}
\hat{f}_{i}(s) & =h_{1}(s), \text { where }  \tag{138.7}\\
h_{1}(s) & = \begin{cases}0 & : s \geq s_{\min } \\
\left(s-s_{\min }\right)^{2} & : s<s_{\min }\end{cases} \tag{138.8}
\end{align*}
$$

- Upper Limit, i.e. $\hat{f}_{i}(s)$ yields a positive value if $s$ is greater than $s_{\max }$ :

$$
\begin{align*}
\hat{f}_{i}(s) & =h_{2}(s), \text { where }  \tag{138.9}\\
h_{2}(s) & = \begin{cases}0 & : s \leq s_{\max } \\
\left(s-s_{\max }\right)^{2} & : s>s_{\max }\end{cases} \tag{138.10}
\end{align*}
$$

- Range, i.e. $\hat{f}_{i}(s)$ yields a positive value if $s$ is not in range $\left[s_{\min }, s_{\max }\right]$ :

$$
\begin{align*}
\hat{f}_{i}(s) & =h_{3}(s), \text { where }  \tag{138.11}\\
h_{3}(s) & =h_{1}(s)+h_{2}(s) \tag{138.12}
\end{align*}
$$

and $h_{1}(s)$ and $h_{2}(s)$ correspond to Eq. (138.8) and Eq. (138.10), respectively.

- Target Value, i.e. $\hat{f}_{i}(s)$ conveys the distance of $s$ to the target value $s_{t}$ (which is allowed to be $\pm \infty$ ):

$$
\begin{align*}
& \hat{f}_{i}(s)=h_{4}(s), \text { where }  \tag{138.13}\\
& h_{4}(s)= \begin{cases}\infty & : s_{t}=+\infty \text { and } s \leq 0 \text { or } \\
s_{t}=-\infty \text { and } s \geq 0 \\
\frac{1}{s^{2}} & : s_{t}=+\infty \text { and } s>0 \text { or } \\
& s_{t}=-\infty \text { and } s<0 \\
\left(s-s_{t}\right)^{2} & : \text { else . }\end{cases} \tag{138.14}
\end{align*}
$$

### 138.2.2 Calculation of the estimated error

For Powell's method the estimated error $\varepsilon$ is calculated from

$$
\varepsilon= \begin{cases}\left|y_{i}-y_{i+1}\right| & :\left|y_{i}\right|+\left|y_{i+1}\right|<1  \tag{138.15}\\ \frac{2\left|y_{i}-y_{i+1}\right|}{\left|y_{i}\right|+\left|y_{i+1}\right|} & : \text { else }\end{cases}
$$

where $y_{i}=f\left(\mathbf{x}_{i}\right)$ and $y_{i+1}=f\left(\mathbf{x}_{i+1}\right)$ are the target function evaluations in subsequent iterations. Note that the estimated error is absolute in the first case and relative in the second.
For the downhill simplex algorithm $\varepsilon$ is calculated similarly:

$$
\varepsilon= \begin{cases}\left|y_{1}-y_{2}\right| & :\left|y_{1}\right|+\left|y_{2}\right|<1  \tag{138.16}\\ \frac{10\left|y_{1}-y_{2}\right|}{\left|y_{1}\right|+\left|y_{2}\right|} & : \text { else }\end{cases}
$$

However, $y_{1}$ and $y_{2}$ are the target function values of the worst and the best vertex of the simplex in each iteration step.

### 138.2.3 Global Optimization Algorithms

### 138.2.3.1 Simulated Annealing

The simulated annealing method is based on an analogy from materials science and enables the global search for the minimum by an random temperature term $t$ that is added to the current target function value. It is obtained from

$$
\begin{equation*}
t=T \log r \tag{138.17}
\end{equation*}
$$

where $r$ is a random value between 0 and 1. $T$ is the temperature, which is gradually decreased according to an annealing schedule. The selected local optimization algorithm is applied to the adapted target function at each annealing step. Currently, the downhill simplex algorithm is the only possible choice for the applied local optimization algorithm.
For locating the global minimum successfully, appropriate values for start temperature and number of annealing steps must be chosen. Unfortunately, this is something of a trial and error process in most cases. If the start temperature is too low the algorithm will possibly get stuck in the surrounding of a local minimum. On the other hand, temperature values that are too high will increase the probability for "jumping out" of the surrounding of an already detected global minimum.

### 138.2.3.2 Evolutionary Algorithm

The Evolutionary Algorithm method is based on an analogy from population-based evolution and enables the global search for the minimum by a random temperature term that is added to the current target function value. An Evolutionary Algorithm is inspired by biological evolution. As such, reproduction, mutation, recombination, and selection act as operators. These operators are continuously used to find desired minimum, maximum or target value just like evolution of a population results in fittest species.

## 139 Miscellaneous

### 139.1 Debye-WoIf Integral

With the Debye-Wolf Integral [Wol59][FT11] one can easily calculate the field in or near the focus of an ideal aplanatic lens which is illuminated with collimated light.
In cylindrical coordinates $(\rho, \varphi, z)$ the field can be expressed as:

$$
\boldsymbol{E}(\rho, \varphi, z)=\left[\begin{array}{c}
E_{x}(\rho, \varphi, z)  \tag{139.1}\\
E_{y}(\rho, \varphi, z) \\
E_{z}(\rho, \varphi, z)
\end{array}\right]=-\mathrm{ikf}\left[\begin{array}{c}
E_{x, \text { in }}\left(I_{0}-I_{2} \cos 2 \varphi\right)-E_{y, \text { in }} I_{2} \sin 2 \varphi \\
E_{y, \text { in }}\left(I_{0}+I_{2} \cos 2 \varphi\right)-E_{x, \text { in }} I_{2} \sin 2 \varphi \\
-2 I_{1}\left(E_{x, \text { in }} \cos \varphi+E_{y, \text { in }} \sin \varphi\right)
\end{array}\right]
$$

where $f$ is the focal length. $k=2 \pi n / \lambda . \lambda$ is the wavelength of the incident field. $n$ is the refractive index of the material around the lens. The cylindrical coordinates $\rho$ and $\varphi$ are given by $\rho=\sqrt{x^{2}+y^{2}}$ and $\varphi=\operatorname{atan} 2 y / x^{1}$. $E_{x, \text { in }}$ and $E_{y, \text { in }}$ are the components of the Jones vector of the incident field.

$$
\begin{align*}
& I_{0}=\int_{0}^{\alpha} \sqrt{\cos \theta} \sin \theta(\cos \theta+1) J_{0}(k \rho \sin \theta) \exp (\mathrm{i} k z \cos \theta) \mathrm{d} \theta  \tag{139.2a}\\
& I_{1}=\int_{0}^{\alpha} \sqrt{\cos \theta} \sin ^{2} \theta J_{1}(k \rho \sin \theta) \exp (\mathrm{i} k z \cos \theta) \mathrm{d} \theta  \tag{139.2b}\\
& I_{2}=\int_{0}^{\alpha} \sqrt{\cos \theta} \sin \theta(\cos \theta-1) J_{2}(k \rho \sin \theta) \exp (\mathrm{i} k z \cos \theta) \mathrm{d} \theta \tag{139.2c}
\end{align*}
$$

where $J_{0}, J_{1}, J_{2}$ are the Bessel functions of first kind. $\alpha$ is related to the numerical aperture NA by

$$
\begin{equation*}
\alpha=\arcsin \left(\frac{\mathrm{NA}}{n}\right) \tag{139.3}
\end{equation*}
$$

### 139.2 Defining Directions and Orientations in $\mathbb{R}^{3}$

In general, we have to differentiate between defining a single direction vector in $\mathbb{R}^{3}$ and defining the orientation of a solid. The first task requires two angles while the latter one has got three degrees of freedom. Nonetheless, both purposes are strongly related.

[^20]There is a large variety of equivalent conventions which can be used to define spatial directions and orientations. This section described all conventions used inside VirtualLab Fusion.

### 139.2.1 Spherical Angles



Figure 796. Example for defining an orientation using spherical angles and a subsequent rotation about the z-axis.

### 139.2.1.1 Defining a Single Direction via Spherical Angles

The "Spherical Angles" convention can be used for defining a direction in reference to another direction using the spherical angles $\theta$ and $\phi$. In VirtualLab Fusion, the reference direction may be given by the $x$-, $y$-, or z-axis if just a single direction is to be defined. The angle $\theta$ is the inclination angle between the defined direction and the reference axis. The plane which contains both the new direction and the reference axis is rotated by the other angle $\phi$ about the reference axis. One can describe the angle $\phi$ as the rotation angle of the node vector for $\theta$ as well.
In Fig. 796, the left picture shows the inclination of the vector $Z^{\prime}$ by $\theta$ and $\phi$. While $\theta$ gives the angle between $Z^{\prime}$ and its reference direction $Z, \phi$ defines the angle between the node vector $N$ and the Y -axis. It is identical to the angle between the plane which is defined by $Z^{\prime}$ and $Z$ and the $X$-Z-plane.

### 139.2.1.2 Defining a Solid's Orientation via Spherical Angles

The spherical angles $\theta$ and $\phi$ provide two out of three degrees of freedom a solid's orientation in $\mathbb{R}^{3}$ has got. Only one of the solid's axes can be set by those two angles as described in Sec. 139.2.1.1 above. The third degree of freedom can be fixed by an additional rotation of the solid about this axis. This additional rotation can be performed either before setting the solid's axis via spherical angles or after it.
In VirtualLab Fusion, the axis which is inclined by the spherical angles $\theta$ and $\phi$ is always the solid's $z$-axis. So, either the solid is rotated by an angle $\zeta$ about the $z$-axis first, followed by the inclination of the solid's $z$-axis according to the spherical angles. Or, the inclination using $\theta$ and $\phi$ is performed in the first step and the solid is rotated by the angle $\zeta$ about the new $z^{\prime}$-axis second.
In Fig. 796, both steps are shown. In the left picture, the z-axis is inclined using $\theta$ and $\phi$. In the right picture, the subsequent rotation about $\zeta$ is shown.

### 139.2.2 Direction Angles



Figure 797. Example for defining an orientation using direction angles and a subsequent rotation about the z-axis.

### 139.2.2.1 Defining a Single Direction via Direction Angles

The direction angles $\rho, \sigma$, and $\tau$ determine a direction in $\mathbb{R}^{3}$. They are defined as the angles between the direction to be defined and the coordinate axes. Please note that only two of this three angles are independent. If, for instance, $\rho$ and $\sigma$ are set, the value of $\tau$ follows from $\rho$ and $\sigma$, except for its sign. The angle's cosines are identical to x -, y - and z -component of the defined direction resp.
In Fig. 797, the left picture shows the definition of the vector $Z^{\prime}$ by $\rho, \sigma$ and $\tau$ being the angles between $Z^{\prime}$ and $X, Y$ and $Z$ respectively.

### 139.2.2.2 Defining a Solid's Orientation via Direction Angles

The direction angles $\rho, \sigma$ and $\tau$ provide two out of three degrees of freedom (because only two angles are independent) a solid's orientation in $\mathbb{R}^{3}$ has got. Only one of the solid's axes can be set by those angles as described in Sec. 139.2.2.1 above. The third degree of freedom can be fixed by an additional rotation of the solid about this axis. This additional rotation can be performed either before setting the solid's axis via spherical angles or after it.
In VirtualLab Fusion, the axis which is inclined by the direction angles $\rho, \sigma$ and $\tau$ is always the solid's z-axis. So, either the solid is rotated by an angle $\zeta$ about the $z$-axis first, followed by the inclination of the solid's z-axis according to the direction angles. Or, the inclination using $\rho, \sigma$ and $\tau$ is performed in the first step and the solid is rotated by the angle $\zeta$ about the new $z$ '-axis second.
In Fig. 797, both steps are shown. In the left picture, the z-axis is inclined using $\rho, \sigma$ and $\tau$. In the right picture, the subsequent rotation about $\zeta$ is shown.

### 139.2.3 Cartesian Angles



Figure 798. Example for defining an orientation using Cartesian angles and a subsequent rotation about the z-axis.

### 139.2.3.1 Defining a Single Direction via Cartesian Angles

The "Cartesian Angles" convention can be used for defining a direction in reference to one of the coordinate system's base axes. The angles $\alpha$ and $\beta$ are defined as the angles of the projections of the direction onto the base planes of the coordinate system.
In Fig. 798, the left picture shows the definition of the vector $Z^{\prime}$ by $\alpha$ and $\beta$ being the angles between $Z$ and the projection of $Z^{\prime}$ onto the x-z-plane and the y-z-plane respectively.

### 139.2.3.2 Defining a Solid's Orientation via Cartesian Angles

The Cartesian angles $\alpha$ and $\beta$ provide two out of three degrees of freedom a solid's orientation in $\mathbb{R}^{3}$ has got. Only one of the solid's axes can be set by those two angles as described in Sec. 139.2.3.1 above. The third degree of freedom can be fixed by an additional rotation of the solid about this axis. This additional rotation can be performed either before setting the solid's axis via Cartesian angles or after it.
In VirtualLab Fusion, the axis which is inclined by the Cartesian angles $\alpha$ and $\beta$ is always the solid's $z$-axis. So, either the solid is rotated by an angle $\zeta$ about the $z$-axis first, followed by the inclination of the solid's z-axis according to the Cartesian angles. Or, the inclination using $\alpha$ and $\beta$ is performed in the first step and the solid is rotated by the angle $\zeta$ about the new $z$ '-axis second.
In Fig. 798, both steps are shown. In the left picture, the z-axis is inclined using $\alpha$ and $\beta$. In the right picture, the subsequent rotation about $\zeta$ is shown.
139.2.4 Sequence of Axis Rotations


Figure 799. Example for defining an orientation using an axis rotation sequence with fix axes.

### 139.2.4.1 Defining a Single Direction via Sequence of Axis Rotations

The "Sequence of Axis Rotations" convention can be used for defining a direction in reference to one of the coordinate system's base axes. A sequence of rotations can be defined, each one performed about one of the coordinate system's base axes.
In Fig. 799, the definition of the vector $Y^{\prime \prime \prime}$ via a sequence of three rotations can be reconstructed. At first, a rotation by angle $\zeta$ about the $z$-axis transfers the reference axis $Y$ into a new vector $Y^{\prime}$. In a second step, $Y^{\prime}$ is transformed by a rotation of angle $\xi$ about the $x$-axis into the vector $Y^{\prime \prime}$. The last step of rotating $Y^{\prime \prime}$ about the y-axis by using an angle $\eta$ results in the final vector $Y^{\prime \prime \prime}$.

### 139.2.4.2 Defining a Solid's Orientation via Sequence of Axis Rotations

There are two ways for defining the orientation of a solid using a sequence of axis rotations. On the one hand, the orientation can be given by a sequence of rotations about axes that are fix in space. On the other hand, the axes for any subsequent rotation can result from former rotations. These two cases are shown as examples in Fig. 799 and Fig. 800.


Figure 800. Example for defining an orientation using an axis rotation sequence with non fix axes.

### 139.2.5 Defining a Solid's Orientation via Euler Angles



Figure 801. Example for defining an orientation using Euler angles.

The definition of the orientation of a solid via Euler angles is shown as an example in Fig. 801. The Euler angles $\Psi, \Theta$, and $\Phi$ represent rotation angles applied to non-fix coordinate axes. The whole coordinate system is rotated about certain coordinate axes in a certain sequence, in this way, Euler angles can be seen as a special case of an axis rotation sequence (see Sec. 139.2.4.2). $\Psi$ is the first rotation angle, performed about the z-axis. $\Theta$ represents the second rotation angle, applied to a rotation about the new $x^{\prime}$-axis, resulting from the first ( $\Psi-)$ rotation. The last step, the $\Phi$-rotation is performed about the new $z^{\prime}$-axis, which is a result from the prior rotation about the x'-axis.

### 139.2.6 Rotation Matrix

### 139.2.6.1 Defining a Single Direction via Rotation Matrix

The "Rotation Matrix" convention can be used for defining a direction in reference to another direction using a $3 \times 3$ - rotation matrix $M$. In VirtualLab Fusion, the reference direction may be given by the $x-, y$-, or $z$-axis if just a single direction is to be defined.
The direction $d$ is calculated by

$$
\begin{equation*}
\boldsymbol{d}=M \cdot \boldsymbol{r} \tag{139.4}
\end{equation*}
$$

where $r$ is the reference direction, being $(0,0,1)$ ( $z$-axis as reference), $(1,0,0)$ ( $x$-axis as reference), or $(0,1,0)$ ( $y$-axis as reference).

### 139.2.6.2 Defining a Solid's Orientation via Rotation Matrix

The orientation of a solid can be completely defined by a $3 \times 3$ - matrix. The solid's new axes can be calculated from the old axes just by applying matrix multiplications as described in Sec. 139.2.6.1.

### 139.2.7 Defining a Single Direction via Direction Vector

A normalized direction vector can be defined by an arbitrary (not-normalized) vector just by normalizing:

$$
\begin{equation*}
\boldsymbol{d}=\boldsymbol{r} / \sqrt{r_{x}^{2}+r_{y}^{2}+r_{z}^{2}} \tag{139.5}
\end{equation*}
$$

with $d$ being the normalized direction vector and $r=\left(r_{x}, r_{y}, r_{z}\right)^{T}$ representing the not-normalized vector.

### 139.3 Wave Direction Conversions

There are different ways how wave directions can be specified:

- Cartesian angles
- Spherical angles
- Wave vector components and
- Spatial frequencies

The Cartesian angles $\alpha$ and $\beta$ are related to the wave vector components $k_{x}$ and $k_{y}$ by

$$
\begin{align*}
\tan \alpha & =\frac{k_{x}}{k_{z}},  \tag{139.6}\\
\tan \beta & =\frac{k_{y}}{k_{z}}, \tag{139.7}
\end{align*}
$$

with wave number

$$
\begin{equation*}
k=\frac{2 \pi n\left(\lambda_{\mathrm{vac}}\right)}{\lambda_{\mathrm{vac}}}=\sqrt{k_{x}^{2}+k_{y}^{2}+k_{z}^{2}} \tag{139.8}
\end{equation*}
$$

The spherical angles $\phi$ and $\theta$ are related to the wave vector components $k_{x}$ and $k_{y}$ by

$$
\begin{align*}
k_{x} & =k \cos \phi \sin \theta \quad \text { and }  \tag{139.9}\\
k_{y} & =k \sin \phi \sin \theta \tag{139.10}
\end{align*}
$$

The spatial frequencies $u$ and $v$ are related to $k_{x}$ and $k_{y}$ by

$$
\begin{align*}
& u=k_{x} /(2 \pi) \quad \text { and }  \tag{139.11}\\
& v=k_{y} /(2 \pi) . \tag{139.12}
\end{align*}
$$

### 139.4 Fresnel Equations

The complex Fresnel coefficients (the transmission coefficients $\tau_{T E}$ and $\tau_{T M}$ for perpendicular (TE) and parallel (TM) polarization as well as the reflection coefficients $\rho_{\mathrm{TE}}$ and $\rho_{\mathrm{TM}}$ ) according to Fresnel's equations:

$$
\begin{align*}
\tau_{\mathrm{TE}} & =\frac{2 \sin \theta^{\prime} \cos \theta}{\sin \left(\theta+\theta^{\prime}\right)}  \tag{139.13}\\
\rho_{\mathrm{TE}} & =-\frac{\sin \left(\theta-\theta^{\prime}\right)}{\sin \left(\theta+\theta^{\prime}\right)}  \tag{139.14}\\
\tau_{\mathrm{TM}} & =\frac{2 \sin \theta^{\prime} \cos \theta}{\sin \left(\theta+\theta^{\prime}\right) \cos \left(\theta-\theta^{\prime}\right)}  \tag{139.15}\\
\rho_{\mathrm{TM}} & =\frac{\tan \left(\theta-\theta^{\prime}\right)}{\tan \left(\theta+\theta^{\prime}\right)} \tag{139.16}
\end{align*}
$$

The refraction angle $\theta^{\prime}$ is given by the law of refraction: $\sin \theta^{\prime}=\tilde{n} / \tilde{n}^{\prime} \sin \theta$, where $\theta$ is the incidence angle and $\tilde{n}$ and $\tilde{n}^{\prime}$ mean the complex refractive indices of the two media.
Furthermore the reflectance $R$ and the transmittance $T$ are calculated using:

$$
\begin{align*}
R_{\mathrm{TE} / \mathrm{TM}} & =\left|\rho_{\mathrm{TE} / \mathrm{TM}}\right|^{2}  \tag{139.17}\\
T_{\mathrm{TE} / \mathrm{TM}} & =\left|\tau_{\mathrm{TE} / \mathrm{TM}}\right|^{2} \frac{n^{\prime} \cos \theta^{\prime}}{n \cos \theta} \tag{139.18}
\end{align*}
$$

Here $n$ and $n^{\prime}$ are the real parts of $\tilde{n}$ and $\tilde{n}^{\prime}$, respectively.

### 139.5 Grating Equation

The components of the wave vector $k_{\text {out }}$ of a diffraction order $(l, m)$ are calculated by the following equations

$$
\begin{align*}
& k_{\mathrm{out}, \mathrm{x}}=k_{\mathrm{in}, \mathrm{x}}+\frac{2 \pi l}{P_{\mathrm{x}}}  \tag{139.19}\\
& k_{\mathrm{out}, \mathrm{y}}=k_{\mathrm{in}, \mathrm{y}}+\frac{2 \pi m}{P_{\mathrm{y}}}  \tag{139.20}\\
& k_{\mathrm{out}, \mathrm{z}}=\operatorname{sign}\left(n_{\mathrm{out}}\right) \sqrt{\left(\frac{2 \pi n_{\mathrm{out}}}{\lambda}\right)^{2}-k_{\mathrm{out}, \mathrm{x}}^{2}-k_{\mathrm{out}, \mathrm{y}}^{2}} \tag{139.21}
\end{align*}
$$

$P_{\mathrm{x}} / P_{\mathrm{y}} \quad$ Period of the grating along the x -/y-axis of the grating coordinate system
$P_{y}=\infty$ for 1D-periodic gratings
$k_{\text {in }}=e \frac{2 \pi n_{\text {in }}}{\lambda} \quad$ Wave vector of the incident field
$\boldsymbol{e} \quad$ Normalized direction vector of the incident field in the grating coordinate system
$\lambda \quad$ Vacuum wavelength
$n_{\text {in }} \quad$ Refractive index the incident wave is defined in.
$n_{\text {out }} \quad$ Refractive index the diffracted light is defined in.
$n_{\text {out }}=-n_{\text {in }}$ for reflected diffraction orders.

### 139.6 Calculation of Efficiencies from Rayleigh Coefficients

The efficiency $\eta$ of a grating order can be calculated from its Rayleigh coefficients vector $R$ as follows.

$$
\begin{equation*}
\eta=\frac{n_{\mathrm{out}}}{A_{\mathrm{in}}^{2} n_{\mathrm{in}} \cos \vartheta_{\mathrm{in}}} \cdot \cos \vartheta_{\mathrm{out}}|\boldsymbol{R}|^{2} \tag{139.22}
\end{equation*}
$$

$n_{\text {in }} / n_{\text {out }}$ is the refractive index of the medium in which the incident wave / outgoing order propagates (with an angle $\vartheta_{\text {in }} / \vartheta_{\text {out }}$ ). $A_{\text {in }}$ is the amplitude of the incident plane wave. $|\boldsymbol{R}|^{2}=R_{x}^{2}+R_{y}^{2}+R_{z}^{2}=R_{\mathrm{TE}}^{2}+R_{\mathrm{TM}}^{2}$.

### 139.7 Paraxial Imaging with a Lens

Two equations are important for calculating distances and sizes for paraxial imaging.
The imaging equation describes the relation between the focal length $f$, the object distance $s_{0}$, and the image distance $s_{i}$ :

$$
\begin{equation*}
\frac{1}{f}=\frac{1}{s_{i}}-\frac{1}{s_{o}} \tag{139.23}
\end{equation*}
$$

while the magnification $y_{i} / y_{0}$ (i.e. the ratio of the image size $y_{i}$ to the object size $y_{0}$ ) is related to the object and image distance as follows:

$$
\begin{equation*}
y_{i} / y_{o}=\frac{s_{i}}{s_{0}} \tag{139.24}
\end{equation*}
$$

## XVIII Appendix

## A Annotations for Catalog Entries

## A. 1 Boundary Responses Catalog

## A.1.1 LightTrans Defined: Axicon

For a given lateral position $(x, y)$ and the vacuum wavelength $\lambda$ this boundary response defines an axicon function $c(x, y, \lambda)$ for a given angle Angle using the following formula:

$$
c(x, y, \lambda)=\exp \left(-i k_{x} r\right)=\cos k_{x} r+i \sin k_{x} r
$$

where

$$
k_{x}=\operatorname{sign}(\text { Angle }) \cdot \frac{2 \pi \mid \tan \text { Angle } \mid}{\lambda \sqrt{1+\tan ^{2} \text { Angle }}}
$$

and

$$
r=\sqrt{x^{2}+y^{2}}
$$

The parameter Angle is a Global Parameter and can also be varied by the parameter run document.

## A.1.2 LightTrans Defined: Cylinder Lens

For a given lateral position $(x, y)$ and the vacuum wavelength $\lambda$ this boundary response defines a complex cylindrical lens function for given angle Angle and focal length FocalLength. The amplitude of the function is 1.0 and the phase $\phi(x, y, \lambda)$ is defined by the following formula:

$$
\phi=\operatorname{sign}(- \text { FocalLength }) \cdot k \cdot \sqrt{\left.r^{2}+\text { FocalLength }^{2}\right)}
$$

where

$$
k=\frac{2 \pi}{\lambda}
$$

and

$$
r=(x \sin \text { Angle }+y \cos \text { Angle }) .
$$

The parameters Angle and FocalLength are Global Parameters and can also be varied by the parameter run document.

## A.1.3 LightTrans Defined: Double Pinhole

For a given lateral position $(x, y)$, this boundary response defines a double pinhole function $f(x, y)$ with two pinholes with a given radius Radius. The pinholes are placed on the x-axis in a distance Distance to each other centered at the origin. So the pinholes are placed at positions $P_{1}:=(-$ Distance $/ 2,0)$ and $P_{2}:=($ Distance $/ 2,0)$. The function $f(x, y)$ is real (imaginary part equals to zero) and is defined by

$$
f(x, y)=\left\{\begin{array}{l}
1, \text { if } \operatorname{dist}\left((x, y), P_{1}\right)<\text { Radius or } \operatorname{dist}\left((x, y), P_{2}\right)<\text { Radius } \\
0, \text { otherwise }
\end{array}\right.
$$

where dist (.,.) is the distance between two points. The parameters Distance and Radius are Global Parameters and can also be varied by the parameter run document.

## A.1.4 LightTrans Defined: Double Slit

For a given lateral position $(x, y)$, this snippet defines a double slit function $f(x, y)$ with two slits with a given width SlitWidth. The slits are infinite in y-direction and are placed on the x -axis in a distance SlitDistance to each other centered at the origin. So the slits are placed at positions $x_{1}:=(-$ SlitDistance $/ 2)$ and $x_{2}:=$ (SlitDistance/2). The function $f(x, y)$ is real (imaginary part equals to zero), independent of $y$ and is defined by

$$
f(x, y)=\left\{\begin{array}{l}
1, \text { if }\left|x-x_{1}\right|<\text { SlitWidth/2 or }\left|x-x_{2}\right|<\text { SlitWidth/2 } \\
0, \text { otherwise }
\end{array}\right.
$$

The parameters SlitDistance and SlitWidth are Global Parameters and can also be varied by the parameter run document.

## A.1.5 LightTrans Defined: Rotated Aperture

This boundary response describes a rotatable rectangular or elliptical aperture.
For the snippet defining this boundary response the internal VirtualLab Fusion-method "ApertureFactor" is used. This method checks if a point of the field which is handed over is within the defined (unrotated!) aperture and modifies its value accordingly.
The starting point is that the coordinate system of the field and the coordinate system in which the aperture is defined are identically oriented.
It is not possible to rotate the coordinate system of the aperture itself, instead this snippet rotates the points of the field in opposite direction before handing them over to the method.
Thus the whole process looks like the following: VirtualLab Fusion hands over all field points to the snippet one after another. The snippet rotates these points in the direction opposite to the desired angle $\alpha$. These rotated points are handed over to the method "ApertureFactor" which compares their position with the unrotated aperture's area and adds a factor in the range of $[0 ; 1]$ to their values. For the method there is no difference whether the aperture is rotated counter-clockwise or the points are rotated clockwise. The method compares two areas rotated to each other. It only depends on the overlap which is the same for both rotating options. Finally the snippet returns all modified field values one after another.
In mathematical words: This means either the coordinate system in which the aperture is described has to be rotated (using the transposed rotational matrix) or the points of the complex field are rotated in opposite direction (using the rotational matrix with negative angle, i. e. the transposed rotational matrix again). Because the first option is not available the latter remains.
Thus the rotational matrix

$$
\mathrm{R}_{i j}=\left(\begin{array}{cc}
\cos (-\alpha) & -\sin (-\alpha)  \tag{A.1}\\
\sin (-\alpha) & \cos (-\alpha)
\end{array}\right)
$$

is used according

$$
\begin{equation*}
\boldsymbol{a}_{\text {rotated }}=\mathrm{R}_{i j} \cdot \boldsymbol{a}_{\text {unrotated }} \tag{A.2}
\end{equation*}
$$

with $\alpha$ as the desired rotation angle in counter-clockwise direction and $a$ as the position vector to any point of the field. Fig. 802 illustrates the snippet's approach.




Figure 802. Illustration of rotating approach. Red denotes the coordinate system for describing the aperture, black denotes the coordinate system of the field. The little circle denotes a point in the field plane which is only within the area of an unrotated aperture. Left: Identically oriented coordinate systems; Middle: Illustration of desired result; Right: Snippet's approach.

The snippet defining this boundary response has the following Global Parameters (which can also be varied by the parameter run document):

| GLOBAL PARAMETER | VARIABLE NAME | PRESET VALUE |
| :--- | :--- | :--- |
| Angle | AngleCounterClockwise | $0^{\circ}$ |
| Rectangular or elliptical | IsRectangular | 1 (TRUE) |
| x-extension of aperture | InitialDiameterX | $250 \mu \mathrm{~m}$ |
| y-extension of aperture | InitialDiameterY | $250 \mu \mathrm{~m}$ |
| Absolute edge width | AbsoluteEdgeWidth | 0 m |
| Shift of the harmonic field in x-direction | OffsetX | 0 m |
| Shift of the harmonic field in y-direction | OffsetY | 0 m |

Fig. 803 shows some apertures created with this boundary response.


Figure 803. Example results of this snippet. Upper left: Rectangular aperture with $250 \mu \mathrm{~m} \times 250 \mu \mathrm{~m}$; Upper right: Circular aperture with same dimensions as left; Lower left: $250 \mu \mathrm{~m} \times 500 \mu \mathrm{~m}$, edge width is set to $50 \%$, the offsets for $x$ and $y$ are $300 \mu \mathrm{~m}$ and $200 \mu \mathrm{~m}$ and $\alpha=30^{\circ}$; Lower right: Circular aperture with same parameters as left but with $\alpha=-30^{\circ}$.

## A.1.6 LightTrans Defined: Multiple Slits

This boundary response allows you to define an arbitrary number of equidistant slits with an arbitrary width and distance. The resulting function is invariant in y-direction.
The snippet defining this boundary response has the following Global Parameters defined (which can also be varied by the parameter run document):

| GLOBAL PARAMETER | DESCRIPTION |
| :--- | :--- |
| NumberOfSlits | The number of slits. |
| SlitWidth | The width of one slit. Within one slit, the amplitude of the function is 1, i.e. <br> light passes unchanged. Outside, the amplitude is zero, which means that <br> the light is blocked. |
| SlitDistance | The distance between two consecutive slits (measured from slit center to slit <br> center). |

## A.1.7 LightTrans Defined: SLM/DMD Function

This boundary response enables the user to simulate a so-called "Digital Micromirror Device" (DMD) which is a type of "Spatial Light Modulator" (SLM).
The snippet defining this boundary response provides the following Global Parameters (which can also be varied by the Parameter Run):

| CONFIGURABLE PARAMETER | VARIABLE NAME | PRESET VALUE |
| :--- | :--- | :--- |
| Values of desired amplitude for each DMD- <br> pixel | AmplitudeValues | Example array with ascending <br> and descending values |
| Values of desired phase for each DMD-pixel | PhaseValues | Example array with arbitrary <br> values |
| Distance in x-direction from the center of one <br> DMD-pixel to the next | PixeIPitchX | $8 \mu \mathrm{~m}$ |
| Distance in y-direction from the center of one <br> DMD-pixel to the next | PixelPitchY | $12 \mu \mathrm{~m}$ |
| Active size of DMD-pixel in x-direction | ActivePixelAreaX | $7 \mu \mathrm{~m}$ |
| Active size of DMD-pixel in y-direction | ActivePixelAreaY | $11 \mu \mathrm{~m}$ |
| Shift of the whole DMD-field in x-direction | ShiftX | 50 nm |
| Shift of the whole DMD-field in y-direction | ShiftY | 50 nm |

Fig. 804 shows the resulting field distribution of an example DMD simulation.


Figure 804. Example of a small DMD simulation

This boundary response works best if the parameters PixelPitchX, PixeIPitchY, ActivePixelAreaX and ActivePixelAreaY are an integer multiple of the sampling distance of the incoming field. And for the parameter ShiftX and ShiftY a good choice is the negligible value of half of the sampling distance if an unshifted result is desired. In order to ensure a suitable sampling distance it is recommended to use the component "Field Size and Sampling" within the Optical Setup.

## A. 2 Components Catalog

## A.2.1 LightTrans Defined: Set Spherical Phase Radius

This programmable component allows you to set the Spherical Phase Radius ( $\hookrightarrow$ Sec. 12.1.1). If the Global Parameter DetectSphericalPhaseRadius is set to 1, the spherical phase radius is determined automatically. Otherwise it is set to the SphericalPhaseRadius set by the user.

## A.2.2 LightTrans Defined: Mirror Field in x/y Plane

This component does a mirror operation along the field's $x$ - or $y$-axis as described in Sec. 22.6. So it does not have to be confused with a component that represents a plane mirror. The operation is only a horizontal or vertical mirroring of the lateral field values but does not change the direction of propagation!
The value of the Global Parameter mirror_horizontally determines whether to mirror in horizontal or vertical direction. If its value equals zero, the mirror operation is done horizontally ( $x_{\min } \leftrightarrow x_{\max }$ ), otherwise the operation is a vertical one ( $y_{\min } \leftrightarrow y_{\max }$ ).


Figure 805. Example for the effect of the Mirror x/y Component. The parameter was: mirror_horizontally $=1$.

## A.2.3 LightTrans Defined: Rotate and Shift Field in $x-y$-Plane

This component does a rotation in the $x$-y-plane (i.e. about the $z$ axis) by an arbitrary angle ( $\hookrightarrow$ Sec. 22.6.1) as well as a lateral shift by a vector $\left(d_{x}, d_{y}\right)$.
The rotation angle is determined by the Global Parameter RotationAngle_Zeta, while the lateral shift is given by the parameters ShiftX and ShiftY. The Global Parameter EmbeddingFactor determines a factor by which the field data are embedded into a larger coordinate range in order to avoid that rotation or shift yield to a result outside the field boundaries.


Figure 806. Example for the effect of the Rotate and Shift Component. The parameters were: RotationAngle_Zeta $=45^{\circ}$; (ShiftX, ShiftY) $=30 \mathrm{~mm},-30 \mathrm{~mm}$; EmbeddingFactor $=2$.

## A.2.4 LightTrans Defined: Radial Birefringent Element

This component represents a birefringent element where the thickness and thus the phase shift depends on the radius $r$. Therefore the following Jones matrix $\mathcal{J}$ is applied on the InputField:

$$
\mathcal{J}=\left(\begin{array}{cc}
1 & 0  \tag{A.3}\\
0 & \exp \left(i\left(\delta_{2}(r)-\delta_{1}(r)\right)\right)
\end{array}\right)
$$

with the phase shift

$$
\begin{equation*}
\delta_{i}(r)=\frac{2 \pi}{\lambda} n_{i}\left(d+\frac{r^{2}}{2 R}\right), \quad i=1,2 \tag{A.4}
\end{equation*}
$$

and

$$
\begin{equation*}
r=\sqrt{x^{2}+y^{2}} \tag{A.5}
\end{equation*}
$$

$R$ is the RadiusOfCurvature and $d$ is the CenterThickness of the element. $n_{1}$ and $n_{2}$ are the refractive indices along the crystal axes.
This formula is taken from [HW97].

## A.2.5 LightTrans Defined: Azimuthal Birefringent Element

This component represents a birefringent element where the refractive indices differ for radially and azimuthally polarized light. This can be described by the following Jones matrix $\mathcal{J}$ :

$$
\mathcal{J}=\left(\begin{array}{cc}
e^{i \delta} \cos ^{2} \theta+\sin ^{2} \theta & \left(e^{i \delta}-1\right) \cos \theta \sin \theta  \tag{A.6}\\
\left(e^{i \delta}-1\right) \cos \theta \sin \theta & e^{i \delta} \sin ^{2} \theta+\cos ^{2} \theta
\end{array}\right)
$$

with the phase shift

$$
\begin{equation*}
\delta_{i}(r)=\frac{2 \pi}{\lambda}\left(n_{r}-n_{\theta}\right) l \tag{A.7}
\end{equation*}
$$

and

$$
\begin{equation*}
r=\sqrt{x^{2}+y^{2}} ; \quad \theta=\arctan \frac{y}{x} \tag{A.8}
\end{equation*}
$$

$l$ is the Length of the element. $n_{r}$ is the refractive index for radially polarized light and $n_{\theta}$ is the refractive index for azimuthally polarized light.
This formula is taken from [HW97].

## A. 3 Surfaces Catalog

## A.3.1 LightTrans Defined: Axicon Surfaces

In the surface catalog axicon surfaces are available. These surfaces are programmable surfaces with a special snippet. For a given lateral position $(x, y)$ this snippet defines the height $h(x, y)$ of an axicon surface with a given angle Angle using the following formula:

$$
\begin{equation*}
h(x, y)=-\left(r_{\max }-r\right) \cdot \tan \text { Angle } \tag{A.9}
\end{equation*}
$$

The minus sign indicates that the apex is orientated in negative z-direction, i. e. towards the light source. If you enter a negative angle the apex is orientated in positive z-direction.
$r_{\text {max }}$ is the maximum of ApertureDiameterX and ApertureDiameterY, i. e. the largest diameter of the current definition area. The radius $r$ is calculated as $r=\sqrt{x^{2}+y^{2}}$. The parameter Angle is a global parameter and can be varied by the parameter run document.

## A. 4 Materials Catalog

## A.4.1 Template: Abbe Number $v_{\mathrm{d}}$ Material

This material calculates the dispersion $n(\lambda)$ from the Abbe number $v_{\mathrm{d}}$ and the refractive index $n_{\mathrm{d}}$.

$$
\begin{equation*}
v_{\mathrm{d}}=\frac{n_{\mathrm{d}}-1}{n_{\mathrm{F}}-n_{\mathrm{C}}} \tag{A.10}
\end{equation*}
$$

$n_{F}$ is the refractive index at the Fraunhofer line $F\left(\lambda_{F}=486.134 \mathrm{~nm}\right), n_{d}$ is the refractive index at the Fraunhofer line $d\left(\lambda_{d}=587.5618 \mathrm{~nm}\right)$ and $n_{C}$ is the refractive index at the Fraunhofer line $C\left(\lambda_{C}=656.281 \mathrm{~nm}\right)$.
This material uses the reduced Cauchy formula

$$
\begin{equation*}
n(\lambda)=A+\frac{B}{\lambda^{2}} \tag{A.11}
\end{equation*}
$$

to calculate the actual dispersion with

$$
\begin{align*}
& B=\frac{n_{\mathrm{d}}-1}{v_{\mathrm{d}}\left(\lambda_{\mathrm{F}}^{-2}-\lambda_{\mathrm{C}}^{-2}\right)}  \tag{A.12}\\
& A=n_{\mathrm{d}}-\frac{B}{\lambda_{\mathrm{d}}^{2}} \tag{A.13}
\end{align*}
$$

## A.4.2 Template: Fused_Silica

This template is identical to that Fused_Silica material which can be found in the LightTrans Defined Catalog "Miscellaneous". It can be used as a base for defining other materials which use a dispersion formula like Sellmeier, Herzberger and so on.

## A.4.3 Template: Sampled $n$ - $\alpha$-Data Material

This is a template for defining the optical data in form of sampled values for the real refractive index $n$ and the absorption coefficient $\alpha$. These data can be set via loading from a text file or via entering single data pairs for $\lambda$ and $n$ or for $\lambda$ and $\alpha$ resp.

## A.4.4 Template: Vacuum

This template represents vacuum and can be used to define other materials with a constant refractive index or constant absorption coefficient.

## A.4.5 Sources for the Optical Material's Data in the LightTrans Defined Catalog

The information for the glass catalogs CDGM, Corning, Dow, Heraeus, Hikari, Hoya, Isuzu, LZOS, NHG, Ohara, Schott, Sumita, and Tecnottica were given by the manufacturers. The sources of the materials in the remaining categories are listed below.

## A.4.5.1 Carbon+Compounds

MATERIAL
DATA SOURCE

| Acrylic | $[B S 94]$ |
| :--- | :--- |
| Carbon(amorphous)-a-C_(1975) | $[H G K 74],[H G K 75]$ |
| Carbon(amorphous)-a-C_(1991+1988) | Concatenation of Carbon(sputtered)-a-C_(1991) |
|  | $[13.3 \AA-304 \AA$ and Carbon(amorphous_evap_thin- |
|  | Film)-a-C_(1988) [327 $\AA-1216 \AA]$ |


| Carbon(amorphous)-a-C_(1997+1988+1991) | Concatenation of Carbon(amorphous)-a-C_2.2gcm3_(1997) [0.124 $\AA-413 \AA]$ and Carbon(amor-phous_evap_thinFilm)-a-C_(1988) [448 Å-1216 Å] and Carbon(evap_thinFilm)-a-C_(1991) [1240 Å-10663 A] |
| :---: | :---: |
| Carbon(amorphous)-a-C_2.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Carbon(amorphous_evap_thinFilm)-a- C_(1988) | [Win+88a] |
| Carbon(diamond)-C_(1997+1985) | Concatenation of Carbon(diamond)-C_3.51gcm3_(1997) [0.124 $\AA-413 \AA$ ] and Carbon(diamond_cu-bic)-C_(1985) [413 A - $6563 \AA$ A ] |
| Carbon(diamond)-C_3.51gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Carbon(diamond_cubic)-C_(1985) | [Pal85] |
| Carbon(diamond_thinFilm)-C_(1988) | [Win+88a] |
| Carbon(evap_thinFilm)-a-C_(1991) | [Pal91] |
| Carbon(graphit)-g-C_2.25gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Carbon(sputtered)-a-C_(1991) | [Win91] |
| COC-(Celanese) | Celanese Spec Sheet |
| Mylar-(C1004H8)n_1.38gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| PMMA-(C5O2H8)n_1.19gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Polycarbonate | [BS94] |
| PolyMethyIMethAcrylate-PMMA | [BS94] |
| Polypropylene-C3H6_0.9gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Polystyrene | [BS94] |
| Saran-(CH2=CCl2)n_1.2129gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| StyreneAcryloNitrile-SAN | [BS94] |
| TOPAS-COC_5013L-10 | Topas Spec Sheet |
| TOPAS-COC_6013L-17 | Topas Spec Sheet |

## A.4.5.2 Coating_Materials

These material's data have been measured using thin film specimen. The data sources are listed in the category which represents the composition of the material respectively (e.g. in Metals+Compounds or in Silicon+Com-pounds_(Non-Glass)).

WARNING: As well-known from thin film physics (see e.g. Handbook of Optical Constants of Solids Vol. II, p. 71), the optical constants of thin layers not only differ from that of bulk material, but depend strongly on the technique of their fabrication. So please use the data provided by VirtualLab Fusion only for an orientation! The best way to get the optical properties of a specific layer is measurement on it.

## A.4.5.3 Infrared

Each Infrared material is contained in one of the other categories at least. So the data sources for the nonglasses are listed in that category which represents the composition of the material respectively (e.g. in Metals+Compounds or in Silicon+Compounds_(Non-Glass)).

## A.4.5.4 Metals+Compounds

| MATERIAL | DATA SOURCE |
| :---: | :---: |
| Actinium-Ac_10.07gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Aluminium_antimonide(cubic)-AISb_(1991) | [Pal91] |
| Aluminium_arsenide(cubic)-AIAs_(1991) | [Pal91] |
| Aluminium_gallium_arsenide(cu-bic)-Al0.3Ga0.7As_(1991) | [Pal91] |
| Aluminium_oxide(amorphous)-a- Al2O3_(1975) | [HGK74], [HGK75] |
| Aluminium_oxide(amorphous)-a- Al2O3_(1997+1991) | Concatenation of phous)-a-Al2O3_(1997) [0.124 $\AA-413 \AA$ _ $]$ and Alu- minium_oxide(amorphous/polyxtal)-a-Al2O3_(1991) $[413 \AA$-249960 $\AA]$ |
| Aluminium_oxide(amorphous)-a-Al2O3_3.965gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Aluminium_oxide(amorphous/polyxtal)-a- Al2O3_(1991) | [Pal91] |
| Aluminium_oxide(trigonal_extraordi-naryRay)-Al2O3-e_(1991) | [Pal91] |
| Aluminium_oxide(trigonal_ordi-naryRay)-Al2O3-o_(1991) | [Pal91] |
| Aluminium_Oxide-Al2O3-ThinFilm | [ESA93] |
| Aluminium_oxynitride-ALON | [BS94] |
| Aluminium-Al_(1980) | [Shi+80] |
| Aluminium-AI_(1985) | [Pal85] |
| Aluminium-AI_(1988) | [Win+88a] |
| Aluminum-AI_(1994) | [BS94] |
| Aluminium-AI_(1997+1985) | Concatenation of Aluminium-Al_2.699gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Aluminium-Al_(1985) <br> $[413 \AA-12398 \AA]$   |
| Aluminium-Al_2.699gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Aluminum_nitride-AIN | [BS94] |
| Aluminum-Al-ThinFilm | [Pal85] |
| Barium_fluoride-BaF2 | [BS94] |


| Barium_titanate(tetragonal_extraordi-naryRay)-BaTiO3-e_(1991) | [Pal91] |
| :---: | :---: |
| Barium_titanate(tetragonal_ordi-naryRay)-BaTiO3-o_(1991) | [Pal91] |
| Beryllium(polyxtal)-Be_(1991) | [Pal91] |
| Beryllium_oxide(ceramic)-BeO_(1991) | [Pal91] |
| Beryllium_oxide(ordinaryRay)-BeO | [BS94] |
| Beryllium_oxide-BeO_3.02gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Beryllium-Be_(1997+1991) | Concatenation of Beryllium-Be_1.848gcm-3_(1997) [0.124 $\AA-413 \AA$ ] and Beryllium(polyxtal)-Be_(1991) [413 Å-619900 Å] |
| Beryllium-Be_1.848ggm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cadmium_selenide(ordinaryRay)-CdSe | [BS94] |
| Cadmium_sulfide-CdS_(1994) | [BS94] |
| Cadmium_Sulphide-CdS-ThinFilm | [Pal91, p. 595] |
| Cadmium_telluride-CdTe | [BS94] |
| Caesium_iodide(cubic)-CsI_(1991) | [Pal91] |
| Caesium_iodide-Csl_6.68gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Calcite(ordinaryRay)-CaCO3 | [BS94] |
| Calcium_fluoride(cubic)-CaF2_(1991) | [Pal91] |
| Calcium_fluoride-CaF2_(1994) | [BS94] |
| Calcium_fluoride-CaF2_(1997+1991) | Concatenation of Calcium_fluoride- CaF2_3.18gcm-3_(1997) $[0.124 \AA-413 \AA]$ and Cal- cium_fluoride(cubic)-CaF2_(1991) $[500 \AA-5793458 \AA]$ |
| Calcium_fluoride-CaF2_3.18gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cerium_Fluoride-CeF3-ThinFilm | [SB79] |
| Cerium_Oxide-CeO2-ThinFilm | [SB79] |
| Cesium_bromide-CsBr | [BS94] |
| $\begin{aligned} & \text { Chromium(III)_oxide- } \\ & \text { Cr2O3_5.21gcm-3_(1997) } \end{aligned}$ | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Chromium(poyxtal)-Cr_(1991) | [Pa191] |
| Chromium_carbide(sputtered)-Cr3C2_(1991) | [Win91] |
| Chromium_carbide-Cr3C2_(1997+1991) | Concatenation of  <br> Chromium_carbide-   <br> Cr3C2_6.68gcm-3_(1997) $[0.124 \AA-413 \AA]$ and <br> Chromium_carbide(sputtered)-Cr3C2_(1991)   <br> $[430 \AA-1302 \AA]$   |
| Chromium_carbide-Cr3C2_6.68gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Chromium-Cr_(1994) | [BS94] |


| Chromium-Cr_(1997+1991) | Concatenation of Chromium-Cr_7.2gcm-3_(1997) [0.124 Å-413 A] and Chromium(poyxtal)-Cr_(1991) [421 Å-309950 Å] |
| :---: | :---: |
| Chromium-Cr_7.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| CLEARTRAN-ZnS | Spec Sheet (Rohm and Haas) |
| CLEARTRAN-ZnS_old | Spec Sheet (Morton International) |
| Cobalt(hcp_bulk+polyxtalThin-Film)-Co_(1991) | [Pal91] |
| Cobalt(II)_oxide-CoO_6.45gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cobalt(II,III)_oxide-Co3O4_6.07gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cobalt(III)_oxide-Co2O3_5.18gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cobalt_silicide-CoSi2_5.3gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Cobalt-Co_(1997+1991) | Concatenation of Cobalt-Co_8.9gcm-3_(1997) <br> $[0.124 \AA-413 \AA]$ and Cobalt(hcp_bulk+polyxtalTh- <br> inFilm)-Co_(1991) $[500 \AA-169999 \AA]$  |
| Cobalt-Co_8.9gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Copper(I)_oxide-Cu2O_(1991) | [Pal91] |
| Copper(I)_oxide-Cu2O_6.0gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Copper(II)_oxide(polyxtal)-CuO_(1991) | [Pal91] |
| Copper(II)_oxide-CuO_6.4gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Copper_silicide-Cu4Si_7.53gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Copper-Cu_(1985) | [Pal85] |
| Copper-Cu_(1994) | [BS94] |
| Copper-Cu_(1997+1985) | Concatenation of Copper-Cu_8.92gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Copper-Cu_(1985) <br> $[413 \AA-95368 \AA]$   |
| Copper-Cu_8.92gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Gallium_antimonide-GaSb_(1991) | [Pal91] |
| Gallium_antimonide-GaSb_5.612gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Gallium_arsenide(singleXtal)-GaAs_(1991) | [Win91] |
| Gallium_arsenide-GaAs | [BS94] |
| Gallium_arsenide-GaAs_(1985) | [Pal85] |
| Gallium_arsenide-GaAs_(1997+1991+1985) | Concatenation of GaAs_5.3gcm-3_(1997) Gallium_arsenide(singleXtal)-GaAs_(1991) [0.124 $\AA-413 \AA$ arsenide- [430 $\AA-1302 \AA$ and $[1378 \AA-9998390 \AA \AA]$ |
| Gallium_arsenide-GaAs_5.3gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Gallium_phosphide-GaP_(1985) | [Pal85] |


| Gallium_phosphide-GaP_(1997+1985) | Concatenation of $\quad$ Gallium_phosphide- GaP_4.129gcm-3_(1997) $[0.124 \AA-413 \AA$ and Gal- lium_phosphide-GaP_(1985) [775 $\AA-9998390 \AA]$ |
| :---: | :---: |
| Gallium_phosphide-GaP_4.129gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Gold(evap_thinFilm)-Au_(1988) | [Win+88b] |
| Gold(polyxtal)-Au_(1985) | [Pal85] |
| Gold-Au_(1964) | [CHH64] |
| Gold-Au_(1970+1980) | [Nil70], [ZAT80] |
| Gold-Au_(1975) | [HGK74], [HGK75] |
| Gold-Au_(1981) | [Wea+81] |
| Gold-Au_(1994) | [BS94] |
| Gold-Au_(1997+1985) | $\begin{aligned} & \text { Concatenation of } \begin{array}{l} \text { Gold-Au_19.32gcm-3_(1997) } \\ {[0.124 \AA-413 \AA]} \\ {[413 \AA-99184 \AA \AA]} \end{array} r \quad \text { and } \\ & \hline \end{aligned}$ |
| Gold-Au_19.32gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Hafnium(evap_thinFilm)-Hf_(1988) | [Win+88b] |
| Hafnium(IV)_oxide-HfO2_9.68gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Hafnium(singleXtal_TE)-Hf-te_(1981) | [Wea+81, p. 253] |
| Hafnium(singleXtal_TM)-Hf-tm_(1981) | [Wea+81, p. 253] |
| Hafnium_Dioxide-HfO2-ThinFilm | [BLP82] |
| Hafnium-Hf_(1997+1988) |  |
| Hafnium-Hf_13.31gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Indium_antimonide-InSb_(1985) | [Pal85] |
| Indium_arsenide-InAs_(1985) | [Pal85] |
| Indium_phosphide-InP_(1985) | [Pal85] |
| Iridium(evap_thinFilm)-Ir_(1988) | [Win+88b] |
| Iridium-Ir_(1985) | [Pal85] |
| Iridium-Ir_(1997+1985) | Concatenation of Iridium-Ir_22.421gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Iridium-Ir_(1985) <br> $[413 \AA-123980 \AA]$   |
| Iridium-Ir_22.421gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Iron(II)_oxide-FeO_5.7gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Iron(II,III)_oxide-Fe3O4_5.18gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Iron(III)_oxide-Fe2O3_5.24gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Iron-Fe_(1991) | [Pal91] |
| Iron-Fe_(1994) | [BS94] |


| Iron-Fe_(1997+1991) | Concatenation of Iron-Fe_7.86gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Iron-Fe_(1991) <br> $[477 \AA-2857340 \AA]$   |
| :---: | :---: |
| Iron-Fe_7.86gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| KRS-5 | [BS94] |
| Lanthanum_Fluoride-LaF3-ThinFilm | [SB79] |
| Lanthanum_Oxide-La2O3-ThinFilm | [SB79] |
| Lanthanum_trifluoride-LaF3_(1994) | [BS94] |
| Lead(II)_fluoride-PbF2 | [BS94] |
| Lead(II)_selenide-PbSe_(1985) | [Pal85] |
| Lead(II)_sulfide(cubic)-PbS_(1985) | [Pal85] |
| Lead_Fluoride-PbF2-ThinFilm | [Pal97, pp. 771-773] |
| Lead_telluride(cubic)-PbTe_(1985) | [Pal85] |
| Lithium_fluoride-LiF | [BS94] |
| Lithium_fluoride-LiF_(1991) | [Pal91] |
| Lithium_niobate(extraordinaryRay)-LiNbO3e_(1985) | [Pal85] |
| Lithium_niobate(ordinaryRay)-LiNbO3o_(1985) | [Pal85] |
| Lithium-Li_(1991) | [Pal91] |
| Magnesium_fluoride(extraordinaryRay)-MgF2 | [BS94] |
| Magnesium_fluoride(extraordinaryRay)-Mg- e_(1991) | [Pal91] |
| Magnesium_fluoride(ordinaryRay)-MgF2 | [BS94] |
| Magnesium_fluoride(ordinaryRay)-Mg- o_(1991) | [Pal91] |
| Magnesium_Fluoride-MgF2-ThinFilm | [BLP82] |
| Magnesium_oxide-MgO | [BS94] |
| Magnesium_oxide-MgO_(1991) | [Pal91] |
| Magnesium_oxide-MgO_(1997+1991) | Concatenation of $\quad$ Magnesium_oxide- MgO_3.58gcm-3_(1997) $[0.124 \AA-413 \AA$ A $]$ and Magne- sium_oxide-MgO_(1991) [413 $\AA-6261620 \AA]$ |
| Magnesium_oxide-MgO_3.58gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Magnesium-Mg_1.74gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Manganese(II,III)_oxide-Mn3O4_4.856gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Manganese(IV)_oxide-MnO2_5.026gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Manganese-Mn_7.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Mercury_telluride-HgTe_(1991) | [Pal91] |


| Mercury-Hg_(1991) | [Pal91] |
| :---: | :---: |
| Mercury-Hg_(1997+1991) | $\begin{aligned} & \text { Concatenation of } \\ & \begin{array}{l} \text { Mercury }-\mathrm{Hg} \_13.5939 \mathrm{gcm}-3 \_(1997) \\ {[0.124 \AA-413 \AA]} \\ {[636 \AA-61990 \AA]} \end{array} \\ & \hline \end{aligned}$ |
| Mercury-Hg_13.5939gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum(evap_thinFilm)-Mo_(1988) | [Win+88b] |
| Molybdenum(IV)_oxide-MoO2_6.47gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum(sputtered)-Mo_(1991) | [Win91] |
| Molybdenum(sputtered)-Mo_(1992) <br> Molybdenum_dicarbide- <br> Mo2C_8.9gcm-3_(1997) | $\begin{aligned} & \diamond(\hookrightarrow \text { Sec. A.4.5.9) } \\ & \bowtie(\hookrightarrow \text { Sec. A.4.5.9 }) \end{aligned}$ |
| Molybdenum_disilicide-MoSi2_(1992) | $\diamond$ ( $\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum_disilicide-MoSi2_6.31gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum_disulfide-MoS2_4.8gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum_monocarbide-MoC_8.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum_trioxide-MoO3_4.692gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Molybdenum-Mo_(1985) | [Pal85] |
| Molybdenum-Mo_(1997+1985) | $\begin{aligned} & \text { Concatenation of Molybdenum-Mo_10.2gcm-3_(1997) } \\ & {[0.124 \AA-413 \AA] \quad \text { and } \quad \text { Molybdenum-Mo_(1985) }} \\ & {[413 \AA-123980 \AA]} \end{aligned}$ |
| Molybdenum-Mo_10.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Neodymium_Fluoride-NdF3-ThinFilm | [SB79] |
| Nickel(II)_oxide-NiO_6.67gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Nickel-Ni_(1985) | [Pal85] |
| Nickel-Ni_(1997+1985) | Concatenation of Nickel-Ni_8.9gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Nickel-Ni_(1985) <br> $[413 \AA-123980 \AA]$   |
| Nickel-Ni_8.9gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Niobium(evap_thinFilm)-Nb_(1988) | [Win+88b] |
| Niobium(II)_oxide-NbO_7.3gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Niobium(IV)_oxide-NbO2_5.9gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Niobium(V)_oxide-Nb2O5_4.47gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Niobium-Nb_(1981) | [Wea+81] |
| Niobium-Nb_(1991) | [Pal91] |


| Niobium-Nb_(1997+1991) | Concatenation of $\begin{aligned} & {[0.124 \AA-413 \AA]} \\ & {[413 \AA-103317 \AA]} \end{aligned}$ | Niobium-Nb_8.57gcm-3_(1997) <br> and Niobium-Nb_(1991) |
| :---: | :---: | :---: |
| Niobium-Nb_8.57 gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Osmium(evap_thinFilm)-Os_(1988) | [Win+88b] |  |
| Osmium_dioxide-OsO2_11.37gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Osmium-Os_(1981) | [Wea+81, p. 253] |  |
| Osmium-Os_(1985) | [Pal85] |  |
| Osmium-Os_(1997+1988+1985) | Concatenation of $\begin{aligned} & {[0.124 \AA-413 \AA]} \\ & \text { Film)-Os_(1988) } \\ & \text { Os_(1985) }[1250 \AA- \end{aligned}$ | Osmium-Os_22.48gcm-3_(1997) and Osmium(evap_thin$448 \AA-1216 \AA$ A and Osmium2000 Å] |
| Osmium-Os_22.48gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Palladium(evap_thinFilm)_(1988) | [Win+88b] |  |
| Palladium(II)_oxide-PdO_8.70gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Palladium-Pd_(1981) | [Wea+81] |  |
| Palladium-Pd_(1991) | [Pal91] |  |
| Palladium-Pd_(1997+1991) | Concatenation of $\begin{aligned} & {[0.124 \AA-413 \AA]} \\ & {[448 \AA-123980 \AA]} \end{aligned}$ | $\begin{aligned} & \text { Palladium-Pd_12.02gcm-3_(1997) } \\ & \text { and Palladium-Pd_(1991) } \end{aligned}$ |
| Palladium-Pd_12.02gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Platinum(evap_thinFilm)-Pt_(1988) | [Win+88b] |  |
| Platinum(II)_oxide-PtO_14.9gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Platinum(IV)_oxide-PtO2_10.2gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Platinum-Pt_(1981) | [Wea+81] |  |
| Platinum-Pt_(1985) | [Pal85] |  |
| Platinum-Pt_(1997+1985) | Concatenation of $\begin{aligned} & {[0.124 \AA-413 \AA]} \\ & {[420 \AA-123980 \AA]} \end{aligned}$ | $\begin{aligned} & \text { Platinum-Pt_21.45gcm-3_(1997) } \\ & \text { and } \\ & \text { Platinum-Pt_(1985) } \end{aligned}$ |
| Platinum-Pt_21.45gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Potassium(polyxtal)-K_(1991) | [Pal91] |  |
| Potassium_bromide(cubic)-KBr_(1991) | [Pal91] |  |
| Potassium_chloride-KCI_(1985) | [Pal85] |  |
| Rhenium(evap_thinFilm)-Re_(1988) | [Win+88b] |  |
| Rhenium(IV)_oxide-ReO2_11.4gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| Rhenium(singleXtal_TE)-Re-te_(1981) | [Wea+81, p. 253] |  |
| Rhenium(singleXtal_TM)-Re-tm_(1981) | [Wea+81, p. 253] |  |
| Rhenium(VI)_oxide-ReO3_7.0gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |
| $\begin{aligned} & \text { Rhenium(VII)_oxide- } \\ & \text { Re2O7_6.103gcm-3_(1997) } \end{aligned}$ | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |  |


| Rhenium-Re_(1997+1988) | Concatenation of <br> Rhenium-Re_20.53gcm-3_(1997) <br> Rhenium(evap_thin- <br> and |
| :--- | :--- | :--- |
|  | $[0.124 \AA-413 \AA]$ |
|  | Film)-Re_(1988) [448 A-1216A] |


| Sodium_chloride-NaCI | [Rog93] |
| :---: | :---: |
| Sodium_chloride-NaCl_(1985) | [Pal85] |
| Sodium_fluoride-NaF_(1991) | [Pal91] |
| Sodium_Fluoride-NaF-ThinFilm | [Pal91, pp. 1028-1031] |
| Sodium-Na_(1991) | [Pal91] |
| Spinel-MgAl2O4 | [BS94] |
| Strontium_fluoride-SrF2 | [BS94] |
| Strontium_titanate-SrTiO3 | [BS94] |
| Strontium_titanate-SrTiO3_(1991) | [Pa191] |
| Ta2O5-ThinFilm_MSO-measured | [Jen10] |
| Tantalum(evap_thinFilm)-Ta_(1988) | [Win+88b] |
| Tantalum_carbide-TaC_13.9gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Tantalum_nitride-TaN_16.3gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Tantalum_pentoxide-Ta2O5_8.2gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Tantalum_Pentoxide-Ta205-ThinFilm | [SB79] |
| Tantalum-Ta_(1981) | [Wea+81] |
| Tantalum-Ta_(1991) | [Pal91] |
| Tantalum-Ta_(1997+1991) | Concatenation of Tantalum-Ta_16.6gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Tantalum-Ta_(1991) <br> $[413 \AA-1249920 \AA]$   |
| Tantalum-Ta_16.6gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Thorium(IV)_fluoride(polyxtal)-ThF4_(1991) | [Pal91] |
| Thorium_Fluoride-ThF4-BulkMaterial | [Pa191, pp. 1056-1057] |
| Thorium_Fluoride-ThF4-ThinFilm | [Pa191, pp. 1056-1057] |
| Tin(II)_oxide-SnO_6.446gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Tin(IV)_oxide-SnO2_6.95gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Tin_telluride-SnTe_(1991) | [Pal91] |
| Tin-Sn_7.28gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Titanium(evap_thinFilm)-Ti_(1988) | [Win+88b] |
| Titanium(IV)_oxide(tetragonal_extraordi-naryRay)-TiO2-e_(1985) | [Pal85] |
| Titanium(IV)_oxide(tetragonal_ordi-naryRay)-TiO2-o_(1985) | [Pal85] |
| Titanium(IV)_oxide-TiO2_4.26gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Titanium(sputtered_thinFilm)-Ti_(1989) | [Kih+89] |
| Titanium_carbide(polyxtal)-TiC_(1991) | [Pal91] |
| Titanium_carbide-TiC_(1997+1991) | Concatenation of Titanium_carbide- <br> TiC_4.93gcm-3_(1997) $[0.124 \AA-413 \AA]$ and Tita-  <br> nium_carbide(polyxtal)-TiC_(1991) $[413 \AA-24796 \AA]$   |


| Titanium_carbide-TiC_4.93gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| :---: | :---: |
| Titanium_Dioxide-TiO2-ThinFilm | [BLP82] |
| Titanium_nitride-TiN_(1991) | [Pal91] |
| Titanium_nitride-TiN_(1997+1991) | Concatenation of Titanium_nitride-  <br> TiN_5.22gcm-3_(1997) $[0.124 \AA-413 \AA]$ and Tita-   <br> nium_nitride-TiN_(1991) $[413 \AA-24796 \AA]$   |
| Titanium_nitride-TiN_5.22gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Titanium-Ti_(1981) | [Wea+81] |
| Titanium-Ti_(1997+1988) | Concatenation of $\quad$ Titanium-Ti_4.5gcm-3_(1997)   <br> $[0.124 \AA-413 \AA]$ and Titanium(evap_thin- <br> Film)-Ti_(1988) $[448 \AA-1216 \AA]$   |
| Titanium-Ti_4.5gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Tungsten(evap_thinFilm)-W_(1988) | [Win+88b] |
| Tungsten(IV)_oxide-WO2_12.11gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Tungsten(polyxtal)-W_(1985) | [Pal85] |
| Tungsten(sputtered)-W_(1991) | [Win91] |
| Tungsten(VI)_oxide-WO3_7.16gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Tungsten_disilicide-WSi2_9.3gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Tungsten-W_(1981) | [Wea+81] |
| Tungsten-W_(1997+1985) | Concatenation of Tungsten-W_19.35gcm-3_(1997) [0.124 $\AA-413 \AA$ ] and Tungsten(polyxtal)-W_(1985) [413 Å-247960 Å] |
| Tungsten-W_19.35gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium(II)_oxide-VO_5.758gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium(III)_nitride-VN_(1991) | [Pal91] |
| Vanadium(III)_nitride-VN_(1997+1991) | Concatenation of $\quad$ Vanadium(III)_nitride- VN_6.13gcm-3_(1997) $[0.124 \AA-413 \AA]$ and Vana- dium(III)_nitride-VN_(1991)[413 $\AA-24796 \AA]$ |
| Vanadium(III)_nitride-VN_6.13gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Vanadium(III)_oxide_4.87gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium(IV)_oxide-VO2_4.339gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium(sputtered_thinFilm)-V_(1989) | [Kih+89] |
| $\begin{aligned} & \text { Vanadium(V)_oxide- } \\ & \text { V2O5_3.357gcm-3_(1997) } \end{aligned}$ | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium_carbide-VC_(1991) | [Pal91] |
| Vanadium_carbide-VC_(1997+1991) | Concatenation VC_5.77gcm-3_(1997) [0.124 $\AA-413 \AA]$ and Vana- dium_carbide-VC_(1991) $[428 \AA-24796 \AA]$ |
| Vanadium_carbide-VC_5.77gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Vanadium-V_(1981) | [Wea+81] |


| Vanadium-V_(1991) | [Pal91] |
| :---: | :---: |
| Vanadium-V_(1997+1991) | Concatenation of Vanadium-V_5.96gcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Vanadium-V_(1991) <br> $[413 \AA-123980 \AA]$   |
| Vanadium-V_5.96gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Yttrium(III)_oxide(cubic)-Y2O3_(1991) | [Pal91] |
| Yttrium(III)_oxide-Y2O3_(1997+1991) | Concatenation $\quad$ of Yttrium(III)_oxide- <br> Y2O3_5.01gcm-3_(1997) $[0.124 \AA-413 \AA]$ <br> and $\quad$ Yttrium(III)_oxide(cubic)-Y2O3_(1991)  <br> $[413 \AA-1.999 E 7 \AA]$  |
| Yttrium(III)_oxide-Y2O3_5.01gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Yttrium(sputtered)-Y_(1992) | $\diamond(\hookrightarrow$ Sec. A.4.5.9) |
| Yttrium_Oxide-Y2O3-ThinFilm | [SB79] |
| Yttrium-Y_4.4689gcm-3_(1997) ZBLA | $\begin{aligned} & \bowtie(\hookrightarrow \text { Sec. A.4.5.9) } \\ & {[B S 94]} \end{aligned}$ |
| ZBLAN | [BS94] |
| Zinc_oxide-ZnO_5.606gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Zinc_selenide(cubic)-ZnSe_(1991) | [Pal91] |
| Zinc_selenide(irtran-4)-ZnSe_(1991) | [Pal91] |
| Zinc_selenide-ZnSe | [BS94] |
| Zinc_sulfide(cubic)-ZnS_(1991) | [Pal91] |
| Zinc_sulfide(hexagonal_extraordi-naryRay)-ZnS-e_(1985) | [Pal85] |
| Zinc_sulfide(hexagonal_ordinaryRay)-ZnSo_(1985) | [Pal85] |
| Zinc_sulfide(irtran-2)-ZnS_(1985) | [Pal85] |
| Zinc_sulfide-ZnS_0.42-1.1 $\mu \mathrm{m}$ | [Rog93] |
| Zinc_sulfide-ZnS_0.42-18.2 $\mu \mathrm{m}$ | [Rog93] |
| Zinc_sulfide-ZnS_4-18 $\mu \mathrm{m}$ | [Rog93] |
| Zinc_Sulfide-ZnS-ThinFilm | [BLP82] The curve in Fig. 1 of the publication was used to sample the dispersion. |
| Zinc_telluride(cubic)-ZnTe_(1991) | [Pal91] |
| Zinc-Zn_7.14gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Zirconium(evap_thinFilm)-Zr_(1988) | [Win+88b] |
| Zirconium(IV)_oxide-ZrO2_5.89gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Zirconium(polyxtal)-Zr_(1981) | [Wea+81, p. 253] |
| Zirconium(singleXtal_TE)-Zr-te_(1981) | [Wea+81, p. 253] |
| Zirconium_Dioxide-ZrO2-ThinFilm | [SB79] |


| Zirconium-Zr_(1997+1988) | Concatenation of <br>  <br>  <br>  <br> $[0.124 \AA-413 \AA]$$\quad$ Zirconium-Zr_6.49gcm-3_(1997) |
| :--- | :--- | :--- |
|  | Film)-Zr_(1988) $[448 \AA-1216 \AA]$ |
| Zirconium-Zr_6.49gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |

## A.4.5.5 Miscellaneous

| MATERIAL | DATA SOURCE |
| :---: | :---: |
| Acrylic | [BS94] |
| Air | [BD94]; air without any water vapor (humidity $0 \%$ ). |
| Air (X-ray spectral region) | Calculated from $\tilde{n}^{2}=\sum_{i}\left(V_{i} / V \cdot \tilde{\epsilon}_{i}\right)$ with $V_{i} / V$ being the volume fraction of the $i$ th gas compound of air. These percentage values are taken from [Lid08]. $\tilde{\epsilon}_{i}$ is the dielectric function of compound $i$ as could be found at the source called CXRO, as described in Sec. A.4.5.9. |
| Air (Zemax OS) | The dispersion equation for air as used by Zemax OpticStudio®. It is identical to that in [EdI53]. |
| AMTIR-1_AMI | Spec Sheet (Amorphous Materials Inc.) |
| AMTIR-1/TI-20 | [BS94] |
| AMTIR-3/TI-1173_3-14 $\mu \mathrm{m}$ | [BS94] |
| AMTIR-3/TI-1173_0.9-14 $\mu \mathrm{m}$ | [BS94] |
| BK7_MSO-measured | [Jen10] |
| Boron_carbide-B4C_2.52gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Boron_nitride-BN_2.25gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Boron_trioxide-B2O3_2.46gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Boron-B_2.37gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Fused_Silica | [BS94] |
| Germanium_dioxide-GeO2 | [BS94] |
| Germanium-Ge_(1957) | [SV57] |
| Germanium-Ge_(1985) | [Pal85] |
| Germanium-Ge_(1985)_2-12 $\mu \mathrm{m}$ | [Pal85] |
| Germanium-Ge_5.323gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Ideal High Absorption Material | This is just an "ideal" material with extreme high absorption. |
| Ideal High Reflectance Material | This is just an "ideal" mirror material with extreme high absorption, which leads to a nearly perfect reflectance. |
| KDP(ordinaryRay)-KH2PO4 | [BS94] |
| Seawater-H2O_3.5pct_Salinity | Dispersion parameters from [Lai06], absorption coefficients from [Ame94]. |
| Selenium(extraordinaryRay)-Se-e_(1991) | [Pal91] |


| Selenium(ordinaryRay)-Se-o_(1991) | [Pal91] |
| :---: | :---: |
| Tellurium(trigonal_extraordinaryRay)-Tee_(1991) | [Pal91] |
| Tellurium(trigonal_ordinaryRay)-Te-o_(1991) | [Pal91] |
| Tellurium_dioxide-TeO2_(1994) | [BS94] |
| Water-H2O_(1991) | [Pal91] |
| Water-H2O_(1997+1991) | Concatenation of Water-H2O_1.Ogcm-3_(1997)  <br> $[0.124 \AA-413 \AA]$ and Water-H2O_(1991) <br> $[460 \AA-1 . \mathrm{E} 11 \AA]$   |
| Water-H2O_(pure) | Dispersion parameters from [Lai06], absorption coefficients from [Ame94]. |
| Water-H2O_1.0gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |

## A.4.5.6 Radiation_Hardened

This category contains glasses which are labeled as radiation hardened by the manufacturers.

## A.4.5.7 Silicon+Compounds_(Non-Glass)

This category contains the element silicon as well as compounds of silicon which are no glasses.

| MATERIAL | DATA SOURCE |
| :---: | :---: |
| Hydrogenated_Silicon(amorphous)-a- Si:H_(1985) | [Pal85] |
| Silicon(amorphous)-a-Si_(1997+1985) | Concatenation of Silicon(amorphous)-a-Si_2.189gcm3_(1997) $[0.124 \AA-413 \AA]$ and Silicon(amor-phous_evap)-a-Si_(1985) [413 Å-355142 Å] |
| Silicon(amorphous)-a-Si_2.189gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Silicon(amorphous)-a-Si_sopra | https://web.archive.org/web/20070101013854/ http://www.sopra-sa.com/index2.htm |
| Silicon(amorphous_evap)-a-Si_(1985) | [Pal85] |
| Silicon(crystalline)-Si_(1985) | [Pal85] |
| Silicon(evap_thinFilm)-a-Si_(1988) | [Win+88a] |
| Silicon(oxidized_(100)_Si_wafer)-Si_(1992) | $\diamond(\hookrightarrow$ Sec. A.4.5.9) |
| Silicon(sputtered)-a-Si_(1991) | [Win91] |
| Silicon(sputtered)-a-Si_(1992) | $\diamond(\hookrightarrow$ Sec. A.4.5.9) |
| Silicon_carbide(6H)-SiC_(1989) | [Yan+89] |
| Silicon_carbide(amorphous)-aSic_(1997+1988) | Concatenation of Silicon_carbide(amorphous)-a-SiC_3.112gcm-3_(1997) [0.124 Å-413 Å] and Sili-con_carbide(sputtered)-a-SiC_(1988) [448 Å-1216 Å] |
| Silicon_carbide(amorphous)-a-SiC_3.112gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |


| Silicon_carbide(CVD)-SiC_(1985) | [Osa85] |
| :---: | :---: |
| Silicon_carbide(CVD)-SiC_(1988) | [Win+88a] |
| Silicon_carbide(hex_xtal_ordinaryRay)-SiC- o_(1985) | [Pal85] |
| Silicon_carbide(sputtered)-a-SiC_(1988) | [KW88] |
| Silicon_carbide-SiC_(1997+1985) | Concatenation of Silicon_carbide- Sic_3.208gcm-3_(1997) $[0.124 \AA-413 \AA$ and Sil- icon_carbide(hex_xtal_ordinaryRay)-SiC-o_(1985) $[413 \AA-250010 \AA]$ |
| Silicon_carbide-SiC_3.208gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Silicon_dioxide(amor-phous)-SiO2_(1997+1991) |  |
| Silicon_dioxide(amorphous)-SiO2_2.19gcm3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Silicon_dioxide(amor- <br> phous_fused_quartz)-SiO2_(1991) | [Pal91] |
| Silicon_dioxide(trigonal_quartz_extraordinaryRay) | [BS94] |
| Silicon_dioxide(trigonal_quartz_extraordi-naryRay)-SiO2-e_(1985) | [Pal85] |
| Silicon_dioxide(trigonal_quartz_extraordi-naryRay)-SiO2-e_(1999) | [Gho99] |
| Silicon_dioxide(trigonal_quartz_ordinaryRay) | [BS94] |
| Silicon_dioxide(trigonal_quartz_ordi-naryRay)-SiO2-o_(1985) | [Pal85] |
| Silicon_dioxide(trigonal_quartz_ordi-naryRay)-SiO2-o_(1999) | [Gho99] |
| Silicon_dioxide-SiO2_(1997+1985) | Concatenation of Silicon_dioxide- SiO2_2.65gcm-3_(1997) $[0.124 \AA-413 \AA$ and Sil- icon_dioxide(trigonal_quartz_ordinaryRay)-SiO2- o_(1985) [420 $\AA$-4999190 $\AA$ ] |
| Silicon_dioxide-SiO2_2.65gcm-3_(1997) | $\bowtie(\checkmark$ Sec. A.4.5.9) |
| Silicon_Dioxide-SiO2-ThinFilm | [BLP82] The curve in Fig. 22 of the publication was used to sample the dispersion instead of the bad fitting Cauchy parameters given. |
| Silicon_monoxide-SiO_(1985) | [Pal85] |
| Silicon_monoxide-SiO_(1997+1985) | Concatenation of $\quad$ Silicon_monoxide- $S_{\text {SiO_2.13gcm-3_(1997) }}[0.124 \AA-413 \AA]$ and Sili- con_monoxide-SiO_(1985) $[496 \AA-139995 \AA]$ |


| Silicon_monoxide-SiO_2.13gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| :---: | :---: |
| Silicon_Monoxide-SiO-ThinFilm | [Pal85, p. 768] |
| Silicon_nitride(polyxtal)-Si3N4_(1985) | [Pal85] |
| Silicon_nitride-Si3N4_(1992) | $\diamond$ ( $\hookrightarrow$ Sec. A.4.5.9) |
| Silicon_nitride-Si3N4_(1997+1985) | Concatenation of $\quad$ Silicon_nitride- Si3N4_3.44gcm-3_(1997) $[0.124 \AA-413 \AA]$ and Sil- icon_nitride(polyxtal)-Si3N4_(1985) $[517 \AA-12398 \AA]$ |
| Silicon_nitride-Si3N4_3.44gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| Silicon-germanium(cu-bic)-Si0.25Ge0.75_(1991a) | [Pal91] |
| Silicon-germanium(cu-bic)-Si0.25Ge0.75_(1991b) | [Pal91] |
| Silicon-germanium(cu-bic)-Si0.5Ge0.5_(1991a) | [Pal91] |
| Silicon-germanium(cu-bic)-Si0.5Ge0.5_(1991b) | [Pa191] |
| Silicon-germanium(cu-bic)-Si0.8Ge0.2_(1991a) | [Pa191] |
| Silicon-germanium(cu-bic)-Si0.8Ge0.2_(1991b) | [Pal91] |
| Silicon-Si_(1997+1985) | Concatenation of Silicon-Si_2.329gcm-3_(1997) $[0.124 \AA-413 \AA]$ and $[420 \AA-3332800 \AA]$ |
| Silicon-Si_1.36-11 mm | [BS94] |
| Silicon-Si_2.329gcm-3_(1997) | $\bowtie(\hookrightarrow$ Sec. A.4.5.9) |
| SiO2-ThinFilm_MSO-measured | [Jen10] |

## A.4.5.8 Birefringent

This category contains birefringent materials, namely uniaxial and biaxial crystals.

| MATERIAL | DATA SOURCE |
| :--- | :--- |
| Calcite_(extraordinaryRay)-CaCO3-e/o_(1999) | [Gho99] |
| CaMoO4(tetragonal_extraordinaryRay)-CaMoO4-e/o_(1965) | [Bon65] |
| CaWO4(tetragonal_extraordinaryRay)-CaWO4-e/o_(1965) | [Bon65] $^{1}$ |
| LYSO:Ce(monoclinic_Index_ $\alpha / \beta / \gamma)-\mathrm{Lu}(\mathbf{x}) \mathrm{Y}(\mathbf{2 - x}) \mathrm{SiO5-} \mathrm{\alpha /} \mathrm{\beta /} \mathrm{\gamma} \mathrm{\_(2012)}$ | $[E r d+12]$ |
| Rutile(tetragonal_extraordinaryRay)-TiO2-e/o_(1965) | [Bon65] $^{2}$ |

[^21]| SrMoO4(tetragonal_extraordinaryRay)-SrMoO4-e/o_(1965) | [Bon65] |
| :--- | :--- |
| YAIO3(1.14\%Nd_orthorhombic_Index_ $\alpha / \beta / \gamma)$-YAIO3- $\alpha / \beta / \gamma_{-}(1973)$ | [MD73] |
| YAIO3(undoped_orthorhombic_Index_ $\alpha / \beta / \gamma)$-YAIO3- $\alpha / \beta / \gamma_{-}(1973)$ | [MD73] |
| ZnWO4(monoclinic_Index_ $\alpha / \beta / \gamma$ )-ZnWO4- $\alpha / \beta / \gamma \_(1965)$ | [Bon65] |
| $\alpha$-BismuthMolybdate(monoclinic_Index_ $\alpha / \beta / \gamma)$-Bi2(MoO4)3- $\alpha / \beta / \gamma \_(2002)$ | [MV02] |

## A.4.5.9 X-ray

Each X-ray material is contained in one of the other categories at least. So the data sources for the non-glasses are listed in that category which represents the composition of the material respectively (e.g. in Metals+Compounds or in Silicon+Compounds_(Non-Glass)).
For all entries marked with $\bowtie$ or $\diamond$ in the table above, the optical data are taken from David Windt's IMD software package (http://www.rxollc.com/imd).

- $\diamond$ : For the materials marked with $\diamond$, only the source "D. L. Windt, unpublished (1992)" is given.
- $\bowtie$ : For the materials marked with $\bowtie$, the user's manual ([Win13], p. 37) of this software states: "The atomic scattering factors f 1 \& f 2 can be used to compute optical constants $\mathrm{n} \& \mathrm{k}$ for elemental or compound materials of known density, as described in [[HGD93]]. [...] Each file is a concatenation of high-energy X-ray data obtained from LLNL extending from 30 keV to 100 keV , and low-energy data from CXRO extending from 30 keV to 10 eV ." The abbreviations LLNL and CXRO refer to data bases, formerly provided by websites of the following institutions:
- LLNL: Lawrence Livermore National Laboratory (https://web.archive.org/web/20001030001803/ http://www-phys.llnl.gov/V_Div/scattering/asf.html)
- CXRO: Center for X-Ray Optics (CXRO), Lawrence Berkeley Laboratory (https://web.archive . org/web/20051117074606fw_/http://www.cxro.lbl.gov/optical_constants/asf.html)

Note: A currently available data base for atomic scattering factors (if someone wants to calculate n -k-data for herself) can be found at https://physics.nist.gov/PhysRefData/FFast/html/form.html.

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[^0]:    1 Up to VirtualLab Fusion 2021.1, Non-Equidistant Field Values documents; Positions, Directions \& Wavefront Phase documents; and Ray Distributions 3D were all saved with the extension *.rays.
    2 A session editor can generate child document views (e.g. Optical Setups). These child views stay linked to the session editor so that clicking Refresh in the session editor updates these documents. This linkage can be removed if you close the session editor and click on Keep Associated Documents in the resulting dialog. If you click Close Associated Documents both the session editor and the child document views are closed.

[^1]:    1 See Sec. 35.1.1 for details on definition areas.

[^2]:    Adapted to fit to 611 nm Adapted to fit to 700 nm Adapted to fit to 525 nm Adapted to fit to 450 nm
    The data of the currently used color profile are determined during runtime.
    Corresponds to 700 nm
    Corresponds to 530 nm
    8 Corresponds to 470 nm
    9 Corresponds to illuminant D65

[^3]:    $1 \quad$ The ellipse marker is only available for gridded data array based documents. You can switch between elliptic marker and and rectangular marker with the Selections > Elliptic Selection entry of the Property browser.

[^4]:    1 Generally, a linear interpolation on real part and imaginary part doesn't result in a linear interpolation in amplitude and phase and vice versa.

[^5]:    1 Part V explains the general catalog concept, its subsection Sec. 34.1 explains the control for loading, editing, and viewing catalog entries.

[^6]:    $\overline{1} \quad$ By using different scaling values for $\mathrm{x}, \mathrm{y}$ and $\mathrm{z}(\hookrightarrow$ Sec. 133.3.1), the spheres may be dilated or compressed to become ellipsoids.

[^7]:    $1 \quad$ In a General Optical Setup only three surface regions per surface layout are allowed.

[^8]:    1 For the parameters within a Multiple Light Source ( $\hookrightarrow$ Sec. 49) the index of the sub light source is appended to the default short name; for the parameters of a Surface Layout ( $\hookrightarrow$ Sec. 40.2) the region index is appended.

[^9]:    †+ High Reflective (Start) Mirrors
    $\ddagger$ Outcoupling Mirrors
    ... Laser Crystal
    Đ- Components
    Ideal Components
    +- Detectors

[^10]:    1 atan2 is a special implementation of the arctangent function for a fraction of two values. See Microsoft C\# documentation or Wikipedia for reference.

[^11]:    1 atan2 is a special implementation of the arctangent function for a fraction of two values. See Microsoft C\# documentation or Wikipedia for reference.

[^12]:    Independent of whether Distortion Data Array or Single Distortion Values is selected, the maximum distortion

[^13]:    $1 \quad$ All three modes of the non-paraxial Far Field Operator are tested.

[^14]:    $1 \quad$ A grating component is per definition periodical and an ideal plane wave fulfills the appropriate condition too.

[^15]:    1 Hereby one period can also contain any periodical substructures.

[^16]:    $1 \quad$ This feature was introduced on initiative of Yifeng Gao and Dr. Yuan Chen.

[^17]:    1 For the parameters within a Multiple Light Source ( $\hookrightarrow$ Sec. 49) the index of the sub light source is appended to the default short name; for the parameters of a Surface Layout ( $\hookrightarrow$ Sec. 40.2) the region index is appended.

[^18]:    $1 \quad$ Note that other optics software often use Noll's sequential indices.

[^19]:    1 atan2 is a special implementation of the arctangent function for a fraction of two values. See Microsoft C\# documentation or Wikipedia for reference.

[^20]:    1 atan2 is a special implementation of the arctangent function for a fraction of two values. See Microsoft C\# documentation or Wikipedia for reference.

[^21]:    1 The value for the extraordinary ray at $1.8 \mu \mathrm{~m}$ is obviously wrong. Since there is a good chance that there were transposed digits, the table value of 1.9848 has been replaced by 1.8948 .
    2 The outlier for the ordinary ray at 500 nm of 2.4058 has been replaced by 2.7058 . The outlier for the extraordinary ray at $1.6 \mu \mathrm{~m}$ of 2.6002 has been replaced by 2.6902.

